

GEOTECHNICAL DATA REPORT

INTERSTATE 95 EMERSON MILL ROAD / B&A RAILROAD
BRIDGES NOS. 5969 AND 1430
HAMPDEN, MAINE
MAINEDOT WIN 21673.00 AND WIN 21673.10

by Haley & Aldrich, Inc.
Portland, Maine

For Maine Department of Transportation
Augusta, Maine

File No. 129380-002
February 2019





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22 February 2019
File No. 129380-002

Maine Department of Transportation
16 State House Station
Augusta, Maine 04333-0016

Attention: Laura Krusinski, P.E.
Senior Geotechnical Engineer

Subject: Geotechnical Data Report
Interstate 95 over Emerson Mill Road/ B&A Railroad, Bridge Nos. 5969 and 1430
Hampden, Maine
MaineDOT WIN 21673.00 and WIN 21673.10

Ladies and Gentlemen:

This geotechnical data report (GDR) presents the results of subsurface investigation and geotechnical laboratory testing programs. This work has been completed in accordance with our proposal dated 10 April 2017, and your subsequent authorization.

Project Understanding

The project consists of the replacement of two existing bridges that carry Route 95 traffic northbound and southbound over Emerson Mill Road and the B&A Railroad in Hampden, Maine. Historic drawings of the existing bridges were provided by MaineDOT and are included in this report in Appendix D. The location of the proposed pair of bridges is shown on Figure 1, Project Locus, and Figure 2, Boring Location Plan.

Horizontal Coordinate System and Elevation Datum

Plan locations of test borings are reported as northing and easting coordinates relative to the Maine State Plane Coordinate System, North American Datum of 1983 (NAD 83), Maine 2000 Central Zone (refer to Table I and boring logs in Appendix A). Elevations referenced herein are in feet and reference the North American Vertical Datum of 1988 (NAVD 88).

Geologic Setting

According to Maine Geological Survey's Surficial Geology of the Bangor Quadrangle, Maine (2011), surficial geologic units mapped at the site consist of the Presumpscot Formation. Deposition of the Presumpscot Formation occurred as a result of melting glacial ice in conjunction with sea level rise during deglaciation in Late Wisconsinan time. These glaciomarine sediments typically consist of silt, clay and sand.

The historic test borings drilled at the site encountered the Presumpscot Formation (i.e., glaciomarine clays, silts and sands) overlying a glacial till (i.e. silt, sand, gravel) deposit. The recent test borings drilled at the site encountered man-placed fill overlying the Presumpscot Formation, overlying glacial till, overlying bedrock. Glacial till soils encountered typically consisted of a heterogeneous mix of silt, sand and gravel with occasional cobbles and boulders.

According to Maine Geological Survey's Bedrock Geology of the Bangor Quadrangle, Maine (2011), bedrock at the site is mapped as Silurian-Ordovician age rocks of the Vassalboro Group (Brewer Formation). Bedrock core samples collected for this site investigation consisted of metamorphic rocks composed of phyllite, slate and quartzite.

Subsurface Explorations

PRELIMINARY DESIGN PHASE EXPLORATIONS BY HALEY & ALDRICH

Haley & Aldrich conducted a preliminary design phase geotechnical exploration program at the site of the two bridges. A total of six test borings (BB-HSS-119 through BB-HSS-124) were completed to identify subsurface conditions along the proposed bridge alignment. Test borings BB-HSS-119, BB-HSS-120, BB-HSS-123, and BB-HSS-124 were drilled through the bridge approach embankments behind the existing abutments. Test boring BB-HSS-121 was drilled through the bridge deck and casing was advanced from the bridge deck to the ground surface below. Test boring BB-HSS-122 was drilled below the bridge, adjacent to Emerson Mill Road.

Boring locations were laid out in the field by taping distances from existing site features. "As-drilled" locations and ground surface elevations at boring locations were determined by MaineDOT using GPS survey methods. As-drilled boring locations are shown on Figure 2. Coordinate location data and ground surface elevations at exploration locations are provided on individual test boring logs provided in Appendix A and are summarized in Table I.

All test borings were drilled by New England Boring Contractors of Hermon, Maine using either a truck-mounted Mobile B59 drill rig or track-mounted Mobile B53 drill rigs. Test borings were drilled to depths ranging from 32.7 ft to 65.4 ft below ground surface (BGS).

Test borings were advanced using cased-wash drilling methods by either driving or spinning casing. Casing consisted of 4.0-in. (HW-size) inside diameter (ID) steel casing and/or 3.0-in. (NW-size) ID steel casing. Casing blow count data is provided on the logs in Appendix A. Soil samples were generally

collected continuously through the man-placed fill and then typically at 5-ft intervals once native soils were encountered. The test borings were extended to bedrock and collected approximately 10 ft of rock core.

Soils samples were collected by driving a 1-3/8-in. ID split-spoon sampler with a 140-lb hammer dropped from a height of 30 in., as indicated on the test boring logs. Drilling and sampling were performed in accordance with MaineDOT specifications. The drill rigs were equipped with automatic hammers calibrated annually per MaineDOT requirements (Appendix A of MaineDOT Geotechnical Drilling Contract Specifications, revised June 2007). A calculated hammer efficiency of 0.75, 0.677 and 0.869 were used for the calibrated automatic hammer system for the steel track-mounted Mobile Drill B-53 rig, the rubber track-mounted Mobile Drill B-53 rig, and the truck-mounted Mobile Drill B-59 rig, respectively.

The number of hammer blows required to advance the sampler through each 6-in. interval was recorded and is provided on the test boring logs. The uncorrected SPT N-value is defined as the total number of blows required to advance the sampler through the middle 12 in. of the 24-in. sampling interval. The energy-corrected SPT N-value (N₆₀) is equal to the uncorrected N-value multiplied by the hammer efficiency factor divided by 0.6 (i.e., 60 percent calculated hammer efficiency). Both the raw blow count data and the corrected N-values are shown on the boring logs.

Samples of the in-situ fill soils collected during the geotechnical explorations were screened in the field with a photoionization detector (PID) to assess the presence of volatile organic compounds (VOCs). No elevated PID readings were detected during the subsurface explorations. No visual or olfactory signs of contamination/environmentally impacted soils were observed during the subsurface explorations. Refer to individual boring logs provided in Appendix A for actual PID readings.

The test borings sampled 10.0 to 11.2 ft of bedrock using a 2.0-in. (NQ-size) ID diamond-tipped core barrel. Refer to rock core photographs provided in Appendix B for detailed information on bedrock core samples collected.

All soil and bedrock samples were classified in accordance with MaineDOT classification system and were preserved in glass sample jars and wooden core boxes. The samples that were not submitted for laboratory testing are available for review upon request. Soil and bedrock samples are being stored at the Haley & Aldrich laboratory facility in Portland, Maine.

Generalized Subsurface Conditions

The subsurface conditions encountered at the site consist of the following geologic units presented in order of increasing depth below ground surface: topsoil, man-placed fill, marine deposits, glacial till and bedrock.

SOIL UNIT AND BEDROCK DESCRIPTIONS

Soil

Refer to Table I for a summary of the soil units and encountered thicknesses at each test boring location. A description of each soil unit is provided separately, below. Detailed soil descriptions are provided on the test boring logs in Appendix A. Please note that the soil descriptions provided on the test boring logs and summarized below do not represent actual field conditions other than at the specific test boring locations. The actual conditions will vary from those described and shown herein.

Unit		Approximate Range in Encountered Thickness (ft)	Generalized Description
Topsoil		0.5	Dark brown fine SAND with trace organics and roots <i>(encountered in BB-HSS-122, located below the existing bridge and next to Emerson Mill Road)</i>
Fill		8.0 to 27.2	Very loose to very dense SAND, trace gravel to gravelly, trace to little silt, occasional trace asphalt pieces (SW, SW-SM, SP); very loose to very dense SAND, trace gravel to gravelly, little to some silt, trace clay, occasional trace wood and wire (SM); very dense GRAVEL, some sand, trace silt (GW-GM); dense GRAVEL, some sand, little sand (GM); very soft to medium stiff SILT, little gravel, some sand, trace to little clay (ML); very soft to medium stiff silty CLAY, trace gravel, trace to little sand, trace organics (CL) <i>(encountered in all test borings)</i>
Marine Deposit	Clay and Silt	4.0 to 9.5	Very stiff SILT, little sand, trace to some clay, occasional trace roots, wood and organics (ML); medium stiff to very stiff silty CLAY, trace to some sand, occasional mottling, trace roots and organics (CL) <i>(encountered in all test borings except BB-HSS-121)</i>
	Sand	0.5	Medium dense SAND, little gravel, little silt (SM) <i>(encountered in BB-HSS-113)</i>
Glacial Till		1.4 to 16.4	Very dense SAND, little gravel, trace silt (SP); medium dense to very dense SAND, trace to some gravel, little silt (SM); very dense GRAVEL, some sand, trace silt (GP); medium dense GRAVEL, some sand, little silt (GM) The glacial till was moderately-bonded to well-bonded and contained occasional cobbles and boulders <i>(encountered in all test borings)</i>

Please note, test borings performed behind the abutments encountered 0.5 to 1.0 ft of bituminous concrete with a 0.6 to 1.2 ft thick concrete approach slab underlying the bituminous concrete. Test boring BB-HSS-121 was performed at the midpoint of the bridge and penetrated the concrete bridge deck, which had a thickness of 0.8 ft.

Bedrock

Bedrock was cored in each test boring. The top of the bedrock surface ranged from approximately 22.5 to 55.0 ft BGS (El. 108.8 to El. 125.9). Test borings BB-HSS-119 and BB-HSS-123 encountered 1.5 to 2.0 ft of weathered bedrock overlying the bedrock. Bedrock encountered at the site consisted of moderately hard to hard phyllite, hard to very hard quartzite and medium hard slate.

Rock quality designation (RQD) is a common parameter that is used to help assess the competency of sampled bedrock. RQD is defined as the sum of pieces of recovered bedrock greater than 4 in. in length divided by the total length of the core run. RQD values for bedrock encountered at the site ranged between 29 to 100 percent, this correlates to a Rock Mass Quality rating of poor to excellent. Refer to rock core photographs provided in Appendix B for detailed information on bedrock core samples collected.

WATER ELEVATIONS

Observation wells were not installed in any of the completed boreholes. As a result, long term static water levels at test boring locations were not determined. Water levels were taken in the completed boreholes after the casing had been extracted from the borehole and are noted on the boring logs in Appendix A. Water depths ranged from 6.0 to 23.1 ft BGS (El. 134.6 to El. 148.5). Please note that the visual observations made during drilling and water levels measured in the completed boreholes may have been affected by drilling means/methods and may not be representative of actual static water levels at the site.

In general, groundwater levels can be expected to fluctuate, subject to seasonal variation, local soil conditions, topography and precipitation. Groundwater levels encountered during construction may differ from those observed in the test borings.

Laboratory Testing Program

A preliminary design phase laboratory testing program was undertaken on soil samples collected during the field investigation to assist in soil classification/identification. In general, laboratory testing was performed on disturbed soil samples collected during SPT sampling. All laboratory soil testing was performed by GeoTesting Express, Inc. of Acton, Massachusetts. Geotechnical laboratory testing was performed in accordance with applicable American Society for Testing Materials (ASTM) testing procedures.

The preliminary design phase testing program included six grain size analyses (sieve only, no hydrometer), five Atterberg Limits analyses and four compressive strength/elastic moduli of rock analyses. A summary of laboratory test results is provided below. Refer to the laboratory test results provided in Appendix C of this report.

Laboratory Test	ASTM Test Designation	Soil Unit	No. of Tests Completed	Range in Test Results
Grain Size	ASTM D 422 (Sieve Only)	Fill	6	AASHTO Classification: A-1-a(0), A-2-4(0), A-1-b(0) USCS Classification: SM
Atterberg Limits	ASTM D 4318	Marine Clay	5	USCS Classification: CL Moisture Content: 24% to 27% Liquid Limit: 26 to 36 Plastic Limit: 18 to 21 Plasticity Index: 8 to 16
Compressive Strength / Elastic Moduli of Rock	ASTM D 7012	Bedrock	4	Peak Compressive Stress: 3,815 psi to 21,452 psi Young's Modulus: 4,600,000 psi to 9,350,000 psi Poisson's Ratio: 0.13 to 0.37

Closure

We appreciate the opportunity to provide geotechnical services on this project. Please do not hesitate to call if you have any questions or comments.

Sincerely yours,
HALEY & ALDRICH, INC.

Erin A. Force

Erin A. Force, P.E.
Project Manager



Wayne A. Chadbourne

Wayne A. Chadbourne, P.E.
Senior Associate

Enclosures:

- Table I – Summary of Subsurface Explorations
- Figure 1 – Project Locus
- Figure 2 – Boring Location Plan and Interpretive Subsurface Profile
- Appendix A – Test Boring Logs
- Appendix B – Rock Core Photographs
- Appendix C – Laboratory Test Results
- Appendix D – Historic Drawings

References

1. Pollock, Stephen G., *Bedrock Geology of the Bangor Quadrangle, Maine*, Maine Geological Survey, Department of Conservation, Augusta, Maine, Open File Report No. 11-57, 2011.
2. Syverson, Kent M., Thompson, Andrew H. *Surficial Geology, Bangor Quadrangle, Maine*, Maine Geological Survey, Department of Conservation, Augusta, Maine, Open File Report No. 11-06, 2011.

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TABLES

TABLE I
Summary of Subsurface Explorations
Interstate 95 over Emerson Mill Road / B&A Railroad
Bridge Nos. 5969 and 1430
Hampden, Maine
MaineDOT WIN 21673.00 and WIN 21673.10

	Test Boring No. ¹	Coordinates ²	
		Easting	Northing
North bound	BB-HSS-120	1,706,750	463,132
	BB-HSS-122	1,706,865	463,167
	BB-HSS-124	1,706,967	463,230
South bound	BB-HSS-119	1,706,754	463,346
	BB-HSS-121	1,706,850	463,391
	BB-HSS-123	1,706,950	463,431

	Test Boring No. ¹	Ground Surface Elevation ^{3,4}	Approximate Strata Thickness ⁵ (ft)							Approximate Top of Bedrock Depth (ft)	Approximate Elevation of Top of Bedrock ^{3,4}	Approximate Top of Bedrock Depth (ft)	Approximate Elevation of Bottom of Exploration ^{3,4}
			Bituminous Concrete	Topsoil	Fill	Marine Clay and Silt	Marine Sand	Glacial Till	Weathered Bedrock				
North bound	BB-HSS-120	163.5	1.0	NE	26.0	7.1	NE	10.2	NE	44.3	119.2	54.3	109.2
	BB-HSS-122	140.6	NE	0.5	8.0	4.0	NE	10.0	NE	22.5	118.1	32.7	107.9
	BB-HSS-124	162.8	1.0	NE	26.0	9.5	NE	1.4	NE	36.9	125.9	47.5	115.3
South bound	BB-HSS-119	163.8	0.5	NE	27.0	9.1	0.5	16.4	1.5	55.0	108.8	65.4	98.4
	BB-HSS-121	139.4	NE ⁶	NE	14.3	NE	NE	14.4	NE	28.7	110.7	38.7	100.7
	BB-HSS-123	162.8	0.9	NE	27.2	9.5	NE	4.6	2.0	44.2	118.6	55.4	107.4

Notes:

¹ Test boring locations are shown on Figure 2, Boring Location Plan.

² As-drilled coordinates of test borings were determined by MaineDOT using GPS survey equipment and reference NAD 83, Maine 2000 Central Zone coordinate system.

³ Ground surface elevations at as-drilled test boring locations were determined by MaineDOT using GPS survey equipment.

⁴ Elevations are measured in feet and reference the National Geodetic Vertical Datum of 1988 (NAVD 88).

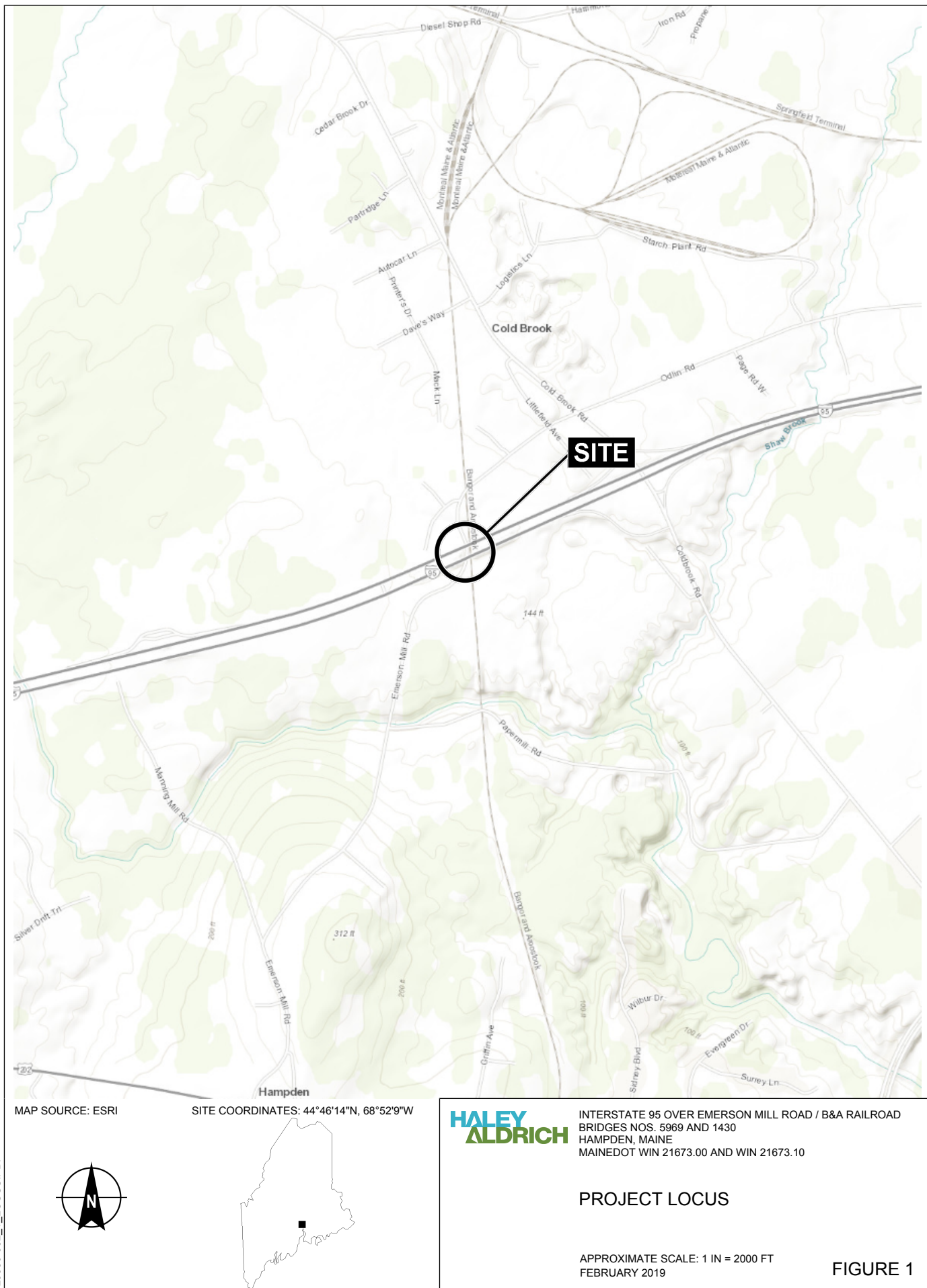
⁵ "NE" indicates stratum was not encountered in test boring.

⁶ Existing concrete bridge deck thickness encountered at BB-HSS-121 was 0.8 ft.

	Individual	Date
Prepared By:	KAR	1/11/2019
Checked By:	EAF	2/18/2019
Reviewed By:	WAC	2/21/2019

FIGURES

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APPENDIX A

Test Boring Logs

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine				Boring No.: BB-HSS-119 WIN: 21673.00			
Driller: New England Boring Contractors				Elevation (ft.): 163.8				Auger ID/OD: --			
Operator: B. Enos				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID			
Logged By: M.Snow/C.Simmons				Rig Type: Mobile Drill B-59				Hammer Wt./Fall: SS-140#/30;HW-300#/16			
Date Start/Finish: 5-23-17/5-24-17				Drilling Method: HW Drive/NW Drive				Core Barrel: NQ-2.0 in. ID			
Boring Location: Bridge #1430: E1706754; N463346				Casing ID/OD: HW-4.0 in. ID/NW-3.0 in. ID				Water Level*: Not observed			
Hammer Efficiency Factor: 0.869				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐							
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test											
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
0							SSA	163.3		-BITUMINOUS CONCRETE-	
	1D	6/6	1.0 - 1.5	12/17(0.0)				162.3		Note: Description from auger cuttings: Brown, dry, fine to coarse SAND and GRAVEL	
								161.1		Brown, dry, medium dense, fine to coarse SAND, some gravel, trace silt, well graded, contains asphalt fragments	
	2D	24/17	3.0 - 5.0	11/9/9/15	18	26				-FILL-(SW) PID=0.0 ppm	
										-CONCRETE-	
5							↘			Brown, dry, medium dense, fine to coarse SAND, some gravel, trace silt, well graded, 1-in. silt nodule	
	3D	24/17	5.0 - 7.0	13/10/8/13	18	26	18			-FILL-(SW-SM) PID=0.0 ppm	
							10			Brown, dry, medium dense, fine to coarse SAND (2-in. silt nodule), little gravel, trace silt, well graded	
	4D	24/18	7.0 - 9.0	15/10/8/11	18	26	11			-FILL-(SW-SM) PID=0.0 ppm	
							10			Brown, dry, medium dense, fine to coarse SAND, little gravel, trace silt, well graded	
										-FILL-(SW) PID=0.0 ppm	
10	5D	24/18	9.0 - 11.0	7/3/10/32	13	19	10			Brown, dry, medium dense, fine to coarse SAND, little gravel, trace silt, well graded, 4-in. clay nodule	
							16			-FILL-(SW-SM) PID=0.0 ppm	
	6D	24/18	11.0 - 13.0	39/22/21/19	43	62	94			Brown, dry, dense, fine to coarse SAND, some gravel, trace silt, well graded	
							120(5.0) 43(7.0)			-FILL-(SW-SM) PID=0.1 ppm	
15	7D	24/16	13.0 - 15.0	16/12/19/19	31	45	94			Note: Drill action indicates gravel/cobbles from 12.5 to 14.0 ft while washing out casing.	
							111			Brown, dry, dense, fine to medium SAND, little gravel, little silt, trace coarse sand	
									-FILL-(SM) PID=0.2 ppm		
	8D	24/16	15.0 - 17.0	17/14/16/25	30	43	105		Brown, moist to wet, medium dense, fine to medium SAND, little gravel, little silt, trace coarse sand		
							100		-FILL-(SM) PID=0.0 ppm		
	9D	24/18	17.0 - 19.0	34/26/27/40	53	77	150		Brown, wet, very dense, fine to coarse SAND, little gravel, little silt, trace coarse sand		
							146		-FILL-(SM) PID=0.0 ppm		
20	10D	24/12	19.0 - 21.0	16/24/24/24	48	70	36		Note: Washed ahead of casing 19.0 to 21.0 ft.		
							30		Brown, wet, dense, GRAVEL, some medium to coarse sand, little silt, trace fine sand		
									-FILL-(GM) PID=0.1 ppm		
	11D	24/14	21.0 - 23.0	23/18/25/40	53	77	41		Brown, wet, very dense, GRAVEL, some medium to coarse sand, little silt, trace fine sand		
							100		-FILL-(GM) PID=0.1 ppm		
	12D	24/13	23.0 - 25.0	24/26/19/15	45	65	158		Brown, wet, dense, fine to medium SAND, some gravel, little silt, trace coarse sand		
25							147		-FILL-(SM) PID=0.1 ppm		
Remarks:											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 1 of 3	
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-119	

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges		Boring No.: BB-HSS-119				
Location: Hampden, Maine				WIN: 21673.00						
Driller: New England Boring Contractors		Elevation (ft.): 163.8		Auger ID/OD: --						
Operator: B. Enos		Datum: NAVD 88		Sampler: Split Spoon-1.375 in. ID						
Logged By: M.Snow/C.Simmons		Rig Type: Mobile Drill B-59		Hammer Wt./Fall: SS-140#/30;HW-300#/16						
Date Start/Finish: 5-23-17/5-24-17		Drilling Method: HW Drive/NW Drive		Core Barrel: NQ-2.0 in. ID						
Boring Location: Bridge #1430: E1706754; N463346		Casing ID/OD: HW-4.0 in. ID/NW-3.0 in. ID		Water Level*: Not observed						
Hammer Efficiency Factor: 0.869		Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐								
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _u = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test										
Depth (ft.)	Sample Information							Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.	
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows			
25	13D	24/16	25.0 - 27.0	18/16/11/9	27	39	-		Brown, wet, medium dense, fine to medium SAND, trace coarse sand, trace fine gravel, little silt, trace clay -FILL-(SM) PID=0.0 ppm -----27.5 Brown-grey, wet, medium dense, fine SAND, little medium sand, little fine gravel, little silt -MARINE DEPOSIT-(SM) -----28.0 Brown grading to grey, moist, very stiff, SILT, trace clay, trace rootlets, trace organics -MARINE DEPOSIT-(ML) Grey-brown, moist, very stiff, SILT (ML), some clay -MARINE DEPOSIT-(ML) -----34.0 Olive-brown, moist, medium stiff, silty CLAY -MARINE DEPOSITS-(CL) -----37.1 Brown to grey, wet, very dense, fine to medium SAND, some gravel, little coarse sand, little silt, well bonded -GLACIAL TILL-(SM) ----- Brown-grey, wet, dense, medium SAND, little coarse and fine sand, little silt, little gravel, well bonded -GLACIAL TILL-(SM) Note: Drill action indicates cobble at 46.6 to 47.0 ft. ----- Grey, wet, medium dense, GRAVEL, some medium to coarse sand, little silt, trace fine sand	G#426850 A-6 CL WC=26% LL=35, PL=20 PI=15
	14D	24/16	27.0 - 29.0	13/10/15/12	25	36	-			
	15D	24/18	29.0 - 31.0	5/7/11/14	18	26	-			
	16D	24/23	34.0 - 36.0	3/4/4/5	8	12	-			
							50			
							41			
							68			
							80			
	17D	24/18	39.0 - 41.0	33/45/42/49	87	126	90			
							NW Drive			
	18D	24/15	44.0 - 46.0	20/24/24/22	48	70	7			
							42			
							72			
							54			
							66			
	19D	24/10	49.0 - 51.0	4/8/9/16	17	25	76			
50										
Remarks:										
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.								Page 2 of 3		
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.								Boring No.: BB-HSS-119		

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Boring Location: Bridge #1430: E1706754; N463346				Casing ID/OD: HW-4.0 in. ID/NW-3.0 in. ID				Water Level*: Not observed																																																																																																																																																																																																																																																																																																																	
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Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine		Boring No.: BB-HSS-120 WIN: 21673.10				
Driller: New England Boring Contractors		Elevation (ft.): 163.5		Auger ID/OD: --						
Operator: B. Enos		Datum: NAVD 88		Sampler: Split Spoon-1.375 in. ID						
Logged By: M.Snow/C.Simmons		Rig Type: Mobile Drill B-59		Hammer Wt./Fall: SS-140#/30;HW-300#/16						
Date Start/Finish: 5-22-17/5-23-17		Drilling Method: HW Drive		Core Barrel: NQ-2.0 in. ID						
Boring Location: Bridge #5969: E1706750; N463132		Casing ID/OD: HW-4.0 in. ID		Water Level*: 15.0 ft						
Hammer Efficiency Factor: 0.869		Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐								
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test										
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0							SSA	162.5	-BITUMINOUS CONCRETE- Note: Observed from auger cuttings.	G#426855 A-1-b (0) SM
								162.0	-CRUSHED STONE-	
								161.7		
								161.0	Note: Observed from auger cuttings: Brown, fine to coarse SAND and GRAVEL -FILL-(SW) PID=0.0 ppm	
	1D	24/14	3.0 - 5.0	7/8/10/8	18	26			-CONCRETE-	
5										
	2D	24/14	5.0 - 7.0	6/6/8/5	14	20	HW Drive		Brown, dry, medium dense, fine to coarse SAND, little gravel, trace silt -FILL-(SW) PID=0.0 ppm	
									Brown, dry, medium dense, fine to coarse SAND, some gravel, little silt -FILL-(SM) PID=0.0 ppm	
	3D	24/14	7.0 - 9.0	8/8/11/12	19	28			Brown, dry to moist, medium dense, fine to coarse SAND, some gravel, trace silt, well graded -FILL-(SW-SM) PID=0.0 ppm	
	4D	24/15	9.0 - 11.0	9/10/11/11	21	30			Brown, dry to moist, medium dense, fine to coarse SAND, some gravel, trace silt -FILL-(SW-SM) PID=0.0 ppm	
10										
	5D	24/18	11.0 - 13.0	11/17/14/13	31	45			Brown, moist, dense, fine to medium SAND, little silt, trace coarse sand, trace gravel -FILL-(SW-SM) PID=0.0 ppm	
	6D	24/18	13.0 - 15.0	35/18/24/30	42	61			Brown, moist, dense, fine to coarse SAND, little gravel, little silt -FILL-(SW-SM) PID=0.0 ppm	
15										
	7D	24/10	15.0 - 17.0	23/28/28/56	56	81			Brown, wet, very dense, fine to coarse SAND, some gravel, little silt -FILL-(SM) PID=0.0 ppm	
	8D	24/22	17.0 - 19.0	77/55/35/27	90	130			Brown, wet, very dense, fine to coarse SAND, some gravel, little silt -FILL-(SM) PID=0.0 ppm	
20								145.5		
									Brown to grey-brown, wet, very dense, GRAVEL, little coarse sand, trace fine to medium sand, trace silt, well bonded (Reworked Glacial Till) -FILL-(GW-GM) PID=0.0 ppm	
	9D	24/17	20.0 - 22.0	14/24/30/40	54	78	36		Brown, wet, very dense, fine to coarse SAND, some gravel, some silt, well bonded (Reworked Glacial Till) -FILL-(SM) PID=0.0 ppm	
							68			
							124			
							157			
25										
Remarks:										
Stratification lines represent approximate boundaries between soil types; transitions may be gradual. * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.									Page 1 of 3 Boring No.: BB-HSS-120	

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Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine		Boring No.: BB-HSS-121 WIN: 21673.00	
Driller: New England Boring Contractors		Elevation (ft.): 139.4		Auger ID/OD: --			
Operator: B. Enos		Datum: NAVD 88		Sampler: Split Spoon-1.375 in. ID			
Logged By: M.Snow/C.Simmons		Rig Type: Mobile Drill B-59		Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16			
Date Start/Finish: 5-24-17/5-24-17		Drilling Method: HW/NW Drive		Core Barrel: NQ-2.0 in. ID			
Boring Location: Bridge #1430; E1706850; N463391		Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID		Water Level*:			
Hammer Efficiency Factor: 0.869		Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐					
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test							

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	1D	24/3	0.0 - 2.0	WOR/WOH/WOH/ WOH			HW Drive		125.1	Note: Bridge deck thickness 9-in., bridge deck to ground surface 24.3 ft. All samples are referenced to depth from ground surface. Brown, moist, very loose, fine to medium SAND, little silt, trace fine gravel -FILL-(SM) PID=0.0 ppm Brown, moist, very loose, fine to medium SAND, little silt, trace fine gravel -FILL-(SM) PID=0.0 ppm Brown, moist, very loose, fine to coarse SAND, some silt, little gravel -FILL-(SM) PID=0.0 ppm Brown, moist, very loose to medium dense, fine to medium SAND, trace silt, little coarse sand, little fine to coarse gravel -FILL-(SW-SM) PID=0.0 ppm Brown, wet, very loose, fine to medium SAND, some gravel, little coarse sand, little silt -FILL-(SM) PID=0.0 ppm No recovery Grey, wet, very soft, SILT, trace clay, little fine sand and fine gravel, trace medium to coarse sand -FILL-(ML) PID=0.0 ppm Brown-grey, wet, very dense, fine to coarse SAND, little silt, trace gravel, well graded, contains wood and wire -FILL-(SM) PID=0.1 ppm Note: Advanced rollerbit through cobble at 14.5 to 15.5 ft. Brown, wet, very dense, fine to coarse SAND, little silt, trace fine to coarse gravel, well graded -GLACIAL TILL-(SM) -----17.0	G#426857 A-2-4 (0) SM	
	2D	24/2	2.0 - 4.0	WOH/WOH/1/1	1	1						
5	3D	24/16	4.0 - 6.0	WOR/1/WOH/WOH	2	3						
	4D	24/10	6.0 - 8.0	WOH/WOH/15/36	15	22						
	5D	24/4	8.0 - 10.0	4/WOH/1/1	1	1						
10	6D	24/0	10.0 - 12.0	1/WOH/WOH/WOH	2	3						
	7D	24/1	12.0 - 14.0	WOH/1/1/5	2	3						
15	8D	4/2	14.0 - 14.3	100(4.0)								
	9D	24/20	15.5 - 17.5	37/33/47/55	80	116						
20	10D	24/10	20.5 - 22.5	17/16/17/16	33	48	NW Drive					
25												

Remarks:

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

 * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

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Boring No.: BB-HSS-121

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine		Boring No.: BB-HSS-121 WIN: 21673.00					
Driller: New England Boring Contractors			Elevation (ft.): 139.4		Auger ID/OD: --						
Operator: B. Enos			Datum: NAVD 88		Sampler: Split Spoon-1.375 in. ID						
Logged By: M.Snow/C.Simmons			Rig Type: Mobile Drill B-59		Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16						
Date Start/Finish: 5-24-17/5-24-17			Drilling Method: HW/NW Drive		Core Barrel: NQ-2.0 in. ID						
Boring Location: Bridge #1430; E1706850; N463391			Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID		Water Level*:						
Hammer Efficiency Factor: 0.869			Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐								
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_u(lab) = Lab Vane Undrained Shear Strength (psf) q_u = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test											
Depth (ft.)	Sample Information							Laboratory Testing Results/AASHTO and Unified Class.			
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
25	11D	24/7	25.5 - 27.5	16/13/13/13	26	38	NW Drive	Elevation (ft.)	Graphic Log	Brown to grey, wet, medium dense, fine to coarse SAND, little coarse gravel, trace fine gravel, little silt -GLACIAL TILL-(SM)	28.7
	R1	60/59	28.7 - 33.7	RQD = 80%			NQ Core				
30								Elevation (ft.)	Graphic Log	R2: Grey, fine grained to aphanitic, PHYLLITE, hard, fresh. Joints moderate to steeply dipping, close to wide, open, planar, smooth to rough, fresh to slightly oxidized. Quartz veins frequent. Rock Mass Quality=Excellent Recovery=98% R2 Core Times (min:sec): 33.7-34.7' (1:40); 34.7-35.7' (1:39) 35.7-36.7' (1:33); 36.7-37.7' (1:26); 37.7-38.7' (1:22)	38.7
	R2	60/59	33.7 - 38.7	RQD = 98%							
35								Elevation (ft.)	Graphic Log		
40								Elevation (ft.)	Graphic Log		
45								Elevation (ft.)	Graphic Log		
50								Elevation (ft.)	Graphic Log		
Remarks:											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 2 of 2	
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-121	

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine				Boring No.: BB-HSS-122 WIN: 21673.10																																																																																																																																																																																																																						
Driller: New England Boring Contractors				Elevation (ft.): 140.6				Auger ID/OD: --																																																																																																																																																																																																																						
Operator: B. Enos				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID																																																																																																																																																																																																																						
Logged By: T.Snow				Rig Type: Mobile Drill B-53				Hammer Wt./Fall: SS-140#/30;HW-300#/16																																																																																																																																																																																																																						
Date Start/Finish: 5-22-17/5-23-17				Drilling Method: HW Drive				Core Barrel: NQ-2.0 in. ID																																																																																																																																																																																																																						
Boring Location: Bridge #5969: E1706865; N463167				Casing ID/OD: HW-4.0 in. ID				Water Level*: 6.0 ft																																																																																																																																																																																																																						
Hammer Efficiency Factor: 0.677				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐																																																																																																																																																																																																																										
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test																																																																																																																																																																																																																														
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Driller: New England Boring Contractors				Elevation (ft.): 140.6				Auger ID/OD: --																																																																																																																																																																																											
Operator: B. Enos				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID																																																																																																																																																																																											
Logged By: T.Snow				Rig Type: Mobile Drill B-53				Hammer Wt./Fall: SS-140#/30;HW-300#/16																																																																																																																																																																																											
Date Start/Finish: 5-22-17/5-23-17				Drilling Method: HW Drive				Core Barrel: NQ-2.0 in. ID																																																																																																																																																																																											
Boring Location: Bridge #5969: E1706865; N463167				Casing ID/OD: HW-4.0 in. ID				Water Level*: 6.0 ft																																																																																																																																																																																											
Hammer Efficiency Factor: 0.677				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐																																																																																																																																																																																															
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Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine		Boring No.: BB-HSS-123 WIN: 21673.00	
Driller: New England Boring Contractors		Elevation (ft.) 162.8		Auger ID/OD: --			
Operator: M. Porter		Datum: NAVD 88		Sampler: Split Spoon-1.375 in. ID			
Logged By: K. Russ		Rig Type: Mobile Drill B-53		Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16			
Date Start/Finish: 5-24-17/5-24-17		Drilling Method: HW Drive/NW Spun		Core Barrel: NQ-2.0 in. ID			
Boring Location: Bridge #1430: E1706950; N463431		Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID		Water Level*: 23.1 ft			
Hammer Efficiency Factor: 0.750		Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐					
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test							

Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
0							7	161.9		-BITUMINOUS CONCRETE-	
	1D	8/7	1.0 - 1.7	19/50(2.0)			39	161.1		Brown, dry, very dense, fine to coarse SAND, little fine gravel, trace silt and coarse gravel, well graded	
	2D	24/13	2.5 - 4.5	6/6/7/9	13	16	123	160.5		-FILL-(SW) PID=0.0 ppm	
							6			-CONCRETE-	
	3D	24/14	4.5 - 6.5	8/12/7/8	19	24	7			Brown, dry, medium dense, fine to coarse SAND, little gravel, little silt	
5							13			-FILL-(SM) PID=0.0 ppm	
	4D	24/13	6.5 - 8.5	9/7/9/6	16	20	34			Note: Advanced Split spoon to 8.5 ft, drove HW to 10.5 ft. Brown, dry, medium dense, fine to coarse SAND, little fine gravel and silt, trace coarse gravel, well graded, several silt chunks	
							35			-FILL-(SM) PID=0.0 ppm	
	5D	24/16	8.5 - 10.5	6/9/8/9	17	21	38			Brown, dry, medium dense, fine to medium SAND, little coarse SAND, trace silt and fine to coarse gravel, well graded	
							61			-FILL-(SW) PID=0.0 ppm	
10										Brown, dry, medium dense, fine to coarse SAND, some gravel, trace silt, well graded	
	6D	24/12	10.5 - 12.5	10/12/11/10	23	29	11			-FILL-(SW-SM) PID=0.0 ppm	
							21			Brown, wet, medium dense, fine to coarse SAND, little silt, little gravel, well graded	
										-FILL-(SM) PID=0.0 ppm	
	7D	24/16	12.5 - 14.5	17/18/17/19	35	44	37			Brown, wet), dense, fine to coarse SAND, trace silt and gravel, well graded	
							67			-FILL-(SW) PID=0.0 ppm	
15	8D	24/13	14.5 - 16.5	14/18/19/21	37	46	64			Brown, wet, dense, fine to coarse SAND, trace silt and gravel, well grade	
							47			-FILL-(SW) PID=0.0 ppm	
	9D	24/14	16.5 - 18.5	18/16/16/23	32	40	57			Brown, wet, dense, fine SAND, trace silt and medium to coarse sand, poorly graded	
							61	145.0		-FILL-(SP) PID=0.0 ppm	
	10D	24/8	18.5 - 20.5	25/40/38/44	78	98	94	144.7		Brown, wet, very dense, fine to coarse SAND, little gravel, trace silt, well graded	
20							83			-FILL-(SW) PID=0.0 ppm	
	11D	24/15	20.5 - 22.5	20/26/21/24	47	59	50			Brown, wet, dense, fine to medium SAND, little coarse sand, little gravel, trace silt, poorly graded	
							48			-FILL-(SP) PID=0.0 ppm	
	12D	24/14	22.5 - 24.5	21/20/19/19	39	49	60			Brown, wet, dense, coarse SAND, little gravel, trace silt, well graded	
							80			-FILL-(SW-SM) PID=0.0 ppm	
25	13D	24/14	24.5 - 26.5	12/12/21/21	33	41	92			Brown, wet, dense, fine to coarse sand, trace silt and fine gravel, well	

Remarks:

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

 * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

Page 1 of 3

Boring No.: BB-HSS-123

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges		Boring No.: BB-HSS-123					
Location: Hampden, Maine				WIN: 21673.00							
Driller: New England Boring Contractors		Elevation (ft.): 162.8		Auger ID/OD: --							
Operator: M. Porter		Datum: NAVD 88		Sampler: Split Spoon-1.375 in. ID							
Logged By: K. Russ		Rig Type: Mobile Drill B-53		Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16							
Date Start/Finish: 5-24-17/5-24-17		Drilling Method: HW Drive/NW Spun		Core Barrel: NQ-2.0 in. ID							
Boring Location: Bridge #1430: E1706950; N463431		Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID		Water Level*: 23.1 ft							
Hammer Efficiency Factor: 0.750		Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _u = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test											
Sample Information											
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
25							68			graded -FILL-(SW) PID=0.0 ppm	
	14D	24/18	26.5 - 28.5	23/26/16/9	42	53	73			Brown, wet, dense, fine to coarse SAND, trace silt and coarse gravel, well graded -FILL-(SW) PID=0.0 ppm	
							71				
							41	134.7		Olive-grey, moist, very stiff SILT, little fine sand, contains roots and single piece of decomposed wood -MARINE DEPOSIT-(ML)	28.1
							49				
30	15D	24/23	30.0 - 32.0	4/8/9/12	17	21	60	132.8		Olive-brown, moist, very stiff, silty CLAY, trace fine sand, contains roots, mottled -MARINE DEPOSIT-(CL)	30.0
							69				
							89				
							102				
							114				
35	16D	24/24	35.0 - 37.0	2/3/3/3	6	8	65			Olive-brown, wet, medium stiff, silty CLAY, some fine sand -MARINE DEPOSIT-(CL)	
							73				
							154	125.2		Note: Drill wash water contents indicate strata change at 37.6 ft.	37.6
							181				
							222				
40	17D	24/12	40.0 - 42.0	15/22/20/18	42	53	NW Spun			Olive-brown, wet, dense, medium to coarse SAND, little silt, little gravel, trace fine sand, poorly graded, moderately bonded, contains highly weathered bedrock -GLACIAL TILL-(SM)	
								120.6		Note: Drill wash contents indicate weathered bedrock from 42.2 to 44.2 ft. Note: Set NW casing at 42.7 ft. Initial attempt for R1 encountered soft zones, stopped coring and removed weathered bedrock from core. Begin NQ rock core at 44.2 ft. -WEATHERED BEDROCK-	42.2
	R1	48/43	44.2 - 48.2	RQD = 77%				118.6		Top of Bedrock at El.118.6 R1: Grey, fine grained, QUARTZITE, very hard, fresh to moderately weathered. Joints dipping at low angles, very close to wide, open, planar, rough, slightly oxidized joint surfaces. Rock Mass Quality=Good Recovery=90% Note: R1 core times (min:sec) not observed. R2: Grey, fine grained, QUARTZITE, very hard, fresh. Joints dipping at low to moderate angles, close to wide, tight to open, planar, rough,	44.2
	R2	31/31	48.2 - 50.8	RQD = 100%							qp=21,452 psi
50											
Remarks:											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 2 of 3	
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-123	

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges				Boring No.: BB-HSS-123			
				Location: Hampden, Maine				WIN: 21673.00			
Driller: New England Boring Contractors				Elevation (ft.): 162.8				Auger ID/OD: --			
Operator: M. Porter				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID			
Logged By: K. Russ				Rig Type: Mobile Drill B-53				Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16			
Date Start/Finish: 5-24-17/5-24-17				Drilling Method: HW Drive/NW Spun				Core Barrel: NQ-2.0 in. ID			
Boring Location: Bridge #1430: E1706950; N463431				Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID				Water Level*: 23.1 ft			
Hammer Efficiency Factor: 0.750				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐							
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_u(lab) = Lab Vane Undrained Shear Strength (psf) q_u = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test											
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
50	R3	55/55	50.8 - 55.4	RQD = 96%			NQ Core	107.4		slightly oxidized joint surfaces. Rock Mass Quality=Excellent Recovery=100% Note: R2 core times not observed. R3: Grey, fine grained, QUARTZITE, very hard, fresh. Joints dipping at low to moderate angles, close to wide, tight, planar, rough, slightly oxidized joint surfaces. Rock Mass Quality=Excellent Recovery=100% R3 Core Times (min:sec): 50.8-51.8' (1:03); 51.8-52.8' (1:23); 52.8-53.8' (1:12); 53.8-54.8' (1:17); 54.8-55.4' (1:21)	
55										Bottom of Exploration at 55.4 feet below ground surface.	
60											
65											
70											
75											
Remarks:											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 3 of 3	
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-123	

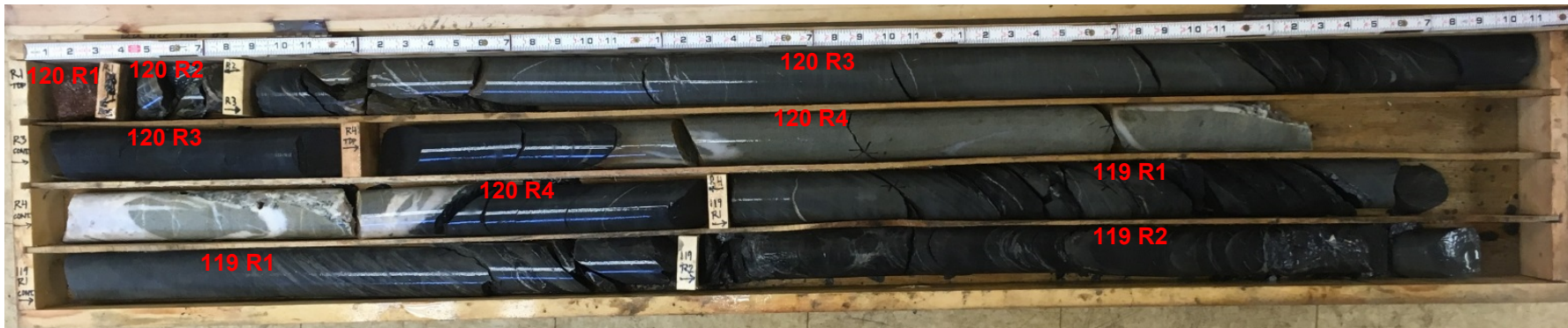
Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine				Boring No.: BB-HSS-124 WIN: 21673.10				
Driller: New England Boring Contractors				Elevation (ft.): 162.8				Auger ID/OD: --				
Operator: M. Porter				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID				
Logged By: K. Russ				Rig Type: Mobile Drill B-53				Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16				
Date Start/Finish: 5-22-17/5-23-17				Drilling Method: HW Drive/NW Drive				Core Barrel: NQ-2.0 in. ID				
Boring Location: Bridge #5969: E1706967; N463230				Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID				Water Level*: 15.5 ft				
Hammer Efficiency Factor: 0.750				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐								
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test												
Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0							2	161.8		-BITUMINOUS CONCRETE-	G#426860 A-1-a (0) SM	
	1D	10/7	1.0 - 1.8	13/50(4.0)			5	161.0		Brown, dry, very dense, fine to medium SAND, some gravel, trace silt and coarse sand, well graded		
							26	160.4		-FILL-(SW) PID=0.0 ppm		
	2D	24/13	3.5 - 5.5	12/8/6/6	14	18	13			-CONCRETE-		
							29			Brown, dry, medium dense, gravelly SAND, little silt		
5							31			-FILL-(SM) PID=0.0 ppm		
	3D		5.5 - 7.5	11/10/14/10	24	30	43			Brown, dry, medium dense, gravelly fine to coarse SAND, well graded		
							49			-FILL-(SW) PID=0.0 ppm		
	4D	24/14	7.5 - 9.5	12/13/10/9	23	29	60			Brown, dry, medium dense, fine to coarse SAND, little fine gravel, trace silt and coarse gravel, well graded, contains several 1-in. balls of reworked native silt		
							58			-FILL-(SW-SM) PID=0.0 ppm		
10	5D	24/14	9.5 - 11.5	6/10/13/14	23	29	27			Brown, moist, medium dense, fine to coarse SAND, little fine gravel, trace silt and coarse gravel, well graded		
							48			-FILL-(SW) PID=0.0 ppm		
	6D	24/15	11.5 - 13.5	16/16/22/21	38	48	86			Brown, moist, dense, fine to coarse SAND, trace silt and gravel, well graded		
							98			-FILL-(SW-SM) PID=0.0 ppm		
							84					
15	7D	24/14	15.0 - 17.0	3/18/17/24	35	44	19	147.3		Brown, moist, dense, fine to coarse SAND, trace silt and gravel, well graded		
							12			-FILL-(SW-SM) PID=0.0 ppm		
	8D	24/18	17.0 - 19.0	23/30/30/32	60	75	6			Brown, wet, dense, medium to coarse SAND, some gravel, little silt, trace fine sand, well bonded (Reworked Glacial Till)		
							23			-FILL-(SM) PID=0.0 ppm		
										Brown, wet, very dense, medium to coarse SAND, some gravel, little silt, trace fine sand, well bonded (Reworked Glacial Till)		
20	9D	24/14	19.0 - 21.0	9/18/39/34	57	71	110		-FILL-(SM) PID=0.0 ppm			
							16		Brown, wet, very dense, fine to coarse SAND, some gravel, little silt (Reworked Glacial Till)			
							9		-FILL-(SW) PID=0.0 ppm			
							16					
							21					
25							22					
Remarks:												
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 1 of 3		
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-124		

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: Emerson Mill Road/B&A Railroad Bridges Location: Hampden, Maine				Boring No.: BB-HSS-124 WIN: 21673.10				
Driller: New England Boring Contractors				Elevation (ft.): 162.8				Auger ID/OD: --				
Operator: M. Porter				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID				
Logged By: K. Russ				Rig Type: Mobile Drill B-53				Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16				
Date Start/Finish: 5-22-17/5-23-17				Drilling Method: HW Drive/NW Drive				Core Barrel: NQ-2.0 in. ID				
Boring Location: Bridge #5969: E1706967; N463230				Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID				Water Level*: 15.5 ft				
Hammer Efficiency Factor: 0.750				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐								
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt												
R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person												
S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _u = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected												
T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test												
Sample Information												
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.	
25	10D	24/14	25.0 - 27.0	1/1/11/5	12	15	22	137.8		G#426854 A-6 CL WC=27% LL=36, PL=21 PI=15		
							42	136.8			Olive-brown, moist, very soft silty CLAY, trace fine sand (Reworked Native Soil) -FILL-(CL) PID=0.0 ppm	
							61				Olive-brown, moist, very stiff, silty CLAY, trace fine sand, mottled -MARINE DEPOSIT-(CL)	
							76					
							86					
30	11D	24/9	30.0 - 32.0	6/6/7/9	13	16	71				Olive-brown, moist, stiff, silty CLAY, trace fine sand, mottled -MARINE DEPOSIT-(CL)	G#426854 A-6 CL WC=27% LL=36, PL=21 PI=15
							77					
							83					
							88					
							86					
35	12D	23/14	35.0 - 36.9	13/19/13/50(5.0)	32	40	NQ Core	127.3	Olive-brown, wet, dense, fine to medium SAND, some gravel, little silt, trace coarse sand, moderately bonded -GLACIAL TILL-(SM)	qp=13,492 psi		
								125.9	Top of Bedrock at El. 125.9 Note: Advanced rollerbit to 37.5 ft, set NW casing to 37.5 ft, begin NQ rock core. R1: Dark grey, fine grained, QUARTZITE, very hard, fresh. Joints dipping at low angles, close to moderately close, tight, planar, rough, slight oxidation on joint surfaces. Single 0.125-in. quartz vein at 39.5 ft. Frequent 0.0625-in. thick biotite bands. Rock Mass Quality=Good Recovery=92% R1 Core Times (min:sec): 37.5-38.5' (4:03); 38.5-39.5' (4:11); 39.5-40.5' (4:45); 40.5-41.5' (4:50); 41.5-42.5' (5:23) R2: Dark grey, fine grained, QUARTZITE, very hard to hard, fresh to slightly weathered. Joints dipping at moderate to low angles, close to very close, tight to open, rough to smooth, planar, slightly oxidized joint surfaces. Several 0.125-in. quartz veins, frequent 0.0625-in. biotite bands. Rock Mass Quality=Good Recovery=100% R2 Core Times (min:sec): 42.5-43.5' (6:37); 43.5-44.5' (5:31); 44.5-45.5' (2:45) R3: Dark grey, fine grained, QUARTZITE, very hard to hard, slightly weathered. Primary joints horizontal to moderately dipping, very close to close, open, rough, planar, slightly oxidized joint surfaces. Secondary joint dipping at high angle, widely spaced, tight, smooth, planar, slightly oxidized joint surfaces. Occasional 0.125-in. quartz veins, frequent 0.0625-in. biotite bands. Note: Low recovery due to core catcher releasing.			
	R1	60/55	37.5 - 42.5	RQD = 87%								
40	R2	36/36	42.5 - 45.5	RQD = 78%								
45	R3	24/15	45.5 - 47.5	RQD = 29%								
50												
Remarks:												
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 2 of 3		
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-124		

Maine Department of Transportation <u>Soil/Rock Exploration Log</u> <u>US CUSTOMARY UNITS</u>				Project: Emerson Mill Road/B&A Railroad Bridges				Boring No.: BB-HSS-124			
				Location: Hampden, Maine				WIN: 21673.10			
Driller: New England Boring Contractors				Elevation (ft.) 162.8				Auger ID/OD: --			
Operator: M. Porter				Datum: NAVD 88				Sampler: Split Spoon-1.375 in. ID			
Logged By: K. Russ				Rig Type: Mobile Drill B-53				Hammer Wt./Fall: SS-140#/30;HW/NW-300#/16			
Date Start/Finish: 5-22-17/5-23-17				Drilling Method: HW Drive/NW Drive				Core Barrel: NQ-2.0 in. ID			
Boring Location: Bridge #5969: E1706967; N463230				Casing ID/OD: HW-4.0 in. ID;NW-3.0 in. ID				Water Level*: 15.5 ft			
Hammer Efficiency Factor: 0.750				Hammer Type: Automatic ☒ Hydraulic ☐ Rope & Cathead ☐							
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_u(lab) = Lab Vane Undrained Shear Strength (psf) q_u = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test											
Depth (ft.)	Sample Information								Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)			
50									Rock Mass Quality=Poor Recovery=63% R3 Core Times (min:sec): 45.5-46.5' (3:07); 46.5-47.5' (4:15) Bottom of Exploration at 47.5 feet below ground surface.		
Remarks:											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 3 of 3	
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-HSS-124	

APPENDIX B

Rock Core Photographs



BORING ID	CORE ID	CORE RUN DEPTH (FT)	CORE RUN EL. ^{NOTE 1}	RECOVERY		RQD ^{NOTE 2}	
				IN.	%	IN.	%
BB-HSS-120	R1 (cobble)	43.2 to 43.8	120.3 to 119.7	NA	NA	NA	NA
BB-HSS-120	R2 (cobble)	43.8 to 44.3	119.7 to 119.2	NA	NA	NA	NA
BB-HSS-120	R3	44.3 to 49.3	119.2 to 114.2	60	100	49	82
BB-HSS-120	R4	49.3 to 54.3	114.2 to 109.2	60	100	57	95
BB-HSS-119	R1	55.0 to 59.5	108.8 to 104.3	53	98	43	80
BB-HSS-119	R2	59.5 to 62.0	104.3 to 101.8	30	100	18	60

NOTES:

1. ELEVATIONS ARE MEASURED IN FEET AND REFERENCE THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
2. "RQD" INDICATES ROCK QUALITY DESIGNATION (PERCENT OF ROCK PIECES RECOVERED EQUAL TO OR GREATER THAN 4 IN. IN LENGTH).

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INTERSTATE 95 OVER EMERSON MILL ROAD/B&A RAILROAD
BRIDGE NOS. 5696 AND 1430
HAMDEN, MAINE
MAINEDOT WIN 21630.00 AND WIN 21673.10

**PHOTOGRAPH OF
BEDROCK CORE
BORING: BB-HSS-120
AND BB-HSS-119**

FILE NO. 129380-002

February 2019



BORING ID	CORE ID	CORE RUN DEPTH (FT)	CORE RUN EL. ^{NOTE 1}	RECOVERY		RQD ^{NOTE 2}	
				IN.	%	IN.	%
BB-HSS-119	R3	62.0 to 65.4	101.8 to 98.4	38	93	29	71
BB-HSS-121	R1	28.7 to 33.7	110.7 to 105.7	59	98	48	80
BB-HSS-121	R2	33.7 to 38.7	105.7 to 100.7	59	98	59	98
BB-HSS-115	R1	2.6 to 4.5	110.7 to 108.8	12	52	NA	NA
BB-HSS-115	R2	7.0 to 8.7	106.3 to 104.6	15	75	8	40
BB-HSS-115	R3	8.7 to 12.6	104.6 to 100.7	13	28	8	17
BB-HSS-115	R4	12.6 to 14.2	100.7 to 99.1	15	79	0	0

NOTES:

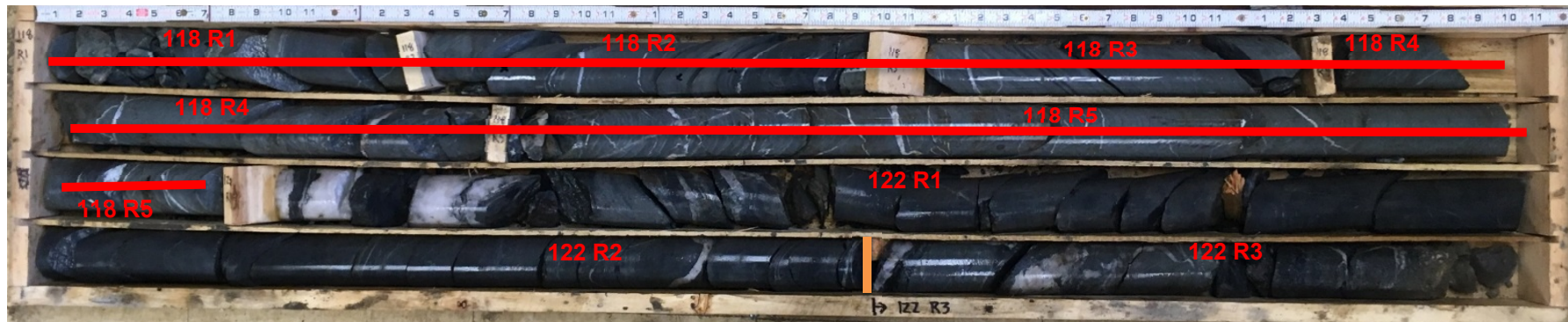
1. ELEVATIONS ARE MEASURED IN FEET AND REFERENCE THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
2. "RQD" INDICATES ROCK QUALITY DESIGNATION (PERCENT OF ROCK PIECES RECOVERED EQUAL TO OR GREATER THAN 4 IN. IN LENGTH).
3. RED LINES DRAWN THROUGH ROCK CORE PHOTOGRAPHS/TABLE INDICATE THAT ROCK CORE WAS COLLECTED FROM AN ADJACENT BRIDGE STRUCTURE. REFER TO OTHER BRIDGE REPORTS.

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**PHOTOGRAPH OF
BEDROCK CORE
BORING: BB-HSS-119 AND
BB-HSS-121**



BORING ID	CORE ID	CORE RUN DEPTH (FT)	CORE RUN EL. ^{NOTE 1}	RECOVERY		RQD ^{NOTE 2}	
				IN.	%	IN.	%
BB-HSS-118	R1	22.5 to 23.2	112.1 to 111.4	8	100	0	0
BB-HSS-118	R2	23.2 to 25.0	111.4 to 109.6	18	85	16	88
BB-HSS-118	R3	25.0 to 25.9	109.6 to 108.7	11	100	9	81
BB-HSS-118	R4	25.9 to 27.9	108.7 to 106.7	20	83	15	75
BB-HSS-118	R5	27.9 to 32.2	106.7 to 102.4	49	90	39	79
BB-HSS-122	R1	22.5 to 25.7	118.1 to 114.9	38	100	27	71
BB-HSS-122	R2	25.7 to 28.7	114.9 to 111.9	36	100	31	86
BB-HSS-122	R3	28.7 to 32.7	111.9 to 107.9	48	100	38	79

NOTES:

1. ELEVATIONS ARE MEASURED IN FEET AND REFERENCE THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
2. "RQD" INDICATES ROCK QUALITY DESIGNATION (PERCENT OF ROCK PIECES RECOVERED EQUAL TO OR GREATER THAN 4 IN. IN LENGTH).
3. RED LINES DRAWN THROUGH ROCK CORE PHOTOGRAPHS/TABLE INDICATE THAT ROCK CORE WAS COLLECTED FROM AN ADJACENT BRIDGE STRUCTURE. REFER TO OTHER BRIDGE REPORTS.

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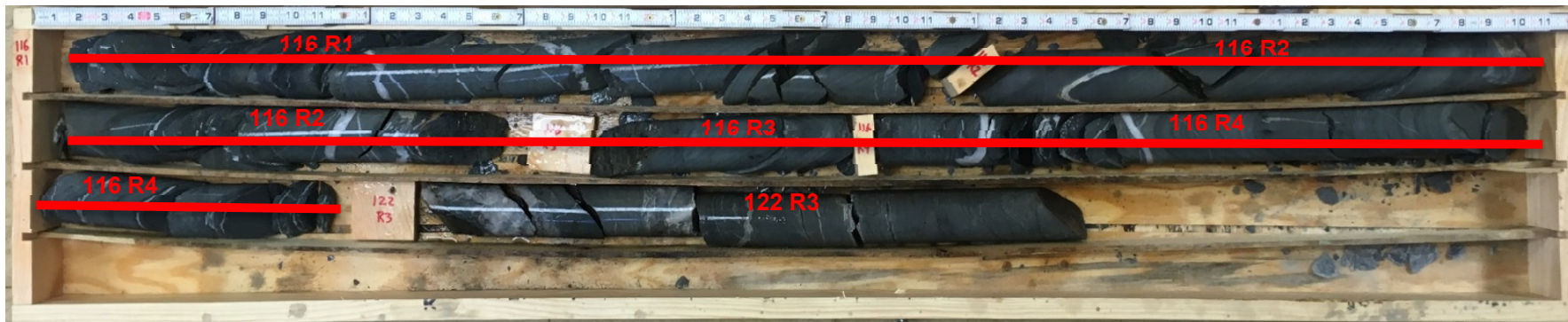
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**PHOTOGRAPH OF
BEDROCK CORE
BORING: BB-HSS-122**

FILE NO. 129380-002

February 2019



BORING ID	CORE ID	CORE RUN DEPTH (FT)	CORE RUN EL. ^{NOTE 1}	RECOVERY		RQD ^{NOTE 2}	
				IN.	%	IN.	%
BB-HSS-116	R1	22.0 to 25.0	112.8 to 109.8	36	100	15	41
BB-HSS-116	R2	25.0 to 28.2	109.8 to 106.6	39	100	13	33
BB-HSS-116	R3	28.2 to 29.0	106.6 to 105.8	10	100	6	60
BB-HSS-116	R4	29.0 to 32.0	105.8 to 102.8	36	100	25	69
BB-HSS-122	R3 cont.	28.7 to 32.7	111.9 to 107.9	48	100	38	79

NOTES:

1. ELEVATIONS ARE MEASURED IN FEET AND REFERENCE THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
2. "RQD" INDICATES ROCK QUALITY DESIGNATION (PERCENT OF ROCK PIECES RECOVERED EQUAL TO OR GREATER THAN 4 IN. IN LENGTH).
3. RED LINES DRAWN THROUGH ROCK CORE PHOTOGRAPHS/TABLE INDICATE THAT ROCK CORE WAS COLLECTED FROM AN ADJACENT BRIDGE STRUCTURE. REFER TO OTHER BRIDGE REPORTS.



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**PHOTOGRAPH OF
BEDROCK CORE
BORING: BB-HSS-122**



BORING ID	CORE ID	CORE RUN DEPTH (FT)	CORE RUN EL. ^{NOTE 1}	RECOVERY		RQD ^{NOTE 2}	
				IN.	%	IN.	%
BB-HSS-124	R3	45.5 TO 47.5	117.3 to 115.3	15	63	7	29
BB-HSS-123	R1	44.2 TO 48.2	118.6 to 114.6	43	90	37	77
BB-HSS-123	R2	48.2 TO 50.8	114.6 to 112.0	31	100	31	100
BB-HSS-123	R3	50.8 TO 55.4	112.0 to 107.4	55	100	53	96

NOTES:

1. ELEVATIONS ARE MEASURED IN FEET AND REFERENCE THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
2. "RQD" INDICATES ROCK QUALITY DESIGNATION (PERCENT OF ROCK PIECES RECOVERED EQUAL TO OR GREATER THAN 4 IN. IN LENGTH).

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**PHOTOGRAPH OF
BEDROCK CORE
BORING: BB-HSS-124
AND BB-HSS-123**

FILE NO. 129380-002

February 2019



BORING ID	CORE ID	CORE RUN DEPTH (FT)	CORE RUN EL. ^{NOTE 1}	RECOVERY		RQD ^{NOTE 2}	
				IN.	%	IN.	%
BB-HSS-114	R1	21.6 to 23.2	113.1 to 111.5	20	100	20	100
BB-HSS-114	R2	23.2 to 28.1	111.5 to 106.6	57	97	34	58
BB-HSS-114	R3	28.1 to 33.4	106.6 to 101.3	54	90	42	70
BB-HSS-124	R1	37.5 to 42.5	125.3 to 120.3	55	92	52	87
BB-HSS-124	R2	42.5 to 45.5	120.3 to 117.3	36	100	28	78

NOTES:

1. ELEVATIONS ARE MEASURED IN FEET AND REFERENCE THE NORTH AMERICAN VERTICAL DATUM OF 1988 (NAVD88).
2. "RQD" INDICATES ROCK QUALITY DESIGNATION (PERCENT OF ROCK PIECES RECOVERED EQUAL TO OR GREATER THAN 4 IN. IN LENGTH).
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PHOTOGRAPH OF BEDROCK CORE BORING: BB-HSS-124

FILE NO. 129380-002

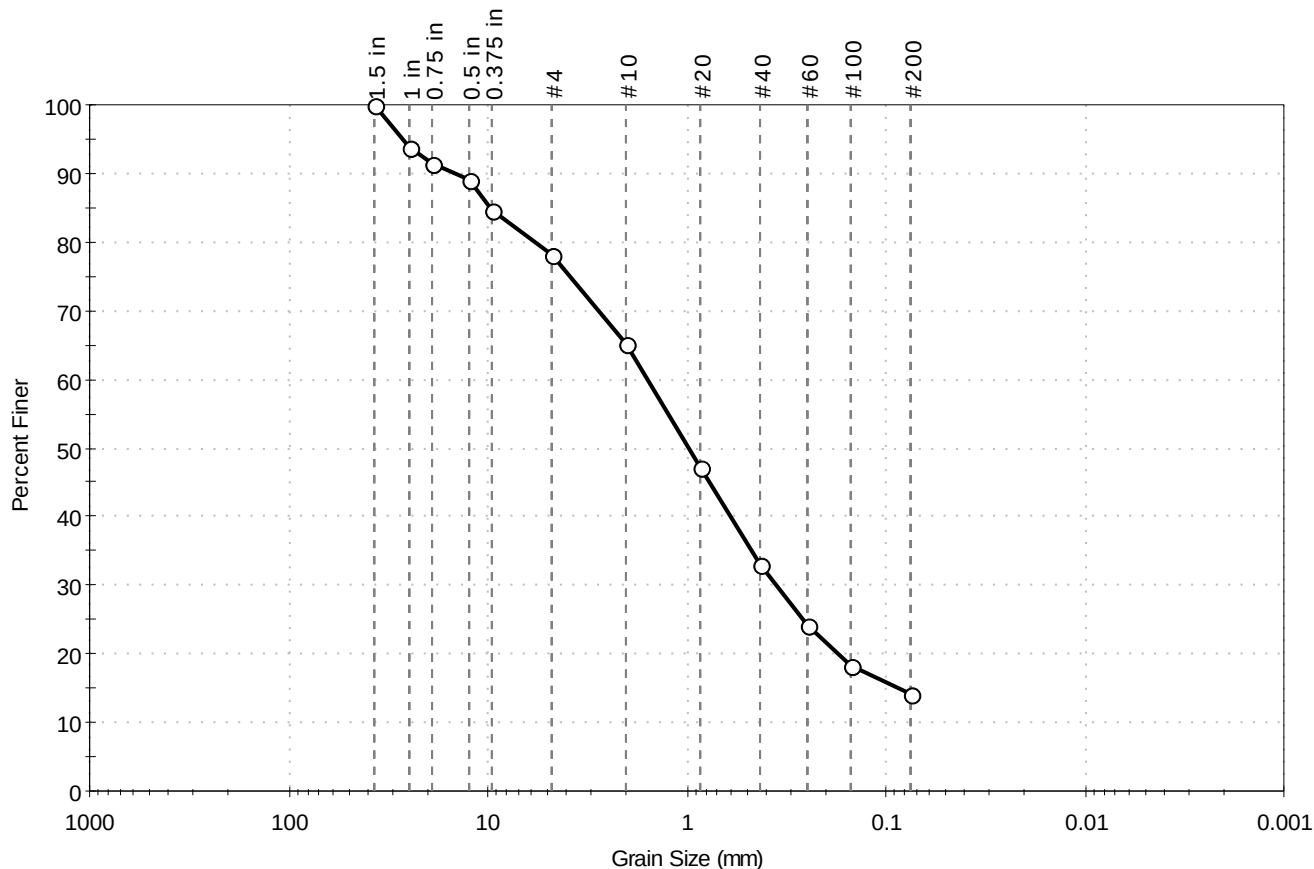
February 2019

APPENDIX C

Laboratory Test Results

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-120	Sample Type:	jar
Sample ID:	2D	Test Date:	10/05/17
Depth:	5.0-7.0 ft	Test Id:	426855
Test Comment:	---		
Visual Description:	Moist, brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D422



% Cobble	% Gravel	% Sand	% Silt & Clay Size
---	22.0	63.8	14.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	94		
0.75 in	19.00	92		
0.5 in	12.50	89		
0.375 in	9.50	85		
#4	4.75	78		
#10	2.00	65		
#20	0.85	47		
#40	0.42	33		
#60	0.25	24		
#100	0.15	18		
#200	0.075	14		

Coefficients

D ₈₅ = 9.7355 mm	D ₃₀ = 0.3550 mm
D ₆₀ = 1.5563 mm	D ₁₅ = 0.0858 mm
D ₅₀ = 0.9676 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

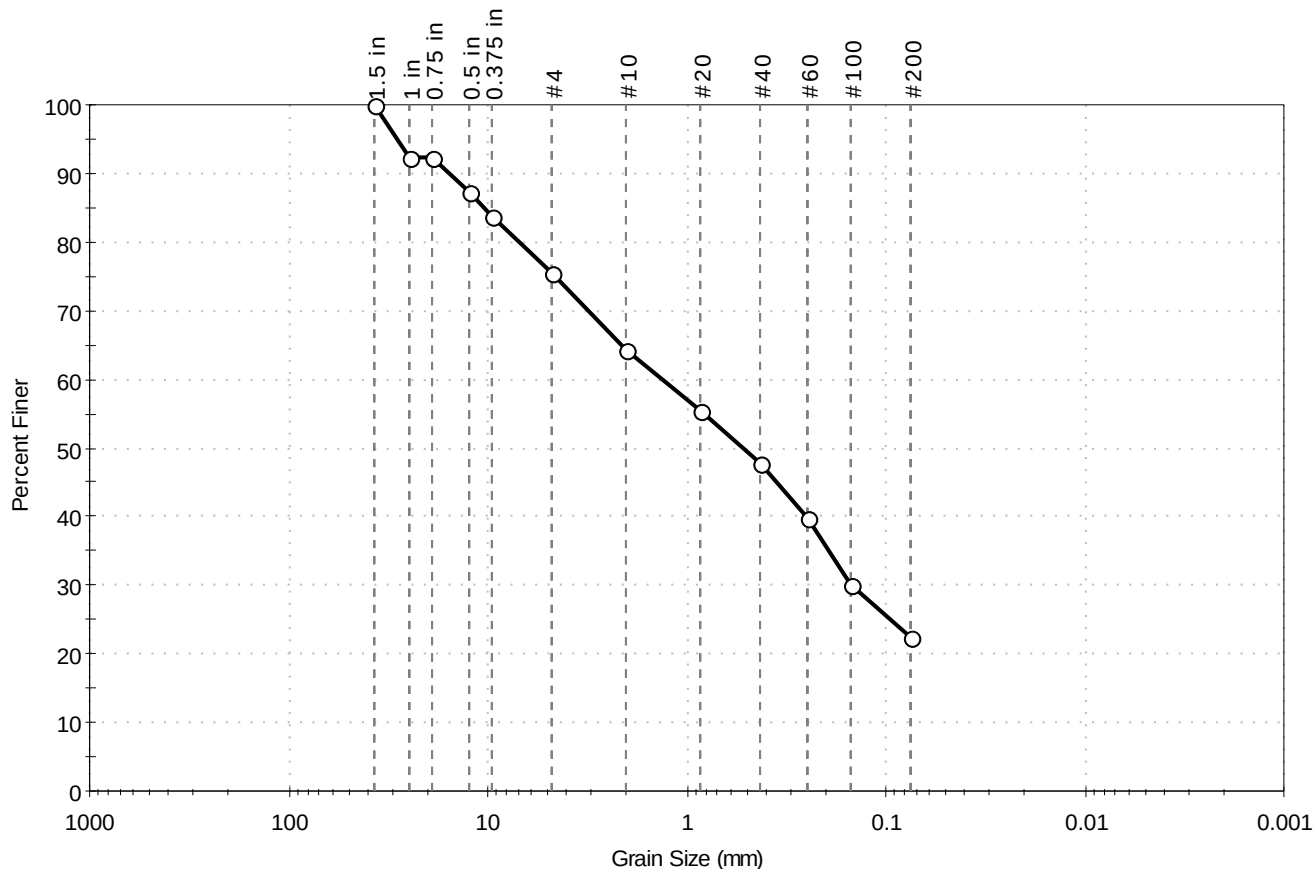
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample / Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-120	Sample Type:	jar
Sample ID:	9D	Test Date:	10/05/17
Depth :	20.0-22.0 ft	Test Id:	426856
Test Comment:	---		
Visual Description:	Moist, brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D422



% Cobble	% Gravel	% Sand	% Silt & Clay Size
---	24.6	53.1	22.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	92		
0.75 in	19.00	92		
0.5 in	12.50	87		
0.375 in	9.50	84		
#4	4.75	75		
#10	2.00	64		
#20	0.85	55		
#40	0.42	48		
#60	0.25	40		
#100	0.15	30		
#200	0.075	22		

Coefficients

D ₈₅ = 10.3823 mm	D ₃₀ = 0.1484 mm
D ₆₀ = 1.3175 mm	D ₁₅ = N/A
D ₅₀ = 0.5229 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

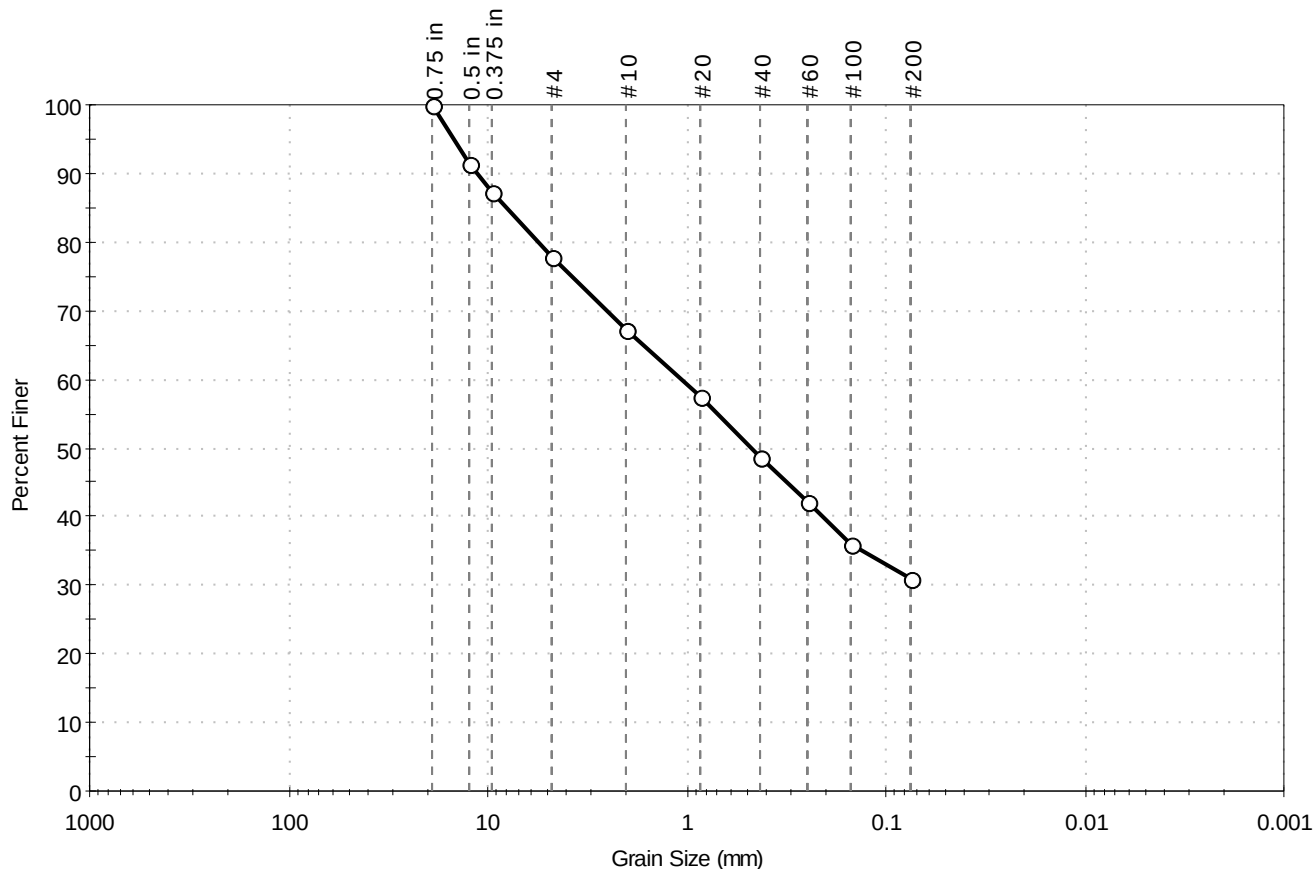
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample / Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-121	Sample Type:	jar
Sample ID:	3D	Test Date:	10/05/17
Depth :	4.0-6.0 ft	Test Id:	426857
Test Comment:	---		
Visual Description:	Moist, brown clayey sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D422



% Cobble	% Gravel	% Sand	% Silt & Clay Size
---	22.0	47.1	30.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	91		
0.375 in	9.50	87		
#4	4.75	78		
#10	2.00	67		
#20	0.85	57		
#40	0.42	49		
#60	0.25	42		
#100	0.15	36		
#200	0.075	31		

Coefficients

D ₈₅ = 8.0383 mm	D ₃₀ = N/A
D ₆₀ = 1.0661 mm	D ₁₅ = N/A
D ₅₀ = 0.4730 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

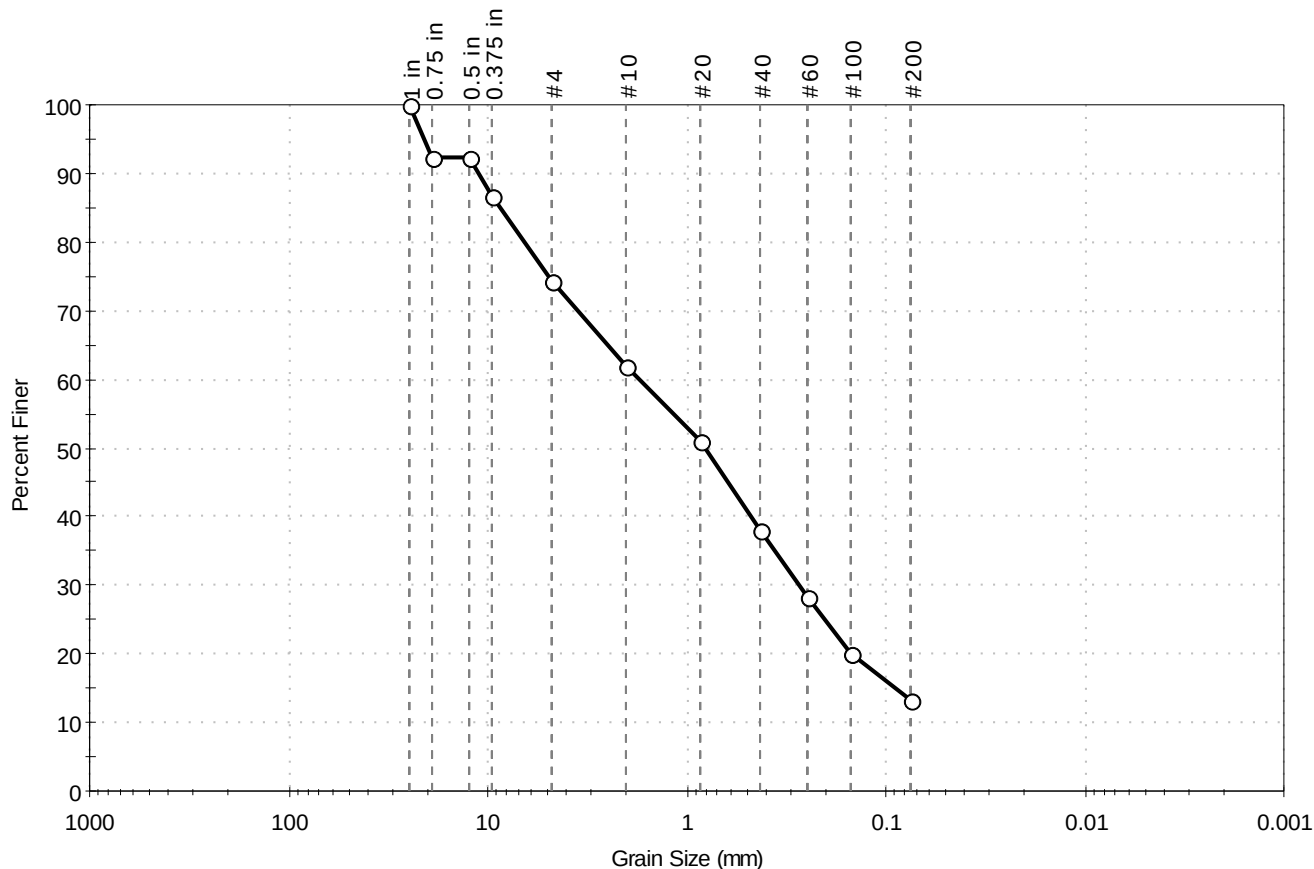
AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample / Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-121	Sample Type:	jar
Sample ID:	5D	Test Date:	10/05/17
Depth :	8.0-10.0 ft	Test Id:	426858
Test Comment:	---		
Visual Description:	Moist, brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D422



% Cobble	% Gravel	% Sand	% Silt & Clay Size
---	25.8	60.8	13.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	92		
0.5 in	12.50	92		
0.375 in	9.50	87		
#4	4.75	74		
#10	2.00	62		
#20	0.85	51		
#40	0.42	38		
#60	0.25	28		
#100	0.15	20		
#200	0.075	13		

Coefficients

D ₈₅ = 8.6753 mm	D ₃₀ = 0.2728 mm
D ₆₀ = 1.7215 mm	D ₁₅ = 0.0883 mm
D ₅₀ = 0.8084 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

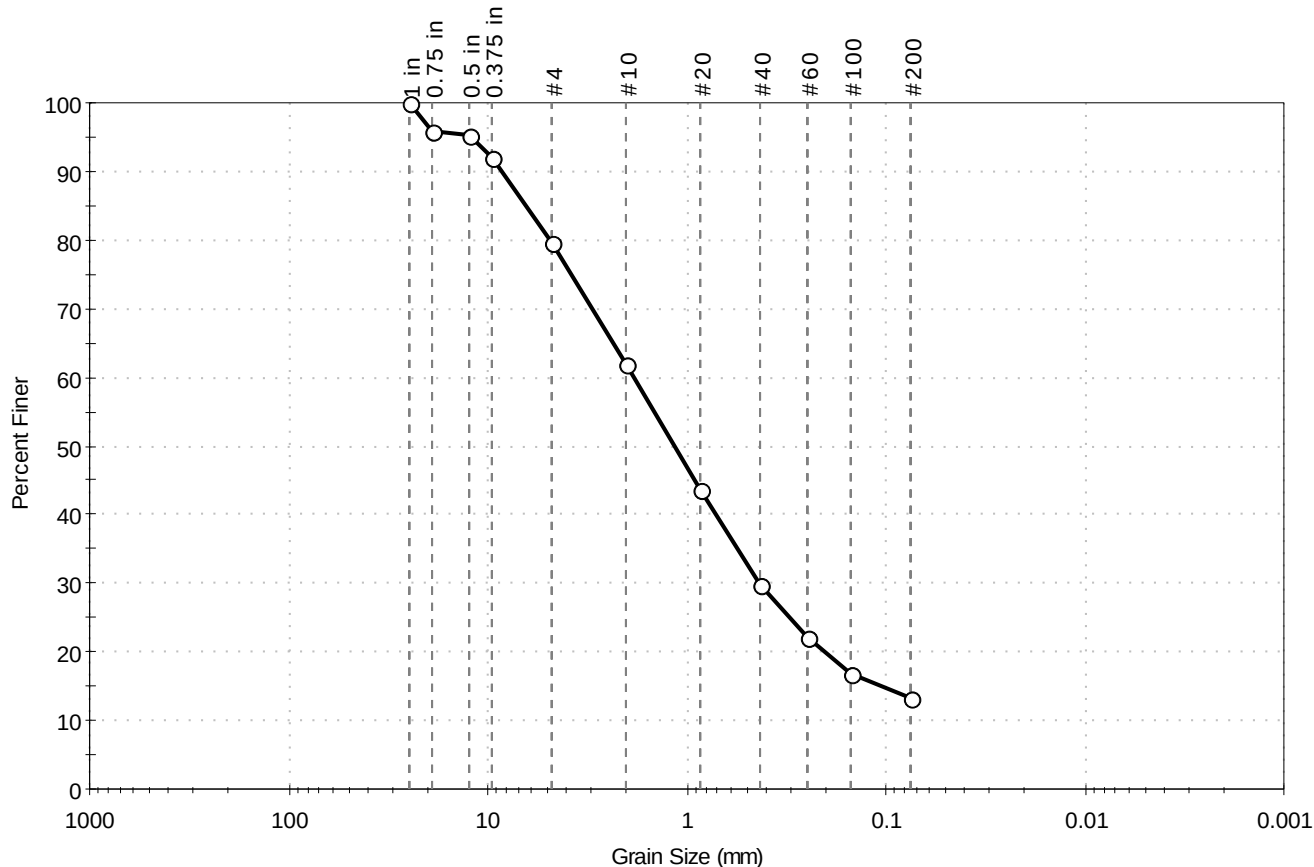
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample / Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-123	Sample Type:	jar
Sample ID:	2D	Test Date:	10/05/17
Depth :	2.5-4.5 ft	Test Id:	426859
Test Comment:	---		
Visual Description:	Moist, brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D422



% Cobble	% Gravel	% Sand	% Silt & Clay Size
---	20.2	66.4	13.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	95		
0.375 in	9.50	92		
#4	4.75	80		
#10	2.00	62		
#20	0.85	44		
#40	0.425	30		
#60	0.25	22		
#100	0.15	17		
#200	0.075	13		

Coefficients

D ₈₅ = 6.4015 mm	D ₃₀ = 0.4264 mm
D ₆₀ = 1.8334 mm	D ₁₅ = 0.1047 mm
D ₅₀ = 1.1465 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

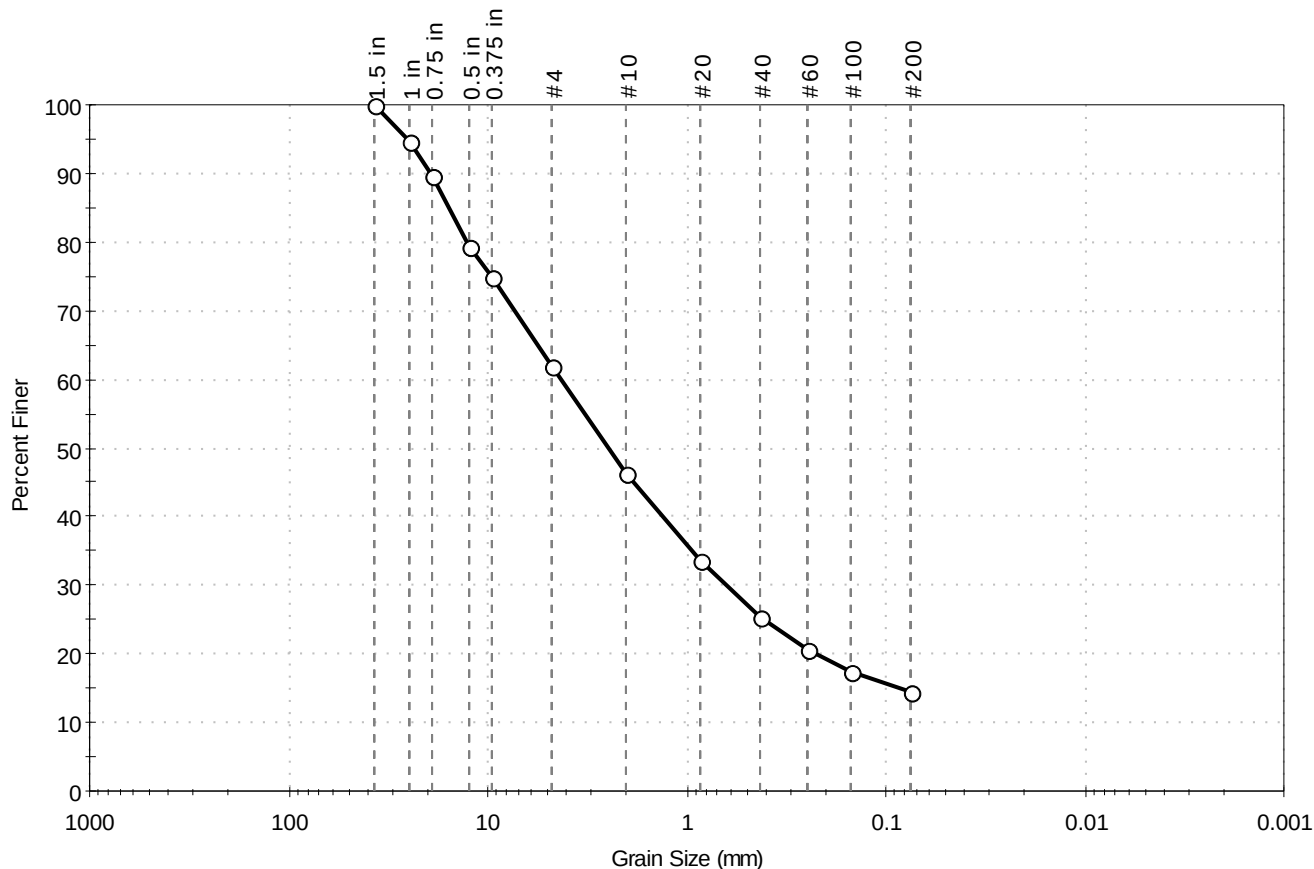
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample / Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-124	Sample Type:	jar
Sample ID:	2D	Test Date:	10/05/17
Depth :	3.5-5.5 ft	Test Id:	426860
Test Comment:	---		
Visual Description:	Moist, brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D422



% Cobble	% Gravel	% Sand	% Silt & Clay Size
---	38.1	47.3	14.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	95		
0.75 in	19.00	90		
0.5 in	12.50	79		
0.375 in	9.50	75		
#4	4.75	62		
#10	2.00	46		
#20	0.85	34		
#40	0.42	25		
#60	0.25	21		
#100	0.15	17		
#200	0.075	15		

Coefficients

D ₈₅ = 15.6934 mm	D ₃₀ = 0.6288 mm
D ₆₀ = 4.2877 mm	D ₁₅ = 0.0836 mm
D ₅₀ = 2.4433 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

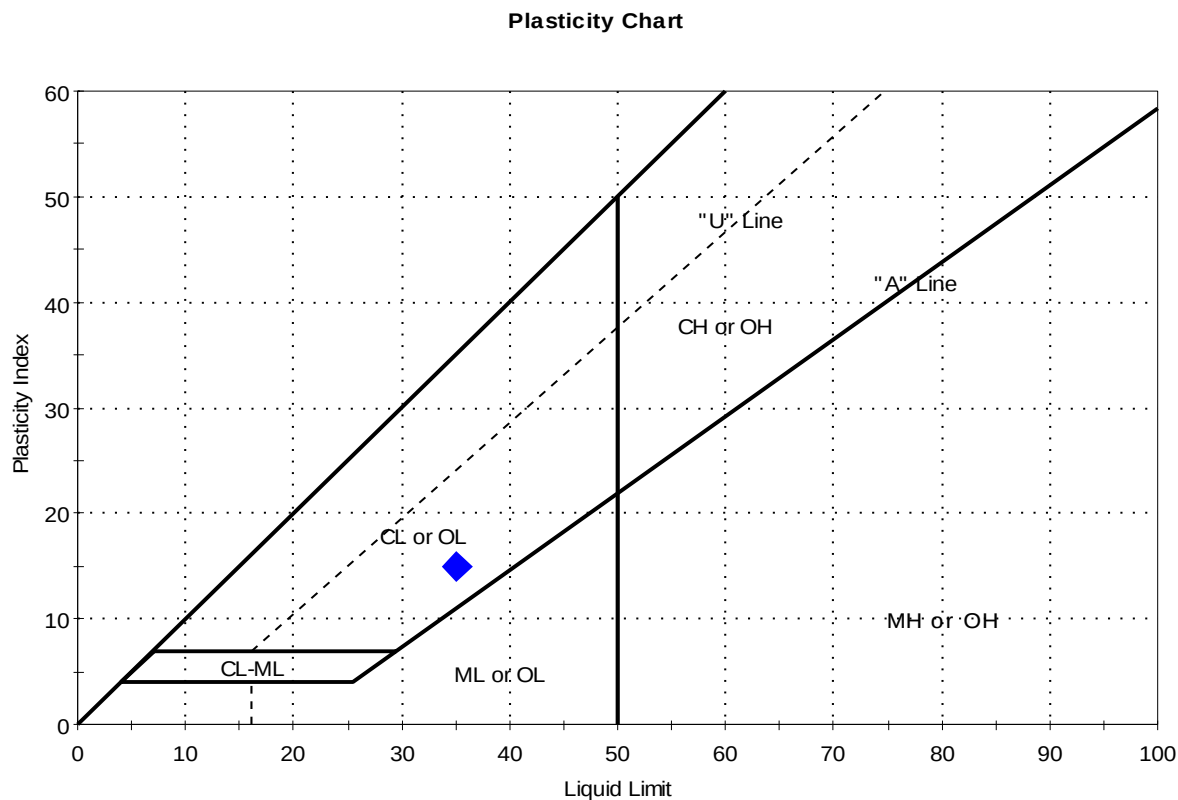
AASHTO Stone Fragments, Gravel and Sand (A-1-a (0))

Sample / Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-119	Sample Type:	jar
Sample ID:	16D	Test Date:	10/06/17
Depth :	34.0-36.0 ft	Test Id:	426850
Test Comment:	---		
Visual Description:	Moist, brown clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	16D	B-HSS-119	34.0-36.0 ft	26	35	20	15	0.4	

Sample Prepared using the WET method

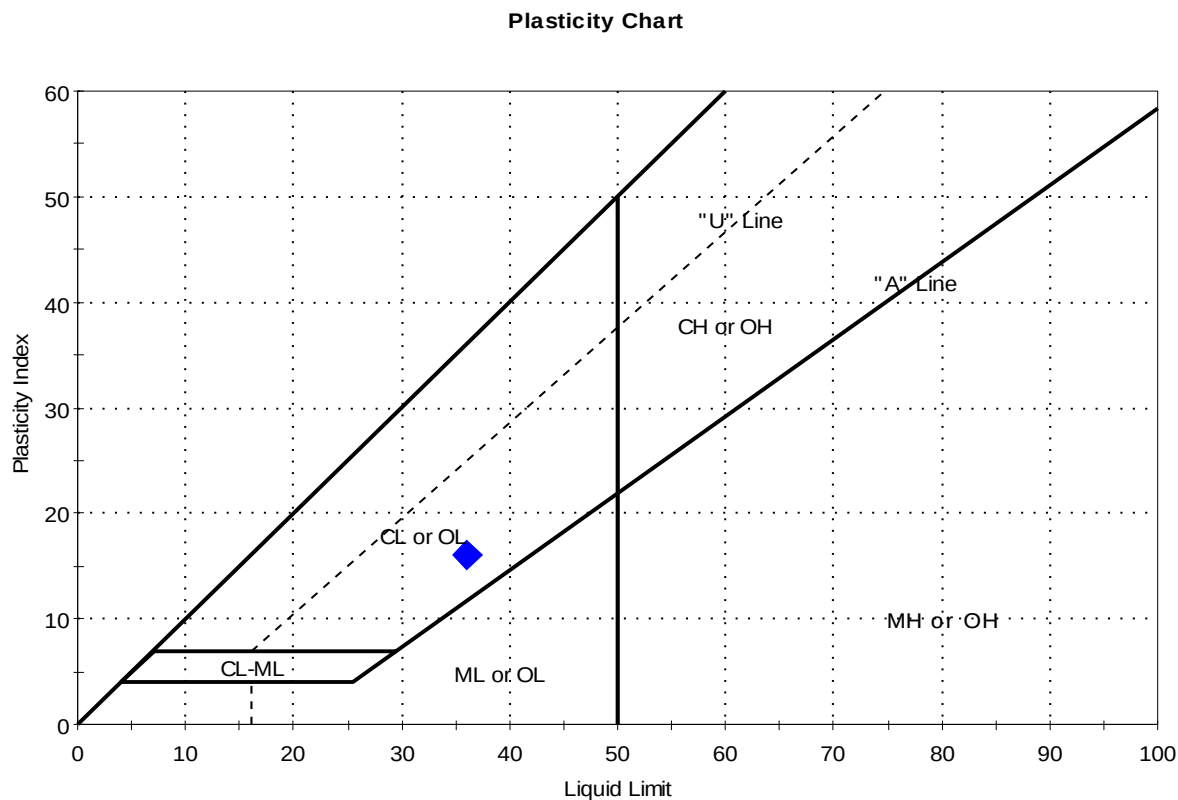
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-120	Sample Type:	jar
Sample ID:	12D	Test Date:	10/06/17
Depth :	30.0-32.0 ft	Test Id:	426851
Test Comment:	---		
Visual Description:	Moist, olive clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	12D	B-HSS-120	30.0-32.0 ft	25	36	20	16	0.3	

Sample Prepared using the WET method

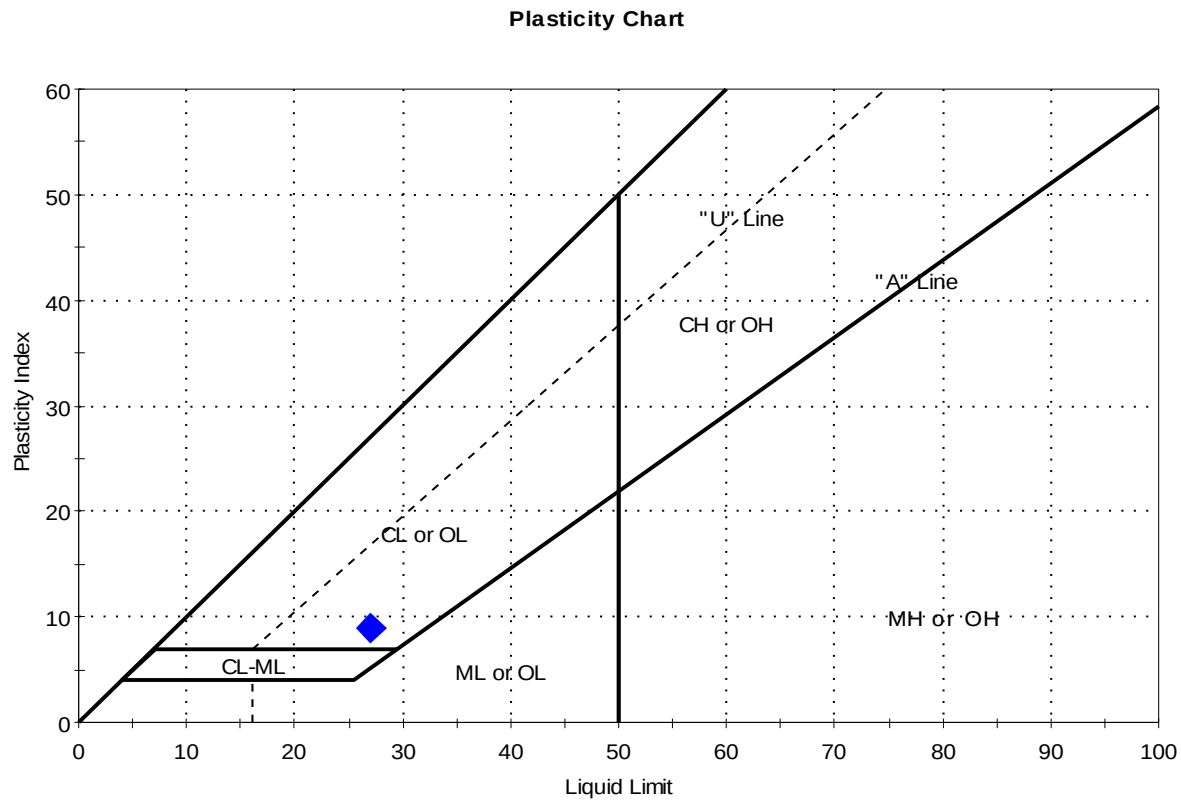
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	Haley & Aldrich, Inc.	Project No:	GTX-307094
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME		
Boring ID:	BB-HSS-122	Sample Type:	jar
Sample ID:	5D	Test Date:	10/06/17
Depth :	8.0-10.0 ft	Test Id:	426852
Test Comment:	---		
Visual Description:	Moist, brown clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	5D	B-HSS-12	8.0-10.0 ft	25	27	18	9	0.8	

Sample Prepared using the WET method

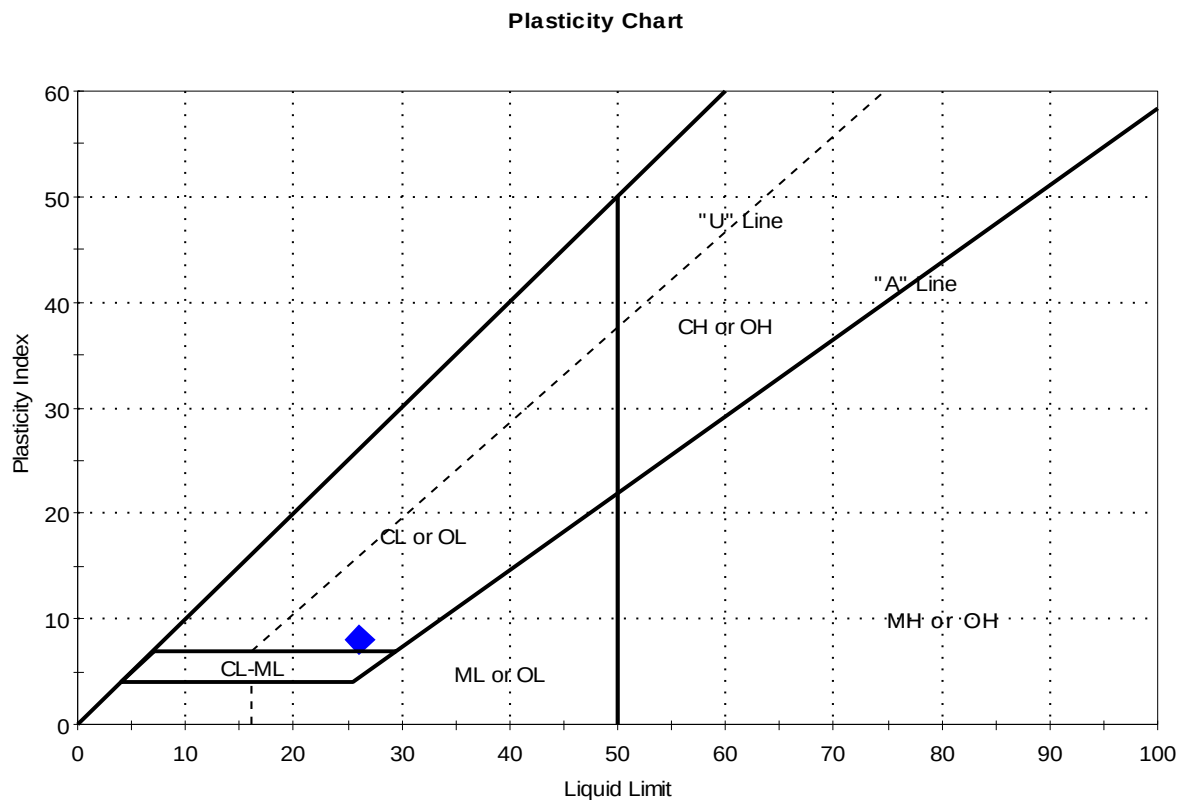
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	Haley & Aldrich, Inc.		
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME	Project No:	GTX-307094
Boring ID:	BB-HSS-123	Sample Type:	jar
Sample ID:	16D	Test Date:	10/05/17
Depth:	35.0-37.0 ft	Test Id:	426853
Test Comment:	---		
Visual Description:	Moist, olive brown clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	16D	B-HSS-123	35.0-37.0 ft	24	26	18	8	0.7	

Sample Prepared using the WET method

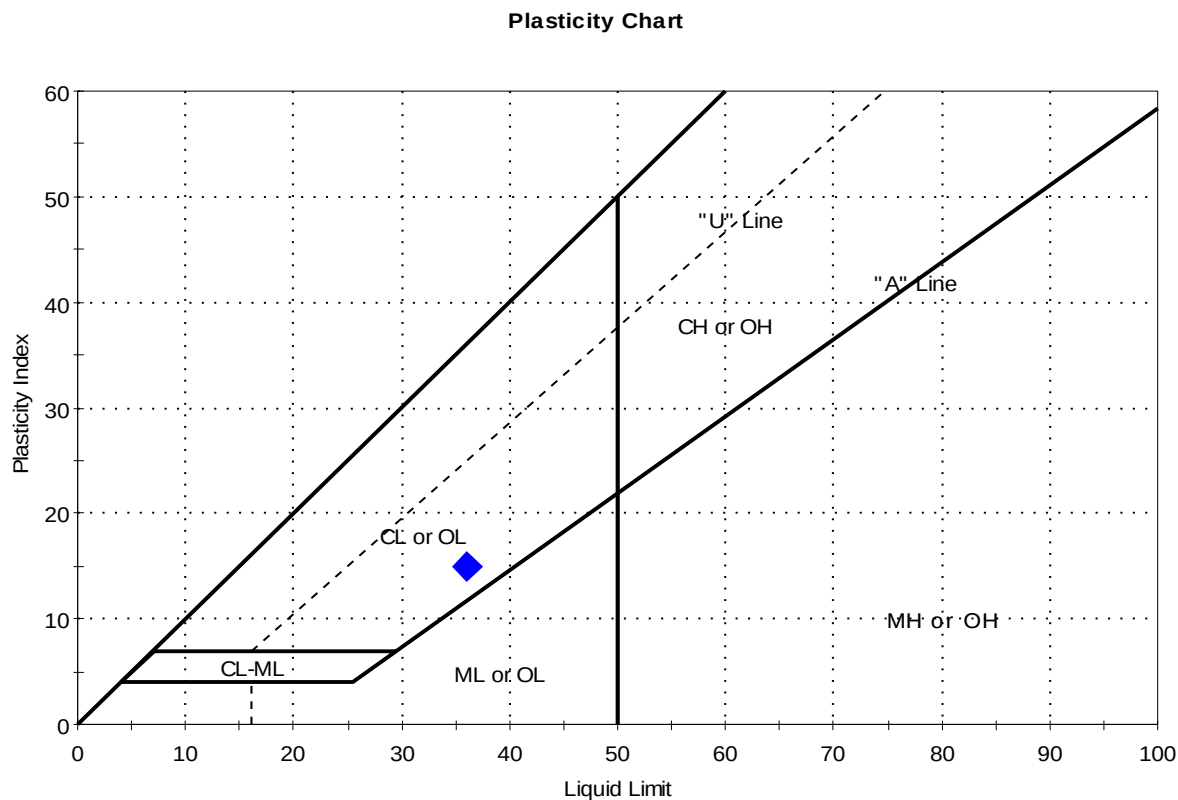
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	Haley & Aldrich, Inc.	Project No:	GTX-307094
Project:	Emerson Mill Bridge #1430 and 5969		
Location:	Hampden, ME		
Boring ID:	BB-HSS-124	Sample Type:	jar
Sample ID:	11D	Test Date:	10/06/17
Depth :	30.0-32.0 ft	Test Id:	426854
Test Comment:	---	Tested By:	cam
Visual Description:	Moist, olive brown clay	Checked By:	emm
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	11D	B-HSS-124	30.0-32.0 ft	27	36	21	15	0.4	

Sample Prepared using the WET method

Dry Strength: VERY HIGH

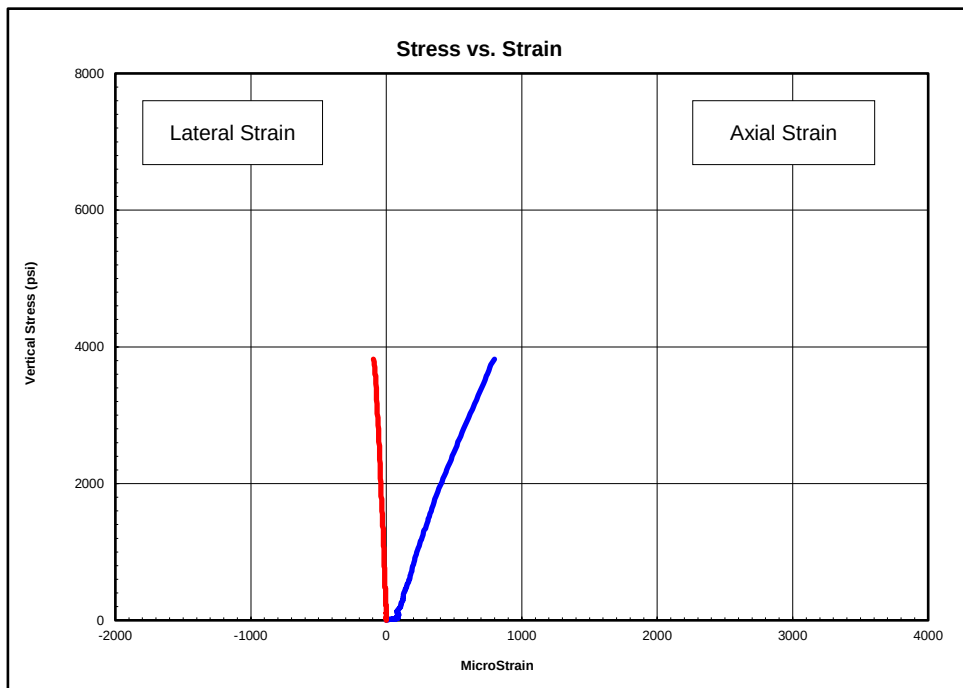
Dilatancy: SLOW

Toughness: LOW



Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-119
Sample ID:	R1
Depth, ft:	55.02-55.38
Sample Type:	rock core
Sample Description:	See photographs Discontinuity failure

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 3,815 psi

One lateral strain gauge failed to record meaningful data. Poisson's Ratio reported based on results of a single lateral strain gauge.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
400-1400	6,270,000	0.13
1400-2400	5,240,000	0.13
2400-3400	4,600,000	0.13

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

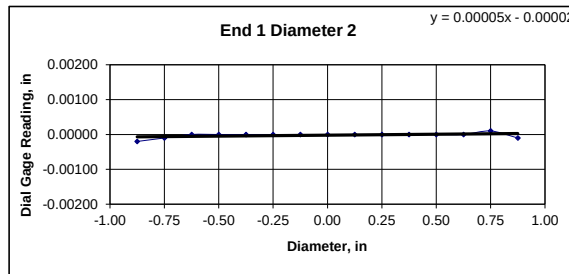
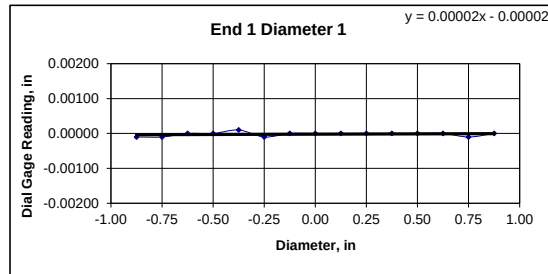


Client:	Haley & Aldrich, Inc.	Test Date:	10/3/2017
Project Name:	Emerson Mill Bridge #1430 and 5969	Tested By:	rlc
Project Location:	Hampden, ME	Checked By:	jsc
GTX #:	307094		
Boring ID:	BB-HSS-119		
Sample ID:	R1		
Depth:	55.02-55.38 ft		
Visual Description:	See photographs		

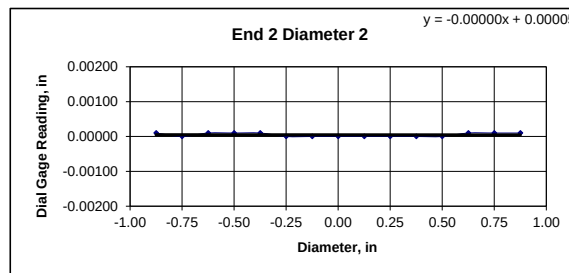
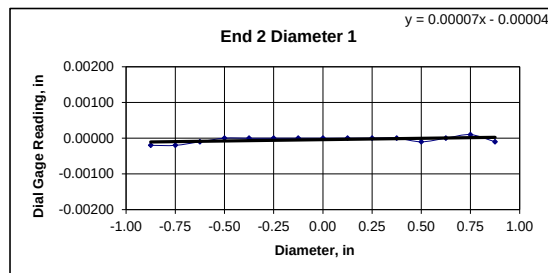
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? YES	
Specimen Length, in:	4.36	4.36	4.36	Maximum difference must be $<$ 0.020 in.	
Specimen Diameter, in:	1.99	1.99	1.99	Straightness Tolerance Met? YES	
Specimen Mass, g:	605.22				
Bulk Density, lb/ft ³ :	170				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES			
		Length to Diameter Ratio Tolerance Met? YES			

END FLATNESS AND PARALLELISM (Procedure FP1)															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00010	-0.00010	0.00000	0.00000	0.00010	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00010	0.00000
Diameter 2, in (rotated 90°)	-0.00020	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010	-0.00010
Difference between max and min readings, in: 0° = 0.00020 90° = 0.00030															
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00020	-0.00020	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00010	0.00000	0.00010	-0.00010
Diameter 2, in (rotated 90°)	0.00010	0.00000	0.00010	0.00010	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010	0.00010	0.00010
Difference between max and min readings, in: 0° = 0.0003 90° = 0.0001 Maximum difference must be < 0.0020 in. Difference = ± 0.00015															
Flatness Tolerance Met? YES															



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00002
Angle of Best Fit Line:	0.00115
End 2:	
Slope of Best Fit Line	0.00007
Angle of Best Fit Line:	0.00401
Maximum Angular Difference:	0.00286
Parallelism Tolerance Met? Spherically Seated	YES

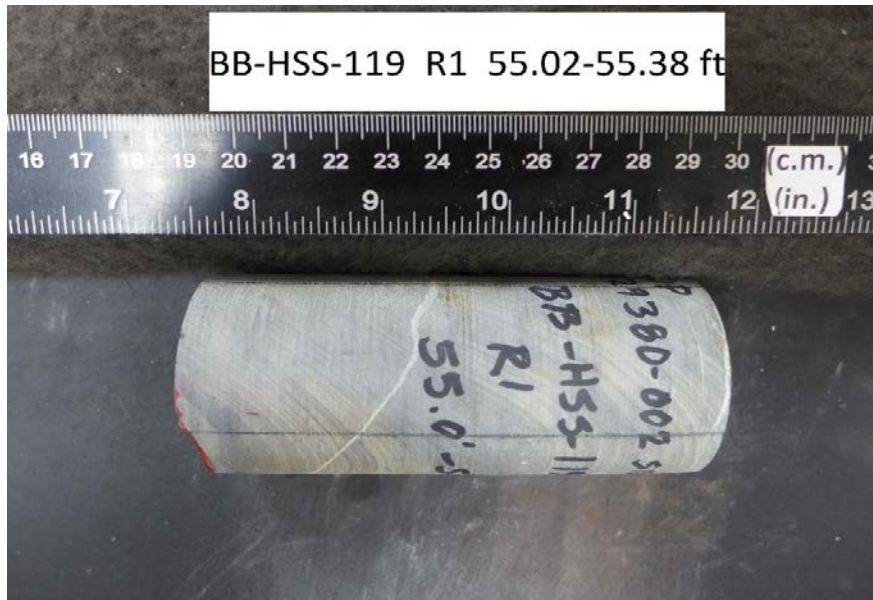


DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00005
Angle of Best Fit Line:	0.00286
End 2:	
Slope of Best Fit Line	0.00000
Angle of Best Fit Line:	0.00000
Maximum Angular Difference:	0.00286
Parallelism Tolerance Met? Spherically Seated	YES

PERPENDICULARITY (Procedure P1)						Maximum angle of departure must be $\leq$ 0.25°	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?		
Diameter 1, in	0.00020	1.990	0.00010	0.006	YES		
Diameter 2, in (rotated 90°)	0.00030	1.990	0.00015	0.009	YES	Perpendicularity Tolerance Met? YES	
END 2							
Diameter 1, in	0.00030	1.990	0.00015	0.009	YES		
Diameter 2, in (rotated 90°)	0.00010	1.990	0.00005	0.003	YES		



Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-119
Sample ID:	R1
Depth, ft:	55.02-55.38



After cutting and grinding

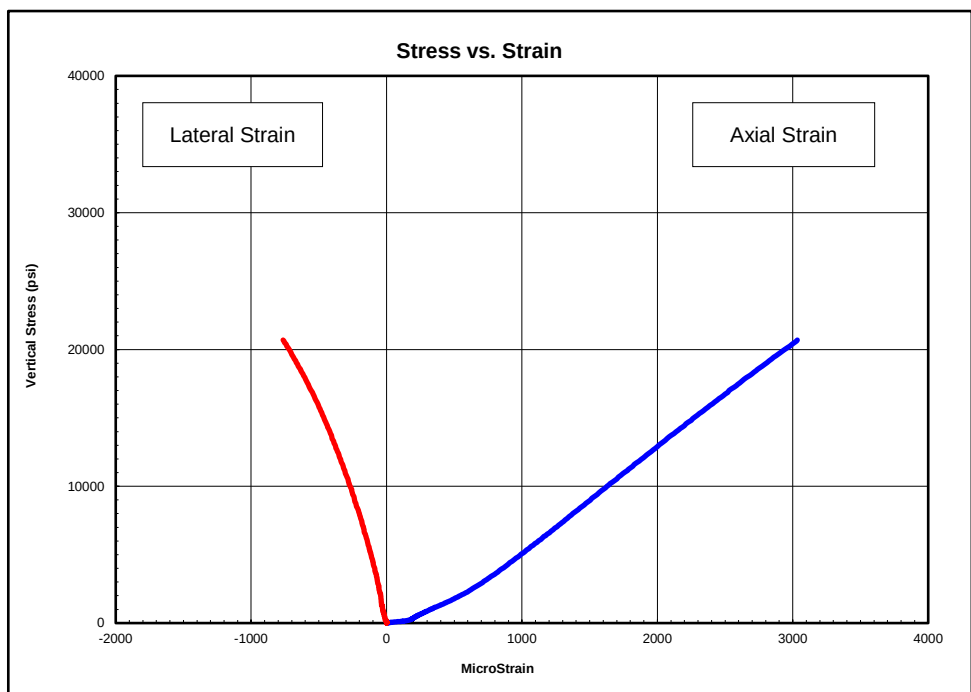


After break



Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-120
Sample ID:	R3
Depth, ft:	45.2-45.56
Sample Type:	rock core
Sample Description:	See photographs Intact material failure

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 20,734 psi

One axial strain gauge failed to record meaningful data. Young's Modulus and Poisson's Ratio reported based on results of a single axial strain gauge.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
2100-7600	7,280,000	0.19
7600-13100	7,880,000	0.28
13100-18600	7,600,000	0.35

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

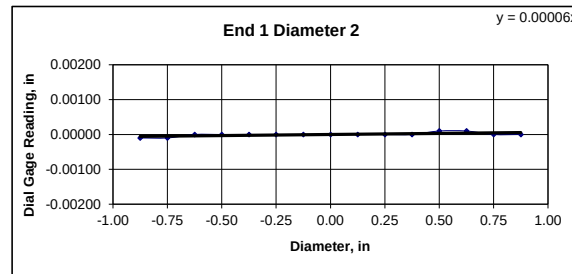
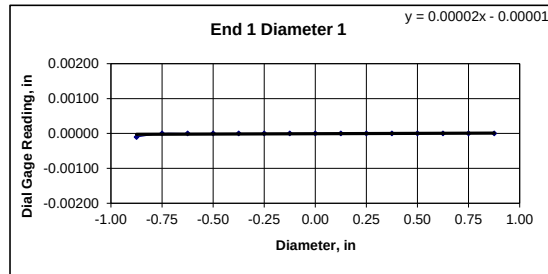


Client:	Haley & Aldrich, Inc.	Test Date:	10/3/2017
Project Name:	Emerson Mill Bridge #1430 and 5969	Tested By:	rlc
Project Location:	Hampden, ME	Checked By:	jsc
GTX #:	307094		
Boring ID:	BB-HSS-120		
Sample ID:	R3		
Depth:	45.2-45.56 ft		
Visual Description:	See photographs		

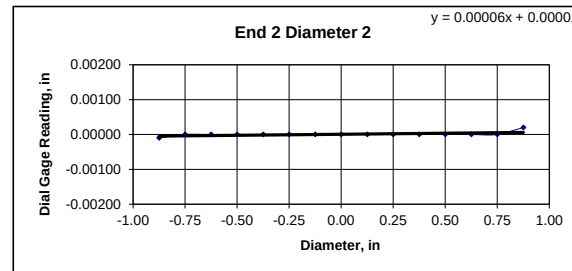
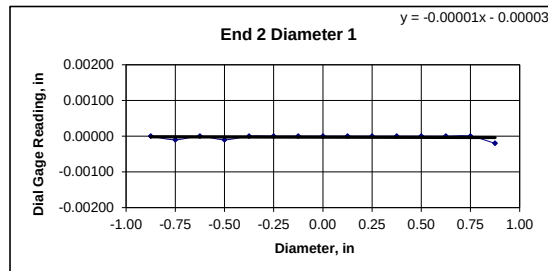
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? YES	
Specimen Length, in:	4.29	4.29	4.29	Maximum difference must be < 0.020 in.	
Specimen Diameter, in:	1.99	1.99	1.99	Straightness Tolerance Met? YES	
Specimen Mass, g:	596.77				
Bulk Density, lb/ft ³ :	170				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES			
		Length to Diameter Ratio Tolerance Met? YES			

END FLATNESS AND PARALLELISM (Procedure FP1)														
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Diameter 2, in (rotated 90°)	-0.00010	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010	0.00010	0.00000
Difference between max and min readings, in:														
0° = 0.00010 90° = 0.00020														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	0.00000	-0.00010	0.00000	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00020
Diameter 2, in (rotated 90°)	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00020
Difference between max and min readings, in:														
0° = 0.0002 90° = 0.0003														
Maximum difference must be < 0.0020 in. Difference = ± 0.00015														
Flatness Tolerance Met? YES														



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00002
Angle of Best Fit Line:	0.00115
End 2:	
Slope of Best Fit Line	0.00001
Angle of Best Fit Line:	0.00057
Maximum Angular Difference:	0.00057
Parallelism Tolerance Met? Spherically Seated	YES



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00006
Angle of Best Fit Line:	0.00344
End 2:	
Slope of Best Fit Line	0.00006
Angle of Best Fit Line:	0.00344
Maximum Angular Difference:	0.00000
Parallelism Tolerance Met? Spherically Seated	YES

PERPENDICULARITY (Procedure P1)					(Calculated from End Flatness and Parallelism measurements above)	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$
Diameter 1, in	0.00010	1.990	0.00005	0.003	YES	
Diameter 2, in (rotated 90°)	0.00020	1.990	0.00010	0.006	YES	Perpendicularity Tolerance Met? YES
END 2						
Diameter 1, in	0.00020	1.990	0.00010	0.006	YES	
Diameter 2, in (rotated 90°)	0.00030	1.990	0.00015	0.009	YES	



Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-120
Sample ID:	R3
Depth, ft:	45.2-45.56



After cutting and grinding

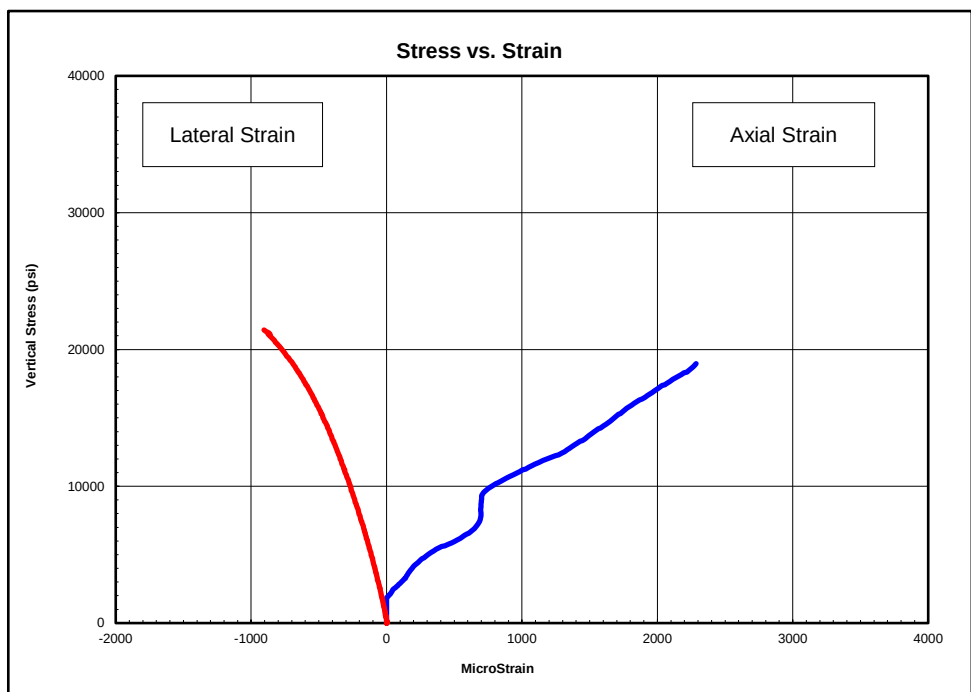


After break



Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-123
Sample ID:	R1
Depth, ft:	46.3-46.65
Sample Type:	rock core
Sample Description:	See photographs Intact material failure

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 21,452 psi

One axial strain gauge failed to record meaningful data. Young's Modulus and Poisson's Ratio reported based on results of a single axial strain gauge.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
2100-7900	8,710,000	0.24
7900-13600	6,760,000	0.24
13600-19300	6,750,000	0.37

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

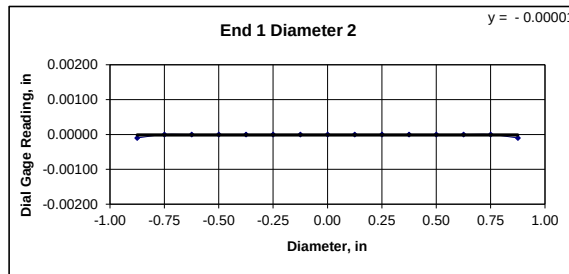
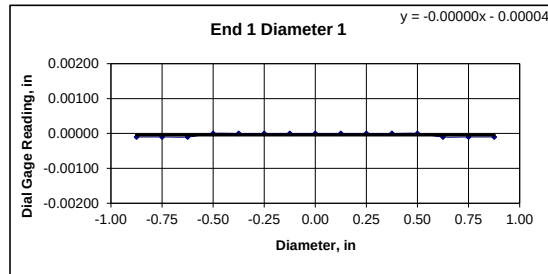


Client:	Haley & Aldrich, Inc.	Test Date:	10/3/2017
Project Name:	Emerson Mill Bridge #1430 and 5969	Tested By:	rlc
Project Location:	Hampden, ME	Checked By:	jsc
GTX #:	307094		
Boring ID:	BB-HSS-123		
Sample ID:	R1		
Depth:	46.3-46.65 ft		
Visual Description:	See photographs		

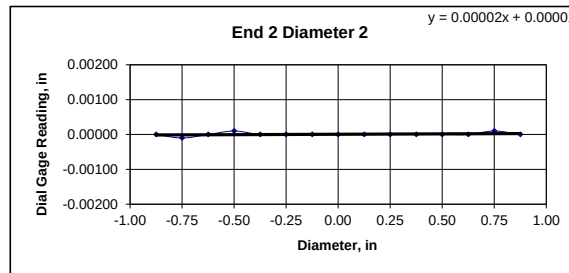
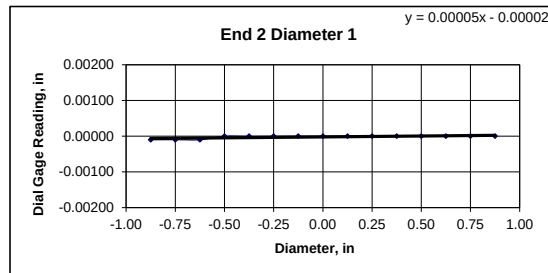
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap $\leq$ 0.02 in.? YES	
Specimen Length, in:	4.26	4.26	4.26	Maximum difference must be < 0.020 in.	
Specimen Diameter, in:	1.99	1.99	1.99	Straightness Tolerance Met? YES	
Specimen Mass, g:	592.13				
Bulk Density, lb/ft ³ :	170				
Length to Diameter Ratio:	2.1	Minimum Diameter Tolerance Met? YES			
		Length to Diameter Ratio Tolerance Met? YES			

END FLATNESS AND PARALLELISM (Procedure FP1)															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00010	-0.00010	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00010	-0.00010	-0.00010
Diameter 2, in (rotated 90°)	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00010
Difference between max and min readings, in: 0° = 0.00010 90° = 0.00010															
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00010	-0.00010	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Diameter 2, in (rotated 90°)	0.00000	-0.00010	0.00000	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010	0.00000
Difference between max and min readings, in: 0° = 0.0001 90° = 0.0002 Maximum difference must be < 0.0020 in. Difference = ± 0.00010															
Flatness Tolerance Met? YES															



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00000
Angle of Best Fit Line:	0.00000
End 2:	
Slope of Best Fit Line	0.00005
Angle of Best Fit Line:	0.00286
Maximum Angular Difference:	0.00286
Parallelism Tolerance Met? Spherically Seated	YES



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00001
Angle of Best Fit Line:	0.00057
End 2:	
Slope of Best Fit Line	0.00002
Angle of Best Fit Line:	0.00115
Maximum Angular Difference:	0.00057
Parallelism Tolerance Met? Spherically Seated	YES

PERPENDICULARITY (Procedure P1)						Maximum angle of departure must be $\leq 0.25^\circ$	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?		
Diameter 1, in	0.00010	1.990	0.00005	0.003	YES		
Diameter 2, in (rotated 90°)	0.00010	1.990	0.00005	0.003	YES	Perpendicularity Tolerance Met? YES	
END 2							
Diameter 1, in	0.00010	1.990	0.00005	0.003	YES		
Diameter 2, in (rotated 90°)	0.00020	1.990	0.00010	0.006	YES		

Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-123
Sample ID:	R1
Depth, ft:	46.3-46.65



After cutting and grinding

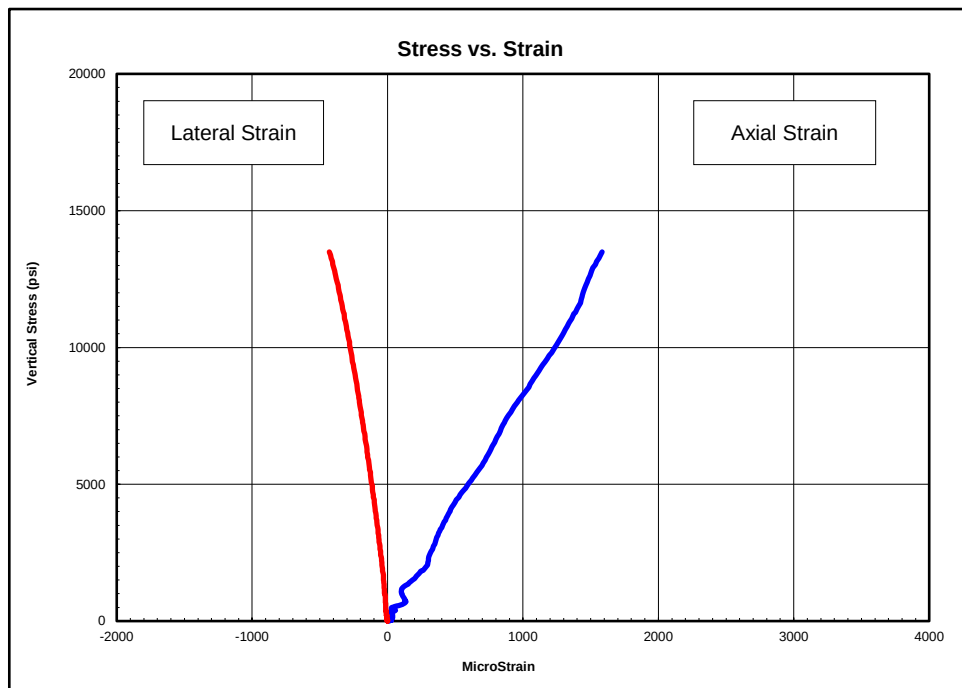


After break



Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-124
Sample ID:	R1
Depth, ft:	37.83-38.2
Sample Type:	rock core
Sample Description:	See photographs Intact material failure

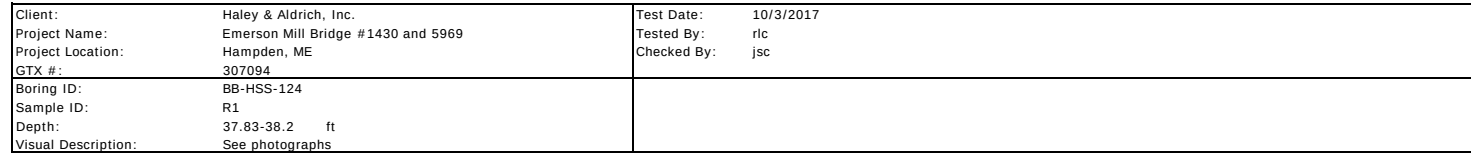
Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 13,492 psi

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
1300-4900	9,350,000	0.23
4900-8500	8,480,000	0.26
8500-12100	8,250,000	0.31

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.



BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)			
	1	2	Average				
Specimen Length, in:	4.31	4.31	4.31	Maximum gap between side of core and reference surface plate:			
Specimen Diameter, in:	1.99	1.99	1.99	Is the maximum gap $\leq$ 0.02 in.? YES			
Specimen Mass, g:	598.02						
Bulk Density, lb/ft ³	170	Minimum Diameter Tolerance Met?	YES	<i>Maximum difference must be < 0.020 in.</i>			
Length to Diameter Ratio:	2.2	Length to Diameter Ratio Tolerance Met?	YES	Straightness Tolerance Met? YES			

End 1 Diameter 1 $y = 0.00009x - 0.00004$

End 1 Diameter 2 $y = 0.00002x - 0.00001$

End 2 Diameter 1 $y = 0.00003x - 0.00003$

End 2 Diameter 2 $y = -0.00005x - 0.00002$

DIAMETER 1		
End 1:	Slope of Best Fit Line	0.00009
	Angle of Best Fit Line:	0.00516
End 2:	Slope of Best Fit Line	0.00003
	Angle of Best Fit Line:	0.00172
Maximum Angular Difference:		0.00344
Parallelism Tolerance Met?		YES
Spherically Seated		

DIAMETER 2		
End 1:	Slope of Best Fit Line	0.00002
	Angle of Best Fit Line:	0.00115
End 2:	Slope of Best Fit Line	0.00005
	Angle of Best Fit Line:	0.00286
Maximum Angular Difference:		0.00172
Parallelism Tolerance Met?		YES
Spherically Seated		

PERPENDICULARITY (Procedure P1)		(Calculated from End Flatness and Parallelism measurements above)			Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle*		
Diameter 1, in	0.00030	1.990	0.00015	0.009	YES	Perpendicularity Tolerance Met? YES
Diameter 2, in (rotated 90°)	0.00010	1.990	0.00005	0.003	YES	
END 2						
Diameter 1, in	0.00010	1.990	0.00005	0.003	YES	
Diameter 2, in (rotated 90°)	0.00030	1.990	0.00015	0.009	YES	

Client:	Haley & Aldrich, Inc.
Project Name:	Emerson Mill Bridge #1430 and 5969
Project Location:	Hampden, ME
GTX #:	307094
Test Date:	10/4/2017
Tested By:	rlc
Checked By:	jsc
Boring ID:	BB-HSS-124
Sample ID:	R1
Depth, ft:	37.83-38.2



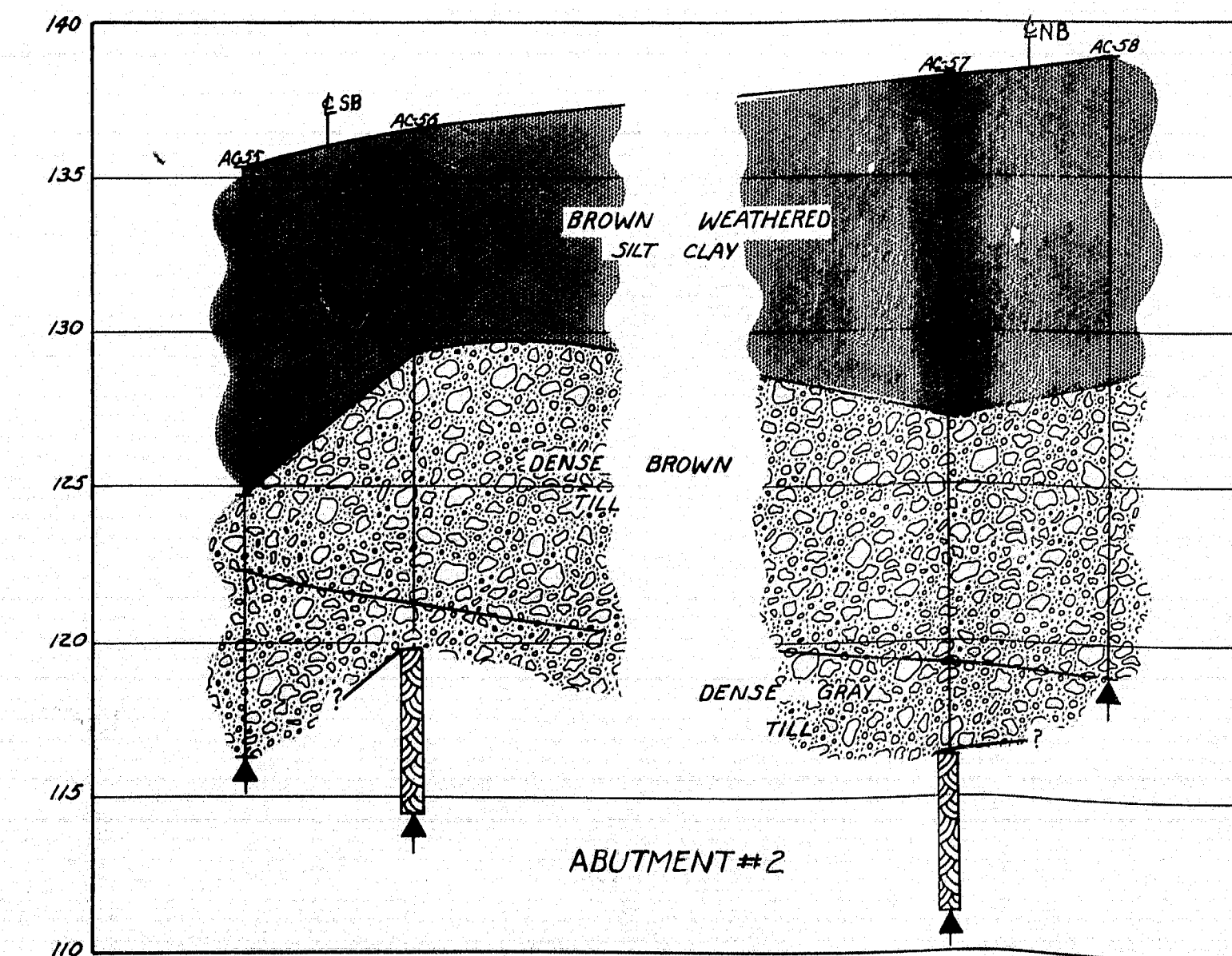
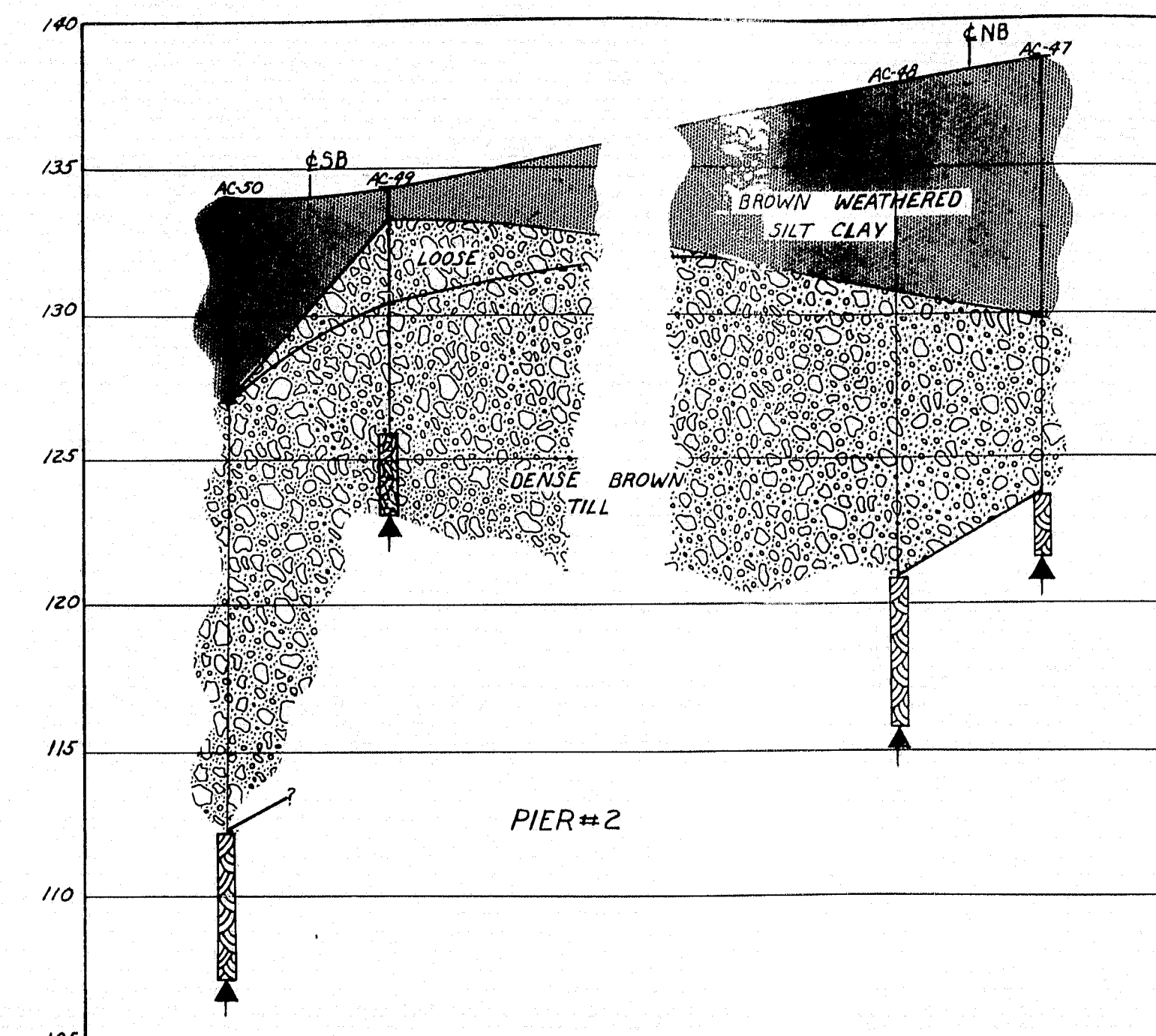
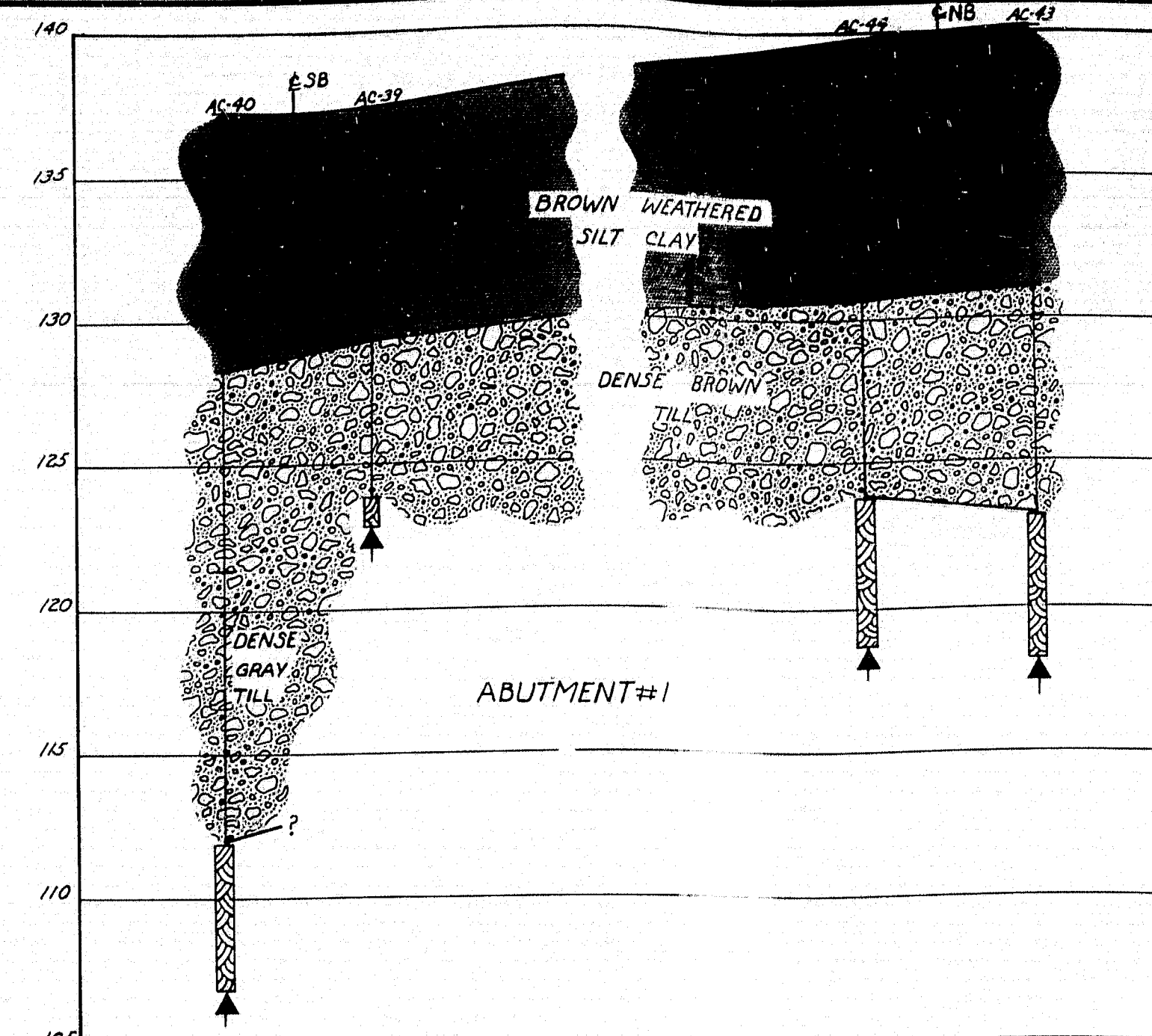
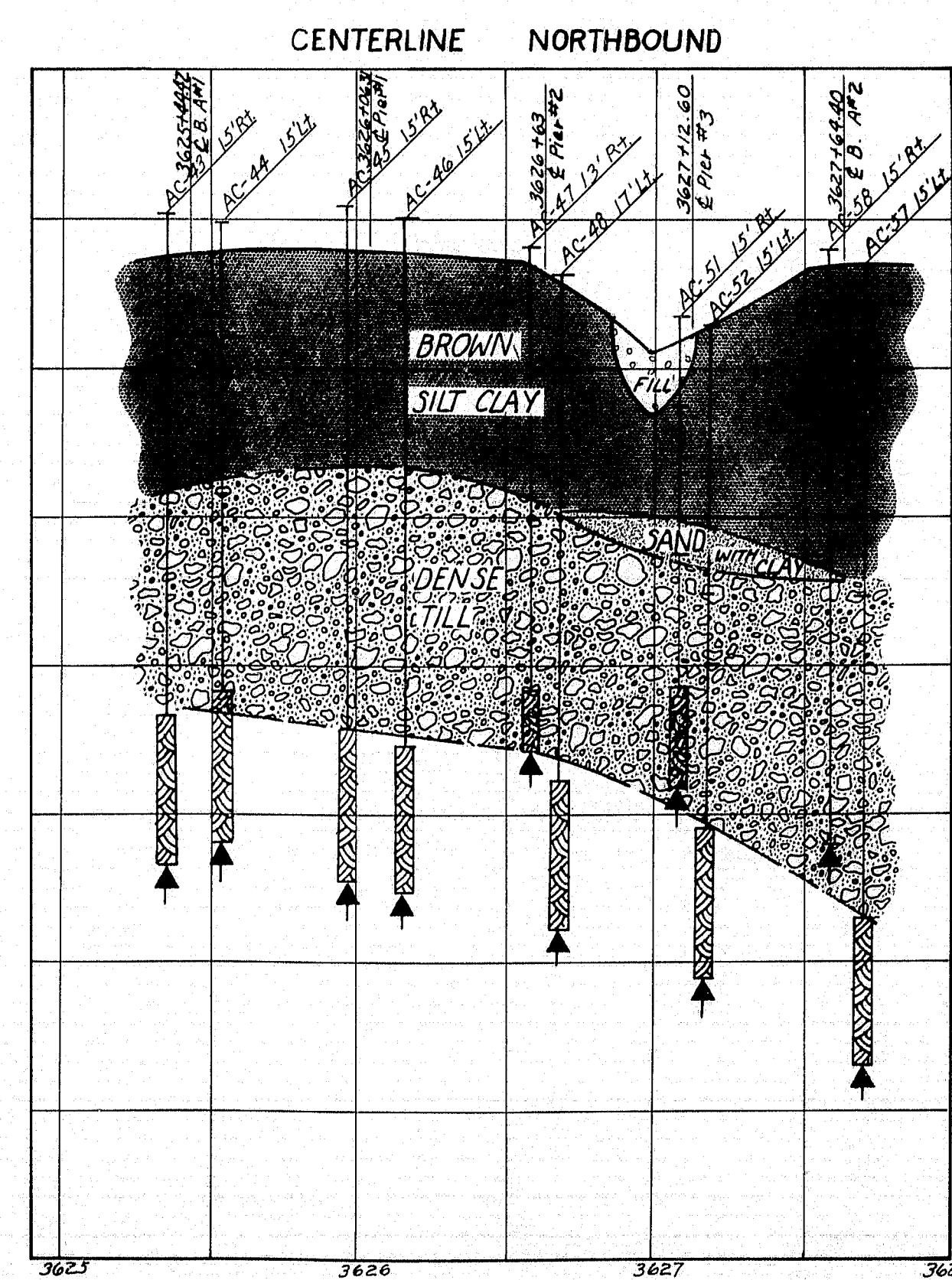
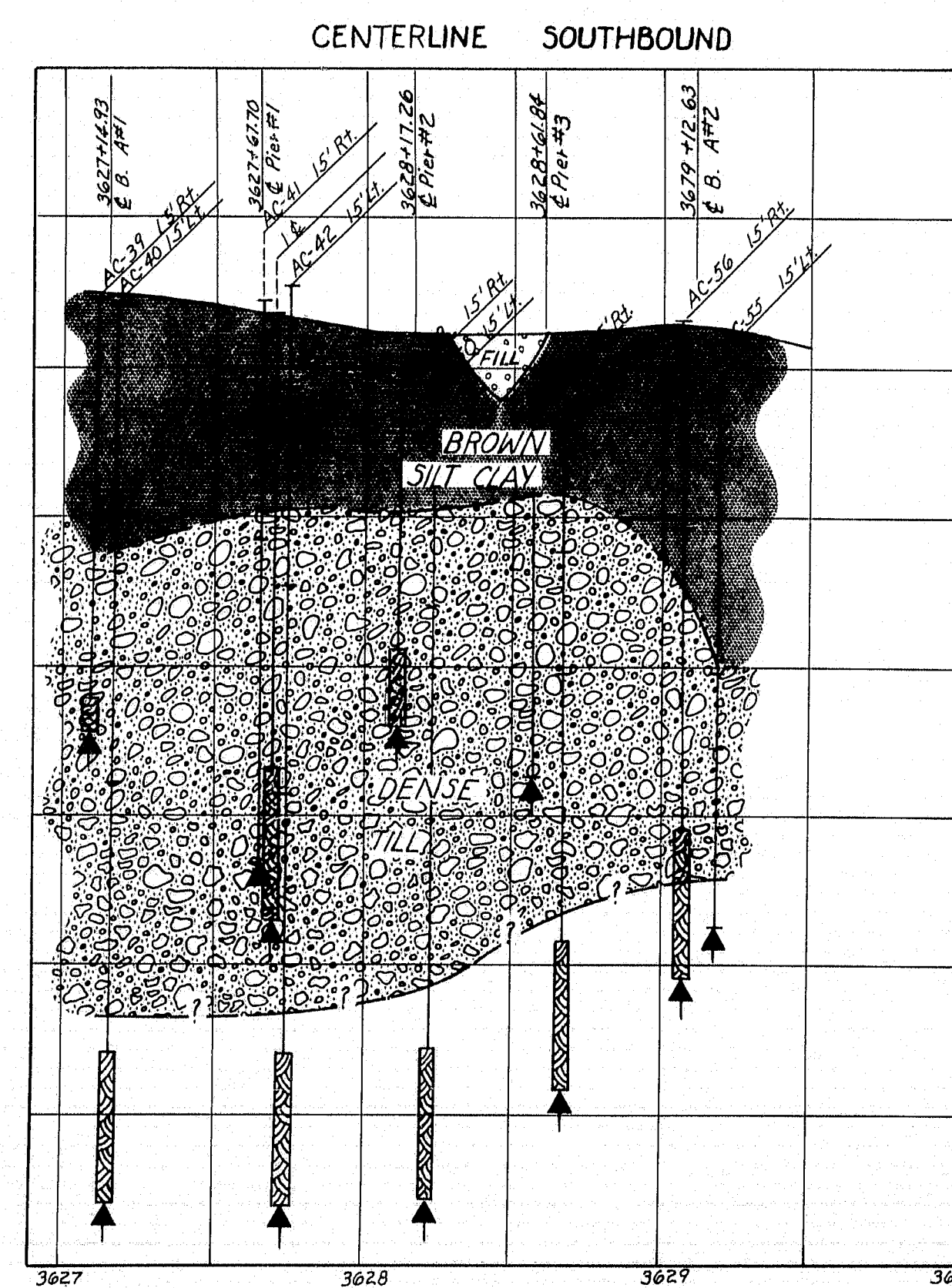
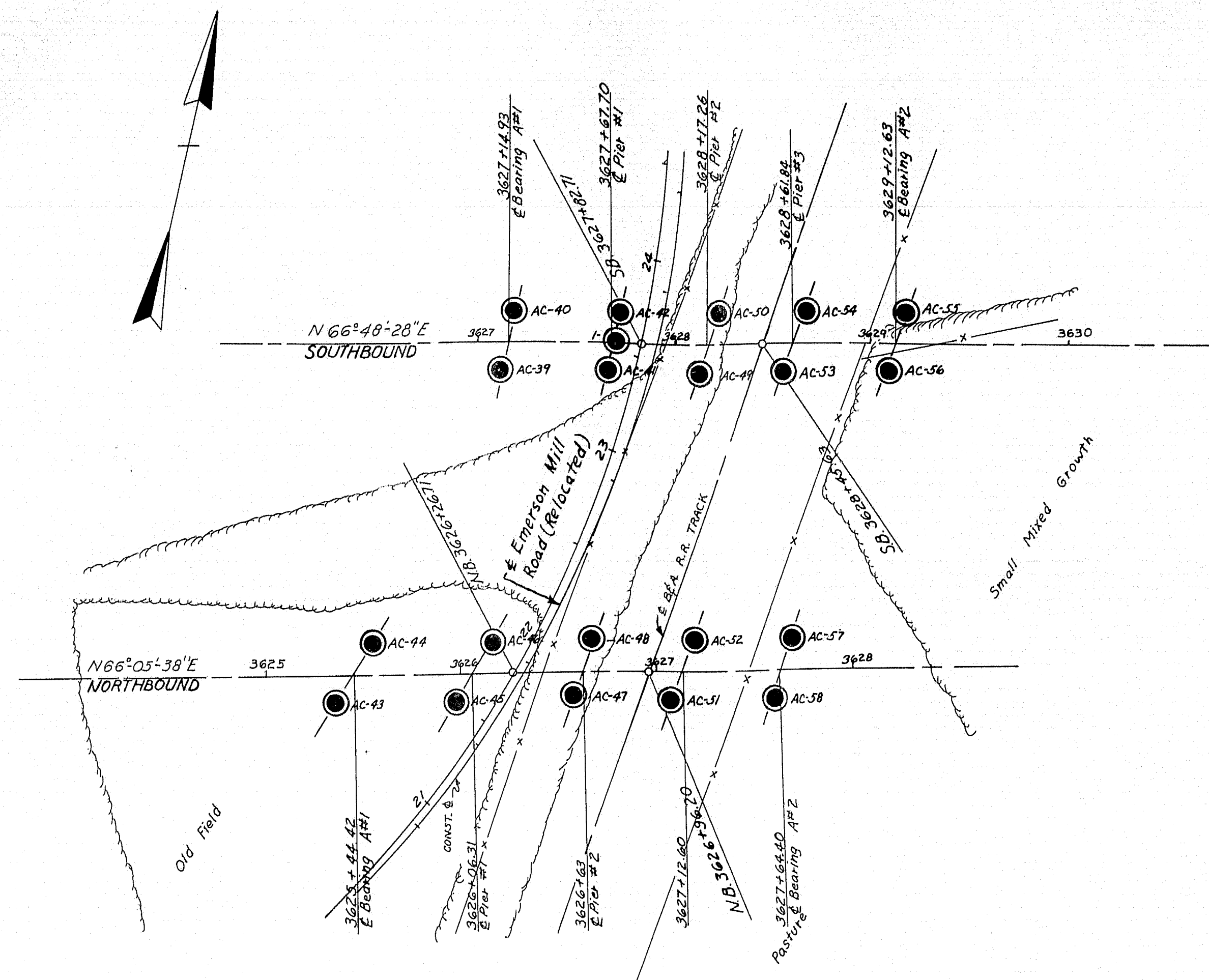
After cutting and grinding



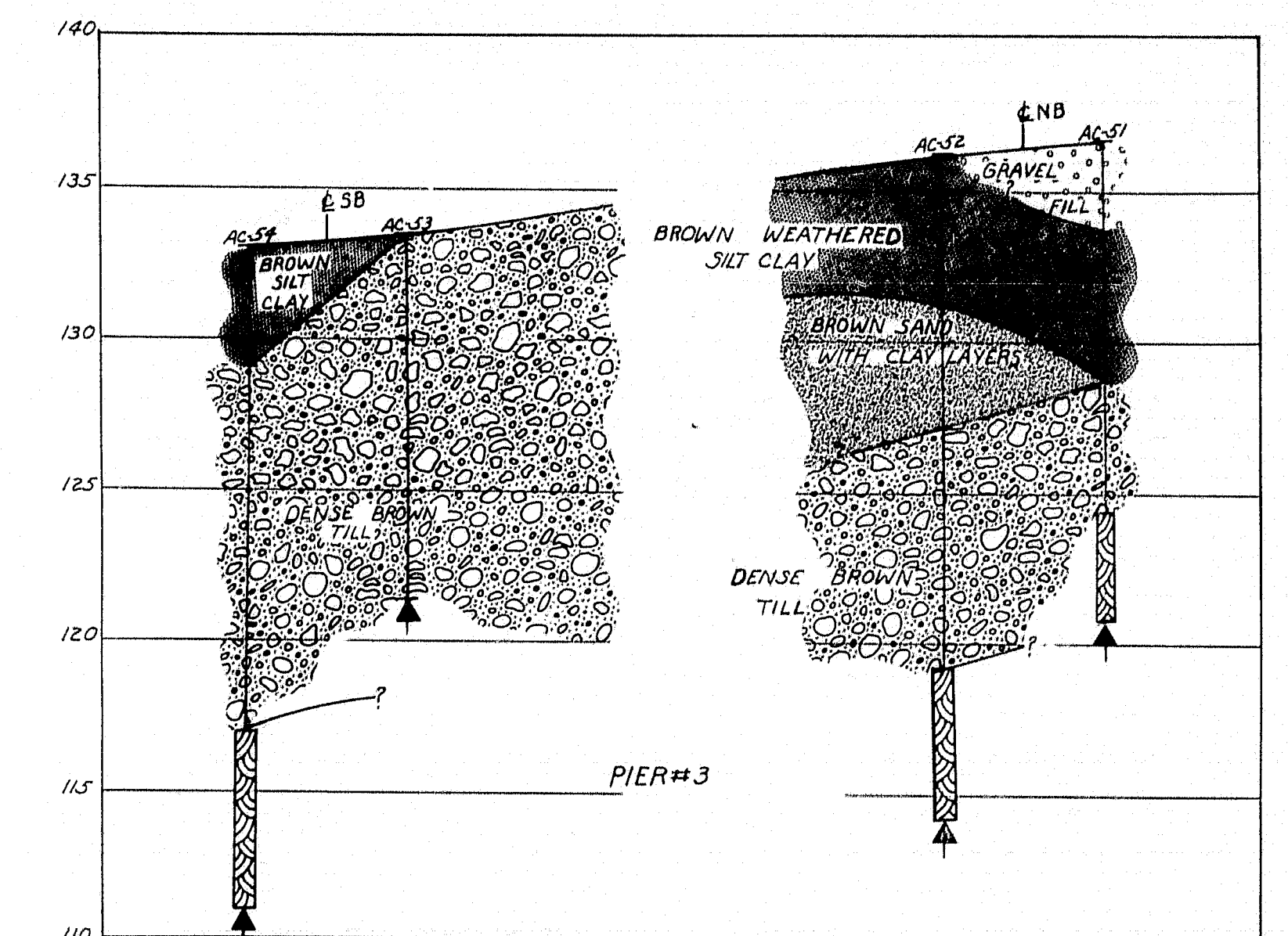
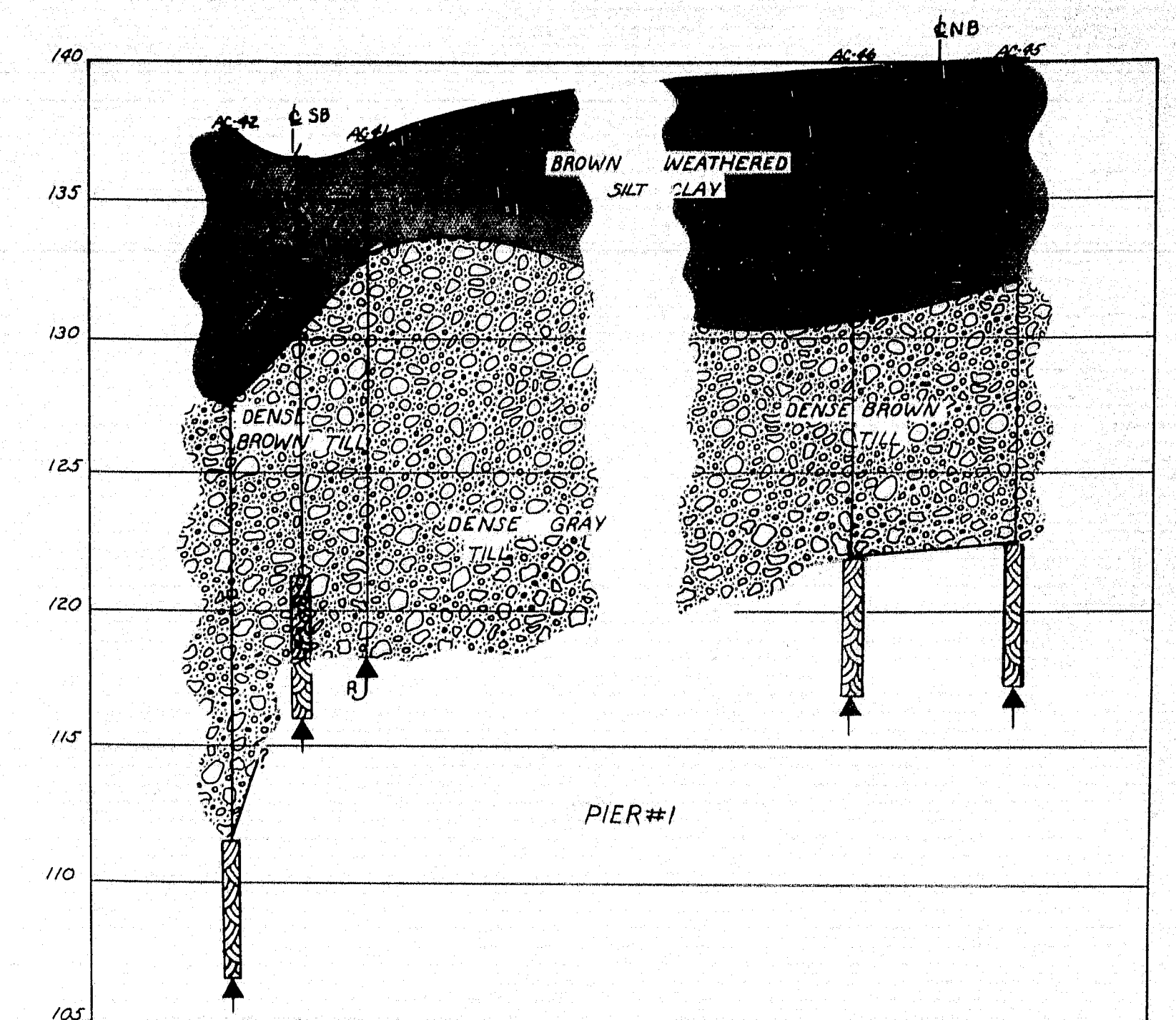
After break

APPENDIX D

Historic Drawings



TRANSVERSE SECTIONS



DESIGN—
TRACE—
CHECK—

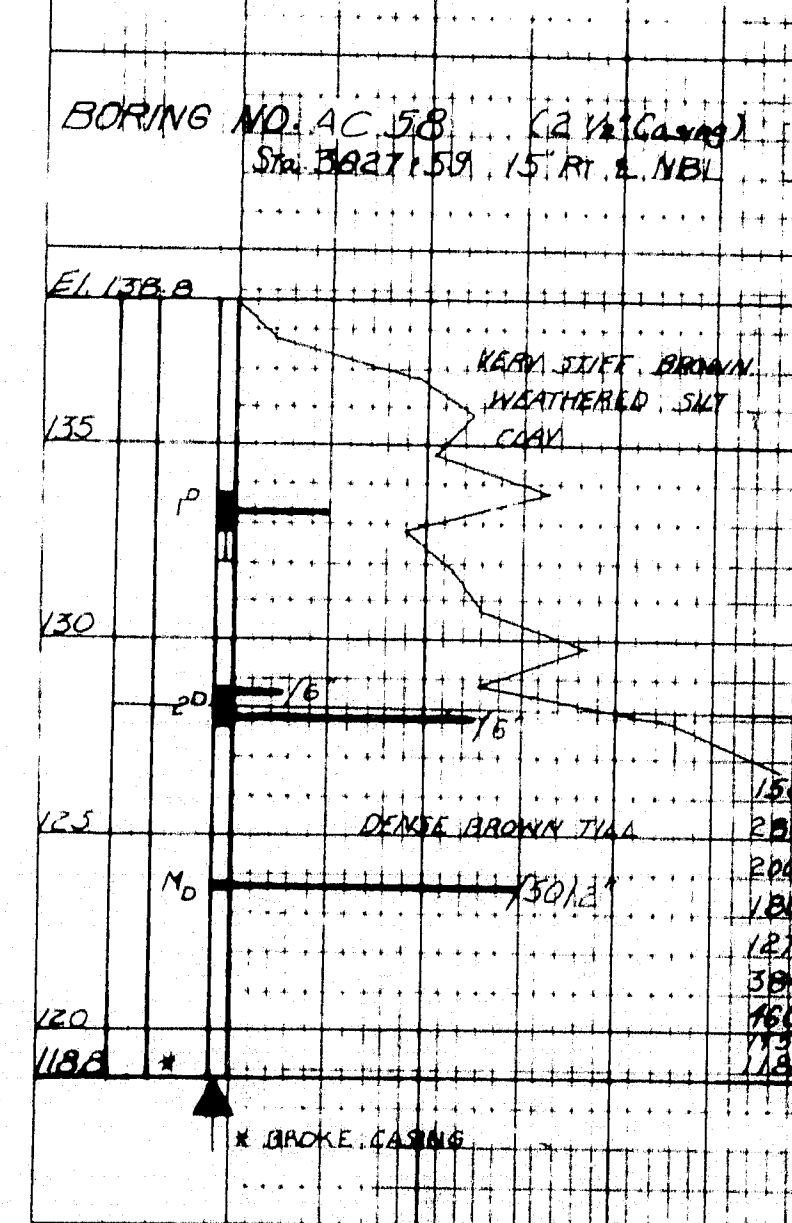
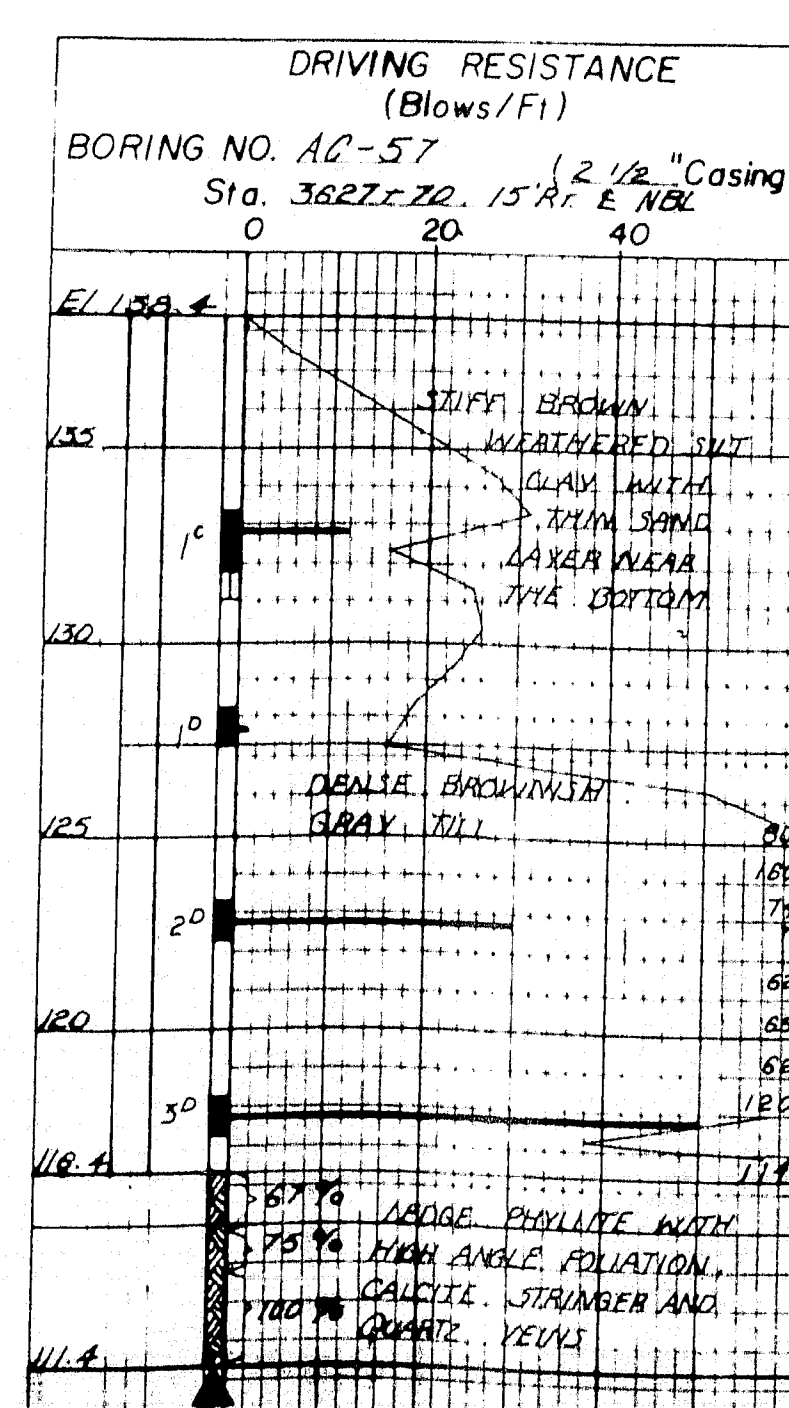
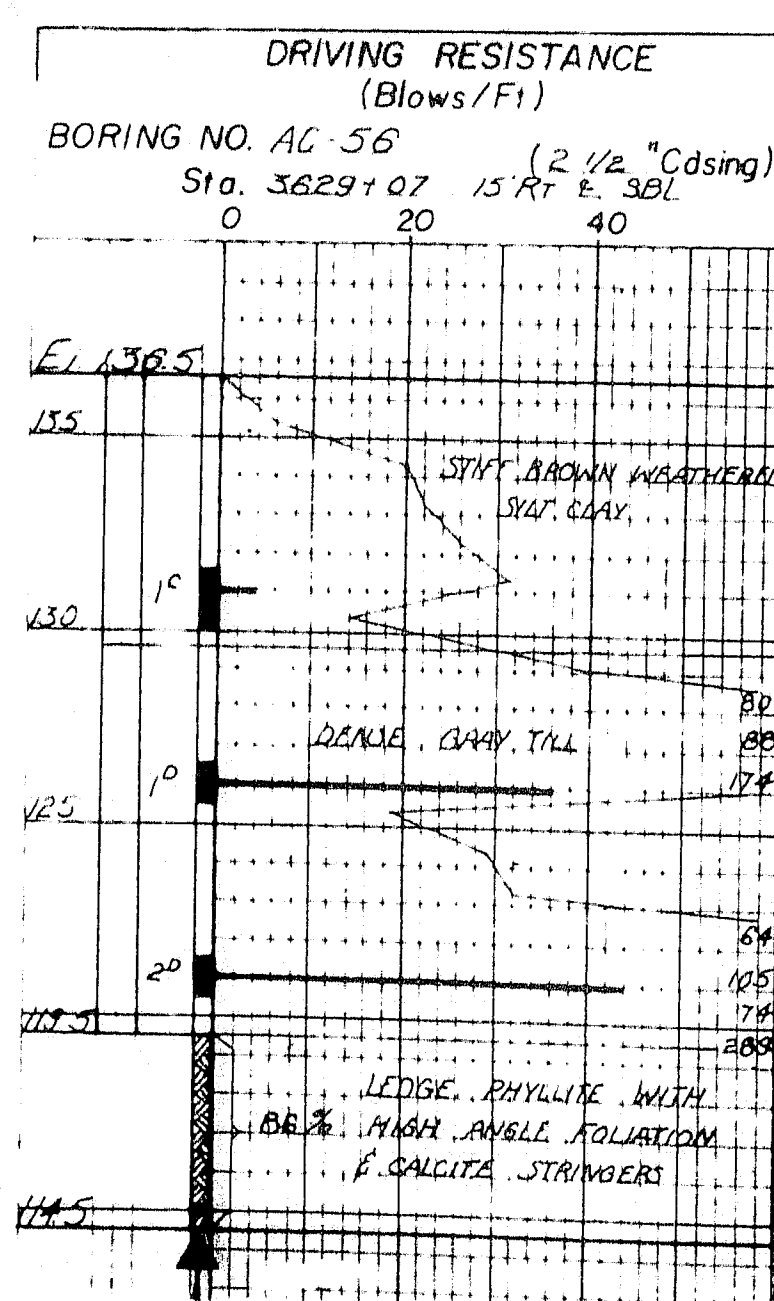
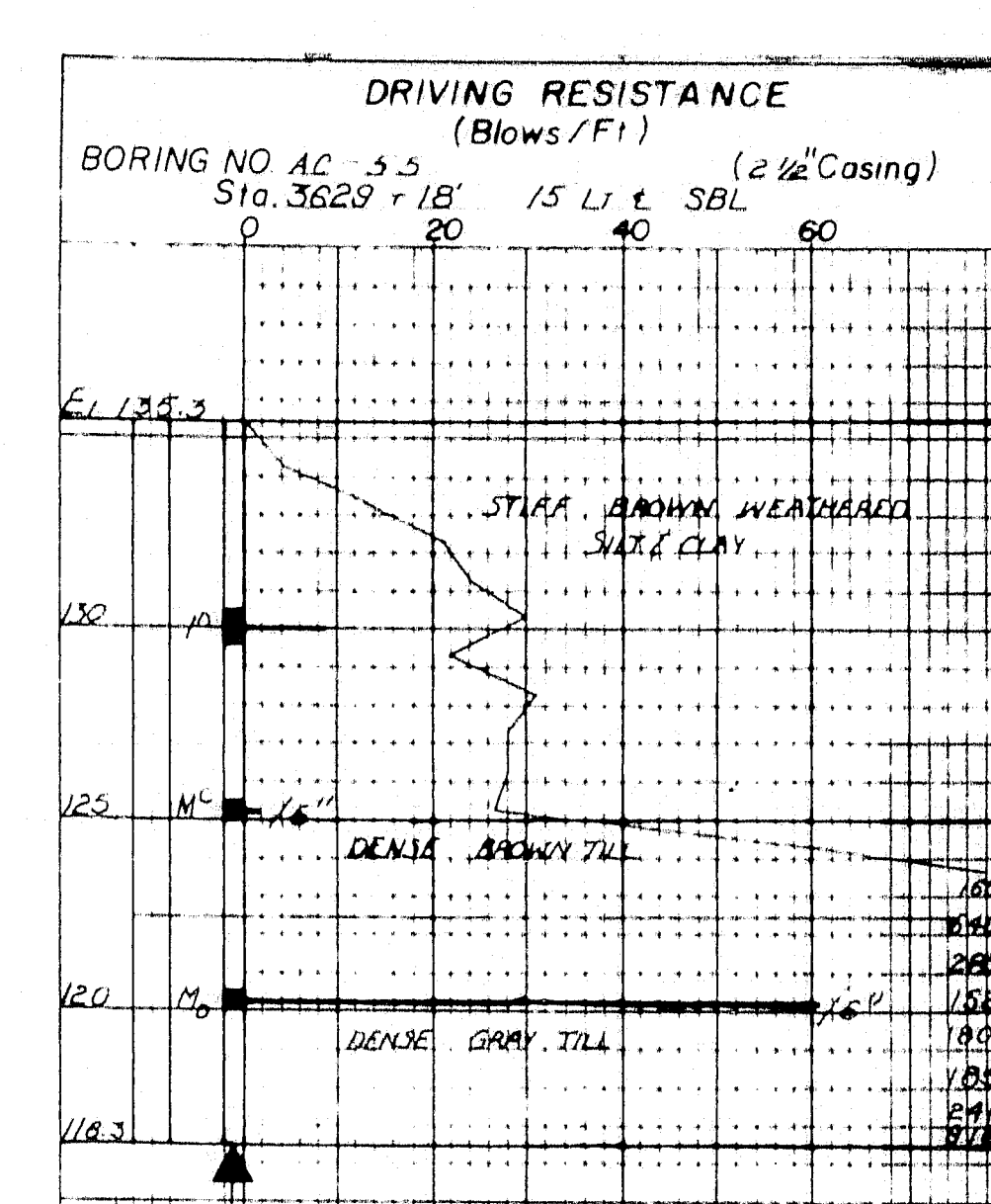
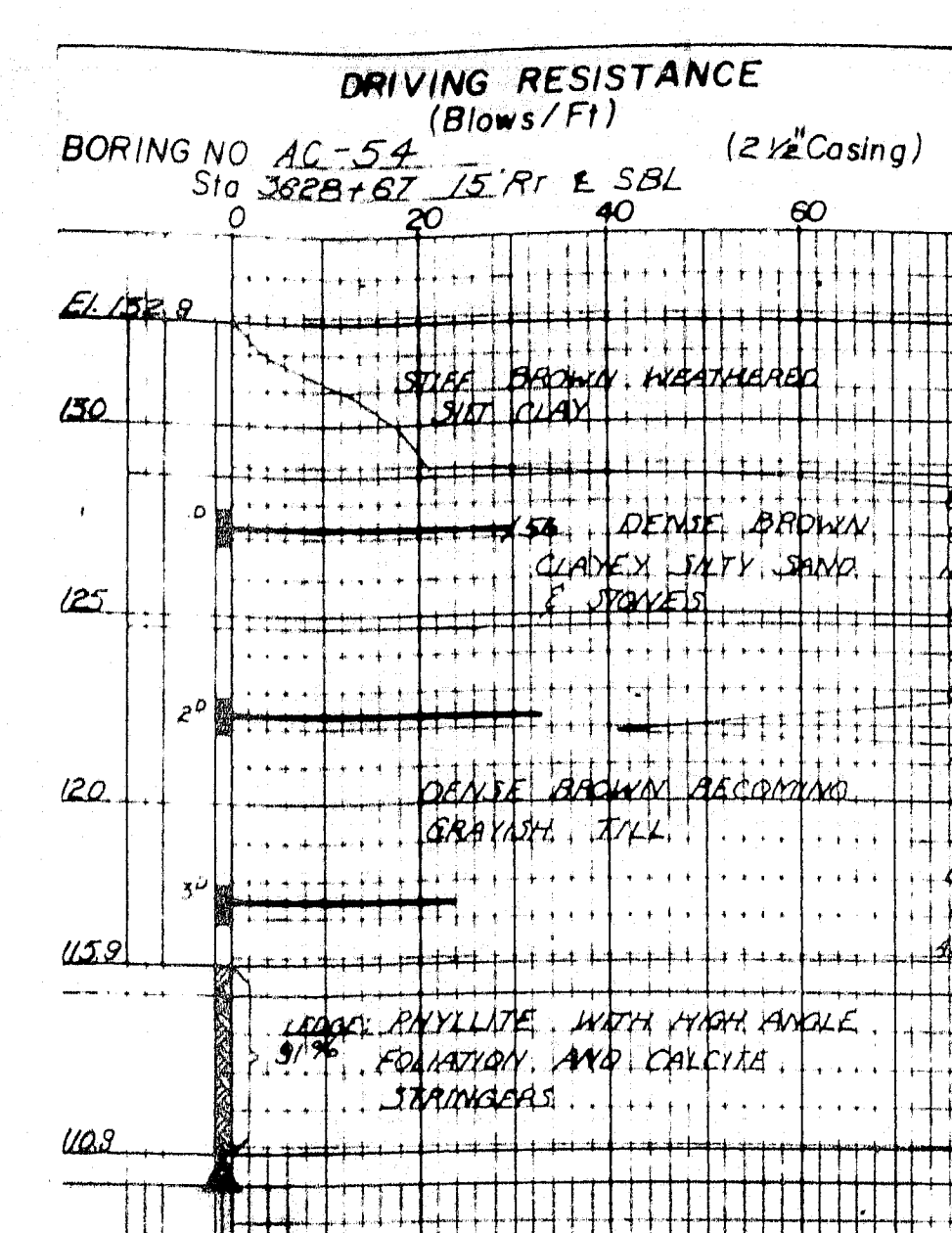
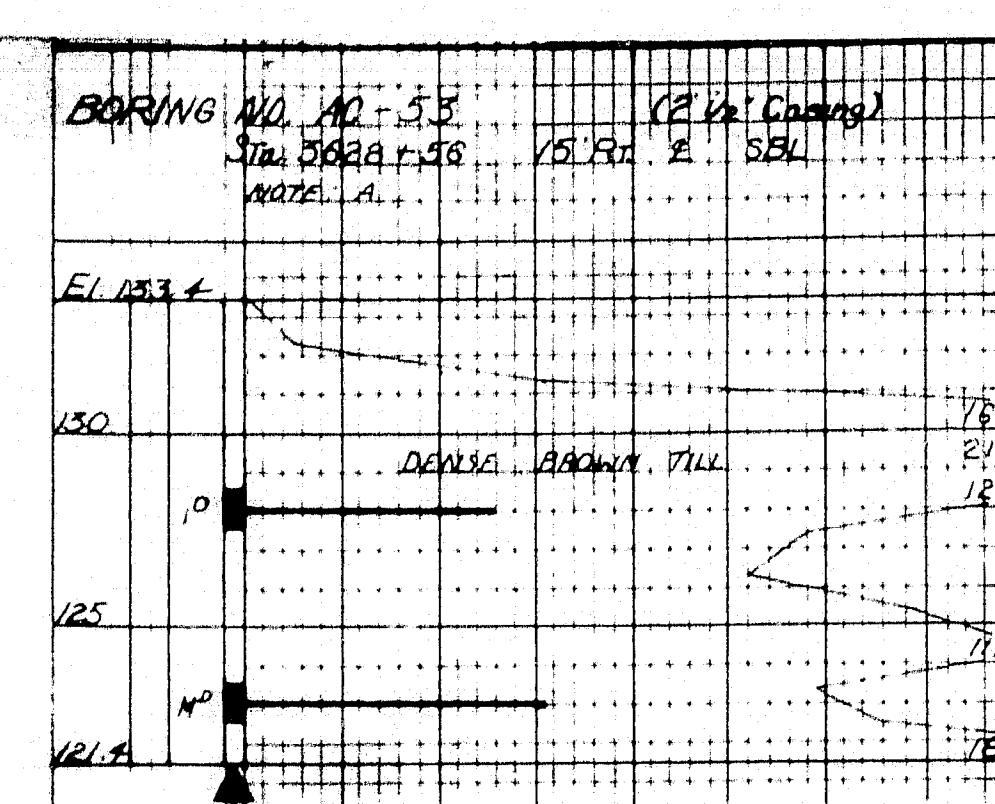
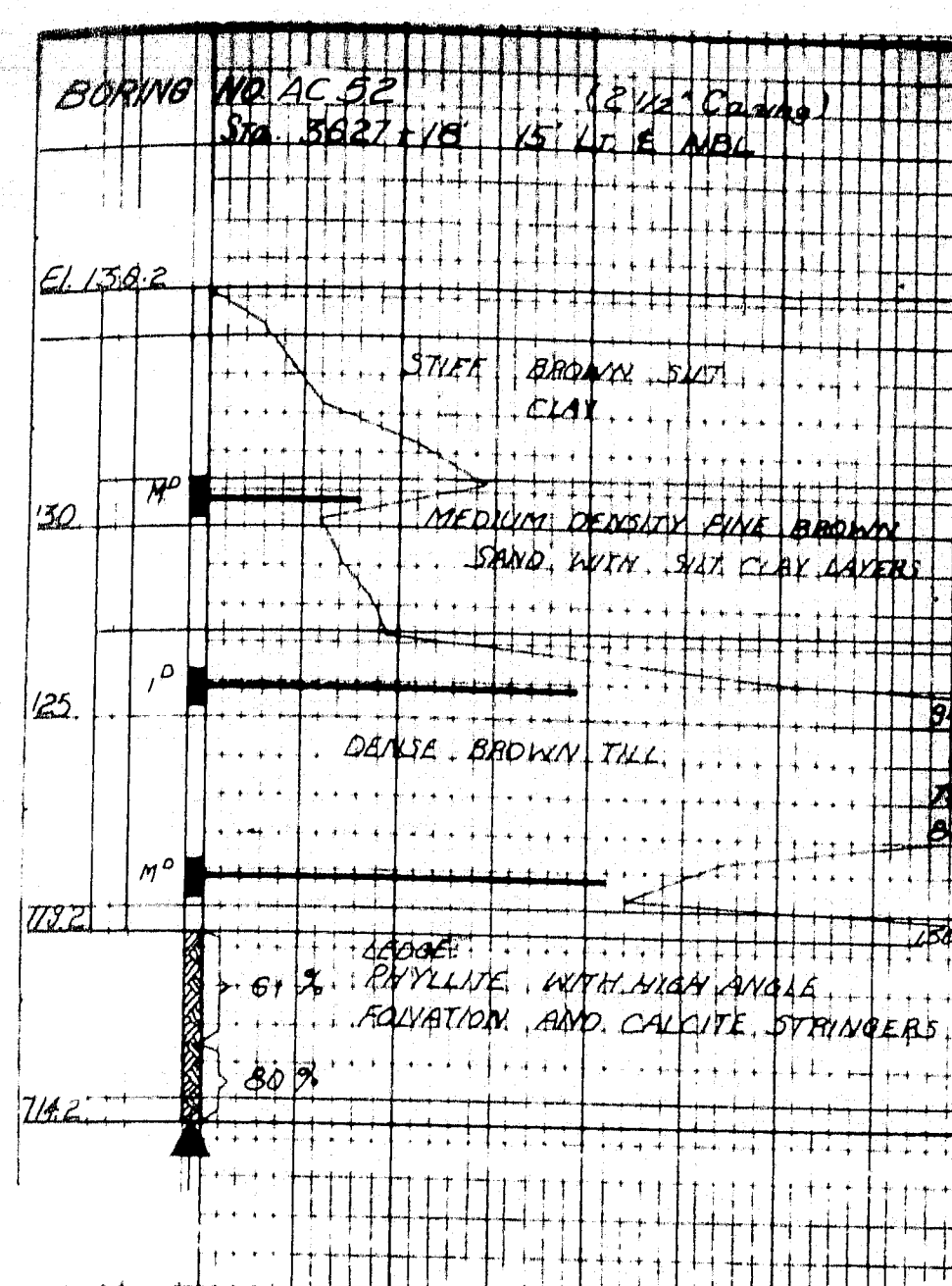
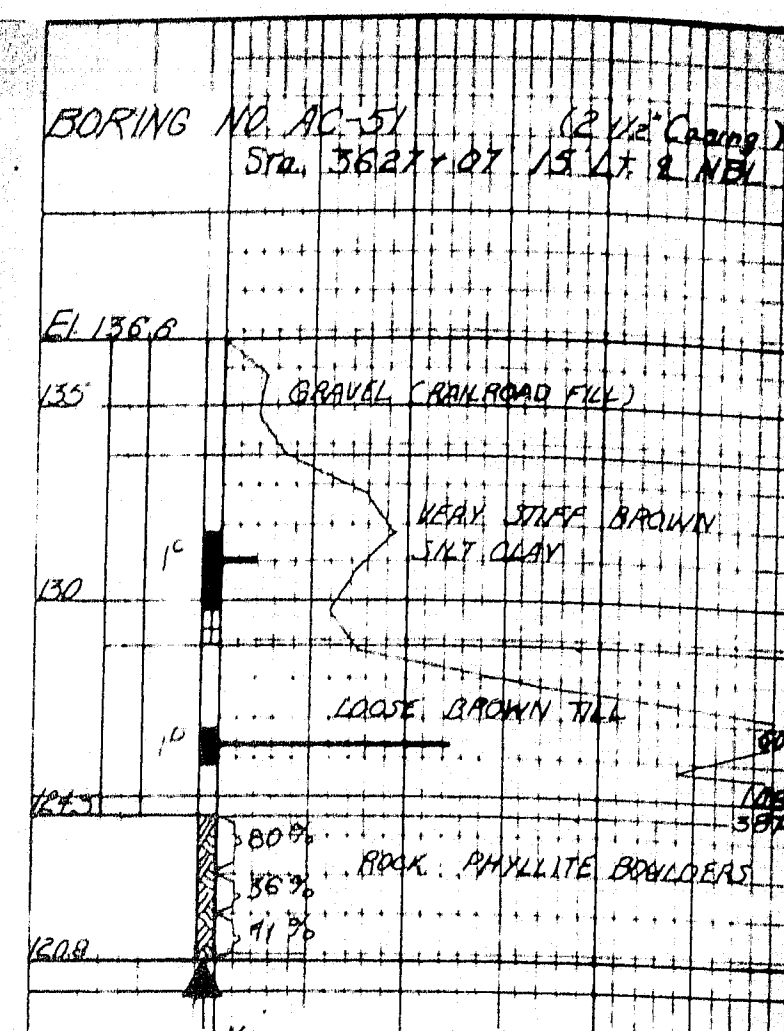
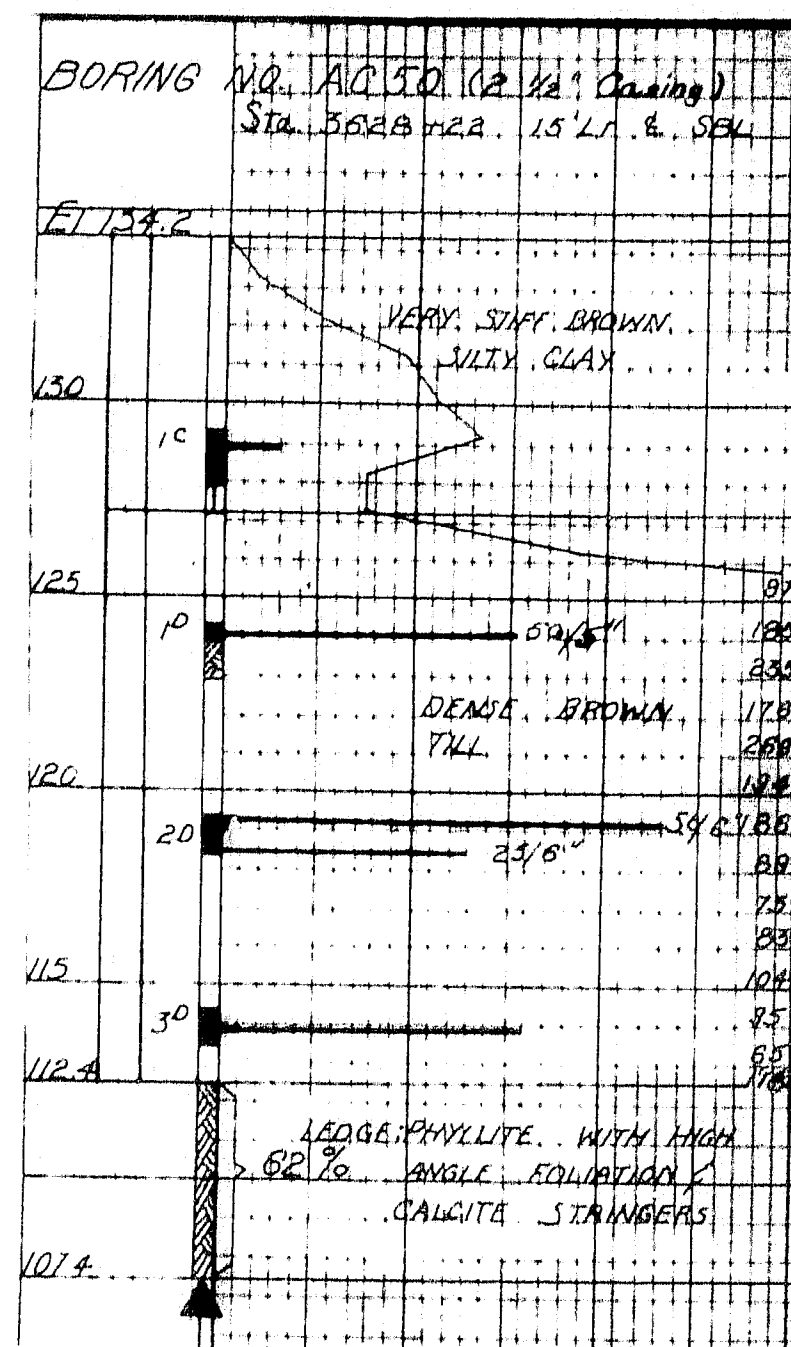
Soils Division

BRIDGE NO.
SURVEY—
PLOT—

STATE HIGHWAY COMMISSION
BRIDGE DIVISION

INTERSTATE 95
OVER
**EMERSON MILL ROAD &
BANGOR & AROOSTOOK RAILROAD**
IN THE TOWN OF
HAMPDEN
PENOBSCOT COUNTY
FOUNDATION SURVEY
SHEET 3 OF 25 AUGUSTA, MAINE SEPT., 1961

0 1 2 3 4 5 INCHES



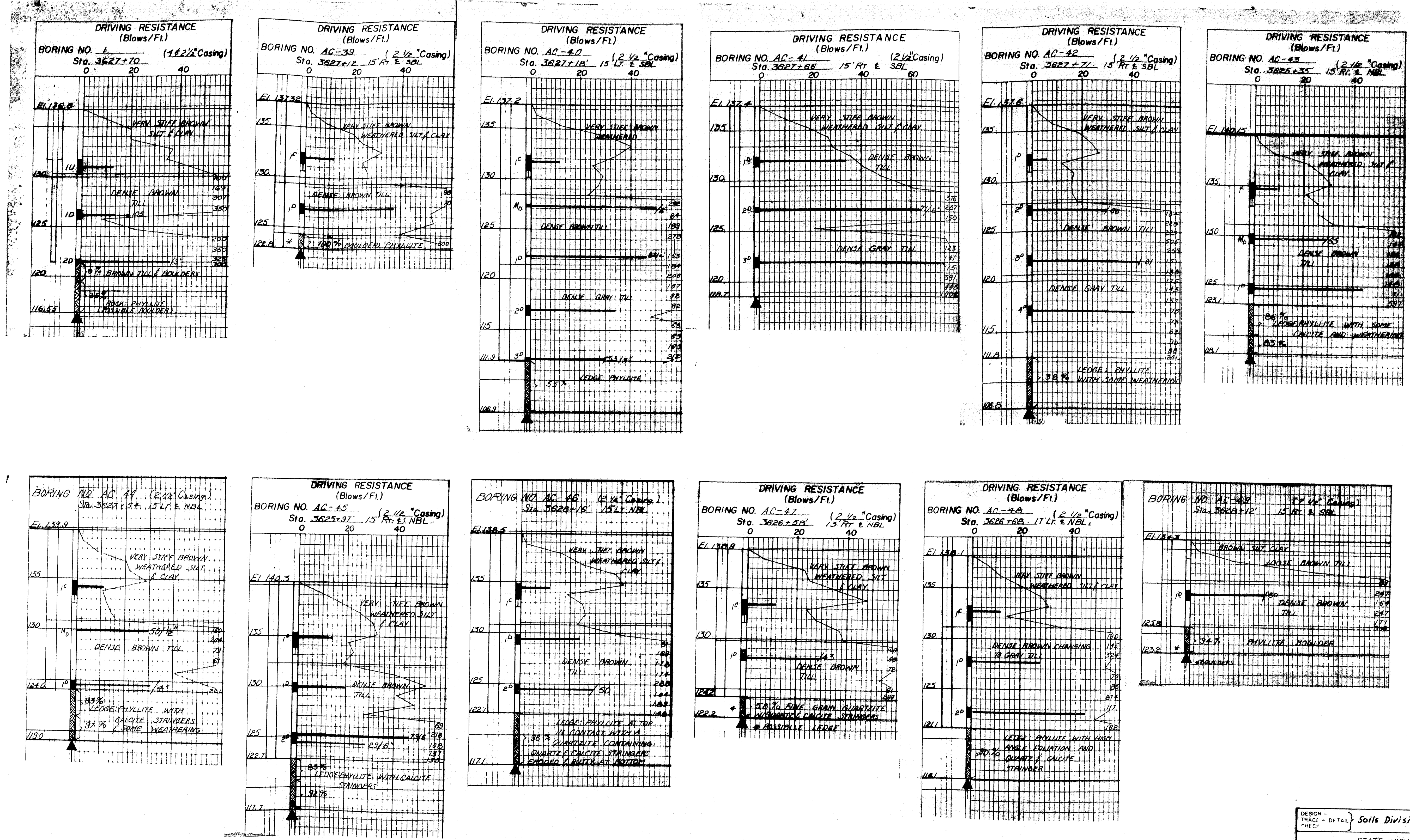
BORING NOTES

All samples and vane are made ahead of casing
Ground water table
Number of blows required to drive extra heavy casing one foot with 400 ft. lbs. of energy per blow
Location of sample or sample attempt
Number and type of dry sample
S&B Sampler #1290's
2" O.D. 16 ga. seamless tubing
3/4" O.D. 16 ga. seamless tubing
Wash sample and number
Unsuccessful sample attempt and type of sampler
Number of blows required to drive spoon or tubing one foot with 400 ft. lbs. of energy per blow
Sampling spoon or seamless tubing driven by static weight of drill rods and hammer
Piston sampler
Field vane test
Bottom of boring (may not be bottom of soil)
Refusal of drill rods or casing (may not be ledge of rock)
Locations noted by diamond bit and left next per very of rock

NOTE:
... TILL REARS TO B. MATHE
... S&B SPOON, S&B
... FOR STONES

DESIGN: 11-11-61
Soils Division
BRIDGE NO. 5
STATE HIGHWAY COMMISSION
BRIDGE DIVISION
INTERSTATE 95
OVER
EMERSON MILL ROAD & BANGOR & AROOSTOOK RAILROAD
IN THE TOWN OF
HAMPDEN
PENOBSCOT COUNTY
BORING DETAILS
SHEET 4 OF 25 AUGUSTA, MAINE
SEPT., 1961

86-36



DESIGN - TRACE & DETAIL
SHEEV

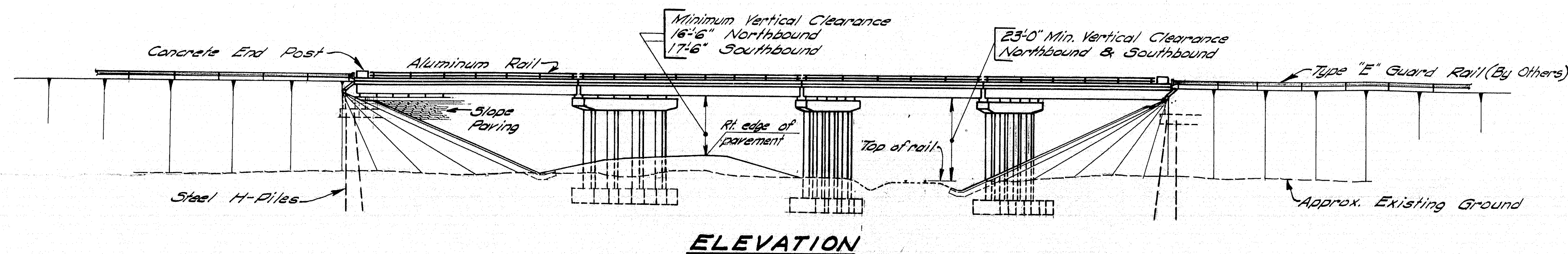
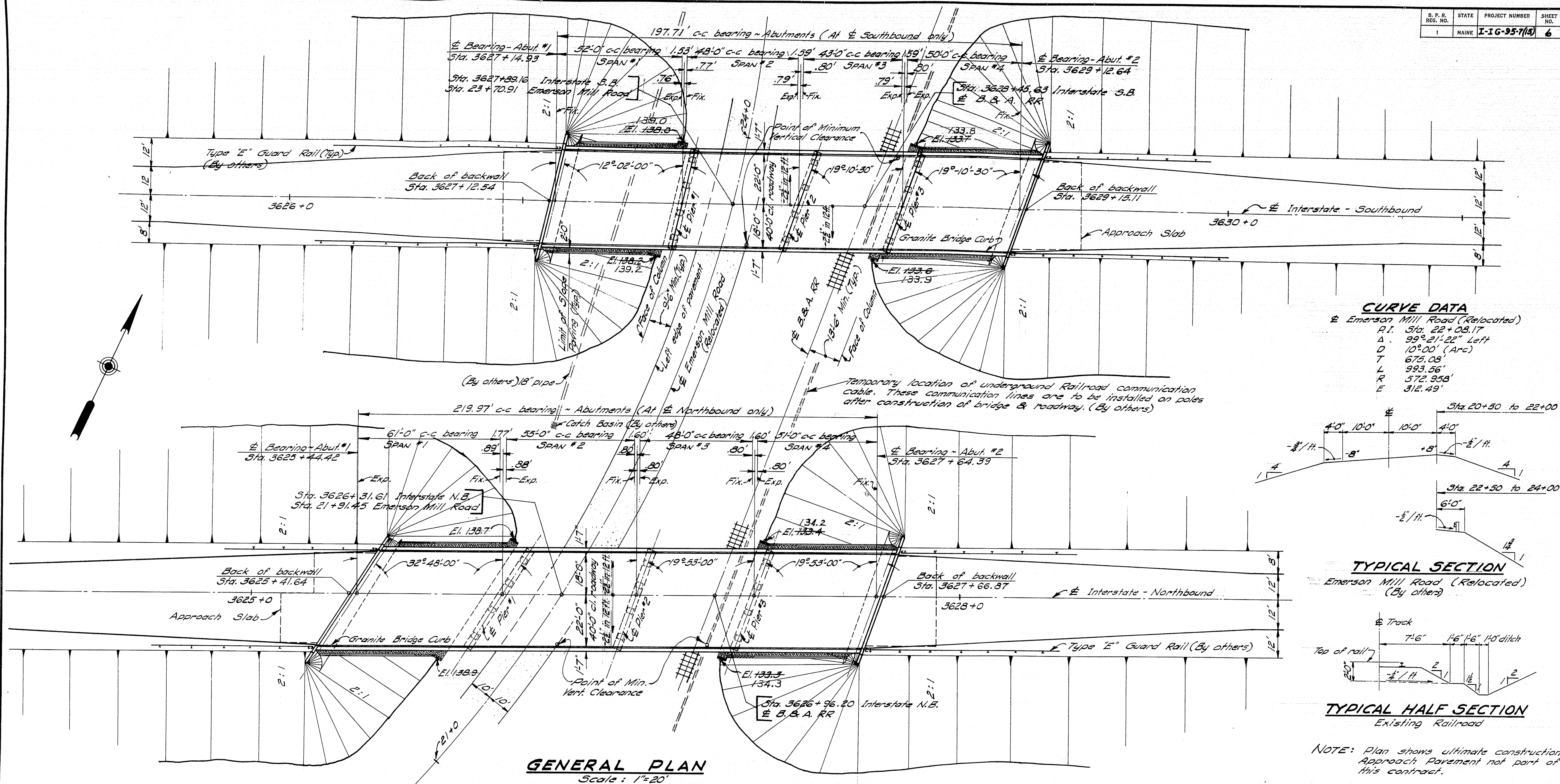
Soils Division

BRIDGE NO. SURVEY PLOT

STATE HIGHWAY COMMISSION
BRIDGE DIVISION

INTERSTATE 95
OVER
**EMERSON MILL ROAD &
BANGOR & AROOSTOOK RAILROAD**
IN THE TOWN OF
HAMPDEN
PENOBSCOT COUNTY
BORING DETAILS

SHEET 5 OF 25 AUGUSTA, MAINE SEPT., 1961

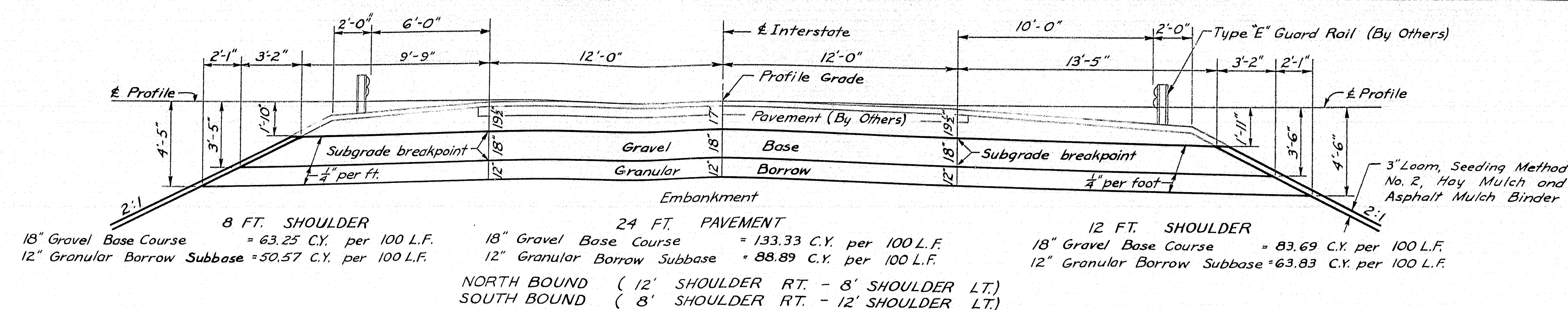


DESIGN - C. D. H.
TRACE - G. M. C.
CHECK - G. M. C.

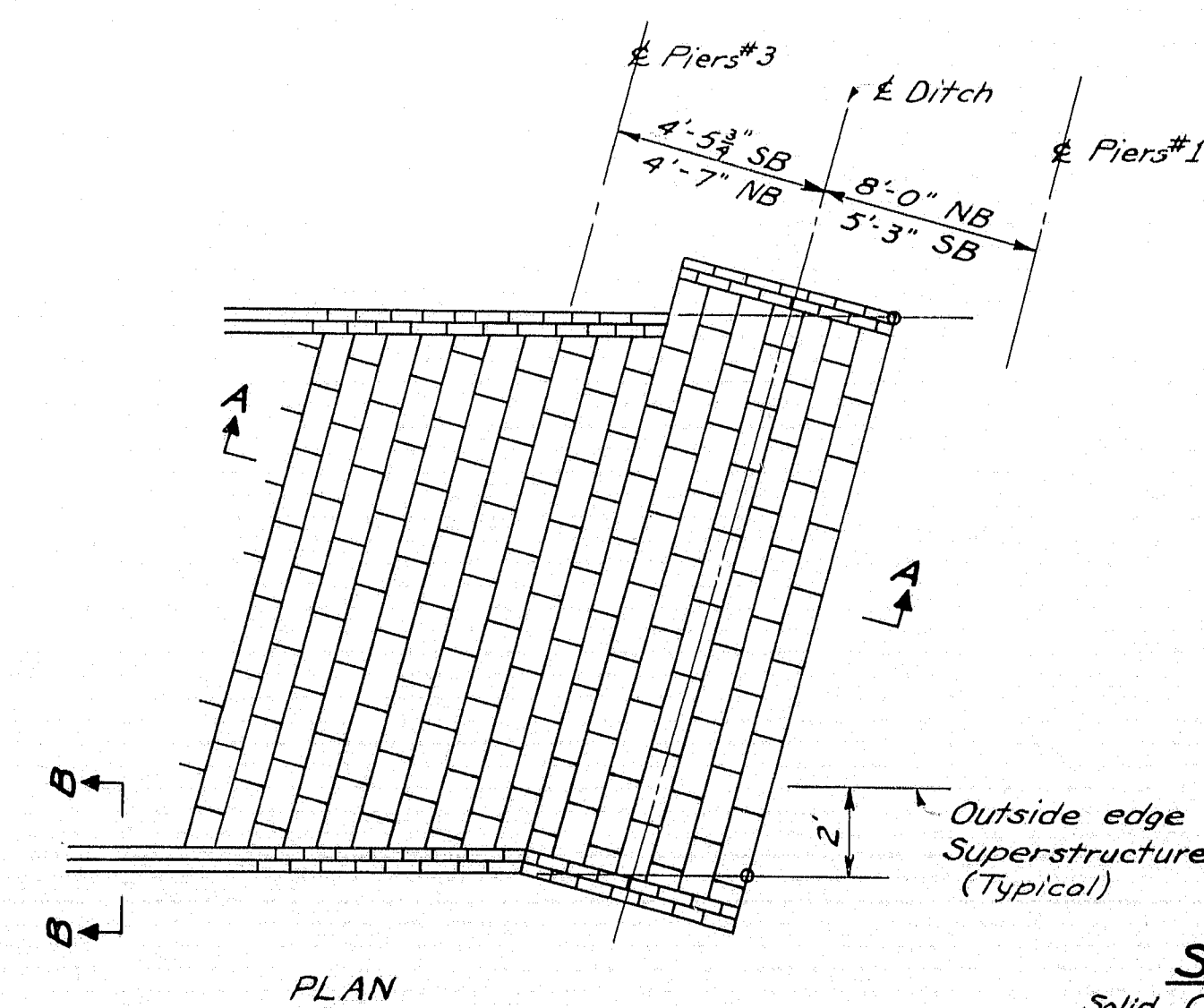
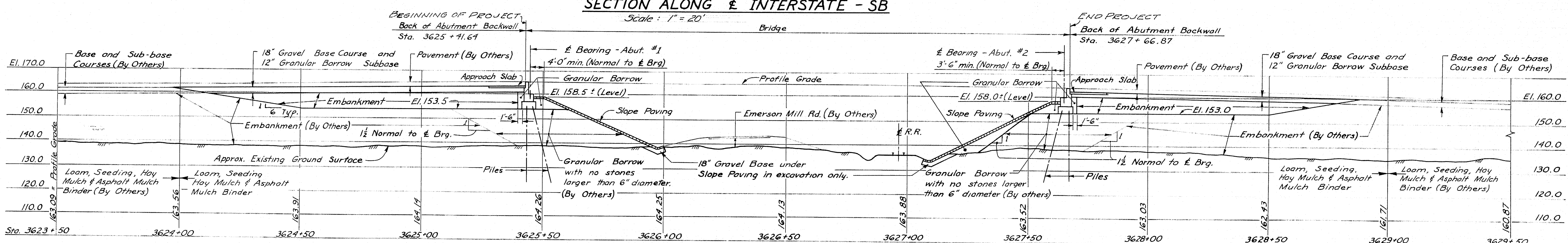
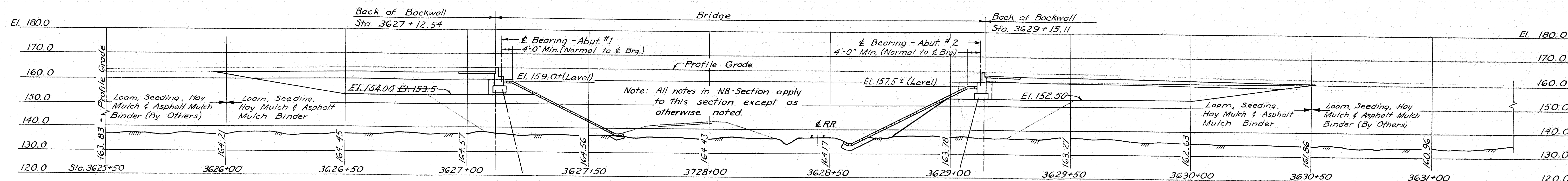
BRIDGE NO. SURVEY - PLOT -

STATE HIGHWAY COMMISSION
BRIDGE DIVISION
INTERSTATE 95
OVER
EMERSON MILL ROAD & BANGOR & AROOSTOOK RAILROAD
IN THE TOWN OF
HAMPDEN
PENOBSCOT COUNTY
GENERAL PLAN & ELEVATION

SHEET 6 OF 25 AUGUSTA, MAINE SEPT. 1961

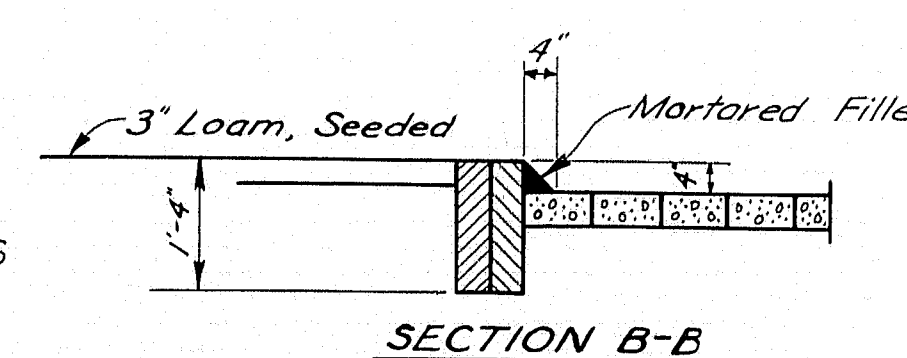
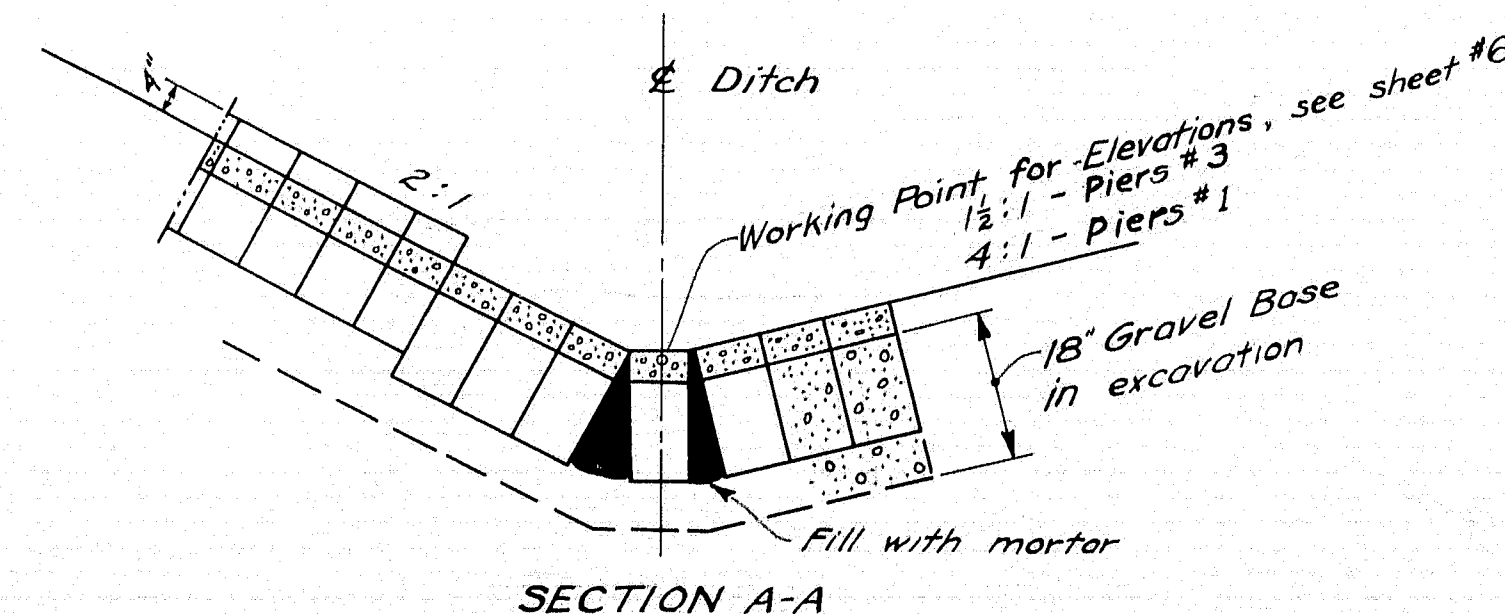


TYPICAL INTERSTATE ROADWAY SECTION



SLOPE PAVING

Solid Concrete Blocks 8"x16"x4"
Mortared Joints



The 18" Gravel Base under Slope Paving may be reduced or omitted, if in the opinion of the Engineer the existing material is suitable. Payment for excavation for Gravel Base under Slope Paving to be made under Item 204-14, Structural Earth Excavation - Piers.

Before piles are driven, granular borrow shall be placed and compacted to bottom of footing elevation. The controlled density method shall be used for placing embankment and granular borrow under this contract.

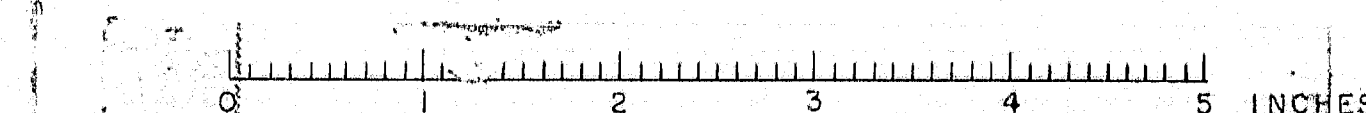
DESIGN - C.D.H.
TRACE - J.W.M.
CHECK - S.C.P.

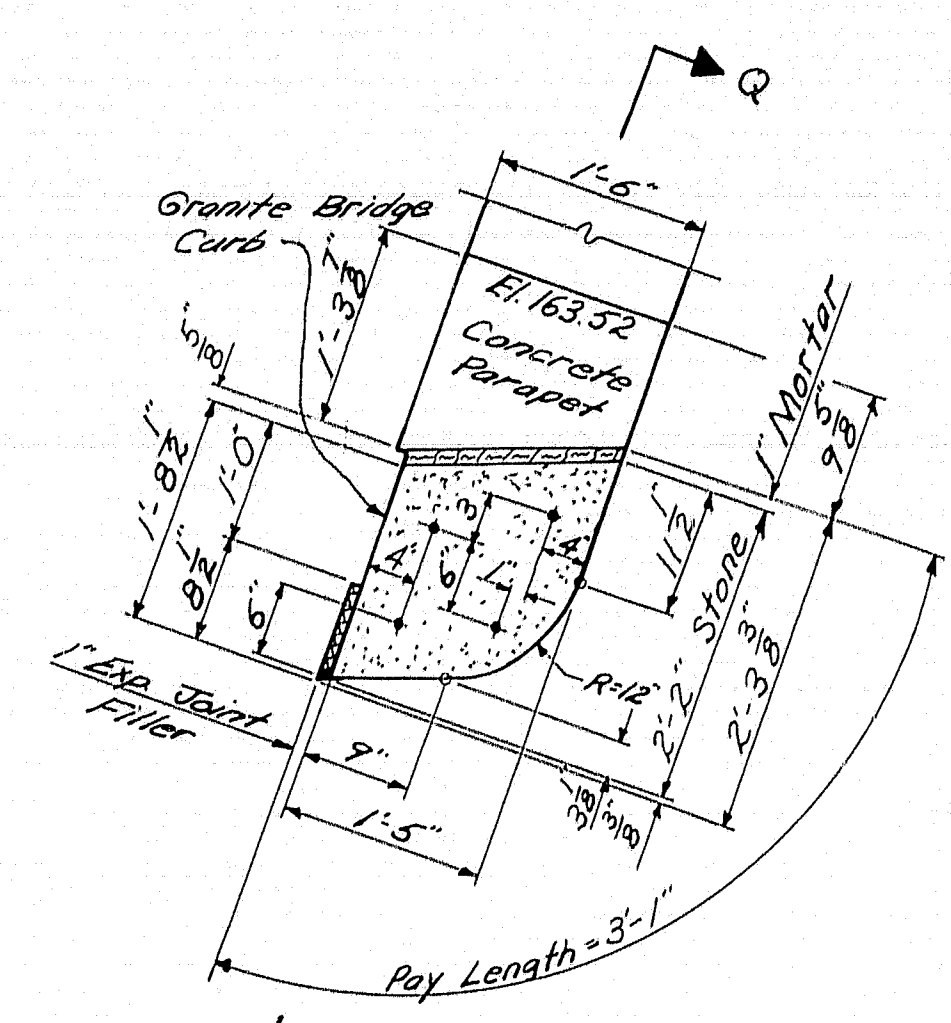
BRIDGE NO. SURVEY PLOT

STATE HIGHWAY COMMISSION
BRIDGE DIVISION

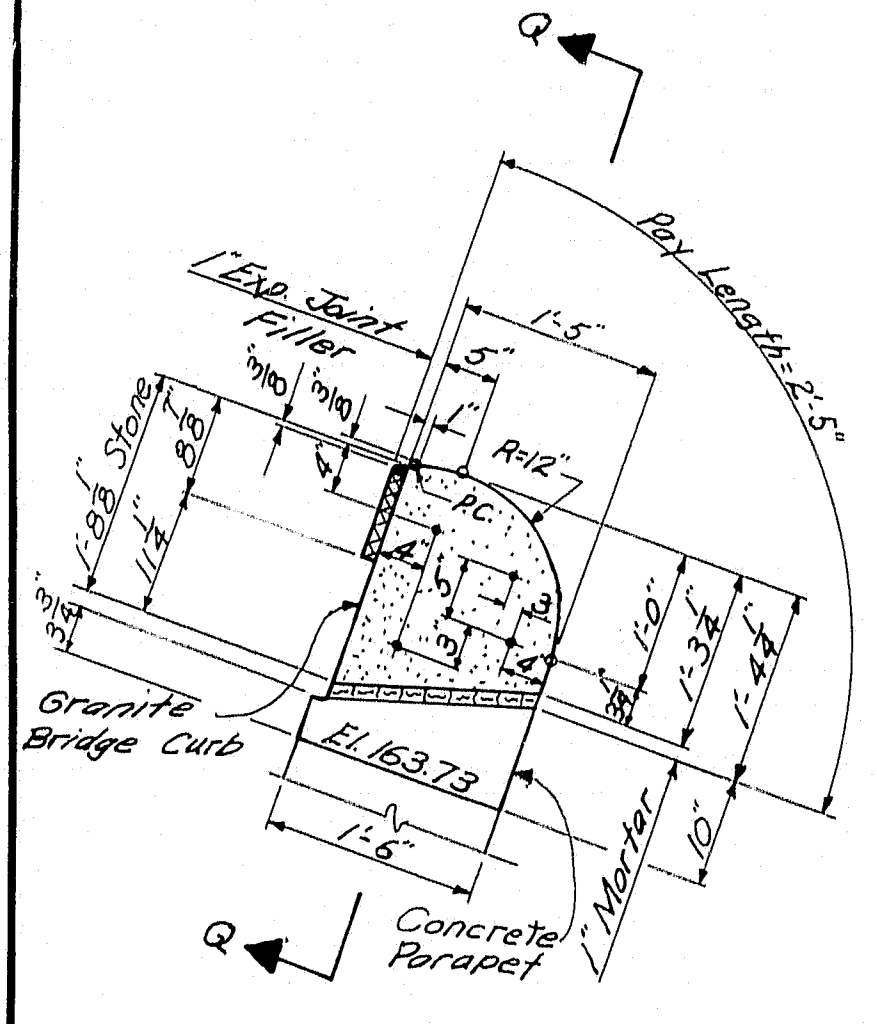
INTERSTATE 95
OVER
**EMERSON MILL ROAD &
BANGOR & AROOSTOOK RAILROAD**
IN THE TOWN OF
HAMPDEN
PENOBSCOT COUNTY
ROADWAY WORK AND SLOPE PAVING

SHEET 7 OF 25 AUGUSTA, MAINE SEPT. 1961

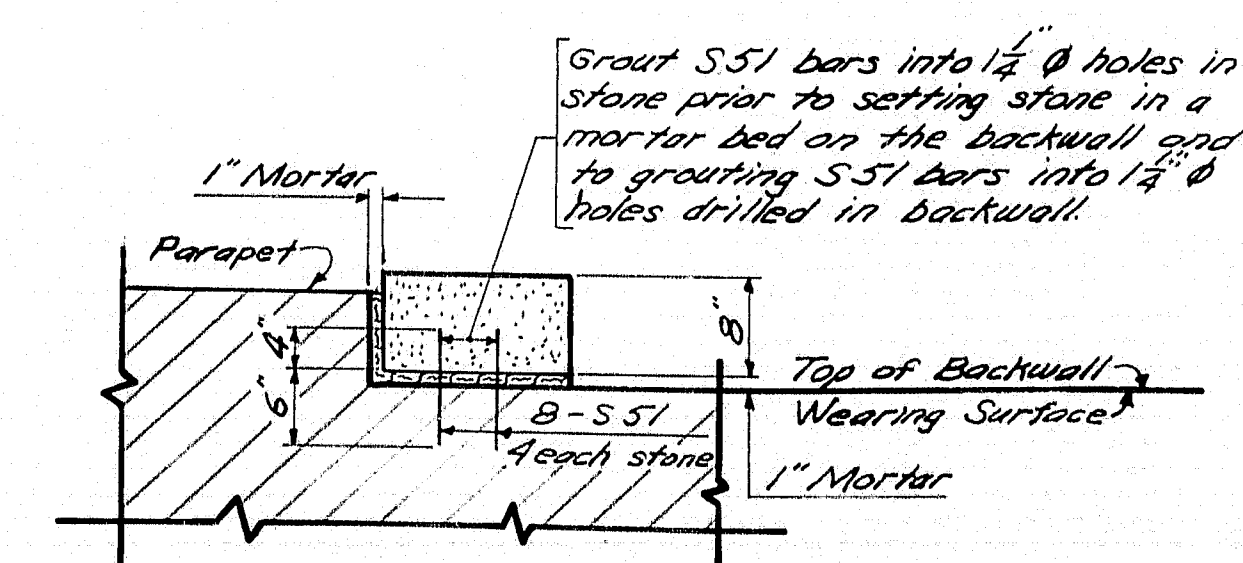




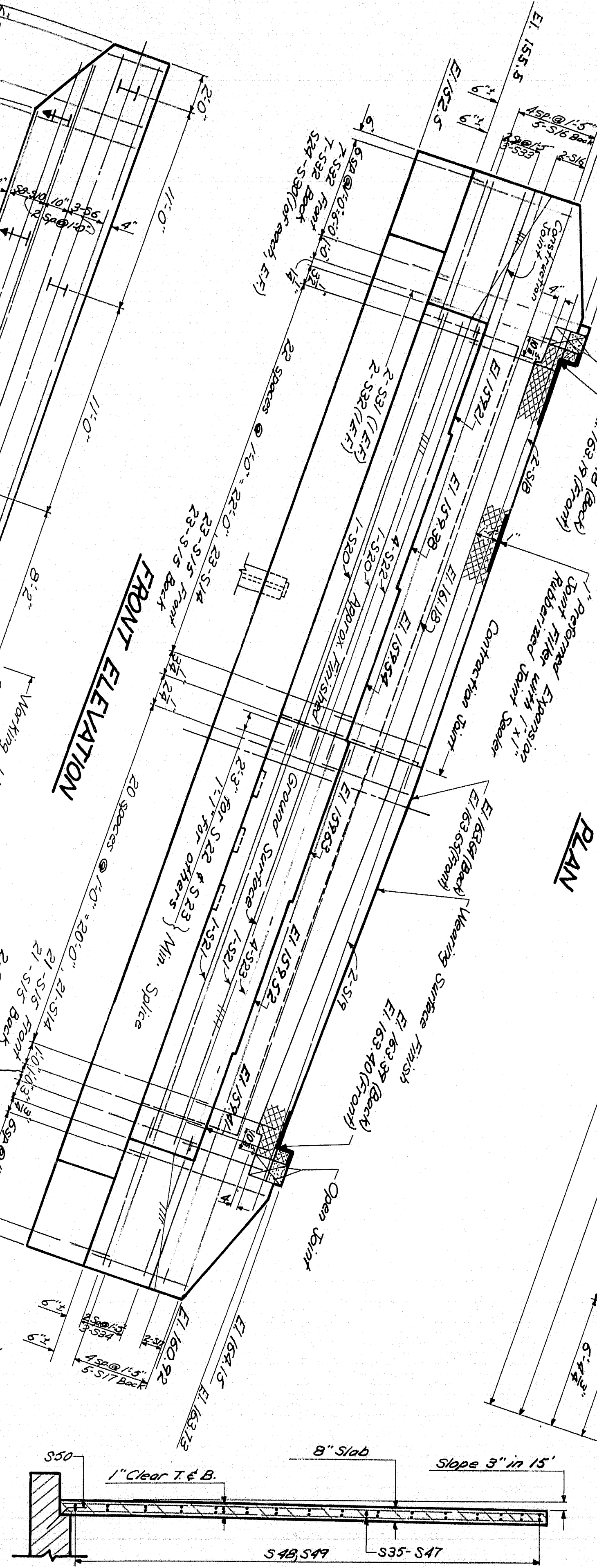
DETAIL E



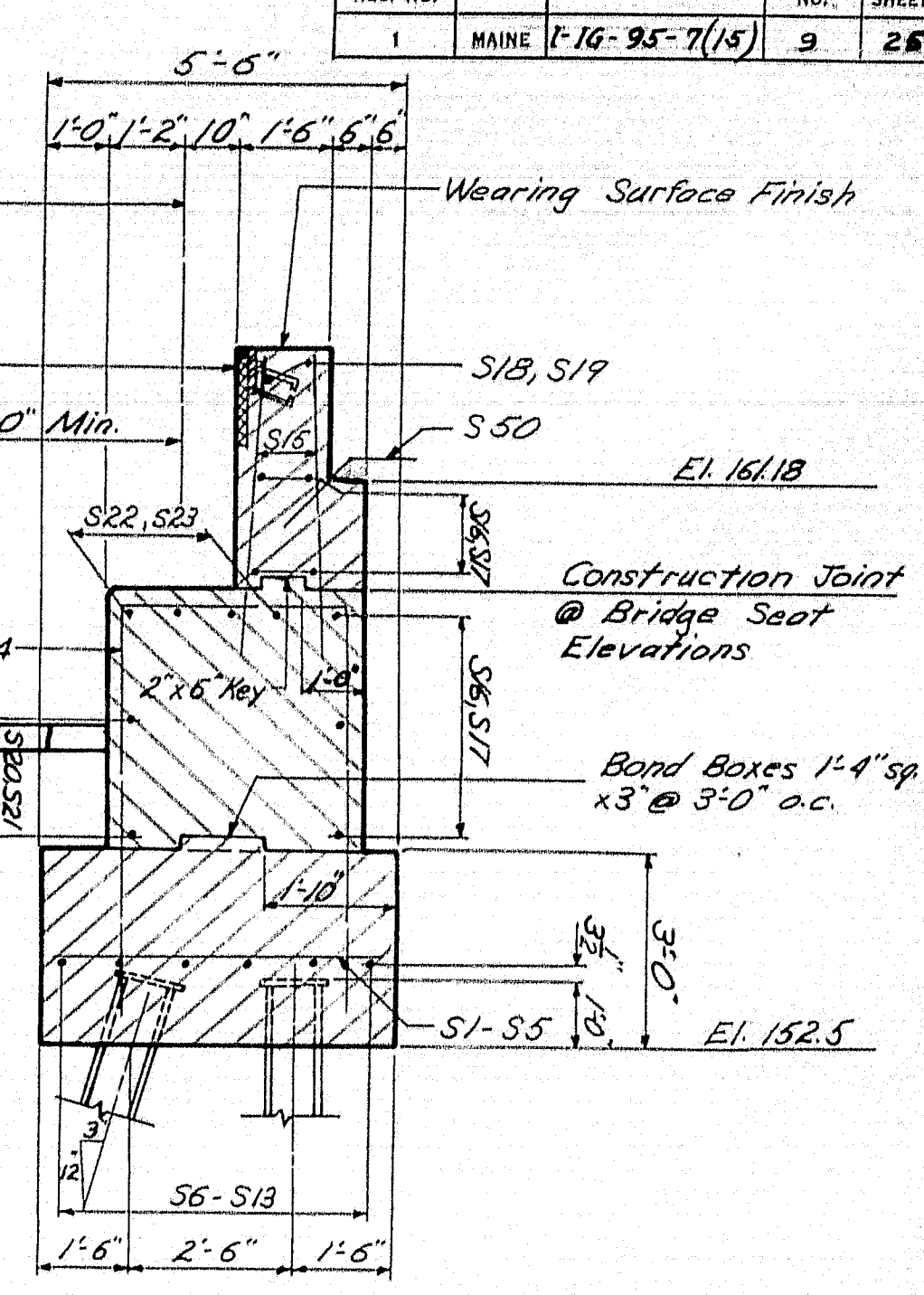
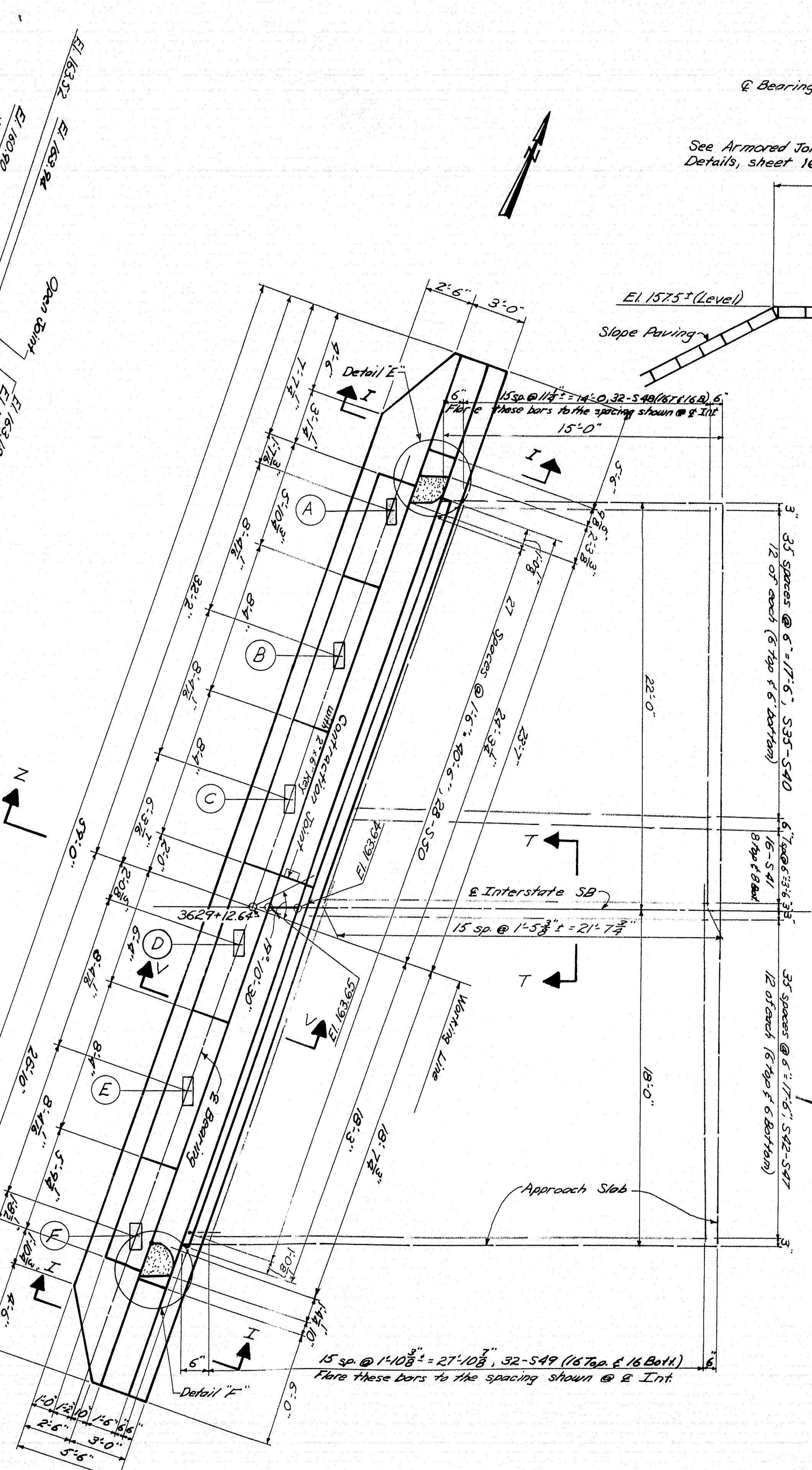
DETAIL F



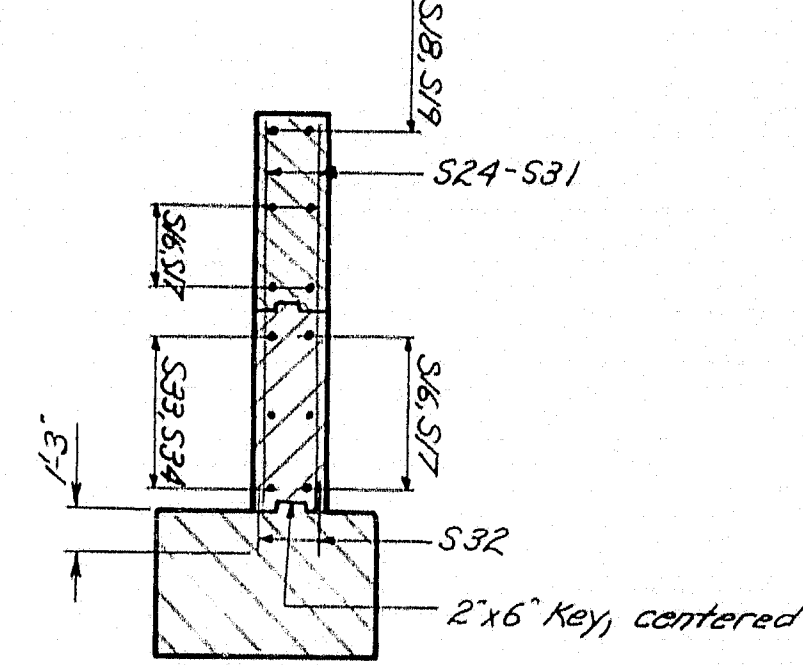
SECTION Q-Q



SECTION Z-Z



SECTION V-V



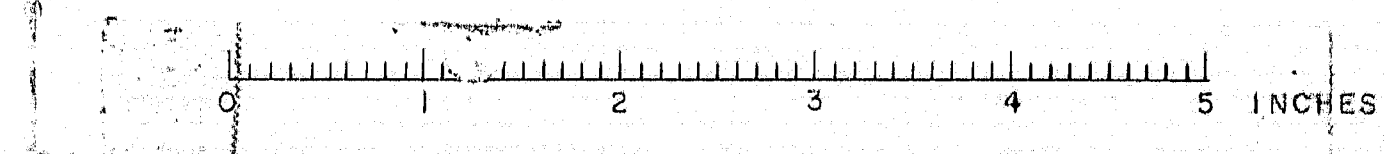
SECTION I-I

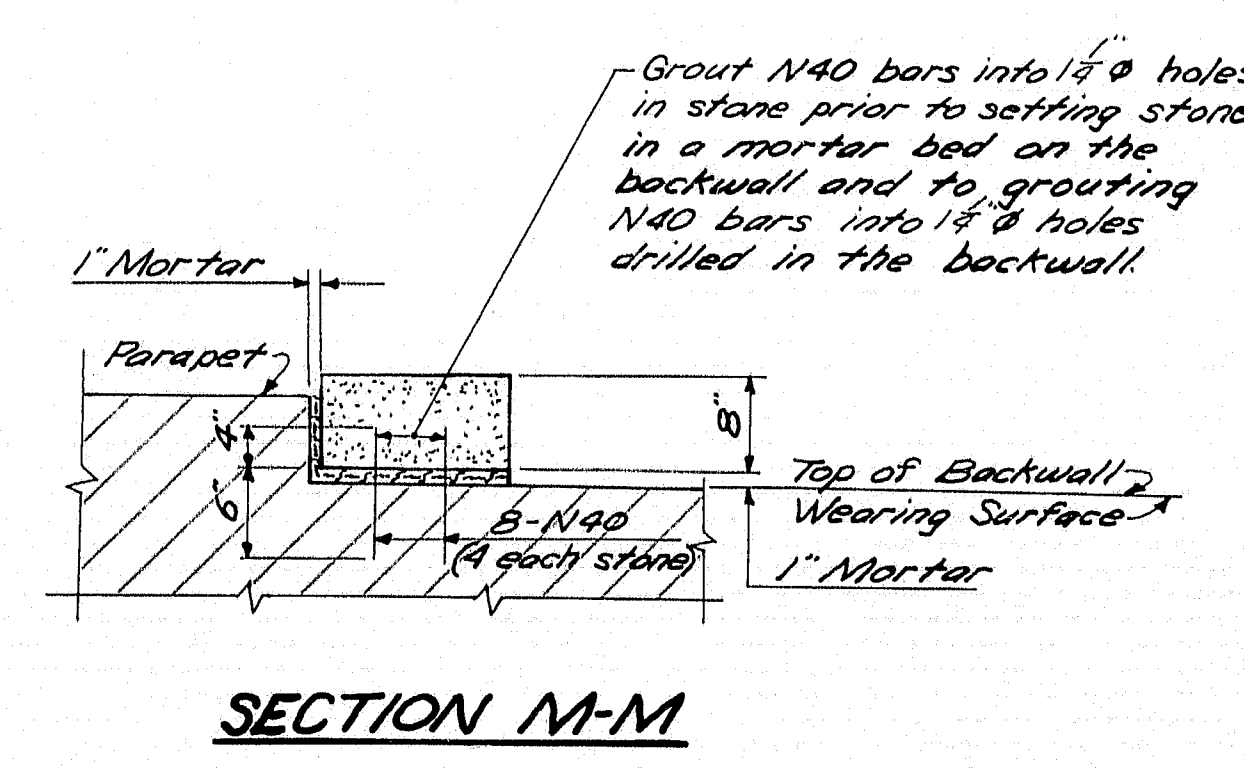
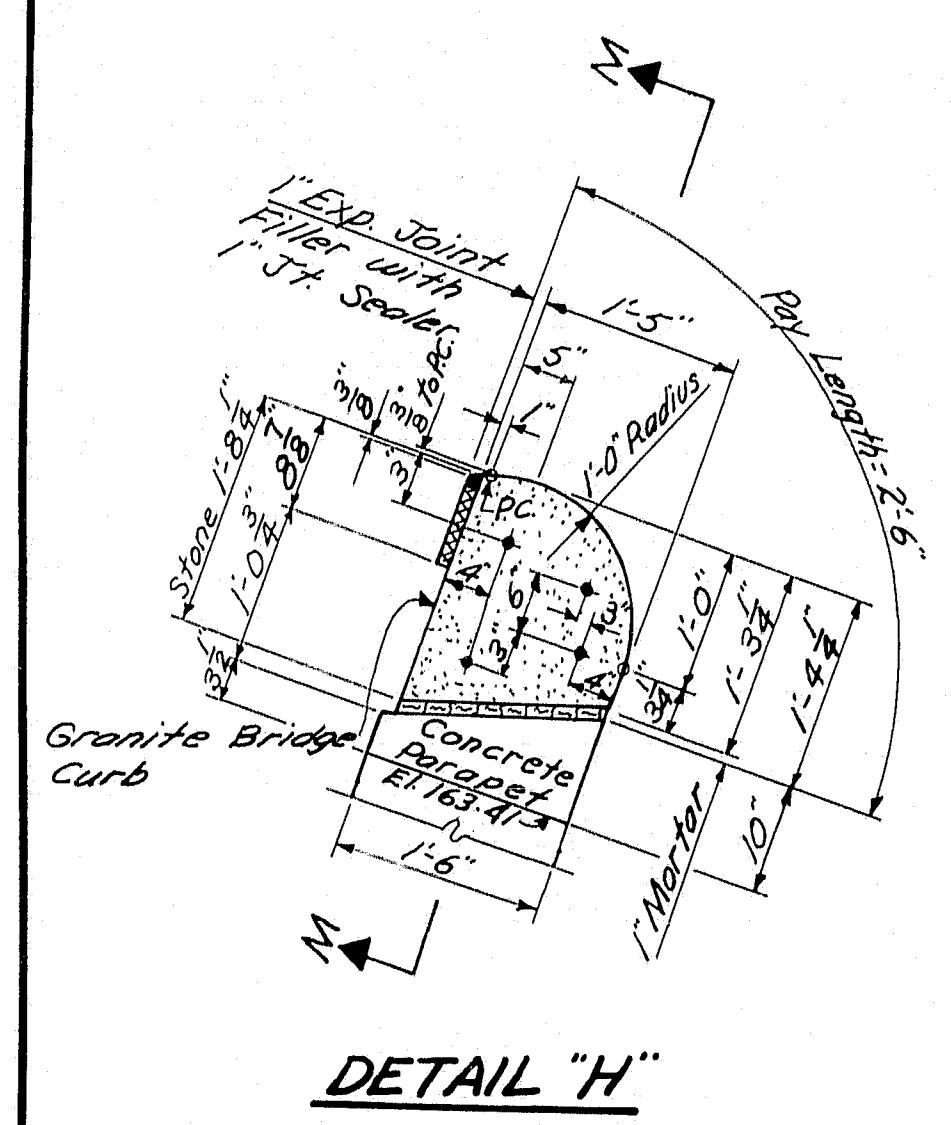
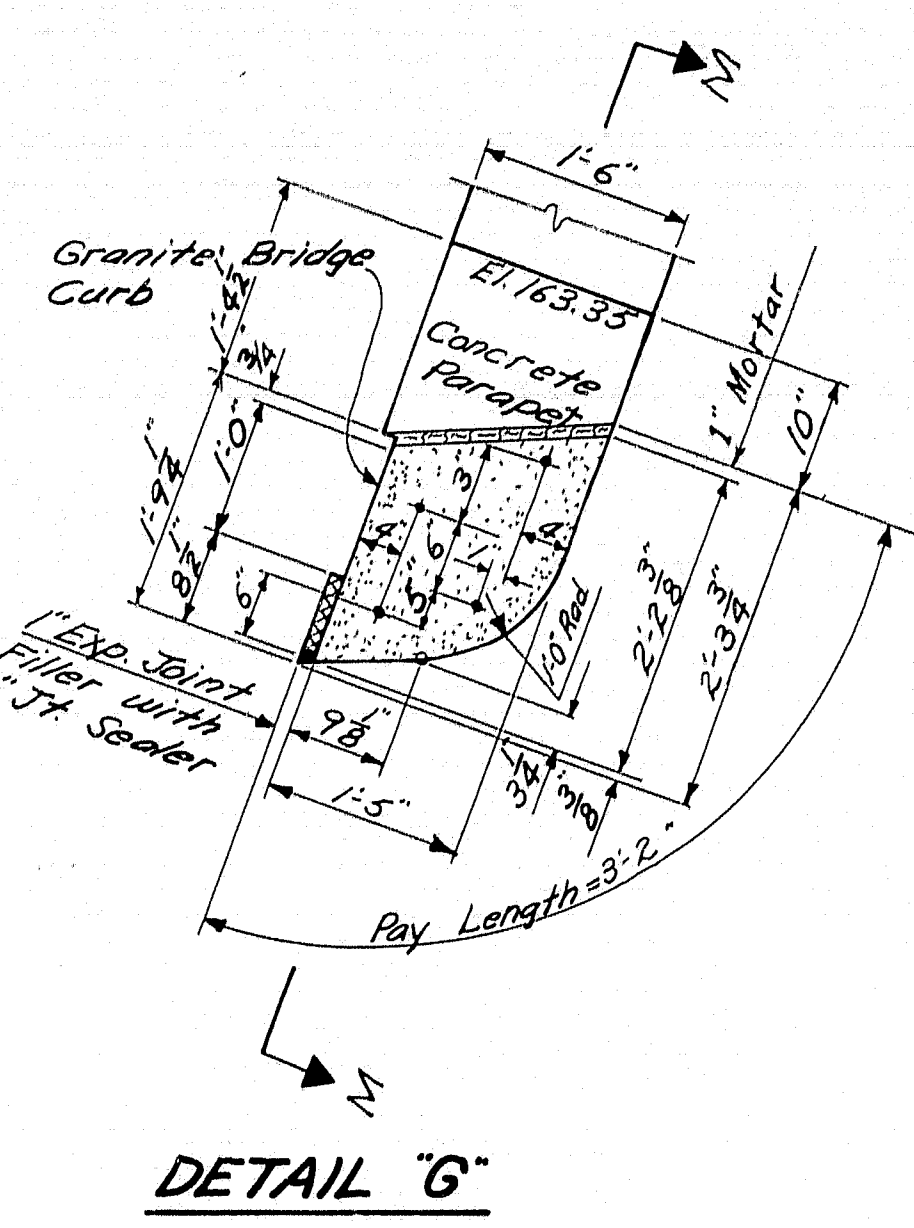
Notes:
For General Abutment Notes, Pile Notes, Pile Cap, and Section T-T, see sheet 8.

DESIGN - C.D.H.
TRACE - R.D.G.
CHECK - R.D.G.

BRIDGE NO. 100
SURVEY - 100
PLOT - 100

STATE HIGHWAY COMMISSION
BRIDGE DIVISION
INTERSTATE 95
OVER
EMERSON MILL ROAD & BANGOR & AROOSTOOK RAILROAD
IN THE TOWN OF
HAMPDEN
PENOBSCOT COUNTY
ABUTMENT #2 S.B.
SHEET 9 OF 25 AUGUSTA, MAINE SEPT., 1961





FOOTING AND PILE PLAN

FRONT ELEVATION

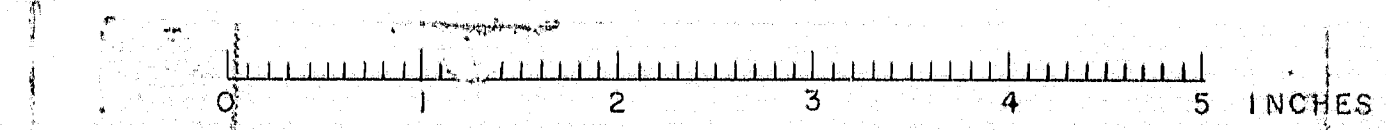
PLAN

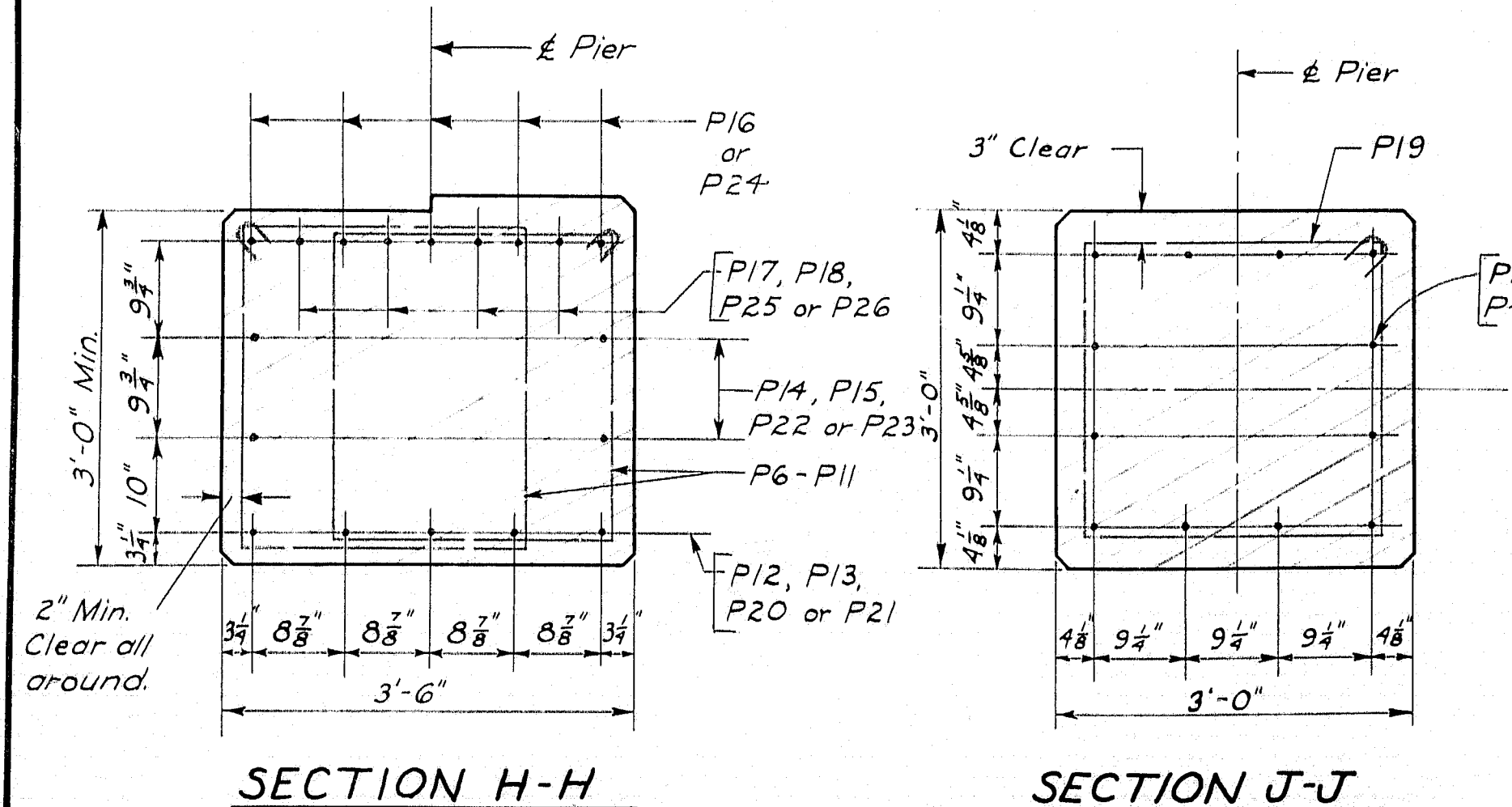
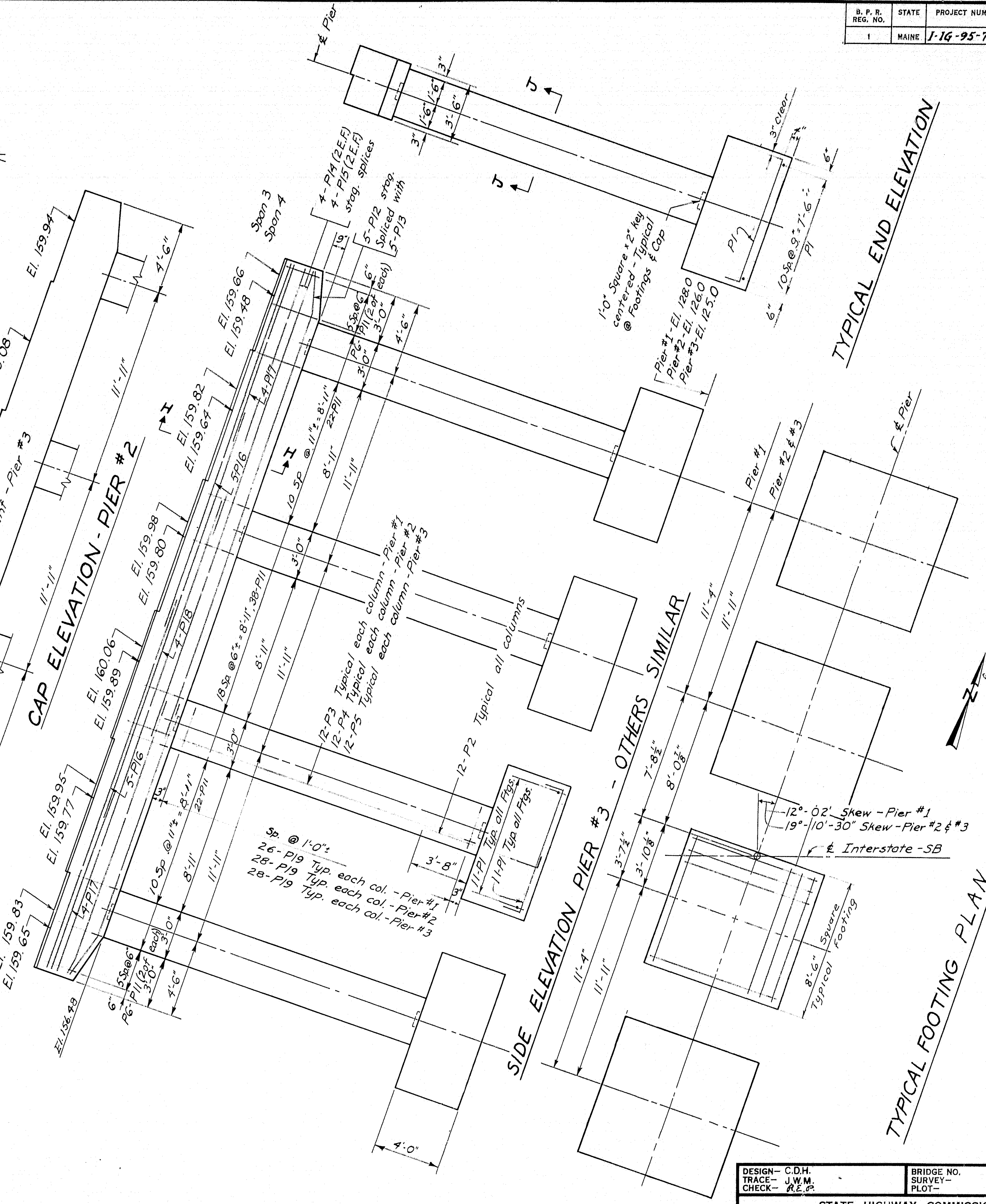
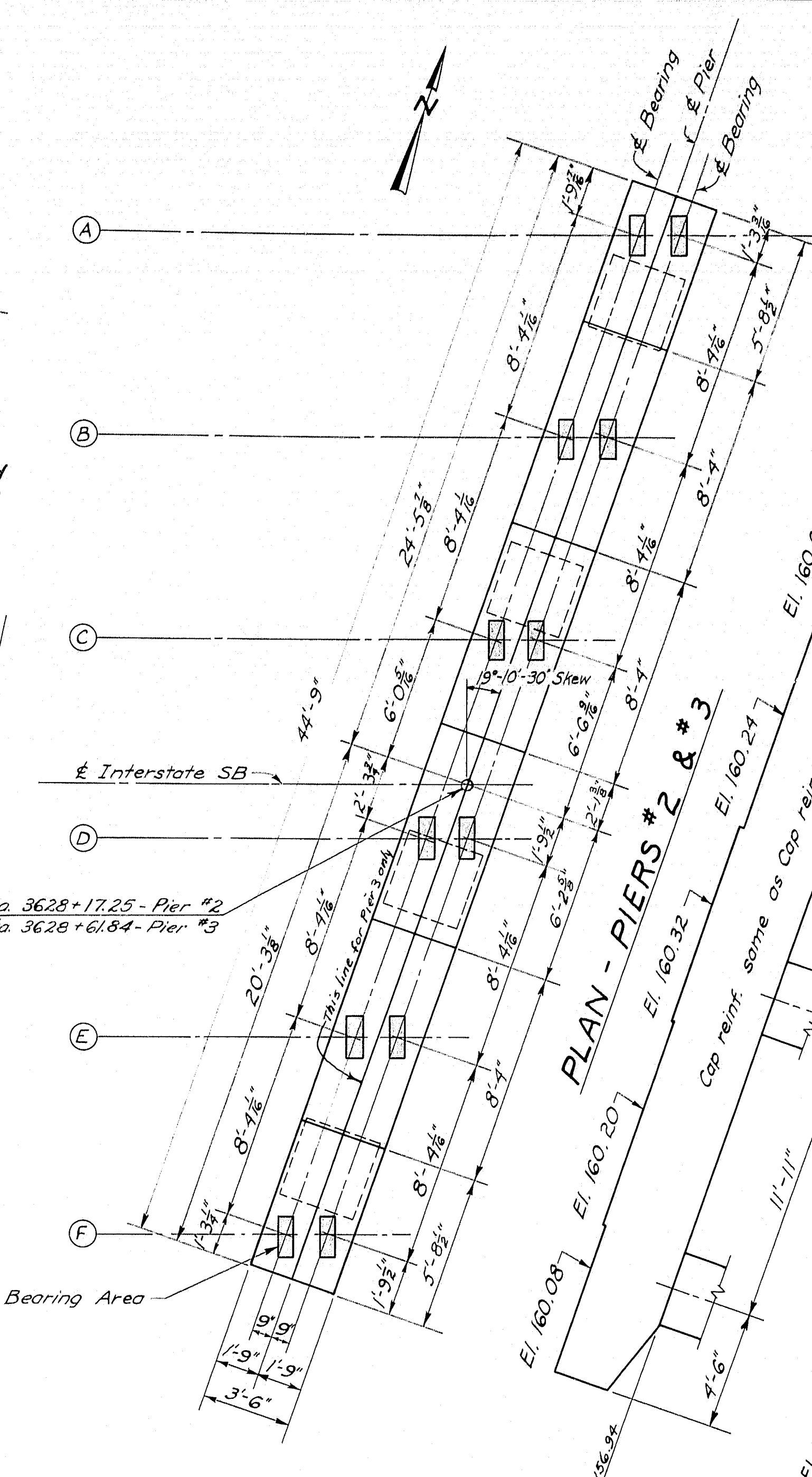
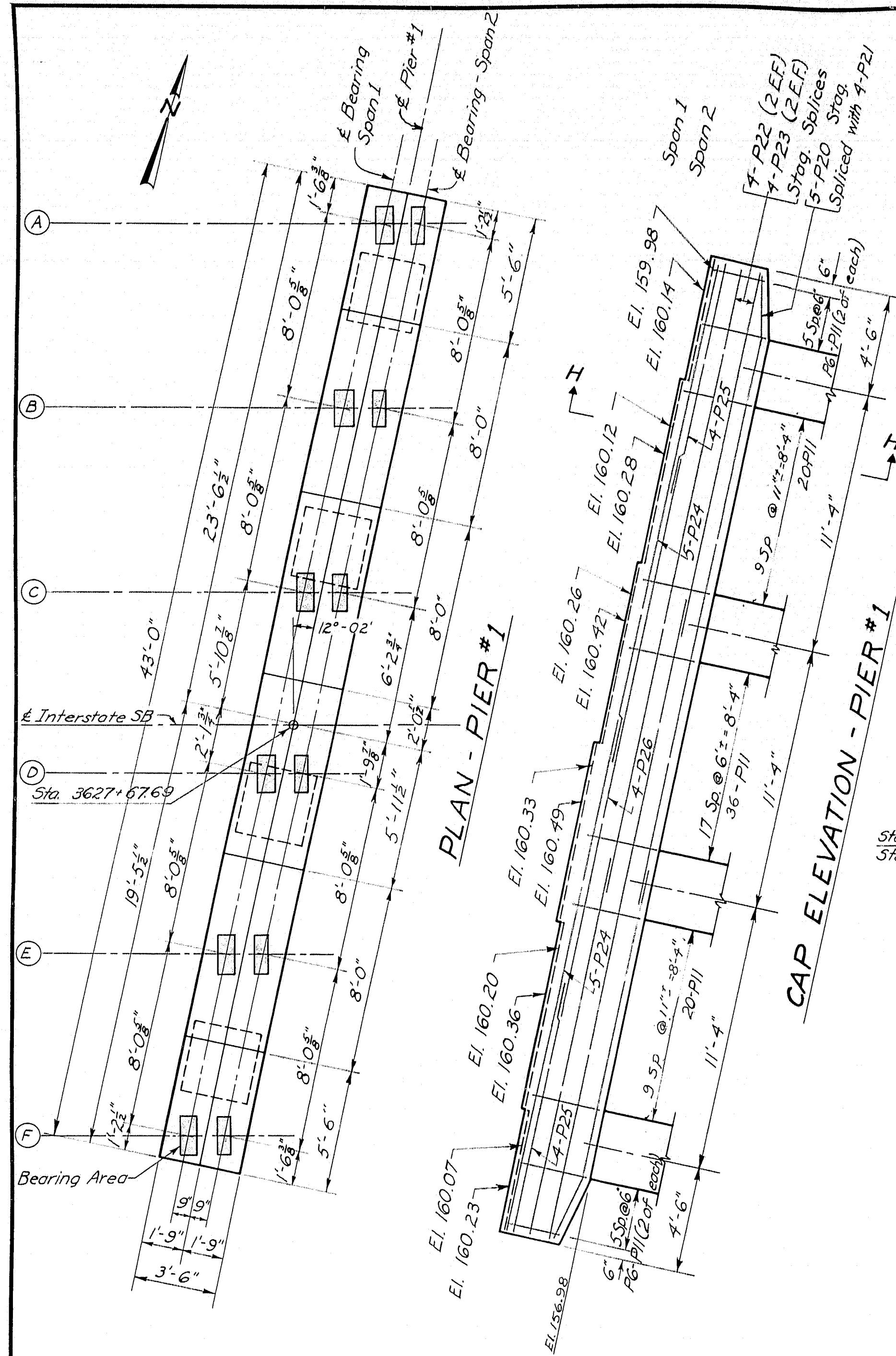
SECTION R-R

SECTION S-S

NOTES:
For General Abutment Notes, Pile Notes, Pile Cap, and Section T-T see sheet B.

DESIGN - C.D.H. TRACE - R.D.G. CHECK - J.E.P.	BRIDGE NO. SURVEY - PLOT -
STATE HIGHWAY COMMISSION BRIDGE DIVISION	
INTERSTATE 95	
OVER	
EMERSON MILL ROAD & BANGOR & AROOSTOOK RAILROAD	
IN THE TOWN OF	
HAMPDEN	
PENOBSCOT COUNTY	
ABUTMENT #2 - N.B.	
SHEET 11 OF 25 AUGUSTA, MAINE SEPT., 1961	





PIER NOTES

1. Position reinforcing steel in pier cap to clear swaged anchor bolts.
2. Chamfer all exposed corners $\frac{1}{4}$ inch.
3. Dress shodded Bearing Areas 1 inch larger all around than Masonry Plates to exact bearing elevations given.
4. E.F. = Each Face
5. Maximum footing pressure = 5.2 tons/sq. ft.

DESIGN - C.D.H.	BRIDGE NO.
TRACE - J.W.H.	195
CHECK - R.E.P.	OVER
STATE HIGHWAY COMMISSION	
BRIDGE DIVISION	
INTERSTATE 95	
EMERSON MILL ROAD &	
BANGOR & AROOSTOOK RAILROAD	
IN THE TOWN OF	
HAMPDEN	
PENOBSCOT COUNTY	
PIERS - SOUTHBOUND	
SHEET 12 OF 25	AUGUSTA, MAINE
SEPT., 1961	

