

HYDROLOGY, HYDRAULICS & SCOUR REPORT

1

June 2019

Hampden – I-95 over Souadabscook Stream (West, Center & East)

**Hydrology, Hydraulics & Scour Report
June 2019**

**Prepared for: Maine Department of Transportation
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June 2019**Hampden – I-95 over Souadabscook Stream (West, Center & East)****INTRODUCTION****PURPOSE**

The purpose of this report is to present the results of a study conducted at the subject bridge sites to evaluate the hydraulic performance of the assumed replacement alternative considered. This investigation was conducted in a manner consistent with Federal Highway Administration (FHWA) and Maine Department of Transportation (MaineDOT) guidelines.

SCOPE

The scope of work for this report consists of gathering and reviewing pertinent hydrologic data for the Souadabscook Stream at the Project sites, and a detailed hydraulic analysis. Data collected, and hydraulic model computer outputs are presented in this report.

EXISTING STRUCTURES

There are a total of six existing structures that carry Interstate 95 over the Souadabscook Stream. The bridges are split into three groups, West, Center, and East. Each group has a northbound and a southbound bridge.

Each bridge is a 130'-0" three-span, continuous steel girder structure. All the abutments are pile supported and founded on fill material. The piers are in-water concrete wall piers founded on piles at the West and Center Bridges and founded directly on bedrock at the East Bridges.

ENGINEERING METHODS**HYDROLOGY**

The Souadabscook Stream is the ninth largest tributary to the Penobscot River. It flows east-southeast for 18.9 miles from the outlet of Etna Pond to its confluence with the Penobscot River in Hampden. Hammond Pond, Hermon Pond, and Ben Annis Pond are all located in the Souadabscook Watershed.

USGS Regression Equations (Hodgkins, 1999 & Lombard/Hodgkins, 2015) were used to determine peak flows for the West, Center, and East Bridges. The maximum flows at the East Bridge were used for all three bridges. USGS data was provided by USGS StreamStats.

The East Bridge has a drainage area of 139 square miles. The watershed is estimated 15.79% storage areas and 6.86% developed (urban). The mean annual precipitation is 42.2 inches.

June 2019**Hampden – I-95 over Souadabscook Stream (West, Center & East)**

Existing plans (1961) report High Water Elevation = 130.5' NGVD, identical to the FEMA (1987) estimates of the 500-year Stillwater elevations for Hammond and Hermon Ponds. The FEMA Q500 at Manning Mill Road estimate is approximately the same as the value estimated from gage data on the adjacent Sebasticook River (6190 ft³/s FEMA vs. 6435 ft³/s gage, data through 2013). Taken together, these three sources provide reasonable estimates for the flood of record at 129.81 (NAVD) (130.5 NGVD).

Design Hydrology Summary	
Drainage Area	139 mi ²
Ordinary High Water (Q _{1.1})	1,204 ft ³ / s
(Q ₁₀)	3,639 ft ³ / s
(Q ₂₅)	4,435 ft ³ / s
Design Discharge (Q ₅₀)	5,036 ft ³ / s
Check Discharge (Q ₁₀₀)	5,672 ft ³ / s
Scour Check Discharge (Q ₅₀₀)	7,178 ft ³ / s

HYDRAULICS

The 1987 Town of Hampden Flood Insurance Study (FIS) provided the peak discharge values at common locations as depicted below.

1987 Town of Hampden Flood Insurance Study (FIS) Peak Discharge Summary				
Location	10-Year	50-Year	100-Year	500-Year
At U.S. Route 1A	3,310	4,680	5,220	6,630
At Manning Mill Road	3,090	4,380	4,880	6,190

Interstate 95 Northbound and Southbound each cross the Souadabscook Stream in three locations, referred to as the West, Center, and East Bridges, for a total of six bridges. The FIS reported the peak discharge of 4,880 cfs for the 100-year event at the Intersection of the Souadabscook Stream and Manning Mill Road. This is less than the 5,672 cfs flow estimated by MDOT.

Since the FIS only evaluated a single storm event, with a magnitude found to be about 15% less than recently estimated value, starting water surface elevations (SWSEL) could not be obtained from the FEMA FIS.

All elevations are based on North American Vertical Datum (NAVD) of 1988. Elevations based on the National Geodetic Vertical Datum (NGVD) of 1929 were converted to NAVD by subtracting 0.69 feet.

June 2019**Hampden – I-95 over Souadabscook Stream (West, Center & East)**

The existing bridge plans (1961) report a high-water Elevation of 130.5' NGVD (EL 129.81' NAVD). FEMA (1987) estimates of the 500-year stillwater elevations for Hammond and Hermon Ponds to be EL 130.5' NGVD (EL 129.81' NAVD).

An existing condition model was developed with a boundary condition of normal depth and estimated channel slopes. A downstream energy grade (EG) was set at 0.00262 for all storm events. Specific stream sections were surveyed and provided by the Maine DOT Survey Section. Geometric data for the existing bridge was taken from the existing bridge plans. All elevations were referenced to the project datum (NAVD 1988).

Manning's "n" values were based on information from the FEMA study, with channel "n" of 0.03 and overbank "n" of 0.092.

The existing conditions model was compared with the FEMA FIS water surface elevations and velocities. In general, the existing conditions model water surface elevations were approximately one to one-and-a-half feet lower than the FEMA FIS. Subsequently, the velocities in the existing conditions model were higher than what was reported in the FEMA FIS.

The proposed bridge was modeled in HEC-RAS with the bottom chord for all bridges set at Elevation 130 for developing hydraulic clearances. Both abutments are assumed to be integral abutments placed in the same locations as the existing abutments such that the face-to-face distance between the abutments matches existing.

A two-span structure was modeled for hydraulic design purposes, but a single-span structure is also an allowed design-build alternative. The two-span structure was modeled because it will provide the most conservative estimate for the computed water surface elevations and velocities.

The proposed typical stream section at the structures was developed to meet the conditions of the U.S. Army Corps of Engineers Maine General Permit. The piers are assumed to be wall piers on buried footings, founded on piles or bedrock, with the top of the footings below the depth of the typical riprap section as defined in the Standard Details. See Figure 1 and Figure 2.

June 2019

Hampden – I-95 over Souadabscook Stream (West, Center & East)

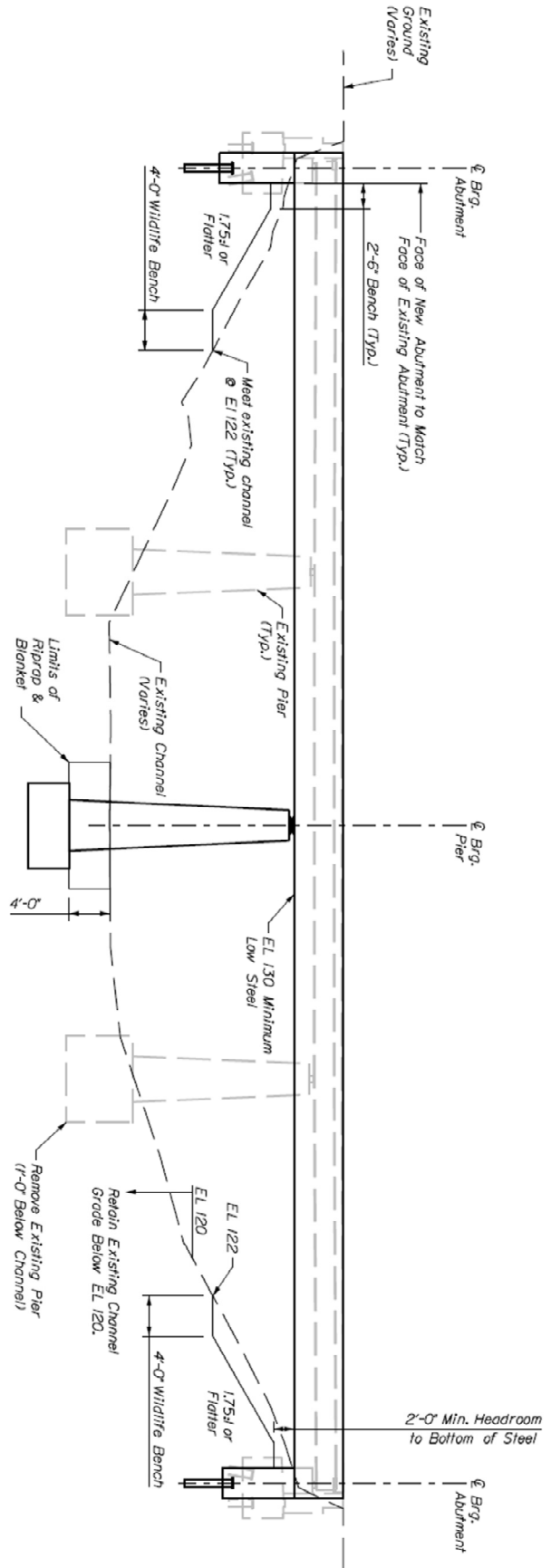


FIGURE 1: ASSUMED BRIDGE ELEVATION SCHEMATIC
Center Bridge Shown, West and East Bridges Similar,
Not to scale.

June 2019

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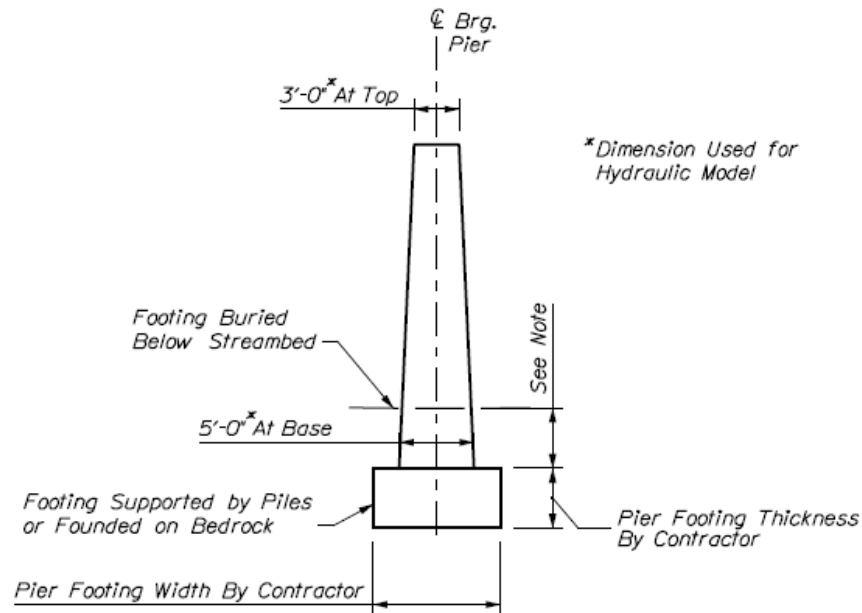


FIGURE 2: ASSUMED PIER GEOMETRY

Note:

The proposed top of footing for the pier is assumed to be placed below the MaineDOT Standard Detail riprap section.

West Bridge Hydraulic Summary						
Elevations, Velocities & Clearances	Existing Structure			Assumed Structure		
	3-Span Steel Girder Bridge 130 feet			2-Span Steel Girder Bridge 130 feet		
	Discharge Velocity (fps)	Headwater Elevation (ft)	Clearance (ft)	Discharge Velocity (fps)	Headwater Elevation (ft)	Clearance (ft)
Q1.1	1.97	122.01	9.69	2.01	121.93	8.07
Q10	3.58	125.48	6.22	3.68	125.23	4.77
Q25	3.93	126.4	5.3	4.07	126.08	3.92
Q50	4.17	127.06	4.64	4.33	126.68	3.32
Q100	4.6	127.27	4.43	4.59	127.29	2.71

Center Bridge Hydraulic Summary						
Elevations, Velocities & Clearances	Existing Structure			Assumed Structure		
	3-Span Steel Girder Bridge 130 feet			2-Span Steel Girder Bridge 130 feet		
	Discharge Velocity (fps)	Headwater Elevation (ft)	Clearance (ft)	Discharge Velocity (fps)	Headwater Elevation (ft)	Clearance (ft)
Q1.1	1.28	121.47	10.23	1.3	121.36	8.64
Q10	2.55	124.91	6.79	2.61	124.67	5.33
Q25	2.85	125.81	5.89	2.93	125.52	4.48
Q50	3.06	126.44	5.26	3.15	126.10	3.9
Q100	3.43	126.5	5.2	3.37	126.69	3.31

June 2019

Hampden – I-95 over Souadabscook Stream (West, Center & East)

East Bridge Hydraulic Summary						
Elevations, Velocities & Clearances	Existing Structure			Assumed Structure		
	3-Span Steel Girder Bridge			2-Span Steel Girder Bridge		
	130 feet			130 feet		
	Discharge Velocity (fps)	Headwater Elevation (ft)	Clearance (ft)	Discharge Velocity (fps)	Headwater Elevation (ft)	Clearance (ft)
Q1.1	2.69	120.91	10.79	2.74	120.85	9.15
Q10	4.45	123.79	7.91	4.62	123.57	6.43
Q25	4.85	124.53	7.17	5.05	124.25	5.75
Q50	5.1	125.07	6.63	5.35	124.73	5.27
Q100	6.16	124.58	7.12	5.63	125.23	4.77

SCOUR

The project geotechnical engineer obtained borings and provided grain-size analyses of the existing channel bed material at various soil depths for estimating contraction scour. Since local scour can be increased by debris lodged on a substructure unit, the pier widths were increased by 25% (to 6.25 feet) to account for debris for local pier scour calculations. Total abutment scour was estimated with NCHRP 24-20 equations, and local pier scour was estimated with CSU equations.

Q100 and Q500 flood events were analyzed and the results are shown below.

West Bridge Scour Summary						
Element	100-Year			500-Year		
	Total Scour (ft)			Total Scour (ft)		
Abutment No. 1	2.2			3.1		
Abutment No. 2	2.2			3.1		
Element	Contraction	Local	Total	Contraction	Local	Total
Pier	2.30	9.12	11.4	2.79	8.75	11.5

Center Bridge Scour Summary						
Element	100-Year			500-Year		
	Total Scour (ft)			Total Scour (ft)		
Abutment No. 1	5.0			8.9		
Abutment No. 2	5.0			8.9		
Element	Contraction	Local	Total	Contraction	Local	Total
Pier	3.18	7.32	10.5	5.21	7.84	13.1

HYDROLOGY, HYDRAULICS & SCOUR REPORT

June 2019

8

Hampden – I-95 over Souadabscook Stream (West, Center & East)

East Bridge Scour Summary						
Element	100-Year			500-Year		
	Total Scour (ft)			Total Scour (ft)		
Abutment No. 1	12.2			17.4		
Abutment No. 2	12.2			17.4		
Element	Contraction	Local	Total	Contraction	Local	Total
Pier*	1.95	8.58	10.5	1.88	8.75	10.6

*Bedrock was discovered 2.0' and 7.5' below the existing streambed at the East Bridges.

All values are in feet. Scour is measured from the bottom of the stream.

The existing riprap slopes below Elevation 120 shall be left in place and unaltered. Plain riprap shall be placed where existing piers are removed and around the proposed piers. Proposed slopes above Elevation 120 shall be protected with a layer of plain riprap in accordance with the Standard Details.

All bridges shall be founded on competent rock or on piles driven to rock. The structures shall meet all the requirements of AASHTO LRFD 2.6.4.4.2, with Q100 = design flood for scour and Q500 = check flood for scour.

The East Bridge substructures shall be designed for a scour depth equal to the depth of bedrock. Substructures shall be founded on competent rock. Weathered, fractured, or otherwise unsuitable rock shall be removed. See provided Geotechnical Data Reports for more information on bedrock depth and composition.

CONCLUSIONS AND RECOMMENDATIONS

The following are recommendations for inclusion into the Request for Proposal document as Technical proposal Responsiveness Requirements:

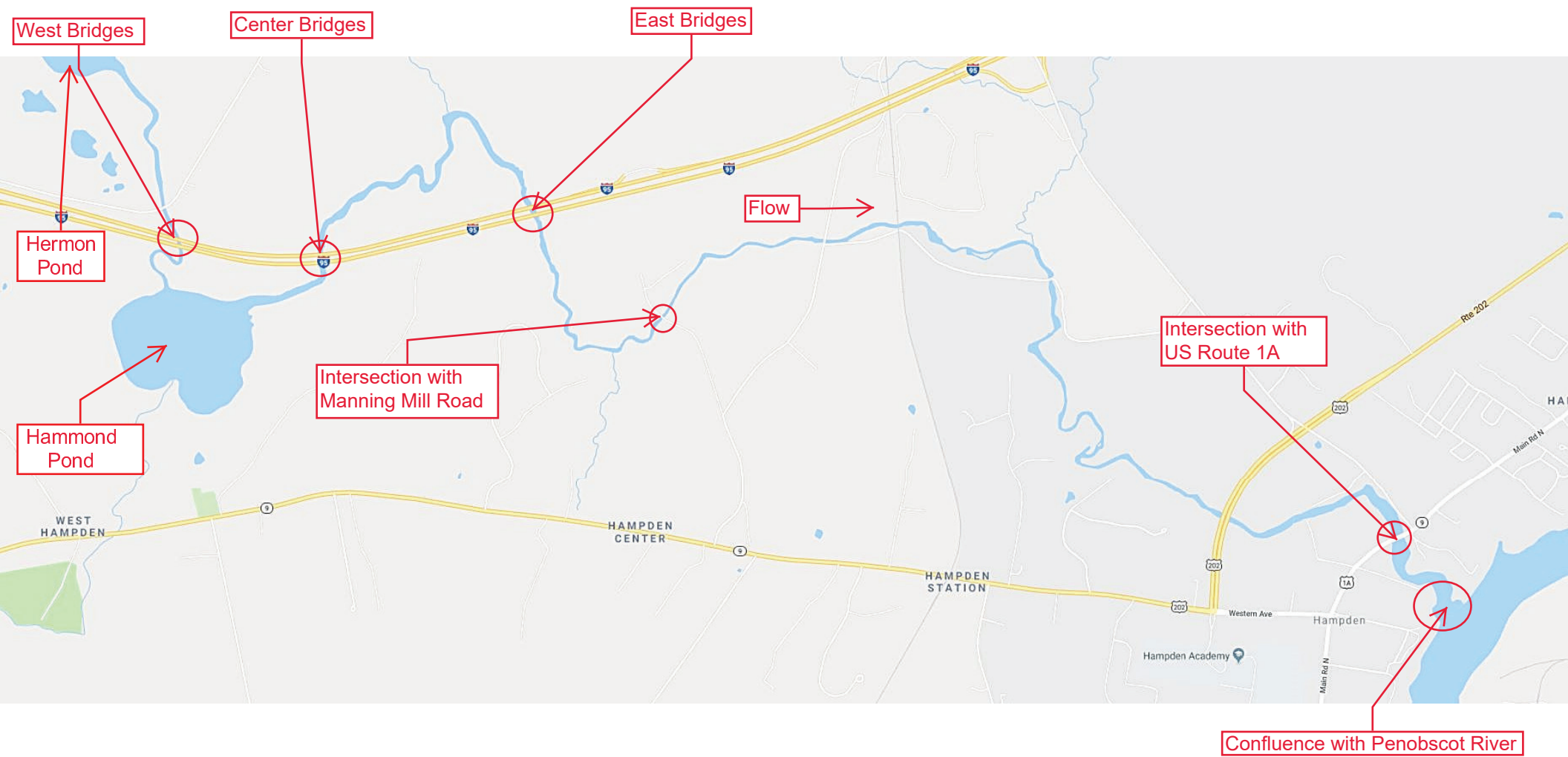
1. The bottom of steel for the proposed structures shall not be lower than Elevation 130 (NAVD88).
2. The length of the proposed bridge opening, measured from face-to-face of the abutments, shall be equal to or greater than the existing structures.
3. The proposed abutments shall not be closer than the existing abutments to the stream.
4. All bridge foundations shall be either founded directly on competent rock or be founded on piles driven into rock.
5. Efforts should be made to retain as much of the existing riprap slopes as feasible. Areas disturbed by work shall be protected with plain riprap installed in accordance with Standard Details and Specifications.

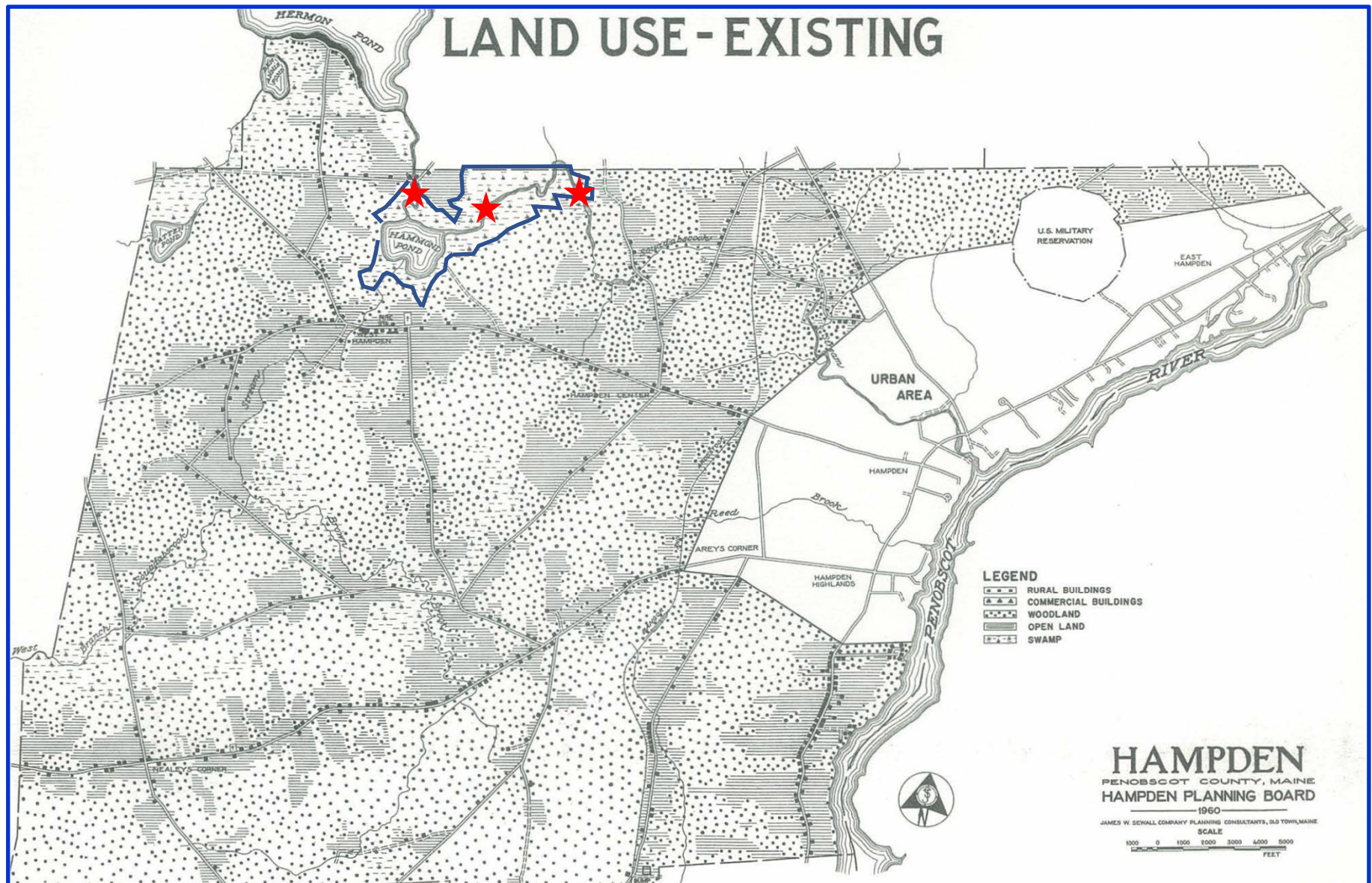
Hydrology, Hydraulic, & Scour Attachments

1. Hydrology	1-1
a. River Study Area Map	1-1
b. 1960 Hampden Land Use Map (Pre-Interstate Construction)	1-2
c. Recorded High Water Records & Project Hydrology (Maine DOT. Environmental Office Hydrology Section) (4 pages)	1-3
d. Peak Flow Calculations by USGS Regression Equations for Souadabscook Stream (Maine DOT. Environmental Office Hydrology Section) (27 pages)	1-7
e. Discharges from 1987 FEMA FIS	1-34
f. Hammond Pond & Hermon Pond Stillwater Elevations from 1987 FEMA FIS	1-35
 2. Hydraulics	 2-1
a. Regulatory Flood Limits from 1987 FEMA FIRM	2-1
b. Flood Profiles from 1987 FIS (3 pages)	2-2
d. Floodway Data from 1987 FIS	2-5
f. HEC-RAS Model Cross Section Location Map	2-6
g. HEC-RAS Existing Model Flood Profiles	2-7
h. HEC-RAS Existing Model Cross Sections	2-8
i. HEC-RAS Proposed Model Flood Profiles	2-23
j. HEC-RAS Proposed Model Cross Sections	2-24
k. HEC-RAS Composite Hydraulic Results Table	2-39
l. HEC-RAS Existing Bridge Velocity Results	2-43
m. HEC-RAS Proposed Bridge Velocity Results	2-49
 3. Scour	 3-1
a. Scour Summary Table	3-3
a. Design D50 Calculations	3-4
b. West Bridge Scour Calculations: Q100	3-5
b. West Bridge Scour Calculations: Q500	3-12
b. Center Bridge Scour Calculations: Q100	3-19
b. Center Bridge Scour Calculations: Q500	3-25
b. East Bridge Scour Calculations: Q100	3-31
b. East Bridge Scour Calculations: Q500	3-38
e. D ₅₀ Classification Data	3-45

d. West Bridge Riprap Design Calculations 3-48

d. Center Bridge Riprap Design Calculations..... 3-49





Memo

To: Jeff Folsom, Leanne Timberlake, Theresa McAuliffe, Ron Joy
From: Charles Hebson
Date: 22 April 2019
Re: 21728 Hampden I-95 Bridges - Hydrology

Executive Summary

Hydrology information for the Souadabscook River near the three I-95 bridges in Hampden are available from four sources: existing MaineDOT plans (1961), FEMA Flood Insurance Study (FIS; 1987), calculated for this project using USGS regression methods (Hodgkins, 1999), and calculated from USGS river gage data on the adjacent Sebasticook River. The water surface elevations from the plans and the FIS match exactly. The peak flow estimates from the FIS and scaled from the Sebasticook gage (Pittsfield, #01049000) are in close agreement. The FIS estimates are given at Manning Mill Rd, just downstream of the East Bridge (#1431). The regression equations applied directly at Manning Mill Rd are significantly (30% - 35%) higher than the FIS and scaled Sebasticook estimates. Given that the estimates from the plans, FIS and Sebasticook gage are all self-consistent, it is reasonable to conclude that these estimates are acceptable representations of the 500-yr water surface elevation and the range of design flows.

Table 1. Peak Flow Estimates, Souadabscook River @ Manning Mill Rd, Hampden, ME

T (yrs)	Peak Flows (ft ³ /s)				Water Elev (ft NGVD)	
	FIS (1987)	USGS ¹	USGS ²	Regr	Plans	FIS
10	3,090	3,445	2,935	4,170		
50	4,380	4,720	4,615	5,810		
100	4,880	5,285	5,145	6,560		
500	6,190	6,625	6,435	8,350	130.5 ³	130.5

Note: 1. Sebasticook weighted gage/regression estimates scaled by watershed area ratio
2. Regression equations applied to Souadabscook River at Manning Mill Rd
3. Reported as “High Water” without an associated return period.

Discussion

The 1961 MaineDOT bridge plans report “High Water” as 130.5’ NGVD, for the years 1936 and 1955. The FEMA Flood Insurance Study (FIS; 1987) reports the same exact value for the 500-yr elevation. The FIS employed the widely used TR-20 rainfall-runoff model for the Souadabscook. The report states that the results were “checked against” the USGS regression equations (Morrill, 1975) current at the time. Given the exact agreement between the noted and modeled water levels, it is possible that the model was calibrated to the 130.5’ NGVD level. It is also possible that the modeled flows are somehow “calibrated” to the regression estimates. It is impossible to conclude what the situation is, since we do not know exactly how the water level data and regression estimates were used with the TR-20 model. Likewise, it is impossible to say whether gage data from the adjacent Seabasticook watershed were used in any way to check the model. However, it does seem reasonable to infer that the TR-20 model results are not entirely independent of the regression calculations and reported water elevation.

Standard MaineDOT hydrology practice is to use the current USGS (Hodgkins, 1999) regression equations when gage data are unavailable. The results for Manning Mill Rd are given in Table 1 under column “Regr”. These values are significantly larger (35%) than the FIS estimates. The Souadabscook is ungaged but the adjacent Seabasticook River was gaged from 1928 through 2013. The Seabasticook regression and gage estimates are similarly inconsistent, as reported by Hodgkins (p. 13). When a river is gaged, the gage and regression estimates are combined to form a final weighted estimate:

$$Q_w = \{n/(n+e)\}Q_g + \{e/(n+e)\}Q_r$$

where Q_w = final weighted estimate
 Q_g = estimate from gage data fitted to LP-III distribution
 Q_r = estimate from regional regression equation
 n = length of record
 e = equivalent record length for regression estimate (Table 2)

The Seabasticook record was $n = 68$ years long with data through 1996 in the 1999 report, so the relative weight for regression (approx. $5.5 / (68 + 5.5) = 0.075$) is small compared to the gage weight (0.925). Thus, even though the regression estimates Q_r are larger than the gage estimate, the final weighted estimates are not much larger than the gage estimates Q_g , as show in Table 2. Since the 1999 report was published, 17 additional years of data ($n = 85$ years) were collected at the Seabasticook gage. The weighted estimates were updated using the program PeakFQ and methods in Hodgkins (1999). The updated estimates (“2013”) are shown in Table 2; the values are noticeably smaller than in the 1999 report because of the weighting. Note that the Flood of Record for the Seabasticook was recorded in 1987 and approximates the 500-yr event; we do not have corresponding water levels for the Souadabscook.

Given the close proximity between the Sebasticook and Souadabscook watersheds, simple area scaling was applied to the Sebasticook estimates to estimate Souadabscook flows at Manning Mill Rd. The Sebasticook gage watershed is 571 mi² while the Souadabscook is 140 mi² at Manning Mill. This difference in areas is outside the usual range for scaling. However, the likely similarities between the watersheds and the evident differences between the Sebasticook gage and regression

estimates makes area scaling a useful approach. Simple area scaling, for annual maximum peak flows Q_T , from watershed 1 to watershed 2 is calculated as

$$Q_{T2} = (A_2/A_1)^{a_T} \times Q_{T1}$$

where a_T is an exponent that depends on return period T and A is watershed area. Values for “ a ” are given in Table 2, watershed areas A in Table 3. This equation was applied using the weighted Sebasticook estimates.

The scaled peak flow estimates for the Souadabscook at Manning Mill Rd are given in Table 1 under the headings “USGS (1996)” and “USGS (2013)”. These estimates are remarkably consistent with the FIS values. Therefore, we conclude that an elevation of 130.5’ NGVD and the area-scaled Sebasticook estimates (based on data through 2013) constitute a reasonable set of hydrologic values for further analysis. The reasoning for this is as follows:

- 1) The Sebasticook estimates are based on real flow data
- 2) The Sebasticook regression results are much bigger than the gage estimates, thus raising questions about the validity of the regression estimates
- 3) Besides watershed area, we expect the Souadabscook and Sebasticook to be similar
- 4) We there expect a similar discrepancy between regression estimates and real Soudabscook flows (were they known)
- 5) Thus, we prefer Sebasticook flows scaled to the Souadabscook watershed area, instead of regression estimates for the Souadabscook.
- 6) The resulting area-scaled peak flow estimates are very similar to the 1987 FIS flow estimates
- 7) Therefore we infer that the FIS water surface elevation (based on the FIS flows) of 130.5’ NGVD is a reasonable estimate of extreme high water (100-yr to 500-yr)

Table 2. Peak Flow Estimates, Sebasticook River Gage (not scaled for area).

				N = 68		N = 85	
			Qr	Qg	Qw	Qg	Qw
T (yysr)	a	e		(1996)	(1996)	(2013)	(2103)
10	0.783	4.00	11,537	10,266	10,337	8,681	8,809
50	0.757	5.33	15,453	13,512	13,653	13,210	13,342
100	0.748	5.86	17,146	14,923	15,100	14,520	14,689
500	0.729	6.89	21,203	18,134	18,416	17,620	17,889
FOR (1987)						17,659	

FOR = Flood of Record

Since the FIS hydrology was evaluated for the watershed at Manning Mill Rd, all other estimates were also made for this watershed outlet point. The three bridges are located at various points upstream of Manning Mill Rd, starting with the East Bridge. Thus, bridge watersheds are somewhat smaller than at Manning Mill Rd. It is conservative to apply the Manning Mill Rd flows to the bridge locations, particularly West Bridge. The bridge watershed areas (as determined with StreamStats) are summarized in Table 3.

Table 3. Souadabscook Watershed Areas (mi²) as Determined by StreamStats

	Manning Mill Rd		East Br #1431	Center Br #1432	West Br #1433	Sebasticoock Gage ¹
	FIS	StreamStats				#01049000
Area (mi ²)	140.4	142.0	138.7	124.3	94.5	571.4
NWI (%)		14.1	15.8	14.7	16.3	15.6

Notes: 1. Sebasticoock data from Hodgkins, 1999.

References

FEMA, 1987. Flood Insurance Study, Town of Hampden, Maine, Penobscot County.

Flynn, K.M., Kirby & Hummel, 2006. User's Manual for Program PeakFQ Annual Flood-Frequency Analysis Using Bulletin 17B Guidelines: U.S. Geological Survey, Techniques and Methods Book 4, Chapter B4.

Hodgkins, G., 1999. Water-Resources Investigations Report 99-4008, Estimating the Magnitude of Peak Flows for Streams in Maine for Selected Recurrence Intervals, U.S. Geological Survey, Augusta, Maine.

Morrill, R.A., 1975. Open-File Report 75-292, A Technique for Estimating the Frequency and Magnitude of Floods in Maine, U.S. Geological Survey, Augusta, Maine.

WIN: 21729.10
 Town: Hamden
 Route No. US 95
 Asset ID: 1431
 Lat: 44.7655 Long: -68.89451

Project Name: Hamden B#1431
 Stream Name: Souadabscook Stream
 Bridge Name: Souadabscook East SB Bridge
 Analysis by: DFB
 Date: 7/6/2017

Peak Flow Calculations by USGS Regression Equations (Hodgkins, 1999 & Lombard/Hodgkins, 2015)

Enter data in blue cells only!

	km ²	mi ²	ac
A	359.23	138.70	88768.0
W	56.72	21.9	14016.5
P _c	498806	4957576	
County	Penobscot S		
pptA	39.5		
SG	0.02		
A (km ²)	359.23		
W (%)	15.79		

Enter data in [mi²]

Watershed Area *DRNAREA*
 Wetlands area (by NWI)

watershed centroid (E, N; UTM 19N; meters)
 choose county from drop-down menu
 mean annual precipitation (inches; by look-up)
 sand & gravel aquifer as decimal fraction of watershed A

Conf Lvl 0.67

NWI Wetlands % *STORNWI*

Worksheet prepared by:

Charles S. Hebson, PE
 Environmental Office
 Maine Dept. Transportation
 Augusta, ME 04333-0016
 207-557-1052
Charles.Hebson@maine.gov
 ver. 2016 Feb 05

References:

Hodgkins, G.A., 1999.
 Estimating the magnitude of peak flows for streams
 in Maine for selected recurrence intervals
WRIR 99-4008, USGS Augusta, ME

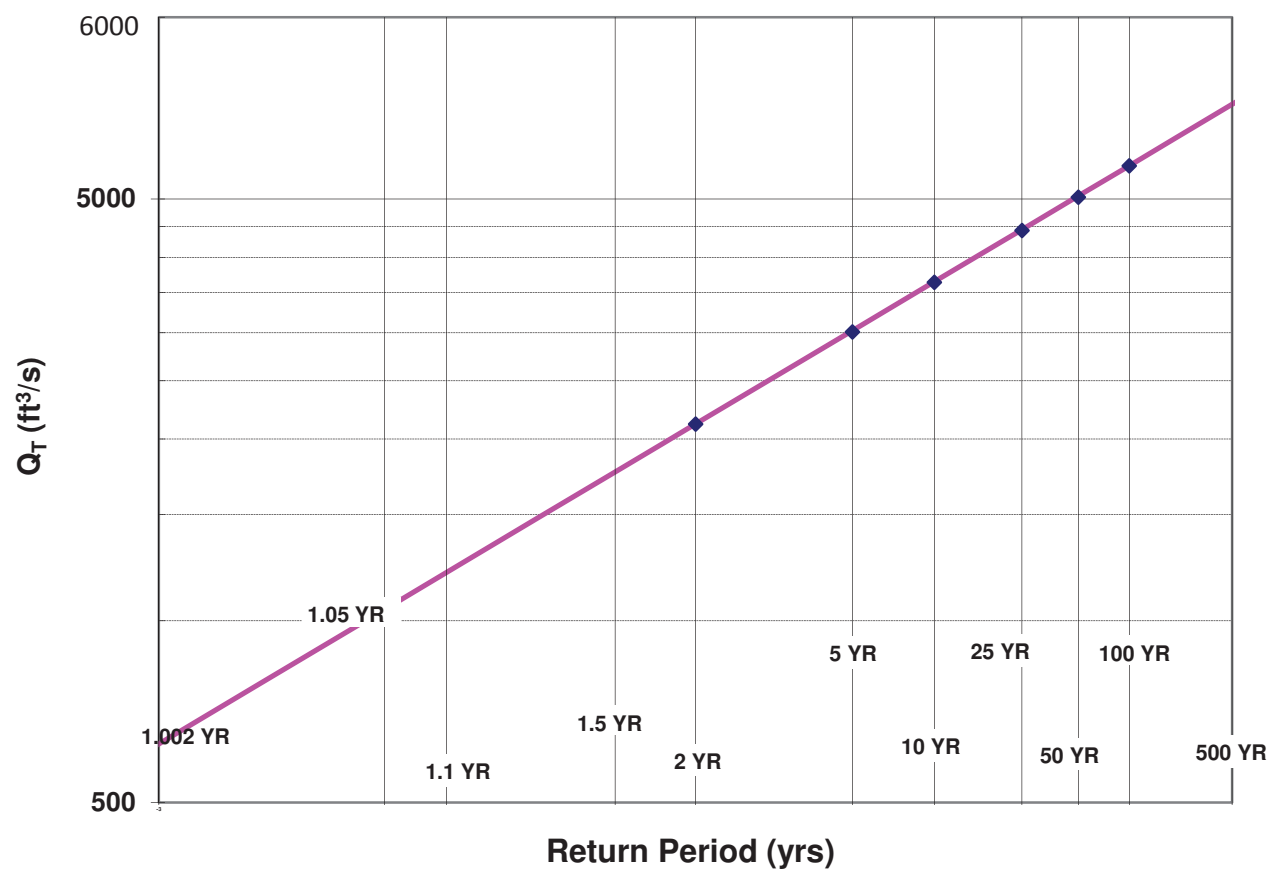
Lombard, P.J. & G.A. Hodgkins, 2015.
 Peak flow regression equations for small, ungaged streams in
 Maine - Comparing map-based to field-based variables
SIR 2015-4059, USGS, Augusta, ME

$$Q_T = b \times A^a \times 10^{-ww}$$

Ret Pd	Peak Flow Estimate		
T (yr)	Lower	Q _T (m ³ /s)	Upper
1.1		34.09	
2		60.03	
5		85.34	
10		103.06	
25		125.59	
50		142.61	
100		160.65	
500		203.27	

Q _T (ft ³ /s)
1203.6
2119.6
3013.2
3639.1
4434.7
5035.6
5672.4
7177.6

Log-Normal Probability Plot



WIN: 21729.10
 Town: Hamden
 Route No. US 95
 Asset ID: 1431
 Lat: 44.76552 Long: -68.89451

Project Name: Hamden B#1431
 Stream Name: Souadabscook Stream
 Bridge Name: Souadabscook East SB Bridge
 Analysis by: DFB
 Date: 7/6/2017

DO NOT ENTER ANY DATA ON THIS PAGE; EVERYTHING IS CALCULATED

MAINE MONTHLY MEDIAN FLOWS and HYDRAULIC GEOMETRY BY USGS REGRESSION EQUATIONS (2004)

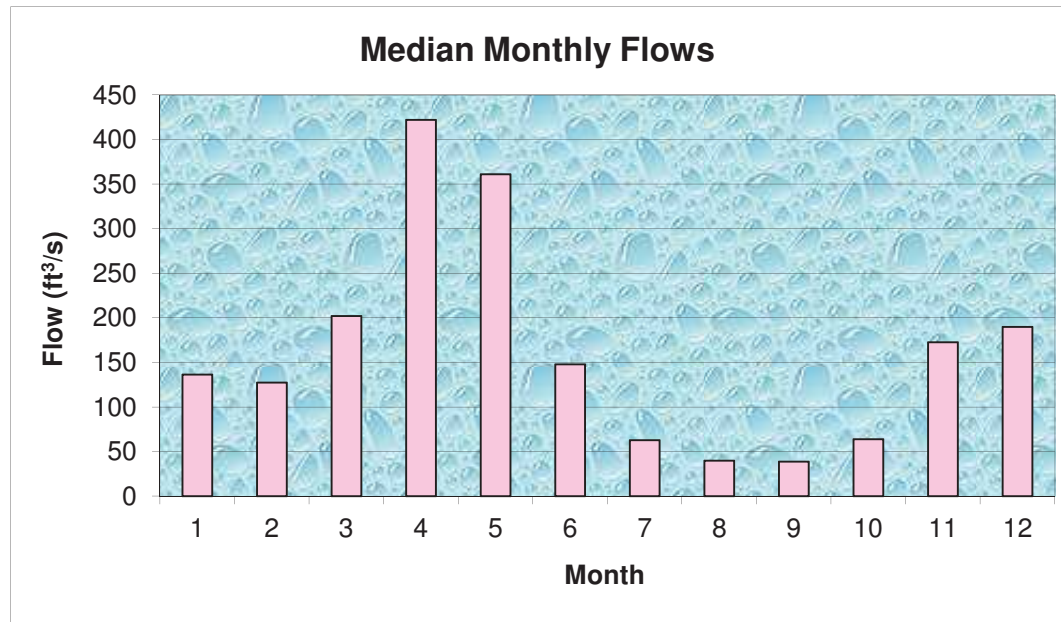
Value	Variable	Explanation
138.70	A	Area (mi ²)
498806.4	P_c	Watershed centroid (E,N; UTM; Zone 19; meters)
68.80	$DIST$	Distance from Coastal reference line (mi)
39.5	$pptA$	Mean Annual Precipitation (inches)
0.02	SG	Sand & Gravel Aquifer (decimal fraction of watershed area)

Month	Q_{median} (ft ³ /s)	(m ³ /s)
Jan	136.50	3.8682
Feb	127.59	3.6157
Mar	202.08	5.7267
Apr	422.20	11.9647
May	360.95	10.2288
Jun	148.11	4.1971
Jul	63.06	1.7872
Aug	39.99	1.1332
Sep	38.83	1.1004
Oct	63.90	1.8108
Nov	172.87	4.8989
Dec	189.92	5.3822

Q_{bf}	921.2
ann avg	257.6
ann med	124.8
$Q_{1.002}$	625.3
$Q_{1.01}$	789.0
$Q_{1.05}$	1044.5
Q_{bf}	1121.3

assume $v = 4\text{ft/s}$

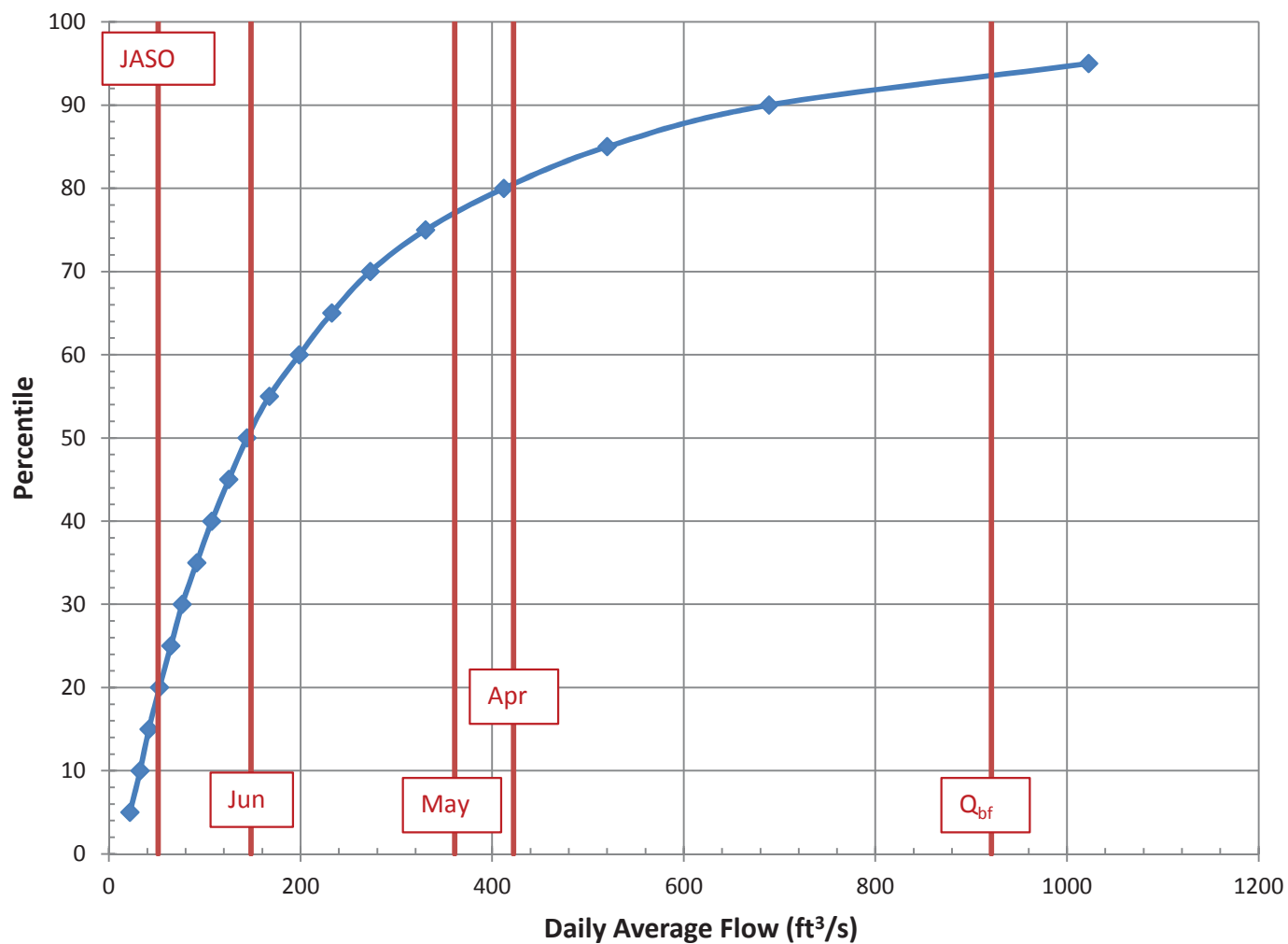
W_{bf}	88.2	estimated bankfull width (ft)
d_{bf}	3.2	estimated bankfull depth (ft)
A_{bf}	316.4	estimated bankfull flow area (ft ²)



References

Dudley, R.W., 2013. FY2013 Progress Report - Phase 1 ..., USFWS QRP Project
 Dudley, R.W., 2004. Estimating Monthly Streamflows ..., SIR 2004-5026

Daily Average Flow Distribution



Daily Avg Flow Dist

$A_{ws} = (mi^2)$ 138.7

$Q (ft^3/s)$

Pctl	Median	84 th pctl
5	21.83	35.14
10	32.43	48.76
15	41.68	60.88
20	52.79	73.84
25	64.58	86.55
30	76.42	98.58
35	91.55	112.66
40	107.36	129.56
45	125.14	146.49
50	144.08	172.95
55	167.31	201.29
60	198.71	236.29
65	232.47	275.29
70	272.68	321.17
75	330.56	386.23
80	412.24	461.13
85	520.16	590.94
90	689.04	793.50
95	1022.60	1233.96

Q_{bf} 921.2

$Q_{1.002}$ 625.3

$Q_{1.1}$ 1203.6

Q_2 2119.6

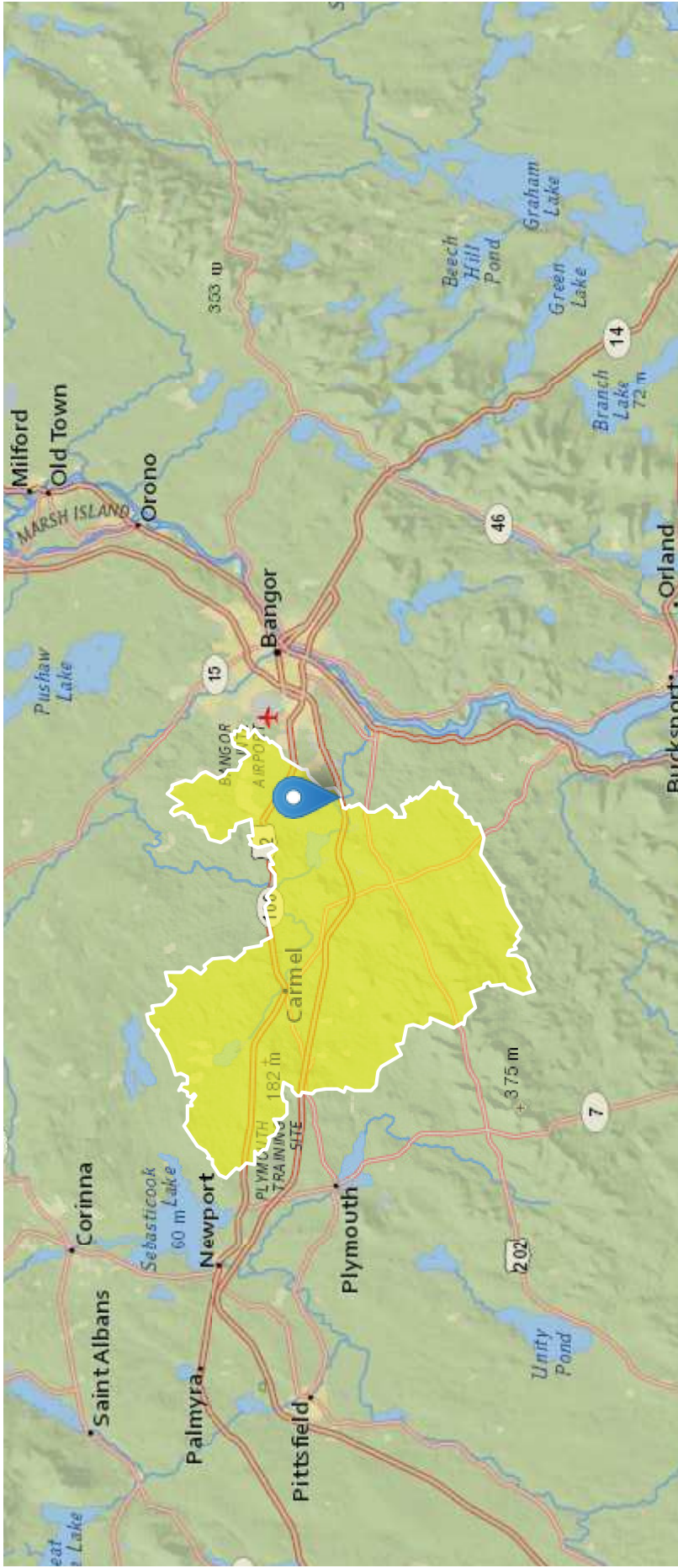
Hampden 21729 B# 1431 on Souadabscook Stream

Region ID:
ME

Workspace ID:
ME20170706093553398000

Clicked Point (Latitude, Longitude):
44.76552, -68.89451

Time:
2017-07-06 09:36:39 -0400



Parameter Code	Parameter Description	Value	Unit
DRNAREA	Area that drains to a point on a stream	138.7	square miles
STORNWI	Percentage of storage (combined water bodies and wetlands) from the National Wetlands Inventory	15.79	percent
SANDGRAVAF	Fraction of land surface underlain by sand and gravel aquifers	0.016	dimensionless
ELEV	Mean Basin Elevation	271.2	feet
BSLDEM10M	Mean basin slope computed from 10 m DEM	5.95	percent
CENTROIDX	Basin centroid horizontal (x) location in state plane coordinates	498806.39	
CENTROIDY	Basin centroid vertical (y) location in state plane units	4957576.38	
COASTDIST	Shortest distance from the coastline to the basin centroid	69.9	miles
ELEVMAX	Maximum basin elevation	1197.2	feet
LC06WATER	Percent of open water, class 11, from NLCD 2006	1.45	percent
LC11DEV	Percentage of developed (urban) land from NLCD 2011 classes 21-24	6.86	percent
LC11IMP	Average percentage of impervious area determined from NLCD 2011 impervious dataset	1.35	percent
PRECIP	Mean Annual Precipitation	42.2	inches
SANDGRAVAP	Percentage of land surface underlain by sand and gravel aquifers	1.65	percent
STATSGOA	Percentage of area of Hydrologic Soil Type A from STATSGO	0.57	percent

Bankfull Statistics Parameters [100 Percent (139 square miles) Central and Coastal Bankfull 2004 5042]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	138.7	square miles	2.92	298

Bankfull Statistics Flow Report [100 Percent (139 square miles) Central and Coastal Bankfull 2004 5042]

Statistic

Value

Unit

Bankfull Streamflow

921

ft^3/s

Bankfull Width

99.7

ft

Bankfull Depth

3.18

ft

Bankfull Area

316

ft^2

Bankfull Statistics Citations

Dudley, R.W.,2004, Hydraulic-Geometry Relations for Rivers in Coastal and Central Maine: U.S. Geological Survey Scientific Investigations Report 2004-5042, 30 p (<http://pubs.usgs.gov/sir/2004/5042/pdf/sir2004-5042.pdf>)

Peak-Flow Statistics Parameters [100 Percent (139 square miles) Statewide Peak Flow Full GT 12sqmi WRI 99 4008]

Parameter Code Parameter Name Value Units Min Limit Max Limit

DRNAREA Drainage Area 138.7 square miles 0.93 1653

STORNWI Percentage of Storage from NWI 15.79 percent 0.7 26.7

Peak-Flow Statistics Flow Report [100 Percent (139 square miles) Statewide Peak Flow Full GT 12sqmi WRI 99 4008]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other --- see report)

Statistic Value Unit PII Plu SE SEp Equiv. Yrs.

2 Year Peak Flood 2120 ft^3/s 1190 3790 35.1 35.1 1.8

5 Year Peak Flood 3010 ft^3/s 1670 5430 36.1 36.1 2.5

10 Year Peak Flood 3640 ft^3/s 1990 6660 36.8 36.8 3.2

25 Year Peak Flood 4430 ft^3/s 2370 8310 38.6 38.6 4.1

50 Year Peak Flood 5040 ft^3/s 2630 9630 39.9 39.9 4.8

100 Year Peak Flood 5670 ft^3/s 2910 11100 41.2 41.2 5.4

500 Year Peak Flood 7180 ft^3/s 3480 14800 44.9 44.9 6.4

Peak-Flow Statistics Citations

Hodgkins, G. A., 1999, Estimating the Magnitude of Peak Flows for Streams in Maine for Selected Recurrence Intervals: U.S. Geological Survey Water-Resources Investigations Report 99-4008, 45 p. (<http://me.water.usgs.gov/99-4008.pdf>)

Flow-Duration Statistics Parameters [100 Percent (139 square miles) Statewide Annual SIR 2015 5151]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	138.7	square miles	14.9	1419
SANDGRAVAF	Fraction of Sand and Gravel Aquifers	0.016	dimensionless	0	0.212
ELEV	Mean Basin Elevation	271.2	feet	239	2120

Flow-Duration Statistics Flow Report [100 Percent (139 square miles) Statewide Annual SIR 2015 5151]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

Statistic	Value	Unit	SEp
1 Percent Duration	2.88	ft^3/s	144
5 Percent Duration	8.91	ft^3/s	62
10 Percent Duration	16.7	ft^3/s	41
25 Percent Duration	46.8	ft^3/s	22
50 Percent Duration	124	ft^3/s	20
75 Percent Duration	310	ft^3/s	17
90 Percent Duration	661	ft^3/s	17
95 Percent Duration	994	ft^3/s	18
99 Percent Duration	1910	ft^3/s	29

Flow-Duration Statistics Citations

Dudley, R.W.,2015, Regression equations for monthly and annual mean and selected percentile streamflows for ungaged rivers in Maine: U.S. Geological Survey Scientific Investigations Report 2015–5151, 35 p. (<http://dx.doi.org/10.3133/sir20155151>)

Annual Flow Statistics Parameters [100 Percent (139 square miles) Statewide Annual SIR 2015 5151]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	138.7	square miles	14.9	1419
SANDGRAVAF	Fraction of Sand and Gravel Aquifers	0.016	dimensionless	0	0.212
ELEV	Mean Basin Elevation	271.2	feet	239	2120

Annual Flow Statistics Flow Report [100 Percent (139 square miles) Statewide Annual SIR 2015 5151]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

Statistic	Value	Unit	SEp
Mean Annual Flow	264	ft^3/s	16

Annual Flow Statistics Citations

Dudley, R.W.,2015, Regression equations for monthly and annual mean and selected percentile streamflows for ungaged rivers in Maine: U.S. Geological Survey Scientific Investigations Report 2015–5151, 35 p. (<http://dx.doi.org/10.3133/sir20155151>)

WIN:	21728.10
Town:	Hamden
Route No.	US 95
Asset ID:	1432
Lat:	44.7627
Long:	-68.90932

Project Name:	Hamden B#1432
Stream Name:	Souadabscook
Bridge Name:	Souadabscook Center SB Bridge
Analysis by:	DFB
Date:	7/6/2017

Peak Flow Calculations by USGS Regression Equations (Hodgkins, 1999 & Lombard/Hodgkins, 2015)

Enter data in blue cells only!

	km ²	mi ²	ac
A	321.94	124.30	79552.0
W	47.36	18.3	11702.1

P _c	497638	4957010
County	Penobscot S	
pptA	39.5	
SG	0.02	

A (km ²)	321.94
W (%)	14.71

Conf Lvl 0.67

Enter data in [mi²]

Watershed Area *DRNAREA*

Wetlands area (by NWI)

watershed centroid (E, N; UTM 19N; meters)

choose county from drop-down menu

mean annual precipitation (inches; by look-up)

sand & gravel aquifer as decimal fraction of watershed A

NWI Wetlands % *STORNWI*

Worksheet prepared by:

Charles S. Hebson, PE

Environmental Office

Maine Dept. Transportation

Augusta, ME 04333-0016

207-557-1052

Charles.Hebson@maine.gov

ver. 2016 Feb 05

References:

Hodgkins, G.A., 1999.

Estimating the magnitude of peak flows for streams

in Maine for selected recurrence intervals

WRIR 99-4008, USGS Augusta, ME

Lombard, P.J. & G.A. Hodgkins, 2015.

Peak flow regression equations for small, ungaged streams in

Maine - Comparing map-based to field-based variables

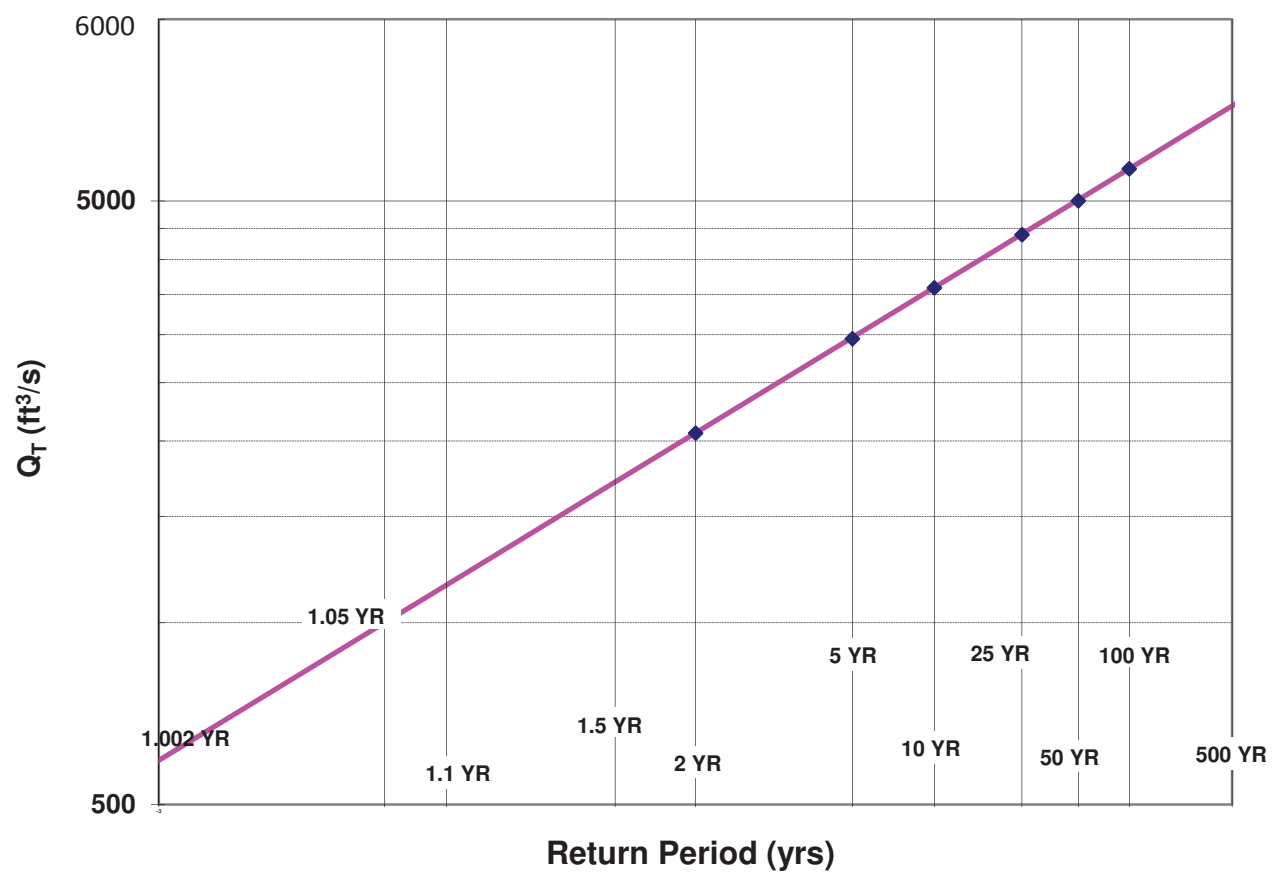
SIR 2015-4059, USGS, Augusta, ME

$$Q_T = b \times A^a \times 10^{-wW}$$

Ret Pd	Peak Flow Estimate		
T (yr)	Lower	Q _T (m ³ /s)	Upper
1.1		32.75	
2		58.44	
5		83.79	
10		101.65	
25		124.47	
50		141.77	
100		160.09	
500		203.66	

Q _T (ft ³ /s)
1156.3
2063.5
2958.7
3589.4
4395.0
5005.8
5652.9
7191.3

Log-Normal Probability Plot



WIN: 21728.10
 Town: Hamden
 Route No. US 95
 Asset ID: 1432
 Lat: 44.76267 Long: -68.90932

Project Name: Hamden B#1432
 Stream Name: Souadabscook
 Bridge Name: Souadabscook Center SB Bridge
 Analysis by: DFB
 Date: 7/6/2017

DO NOT ENTER ANY DATA ON THIS PAGE; EVERYTHING IS CALCULATED

MAINE MONTHLY MEDIAN FLOWS and HYDRAULIC GEOMETRY BY USGS REGRESSION EQUATIONS (2004)

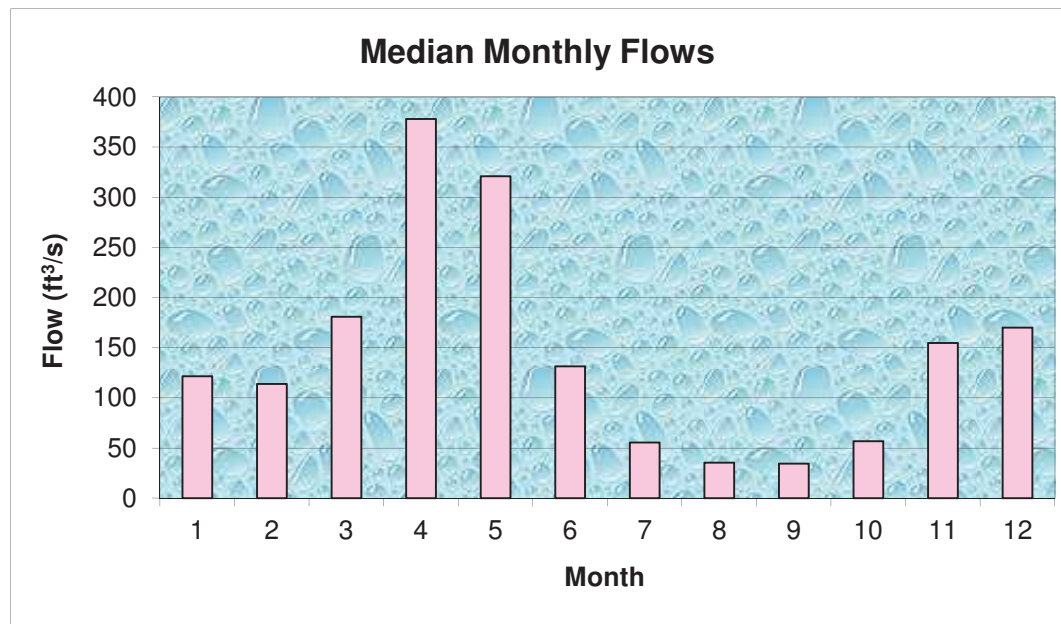
Value	Variable	Explanation
124.30	A	Area (mi ²)
497637.9	P_c	Watershed centroid (E,N; UTM; Zone 19; meters)
68.86	$DIST$	Distance from Coastal reference line (mi)
39.5	$pptA$	Mean Annual Precipitation (inches)
0.02	SG	Sand & Gravel Aquifer (decimal fraction of watershed area)

Month	Q_{median} (ft ³ /s)	(m ³ /s)
Jan	121.77	3.4508
Feb	114.04	3.2318
Mar	180.95	5.1278
Apr	377.96	10.7108
May	321.13	9.1003
Jun	131.63	3.7301
Jul	55.73	1.5794
Aug	35.47	1.0053
Sep	34.55	0.9790
Oct	56.95	1.6138
Nov	154.85	4.3883
Dec	170.13	4.8213

Q_{bf}	821.0
ann avg	231.1
ann med	111.8
$Q_{1.002}$	591.5
$Q_{1.01}$	750.5
$Q_{1.05}$	1000.0
Q_{bf}	1030.6

assume $v = 4\text{ft/s}$

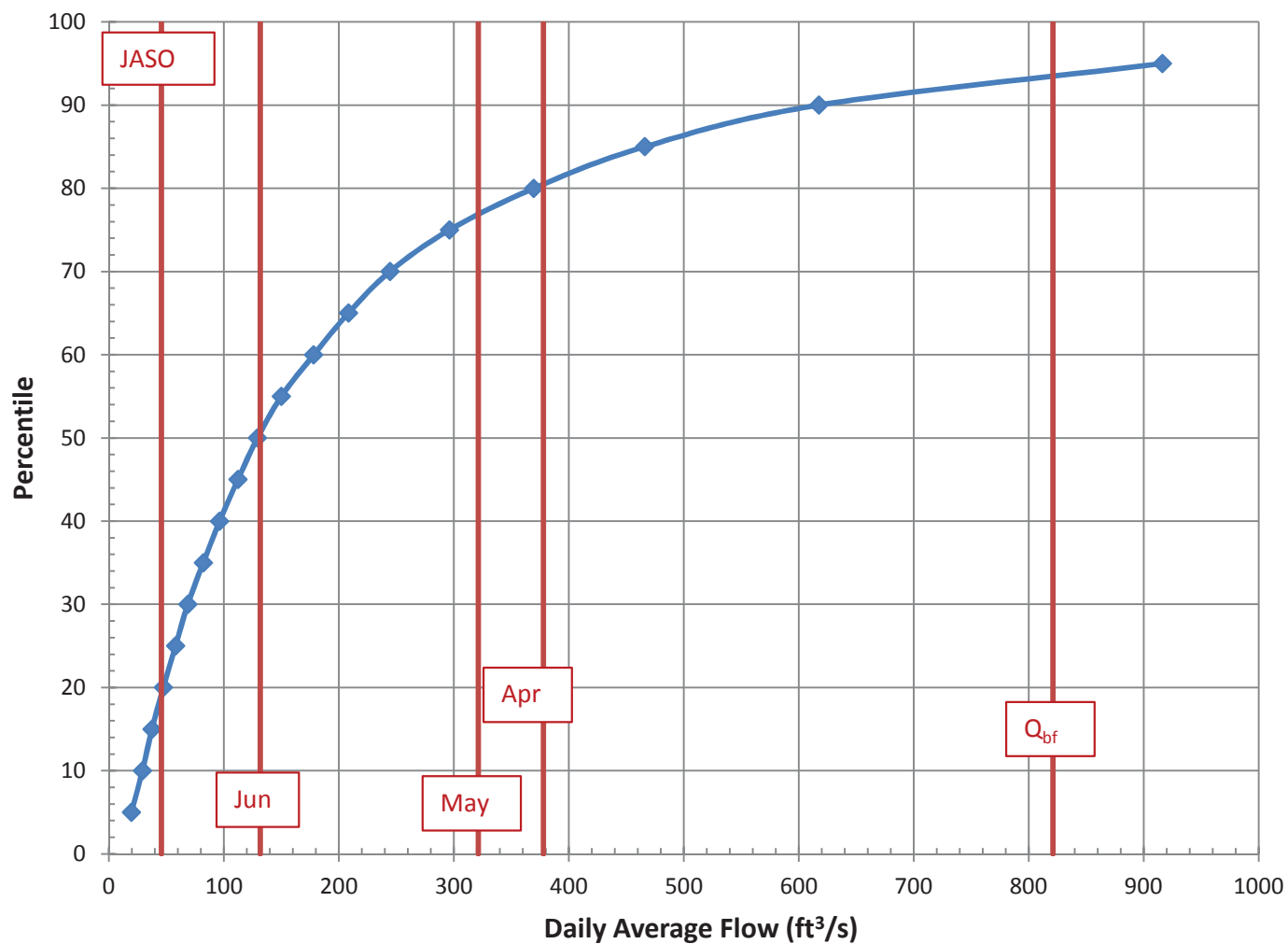
W_{bf}	84.2	estimated bankfull width (ft)
d_{bf}	3.1	estimated bankfull depth (ft)
A_{bf}	287.9	estimated bankfull flow area (ft ²)



References

Dudley, R.W., 2013. FY2013 Progress Report - Phase 1 ..., USFWS QRP Project
 Dudley, R.W., 2004. Estimating Monthly Streamflows ..., SIR 2004-5026

Daily Average Flow Distribution



Daily Avg Flow Dist

$A_{ws} = (mi^2)$ 124.3

Q (ft³/s)

Pctl	Median	84 th pctl
5	19.57	31.49
10	29.06	43.70
15	37.36	54.56
20	47.31	66.17
25	57.87	77.57
30	68.48	88.34
35	82.05	100.97
40	96.22	116.11
45	112.15	131.28
50	129.12	154.99
55	149.94	180.40
60	178.08	211.76
65	208.33	246.71
70	244.37	287.83
75	296.24	346.13
80	369.44	413.26
85	466.16	529.59
90	617.50	711.12
95	916.43	1105.85

Q_{bf} 821.0

Q_{1.002} 591.5

Q_{1.1} 1156.3

Q₂ 2063.5

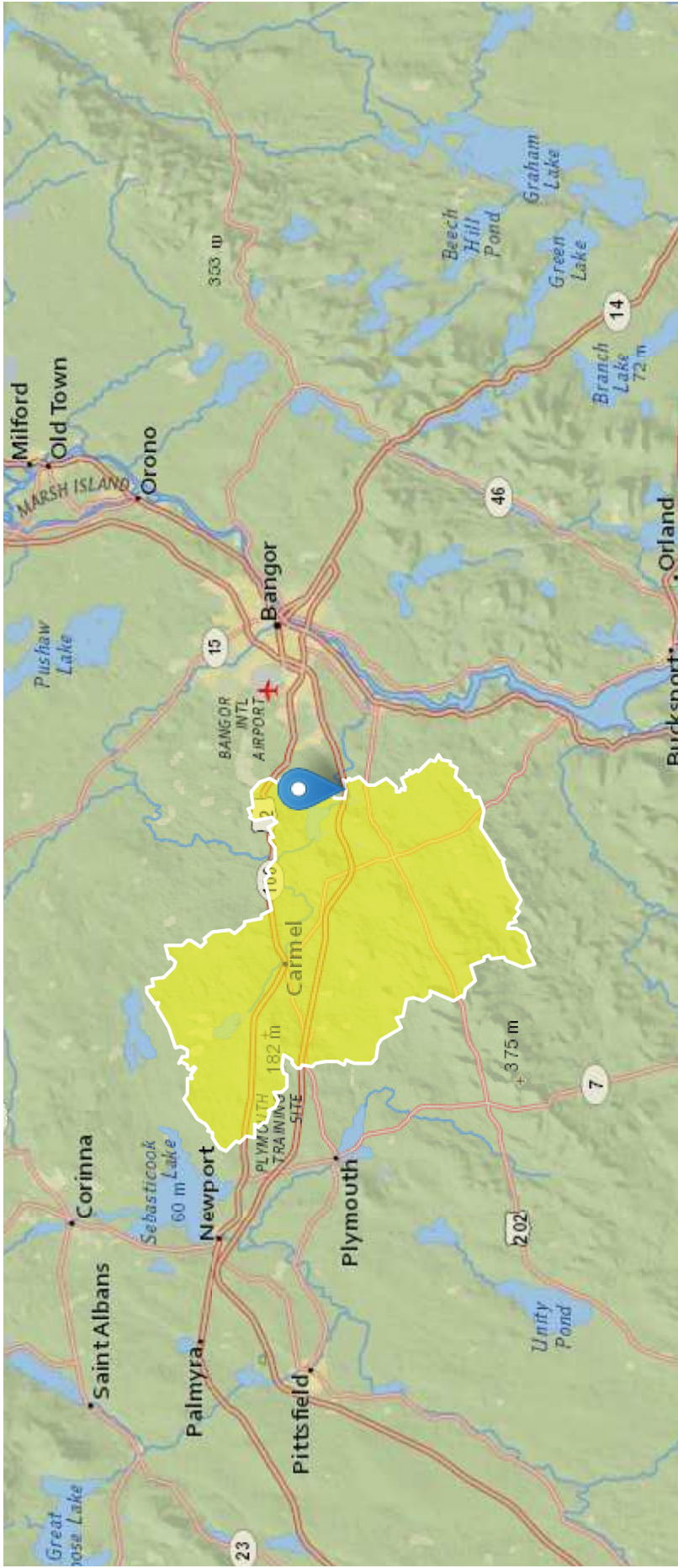
Hampden 21278 B#1432 on Souadabscook Stream

Region ID:
ME

Workspace ID:
ME20170706092250781000

Clicked Point (Latitude, Longitude):
44.76266, -68.90934

Time:
2017-07-06 09:23:35 -0400



Parameter Code	Parameter Description	Value	Unit
DRNAREA	Area that drains to a point on a stream	124.3	square miles
STORNWI	Percentage of storage (combined water bodies and wetlands) from the National Wetlands Inventory	14.71	percent
SANDGRAVAF	Fraction of land surface underlain by sand and gravel aquifers	0.017	dimensionless
ELEV	Mean Basin Elevation	281.8	feet
BSLDEM10M	Mean basin slope computed from 10 m DEM	6.22	percent
CENTROIDX	Basin centroid horizontal (x) location in state plane coordinates	497637.9	
CENTROIDY	Basin centroid vertical (y) location in state plane units	4957010.36	
COASTDIST	Shortest distance from the coastline to the basin centroid	69.9	miles
ELEVMAX	Maximum basin elevation	1197.2	feet
LC06WATER	Percent of open water, class 11, from NLCD 2006	1.54	percent
LC11DEV	Percentage of developed (urban) land from NLCD 2011 classes 21-24	6.31	percent
LC11IMP	Average percentage of impervious area determined from NLCD 2011 impervious dataset	1.17	percent
PRECIP	Mean Annual Precipitation	42.3	inches
SANDGRAVAP	Percentage of land surface underlain by sand and gravel aquifers	1.69	percent
STATSGOA	Percentage of area of Hydrologic Soil Type A from STATSGO	0.38	percent

Bankfull Statistics Parameters [100 Percent (124 square miles) Central and Coastal Bankfull 2004 5042]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	124.3	square miles	2.92	298

Bankfull Statistics Flow Report [100 Percent (124 square miles) Central and Coastal Bankfull 2004 5042]

Statistic

Value

Unit

Bankfull Streamflow

821

ft^3/s

Bankfull Width

94.2

ft

Bankfull Depth

3.06

ft

Bankfull Area

288

ft^2

Bankfull Statistics Citations

Dudley, R.W.,2004, Hydraulic-Geometry Relations for Rivers in Coastal and Central Maine: U.S. Geological Survey Scientific Investigations Report 2004-5042, 30 p (<http://pubs.usgs.gov/sir/2004/5042/pdf/sir2004-5042.pdf>)

Peak-Flow Statistics Parameters [100 Percent (124 square miles) Statewide Peak Flow Full GT 12sqmi WRI 99 4008]

Parameter Code Parameter Name Value Units Min Limit Max Limit

DRNAREA Drainage Area 124.3 square miles 0.93 1653

STORNWI Percentage of Storage from NWI 14.71 percent 0.7 26.7

Peak-Flow Statistics Flow Report [100 Percent (124 square miles) Statewide Peak Flow Full GT 12sqmi WRI 99 4008]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other --- see report)

Statistic Value Unit PII Plu SE SEp Equiv. Yrs.

2 Year Peak Flood 2060 ft^3/s 1150 3690 35.1 35.1 1.8

5 Year Peak Flood 2960 ft^3/s 1640 5330 36.1 36.1 2.5

10 Year Peak Flood 3590 ft^3/s 1960 6560 36.8 36.8 3.2

25 Year Peak Flood 4390 ft^3/s 2350 8230 38.6 38.6 4.1

50 Year Peak Flood 5010 ft^3/s 2620 9570 39.9 39.9 4.8

100 Year Peak Flood 5650 ft^3/s 2900 11000 41.2 41.2 5.4

500 Year Peak Flood 7190 ft^3/s 3490 14800 44.9 44.9 6.4

Peak-Flow Statistics Citations

Hodgkins, G. A., 1999, Estimating the Magnitude of Peak Flows for Streams in Maine for Selected Recurrence Intervals: U.S. Geological Survey Water-Resources Investigations Report 99-4008, 45 p. (<http://me.water.usgs.gov/99-4008.pdf>)

Flow-Duration Statistics Parameters [100 Percent (124 square miles) Statewide Annual SIR 2015 5151]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	124.3	square miles	14.9	1419
SANDGRAVAF	Fraction of Sand and Gravel Aquifers	0.017	dimensionless	0	0.212
ELEV	Mean Basin Elevation	281.8	feet	239	2120

Flow-Duration Statistics Flow Report [100 Percent (124 square miles) Statewide Annual SIR 2015 5151]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

Statistic	Value	Unit	SEp
1 Percent Duration	2.49	ft^3/s	144
5 Percent Duration	7.8	ft^3/s	62
10 Percent Duration	14.7	ft^3/s	41
25 Percent Duration	41.9	ft^3/s	22
50 Percent Duration	111	ft^3/s	20
75 Percent Duration	279	ft^3/s	17
90 Percent Duration	595	ft^3/s	17
95 Percent Duration	896	ft^3/s	18
99 Percent Duration	1740	ft^3/s	29

Flow-Duration Statistics Citations

Dudley, R.W.,2015, Regression equations for monthly and annual mean and selected percentile streamflows for ungaged rivers in Maine: U.S. Geological Survey Scientific Investigations Report 2015–5151, 35 p. (<http://dx.doi.org/10.3133/sir20155151>)

Annual Flow Statistics Parameters [100 Percent (124 square miles) Statewide Annual SIR 2015 5151]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	124.3	square miles	14.9	1419
SANDGRAVAF	Fraction of Sand and Gravel Aquifers	0.017	dimensionless	0	0.212
ELEV	Mean Basin Elevation	281.8	feet	239	2120

Annual Flow Statistics Flow Report [100 Percent (124 square miles) Statewide Annual SIR 2015 5151]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

Statistic	Value	Unit	SEp
Mean Annual Flow	238	ft^3/s	16

Annual Flow Statistics Citations

Dudley, R.W.,2015, Regression equations for monthly and annual mean and selected percentile streamflows for ungaged rivers in Maine: U.S. Geological Survey Scientific Investigations Report 2015–5151, 35 p. (<http://dx.doi.org/10.3133/sir20155151>)

WIN:	21730.10
Town:	Hamden
Route No.	US 95
Asset ID:	1433
Lat:	44.7634
Long:	-68.91945

Project Name:	Hamden B#1433
Stream Name:	Souadabscook Stream
Bridge Name:	Souadabscook West SB Bridge
Analysis by:	DFB
Date:	7/6/2017

Peak Flow Calculations by USGS Regression Equations (Hodgkins, 1999 & Lombard/Hodgkins, 2015)

Enter data in blue cells only!

	km ²	mi ²	ac
A	244.76	94.50	60480.0
W	39.82	15.4	9840.1

P _c	495972	4959200
County	Penobscot S	
pptA	39.5	
SG	0.01	

A (km ²)	244.76
W (%)	16.27

Conf Lvl 0.67

Enter data in [mi²]

Watershed Area *DRNAREA*

Wetlands area (by NWI)

watershed centroid (E, N; UTM 19N; meters)

choose county from drop-down menu

mean annual precipitation (inches; by look-up)

sand & gravel aquifer as decimal fraction of watershed A

NWI Wetlands % *STORNWI*

Worksheet prepared by:

Charles S. Hebson, PE

Environmental Office

Maine Dept. Transportation

Augusta, ME 04333-0016

207-557-1052

Charles.Hebson@maine.gov

ver. 2016 Feb 05

References:

Hodgkins, G.A., 1999.

Estimating the magnitude of peak flows for streams

in Maine for selected recurrence intervals

WRIR 99-4008, USGS Augusta, ME

Lombard, P.J. & G.A. Hodgkins, 2015.

Peak flow regression equations for small, ungaged streams in

Maine - Comparing map-based to field-based variables

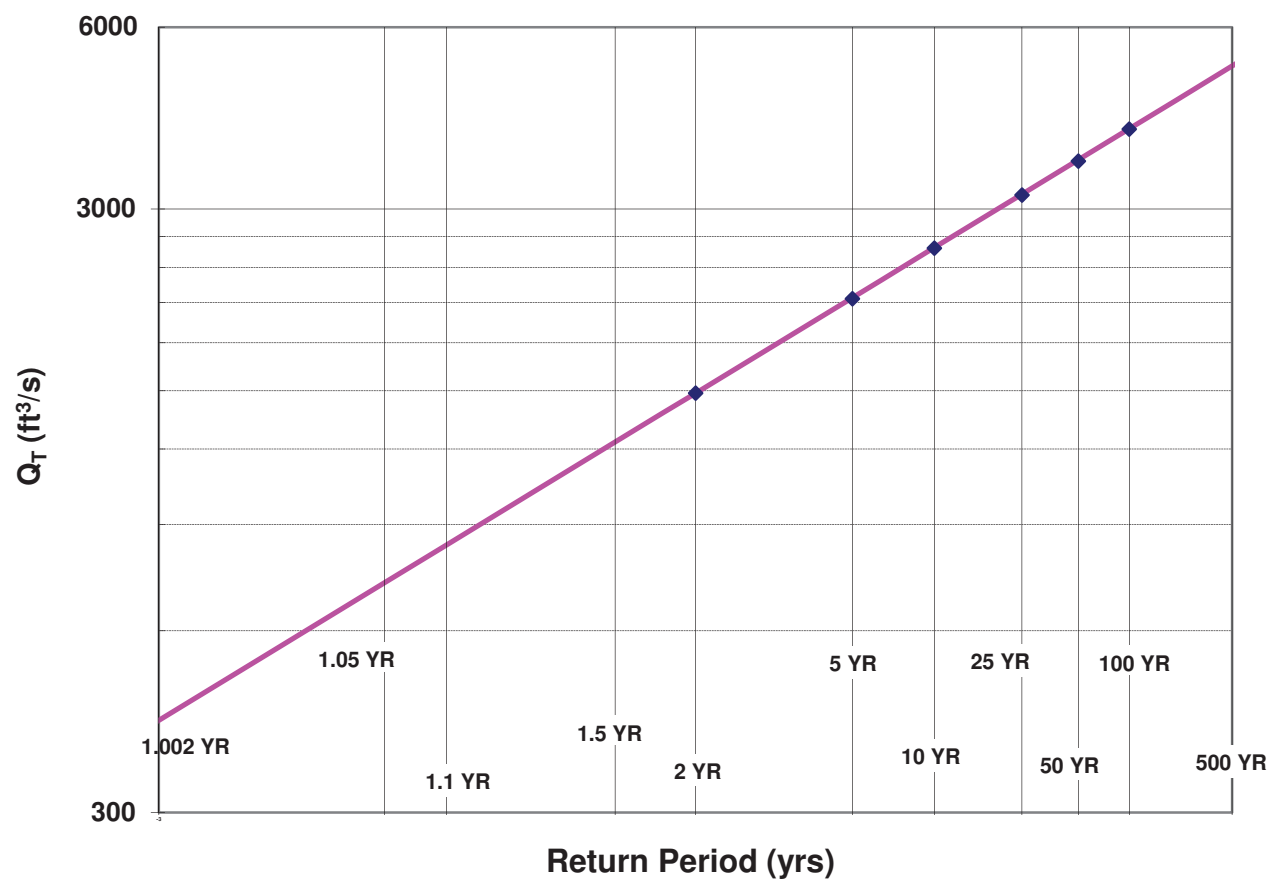
SIR 2015-4059, USGS, Augusta, ME

$$Q_T = b \times A^a \times 10^{-wW}$$

Ret Pd	Peak Flow Estimate	
T (yr)	Lower	Upper
1.1	23.60	
2	42.10	
5	60.35	
10	73.18	
25	89.61	
50	102.05	
100	115.28	
500	146.59	

Q _T (ft ³ /s)
833.3
1486.5
2130.9
2583.9
3164.0
3603.3
4070.4
5176.2

Log-Normal Probability Plot



WIN: 21730.10
 Town: Hamden
 Route No. US 95
 Asset ID: 1433
 Lat: 44.76337 Long: -68.91945

Project Name: Hamden B#1433
 Stream Name: Souadabscook Stream
 Bridge Name: Souadabscook West SB Bridge
 Analysis by: DFB
 Date: 7/6/2017

DO NOT ENTER ANY DATA ON THIS PAGE; EVERYTHING IS CALCULATED

MAINE MONTHLY MEDIAN FLOWS and HYDRAULIC GEOMETRY BY USGS REGRESSION EQUATIONS (2004)

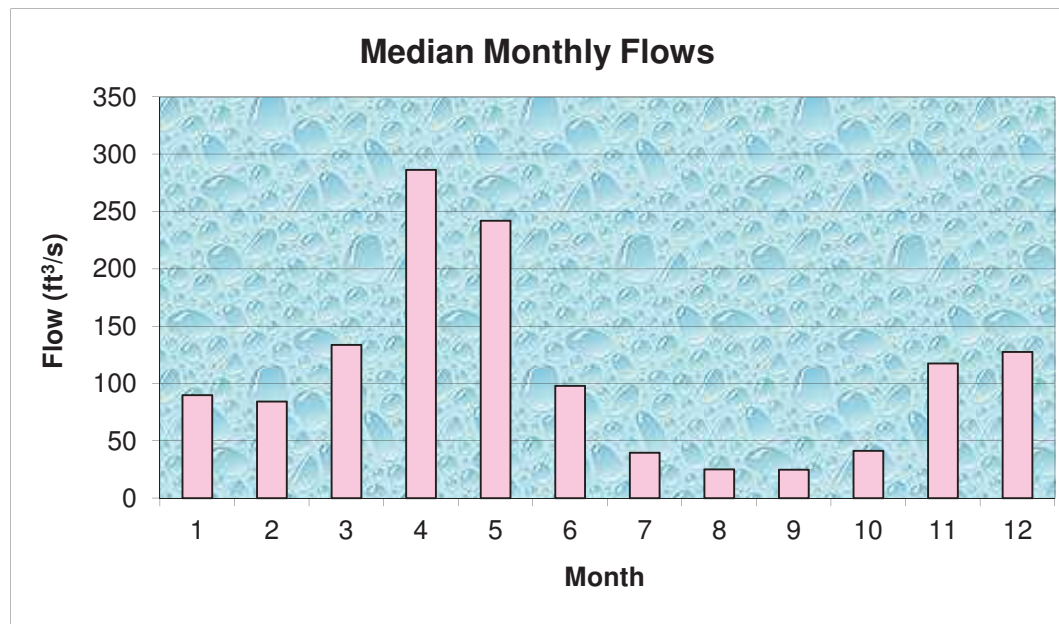
	Value	Variable	Explanation
	94.50	A	Area (mi ²)
495971.6	4959200	P_c	Watershed centroid (E,N; UTM; Zone 19; meters)
	70.54	$DIST$	Distance from Coastal reference line (mi)
	39.5	$pptA$	Mean Annual Precipitation (inches)
	0.01	SG	Sand & Gravel Aquifer (decimal fraction of watershed area)

Month	Q_{median} (ft ³ /s)	(m ³ /s)
Jan	89.99	2.5503
Feb	84.46	2.3936
Mar	133.86	3.7933
Apr	286.56	8.1206
May	242.18	6.8632
Jun	98.01	2.7774
Jul	39.73	1.1259
Aug	25.32	0.7176
Sep	24.88	0.7050
Oct	41.35	1.1719
Nov	117.60	3.3326
Dec	127.75	3.6202

Q_{bf}	615.7
ann avg	176.1
ann med	84.8
$Q_{1.002}$	426.5
$Q_{1.01}$	541.0
$Q_{1.05}$	720.8
Q_{bf}	834.5

assume $v = 4\text{ft/s}$

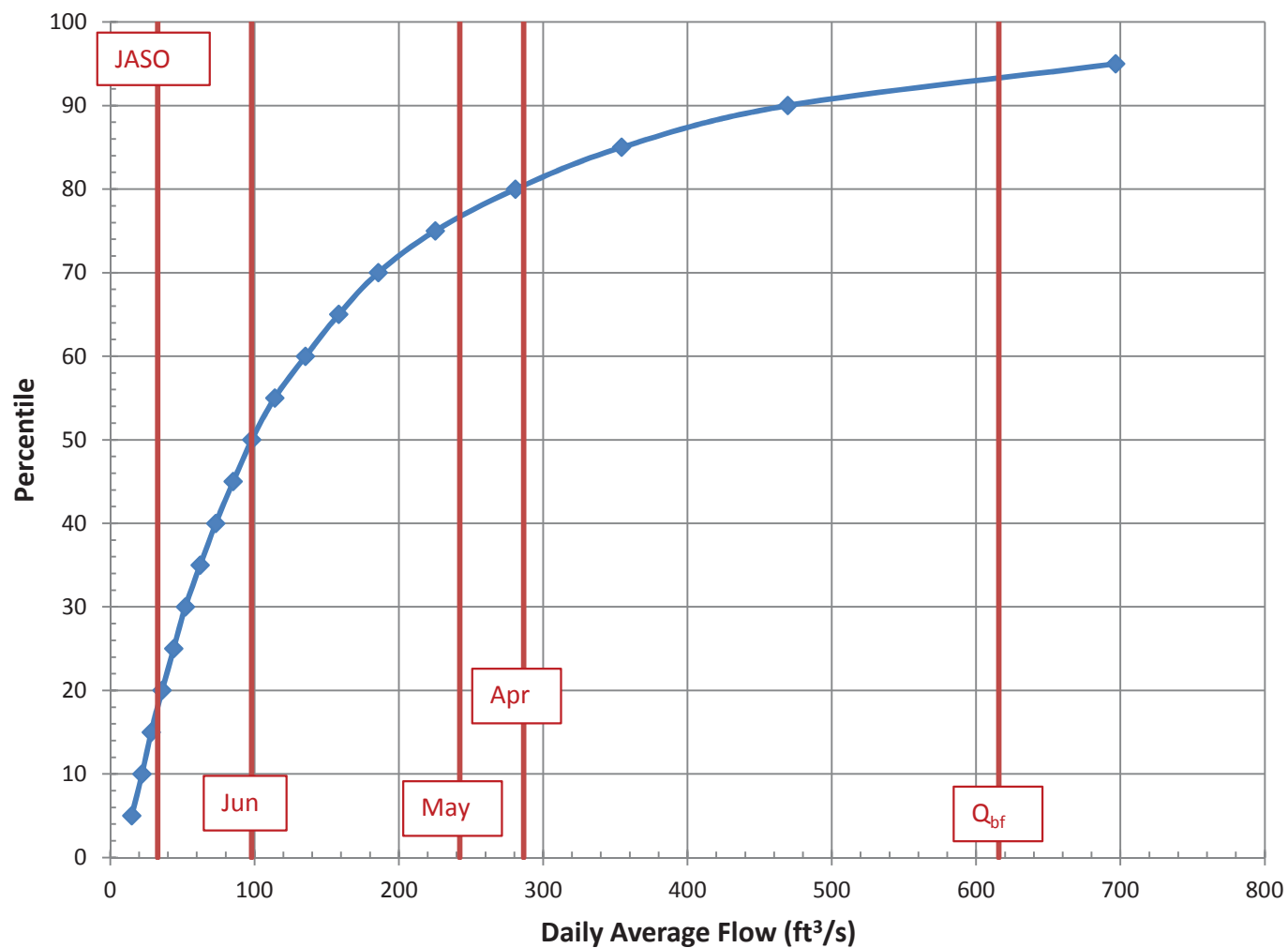
W_{bf}	74.8	estimated bankfull width (ft)
d_{bf}	2.8	estimated bankfull depth (ft)
A_{bf}	227.4	estimated bankfull flow area (ft ²)



References

Dudley, R.W., 2013. FY2013 Progress Report - Phase 1 ..., USFWS QRP Project
 Dudley, R.W., 2004. Estimating Monthly Streamflows ..., SIR 2004-5026

Daily Average Flow Distribution



Daily Avg Flow Dist

$A_{ws} = (mi^2)$

94.5

$Q (ft^3/s)$

Pctl	Median	84 th pctl
5	14.88	23.94
10	22.09	33.22
15	28.40	41.48
20	35.97	50.31
25	44.00	58.97
30	52.07	67.16
35	62.38	76.76
40	73.15	88.27
45	85.26	99.81
50	98.16	117.83
55	114.00	137.15
60	135.38	160.99
65	158.39	187.56
70	185.78	218.82
75	225.22	263.15
80	280.87	314.18
85	354.40	402.62
90	469.46	540.64
95	696.72	840.73

Q_{bf} 615.7

$Q_{1.002}$ 426.5

$Q_{1.1}$ 833.3

Q_2 1486.5

Hampden 21730.10 B#1433 on Souadabscook Stream

Region ID:

ME

Workspace ID:

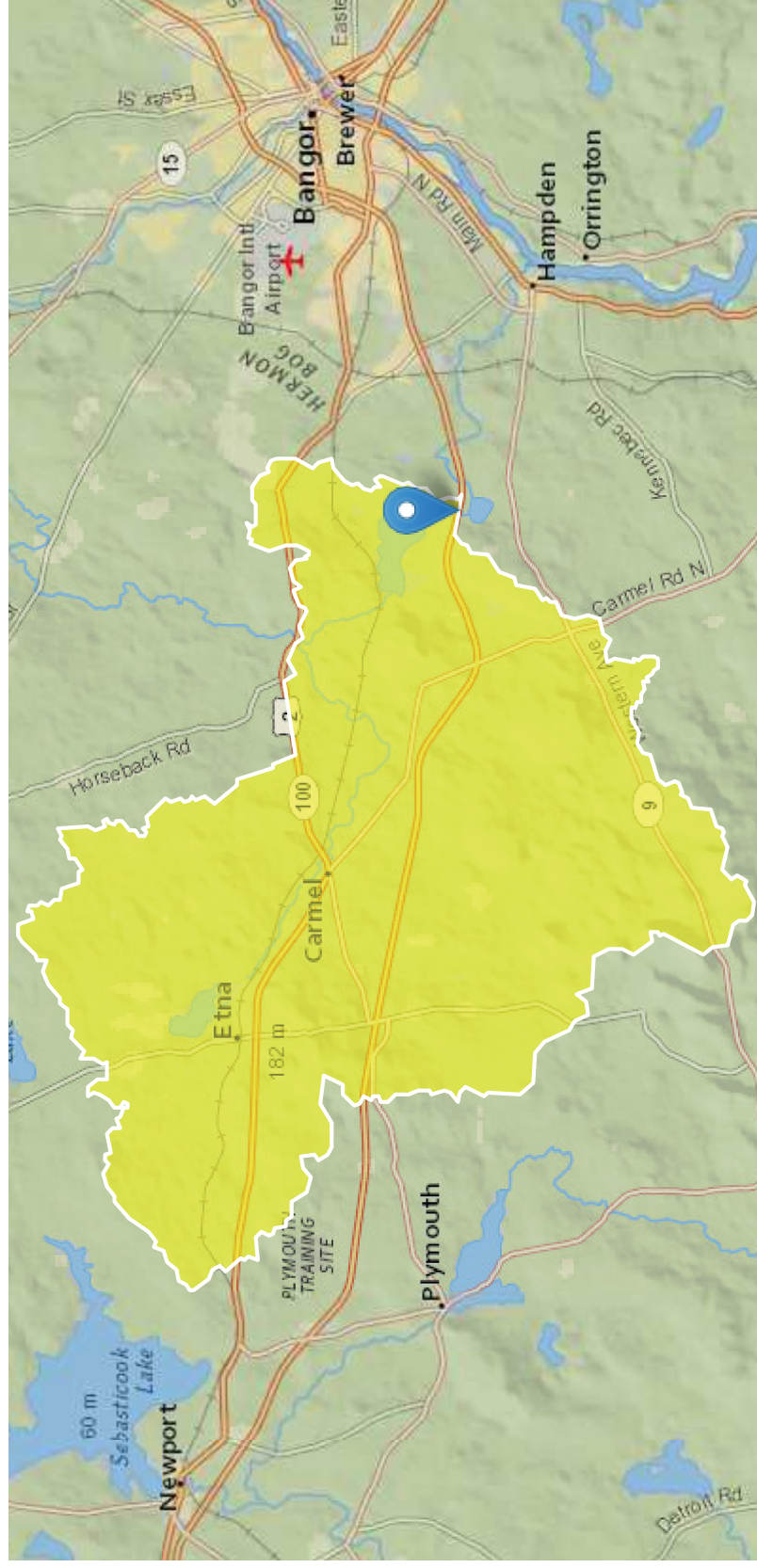
ME20170706085939593000

Clicked Point (Latitude, Longitude):

44.76337, -68.91945

Time:

2017-07-06 09:00:23 -0400



Parameter Code	Parameter Description	Value	Unit
DRNAREA	Area that drains to a point on a stream	94.5	square miles
STORNWI	Percentage of storage (combined water bodies and wetlands) from the National Wetlands Inventory	16.27	percent
SANDGRAVAF	Fraction of land surface underlain by sand and gravel aquifers	0.007	dimensionless
ELEV	Mean Basin Elevation	275	feet
BSLDEM10M	Mean basin slope computed from 10 m DEM	6	percent
CENTROIDX	Basin centroid horizontal (x) location in state plane coordinates	495971.64	
CENTROIDY	Basin centroid vertical (y) location in state plane units	4959199.98	
COASTDIST	Shortest distance from the coastline to the basin centroid	71.7	miles
ELEVMAX	Maximum basin elevation	1197.2	feet
LC06WATER	Percent of open water, class 11, from NLCD 2006	1.83	percent
LC11DEV	Percentage of developed (urban) land from NLCD 2011 classes 21-24	6.5	percent
LC11IMP	Average percentage of impervious area determined from NLCD 2011 impervious dataset	1.24	percent
PRECIP	Mean Annual Precipitation	42.2	inches
SANDGRAVAP	Percentage of land surface underlain by sand and gravel aquifers	0.69	percent
STATSGOA	Percentage of area of Hydrologic Soil Type A from STATSGO	0.16	percent

Bankfull Statistics Parameters [100 Percent (94.4 square miles) Central and Coastal Bankfull 2004 5042]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	94.5	square miles	2.92	298

Bankfull Statistics Flow Report [100 Percent (94.4 square miles) Central and Coastal Bankfull 2004 5042]

Statistic

Value

Unit

Bankfull Streamflow

616

ft^3/s

Bankfull Width

81.7

ft

Bankfull Depth

2.79

ft

Bankfull Area

227

ft^2

Bankfull Statistics Citations

Dudley, R.W.,2004, Hydraulic-Geometry Relations for Rivers in Coastal and Central Maine: U.S. Geological Survey Scientific Investigations Report 2004-5042, 30 p (<http://pubs.usgs.gov/sir/2004/5042/pdf/sir2004-5042.pdf>)

Peak-Flow Statistics Parameters [100 Percent (94.4 square miles) Statewide Peak Flow Full GT 12sqmi WRI 99 4008]

Parameter Code Parameter Name Value Units Min Limit Max Limit

DRNAREA Drainage Area 94.5 square miles 0.93 1653

STORNWI Percentage of Storage from NWI 16.27 percent 0.7 26.7

Peak-Flow Statistics Flow Report [100 Percent (94.4 square miles) Statewide Peak Flow Full GT 12sqmi WRI 99 4008]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other --- see report)

Statistic Value Unit PII Plu SE SEp Equiv. Yrs.

2 Year Peak Flood 1490 ft^3/s 832 2660 35.1 35.1 1.8

5 Year Peak Flood 2130 ft^3/s 1180 3840 36.1 36.1 2.5

10 Year Peak Flood 2580 ft^3/s 1410 4730 36.8 36.8 3.2

25 Year Peak Flood 3160 ft^3/s 1690 5930 38.6 38.6 4.1

50 Year Peak Flood 3600 ft^3/s 1880 6890 39.9 39.9 4.8

100 Year Peak Flood 4070 ft^3/s 2080 7950 41.2 41.2 5.4

500 Year Peak Flood 5180 ft^3/s 2510 10700 44.9 44.9 6.4

Peak-Flow Statistics Citations

Hodgkins, G. A., 1999, Estimating the Magnitude of Peak Flows for Streams in Maine for Selected Recurrence Intervals: U.S. Geological Survey Water-Resources Investigations Report 99-4008, 45 p. (<http://me.water.usgs.gov/99-4008.pdf>)

Flow-Duration Statistics Parameters [100 Percent (94.4 square miles) Statewide Annual SIR 2015 5151]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	94.5	square miles	14.9	1419
SANDGRAVAF	Fraction of Sand and Gravel Aquifers	0.007	dimensionless	0	0.212
ELEV	Mean Basin Elevation	275	feet	239	2120

Flow-Duration Statistics Flow Report [100 Percent (94.4 square miles) Statewide Annual SIR 2015 5151]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

Statistic	Value	Unit	SEp
1 Percent Duration	1.44	ft^3/s	144
5 Percent Duration	4.98	ft^3/s	62
10 Percent Duration	9.91	ft^3/s	41
25 Percent Duration	30.4	ft^3/s	22
50 Percent Duration	83.3	ft^3/s	20
75 Percent Duration	211	ft^3/s	17
90 Percent Duration	455	ft^3/s	17
95 Percent Duration	690	ft^3/s	18
99 Percent Duration	1360	ft^3/s	29

Flow-Duration Statistics Citations

Dudley, R.W.,2015, Regression equations for monthly and annual mean and selected percentile streamflows for ungaged rivers in Maine: U.S. Geological Survey Scientific Investigations Report 2015–5151, 35 p. (<http://dx.doi.org/10.3133/sir20155151>)

Annual Flow Statistics Parameters [100 Percent (94.4 square miles) Statewide Annual SIR 2015 5151]

Parameter Code	Parameter Name	Value	Units	Min Limit	Max Limit
DRNAREA	Drainage Area	94.5	square miles	14.9	1419
SANDGRAVAF	Fraction of Sand and Gravel Aquifers	0.007	dimensionless	0	0.212
ELEV	Mean Basin Elevation	275	feet	239	2120

Annual Flow Statistics Flow Report [100 Percent (94.4 square miles) Statewide Annual SIR 2015 5151]

PII: Prediction Interval-Lower, Plu: Prediction Interval-Upper, SEp: Standard Error of Prediction, SE: Standard Error (other -- see report)

Statistic	Value	Unit	SEp
Mean Annual Flow	181	ft^3/s	16

Annual Flow Statistics Citations

Dudley, R.W.,2015, Regression equations for monthly and annual mean and selected percentile streamflows for ungaged rivers in Maine: U.S. Geological Survey Scientific Investigations Report 2015–5151, 35 p. (<http://dx.doi.org/10.3133/sir20155151>)

3.1 Hydrologic Analyses

Hydrologic analyses were carried out to establish the peak discharge-frequency relationships for each flooding source studied in detail affecting the community.

Flood discharges on the Penobscot River in Hampden were computed from data contained in the Flood Insurance Study for the City of Bangor (Reference 5). Discharges from the Bangor study were in agreement with a log-Pearson Type III analysis of USGS stream gage No. 01034500 on the Penobscot River at West Enfield (References 6 and 4). That analysis utilized 82 years of gage records and was prepared for a Flood Plain Management Study in the Town of Howland (Reference 7). Discharges at sites in Hampden were computed using the following equation:

$$Q_s = Q_g (A_s/A_g)^{0.80}$$

where Q_s is the discharge at the site, Q_g is the discharge from the Bangor study, A_s is the drainage area of the site, A_g is the drainage area of the location in Bangor (8,024 square miles).

Discharges of Souadabscook Stream and Sucker Brook were generated from the SCS Technical Release No. 20 hydrologic evaluation model and checked against the USGS regression equation for Maine (References 8 and 9).

A summary of the drainage area-peak discharge relationships for the streams studied by detailed methods is shown in Table 1, "Summary of Discharges."

TABLE 1 - SUMMARY OF DISCHARGES

<u>FLOODING SOURCE AND LOCATION</u>	<u>DRAINAGE AREA</u>	<u>PEAK DISCHARGES (cfs)</u>			
	<u>(sq. miles)</u>	<u>10-YEAR</u>	<u>50-YEAR</u>	<u>100-YEAR</u>	<u>500-YEAR</u>
PENOBSCOT RIVER					
Downstream of Souadabscook Stream	8,210.0	113,600	155,300	174,100	220,000
Upstream of corporate limits	8,027.3	111,500	152,500	171,100	216,100
SOUADABSCOOK STREAM					
At U. S. Route 1A	152.0	3,310	4,680	5,220	6,630
At Manning Mill Road	140.4	3,090	4,380	4,880	6,190
SUCKER BROOK					
At U. S. Route 1A	2.7	570	870	1,020	1,310

Water-surface elevations for Hammond, Hermon, and Ben Annis Ponds were generated from the SCS Technical Release No. 20 hydrologic evaluation model's reservoir routing procedure (Reference 8).

The stillwater elevations for the 10-, 50-, 100-, and 500-year floods have been determined for Hammond Pond, Hermon Pond, and Ben Annis Pond and are summarized in Table 2, "Summary of Stillwater Elevations."

TABLE 2 - SUMMARY OF STILLWATER ELEVATIONS

<u>FLOODING SOURCE AND LOCATION</u>	<u>ELEVATION (feet)</u>			
	<u>10-YEAR</u>	<u>50-YEAR</u>	<u>100-YEAR</u>	<u>500-YEAR</u>
HAMMOND POND				
Entire shoreline within community	126.3	128.4	129.0	130.5
HERMON POND				
Entire shoreline within community	126.3	128.4	129.0	130.5
BEN ANNIS POND				
Entire shoreline within community	126.3	128.4	129.0	130.5

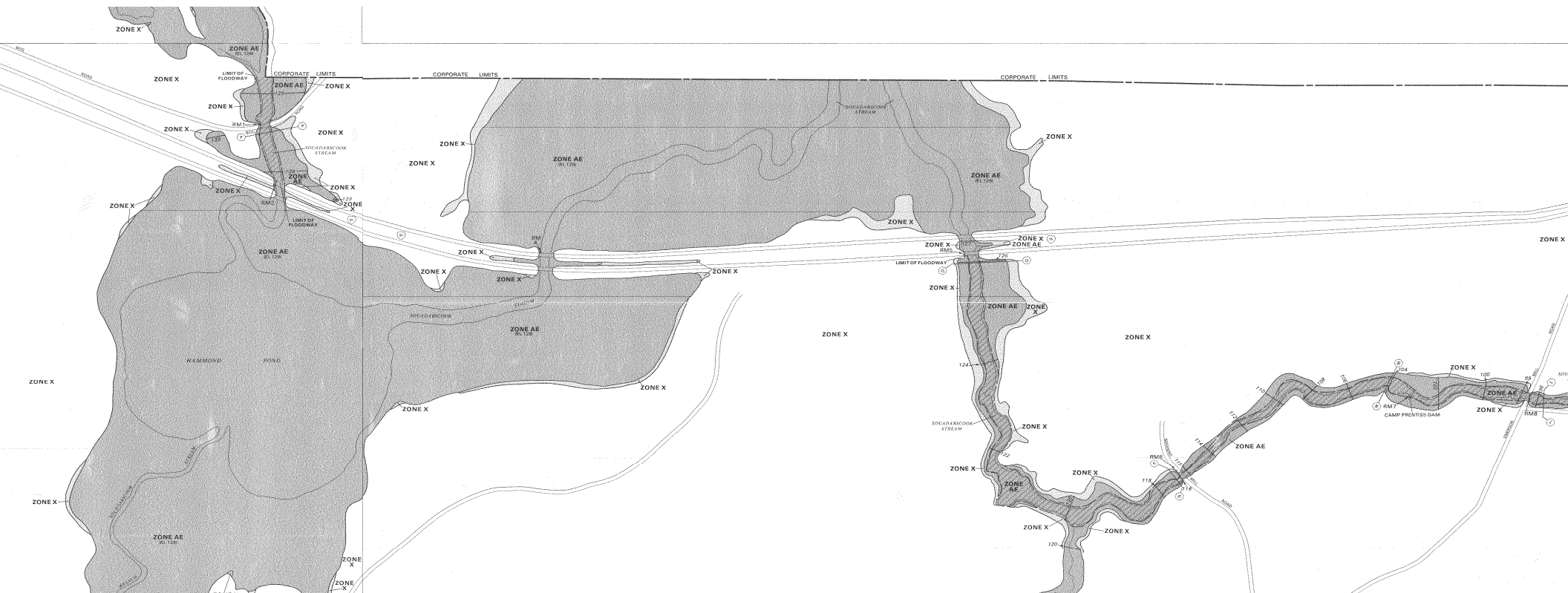
3.2 Hydraulic Analyses

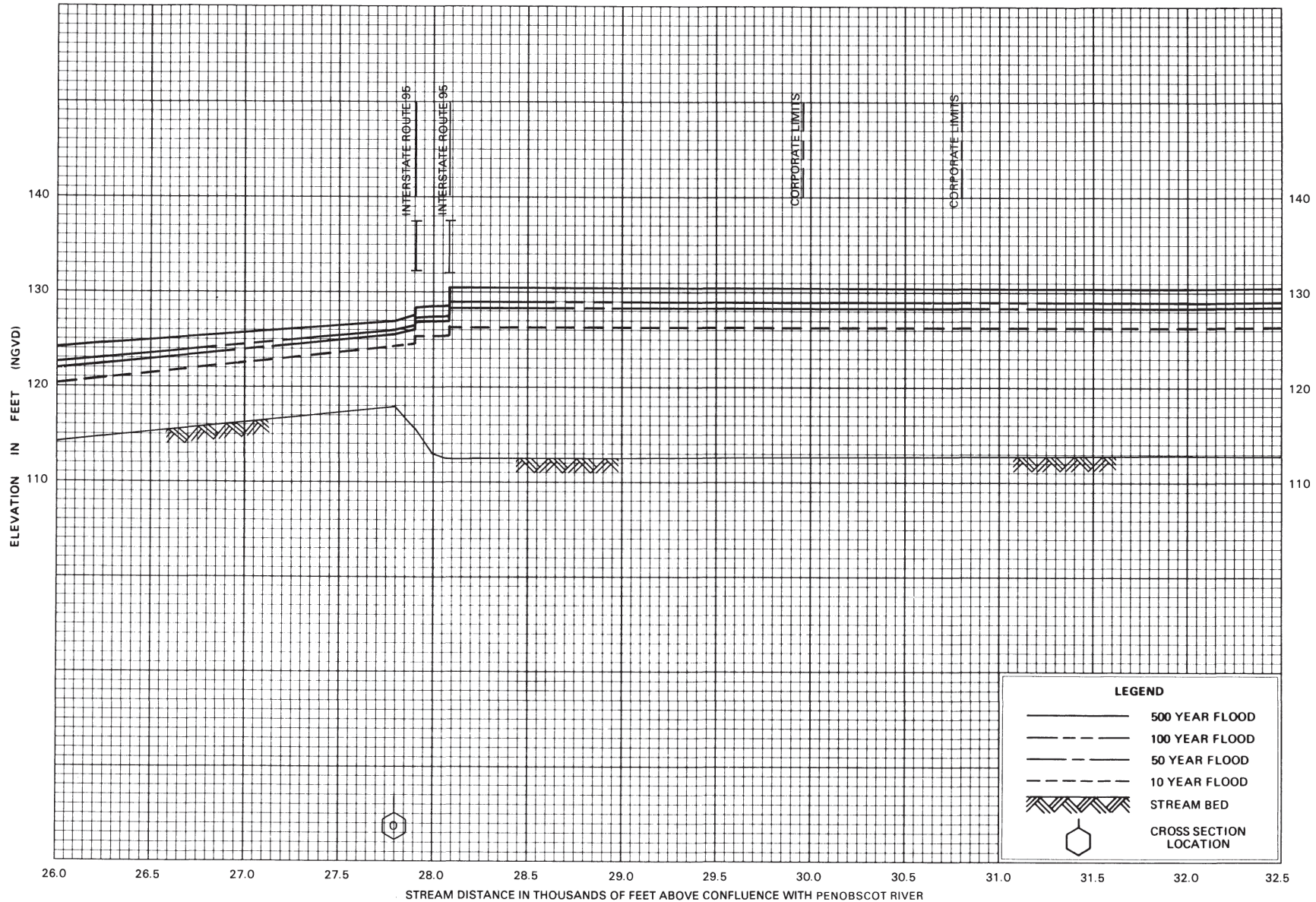
Analyses of the hydraulic characteristics of flooding from the sources studied were carried out to provide estimates of the elevations of floods of the selected recurrence intervals.

Cross sections for the streams studied by detailed methods were obtained from aerial photographs at a scale of 1:14,400 (Reference 10). The below-water sections were obtained from field surveys. All bridges, dams, and culverts were surveyed to obtain elevation data and structural geometry.

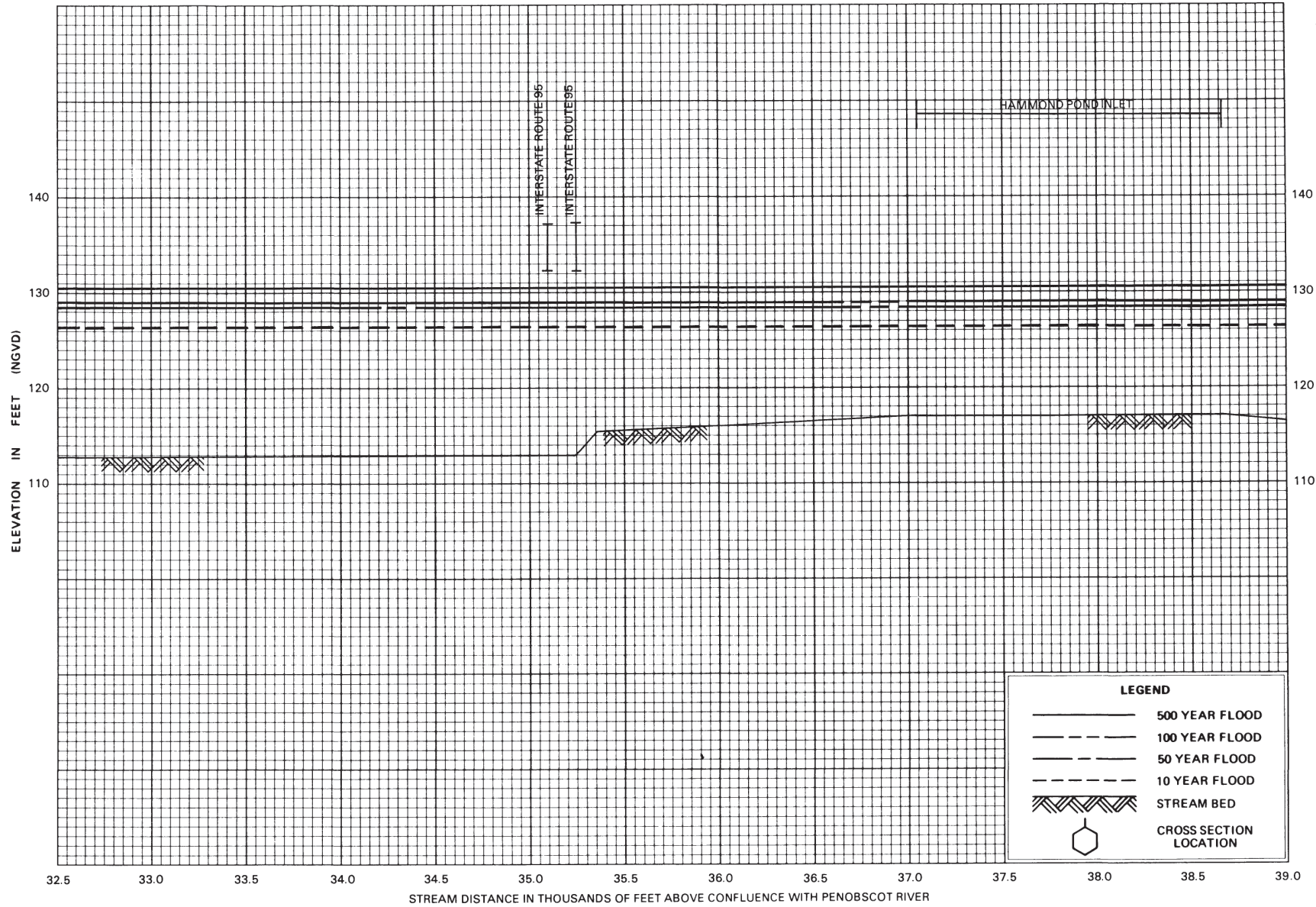
Locations of selected cross sections used in the hydraulic analyses are shown on the Flood Profiles (Exhibit 1). For stream segments for which a floodway was computed (Section 4.2), selected cross-section locations are also shown on the Flood Insurance Rate Map (Exhibit 2).

Water-surface elevations of floods of the selected recurrence intervals were computed using the SCS WSP-2 computer program (Reference 11). Flood





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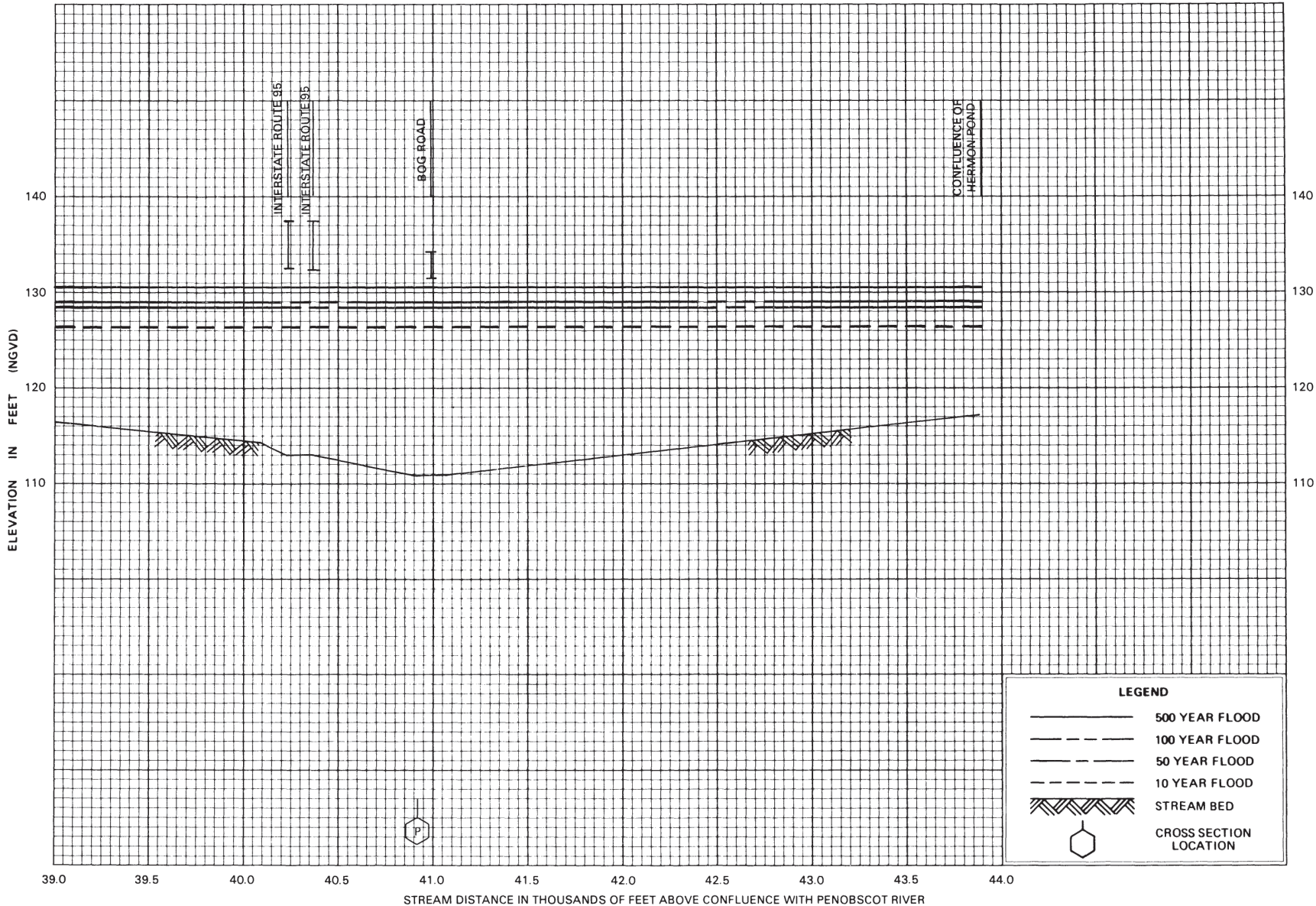


FEDERAL EMERGENCY MANAGEMENT AGENCY

TOWN OF HAMPDEN, ME
(PENOBSCOT CO.)

FLOOD PROFILES

SQUADABSCOOK STREAM



LEGEND

- 500 YEAR FLOOD
- 100 YEAR FLOOD
- 50 YEAR FLOOD
- 10 YEAR FLOOD
- STREAM BED
- CROSS SECTION LOCATION

FLOODING SOURCE		FLOODWAY			BASE FLOOD WATER SURFACE ELEVATION			
CROSS SECTION	¹ DISTANCE	WIDTH (FEET)	SECTION AREA (SQUARE FEET)	MEAN VELOCITY (FEET PER SECOND)	REGULATORY	WITHOUT FLOODWAY (FEET NGVD)	WITH FLOODWAY	INCREASE
Souadabscook Stream (continued)								
J	17,725	55	474	10.3	88.2	88.2	89.2	1.0
K	17,900	101	799	6.1	89.8	89.8	90.8	1.0
L	19,100	56	469	10.5	95.7	95.7	96.7	1.0
M	20,685	107	601	8.1	104.1	104.1	105.1	1.0
N	23,195	57	522	9.3	117.6	117.6	118.6	1.0
O	27,800	101	813	5.9	126.0	126.0	127.0	1.0
P	40,920	115	1,207	2.9	129.0	129.0	130.0	1.0
Sucker Brook								
A	0	136	1,174	1.1	15.2	9.1 ²	10.1	1.0
B	1,150	115	916	1.2	15.2	9.4 ²	10.4	1.0
C	2,170	25	199	5.3	15.2	14.1 ²	15.1	1.0
D	3,255	23	193	5.4	23.8	23.8	24.8	1.0
E	3,410	62	397	2.6	26.7	26.7	27.7	1.0
F	3,970	46	216	4.7	30.5	30.5	31.5	1.0
G	4,115	253	992	1.0	31.0	31.0	32.0	1.0
H	4,950	31	154	6.6	46.8	46.8	47.8	1.0
I	5,510	71	619	1.6	56.2	56.2	57.2	1.0

¹Feet above confluence with Penobscot River

²Elevation computed without consideration of backwater effects from Penobscot River

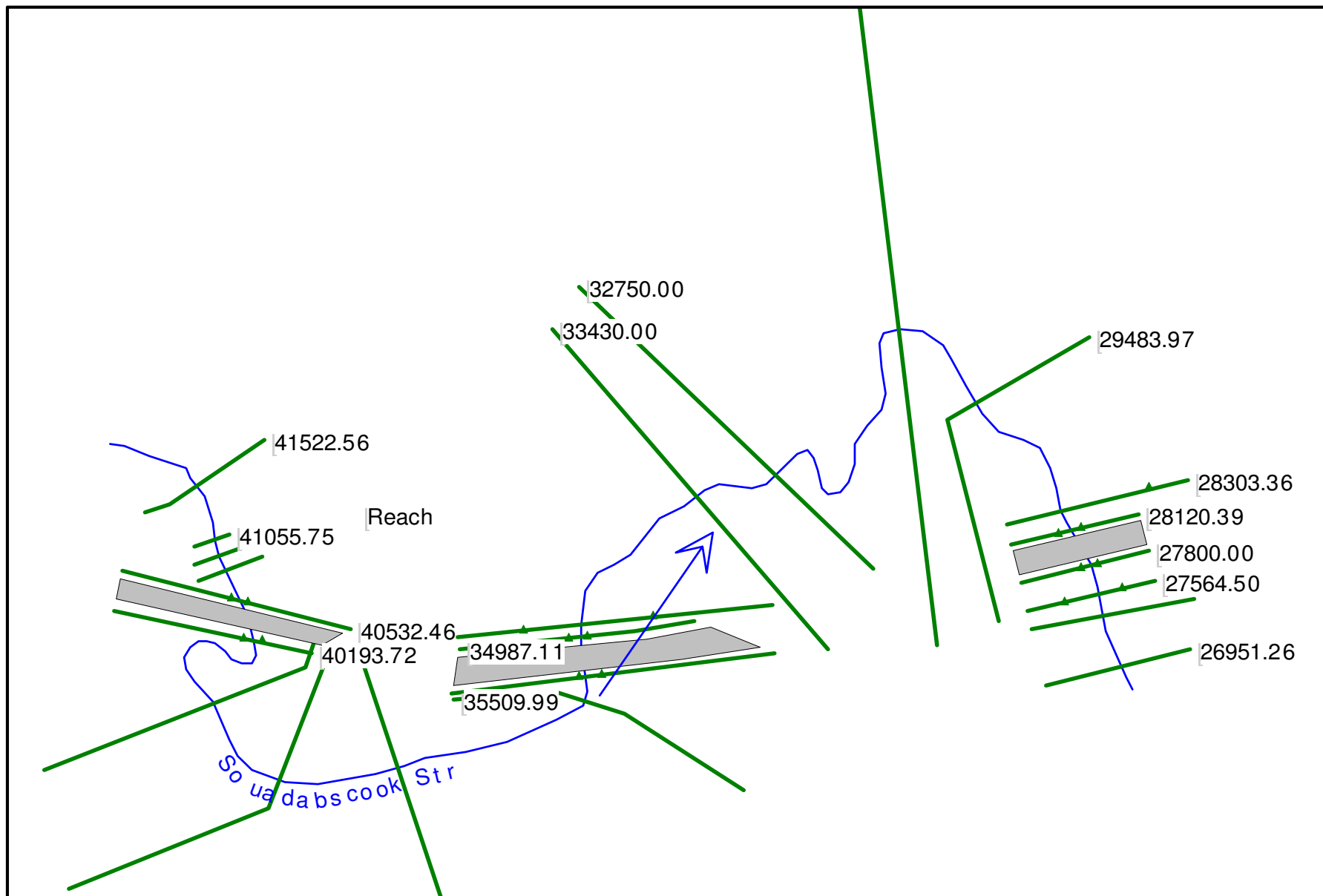
TABLE 3

FEDERAL EMERGENCY MANAGEMENT AGENCY

TOWN OF HAMPDEN, ME
(PENOBSCOT CO.)

FLOODWAY DATA

SOUADABSCOOK STREAM-SUCKER BROOK

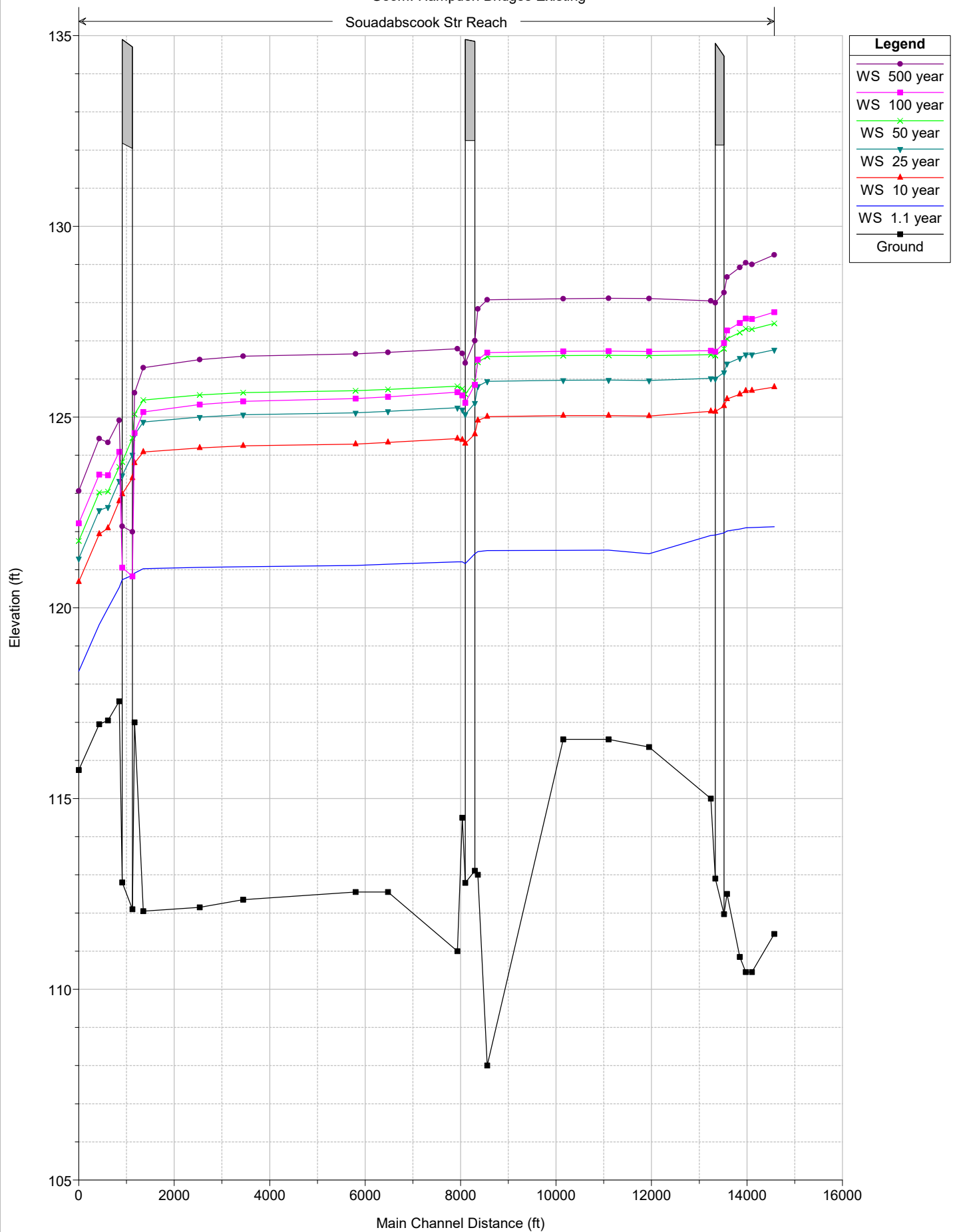


HEC-RAS Cross Section Location Map

Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

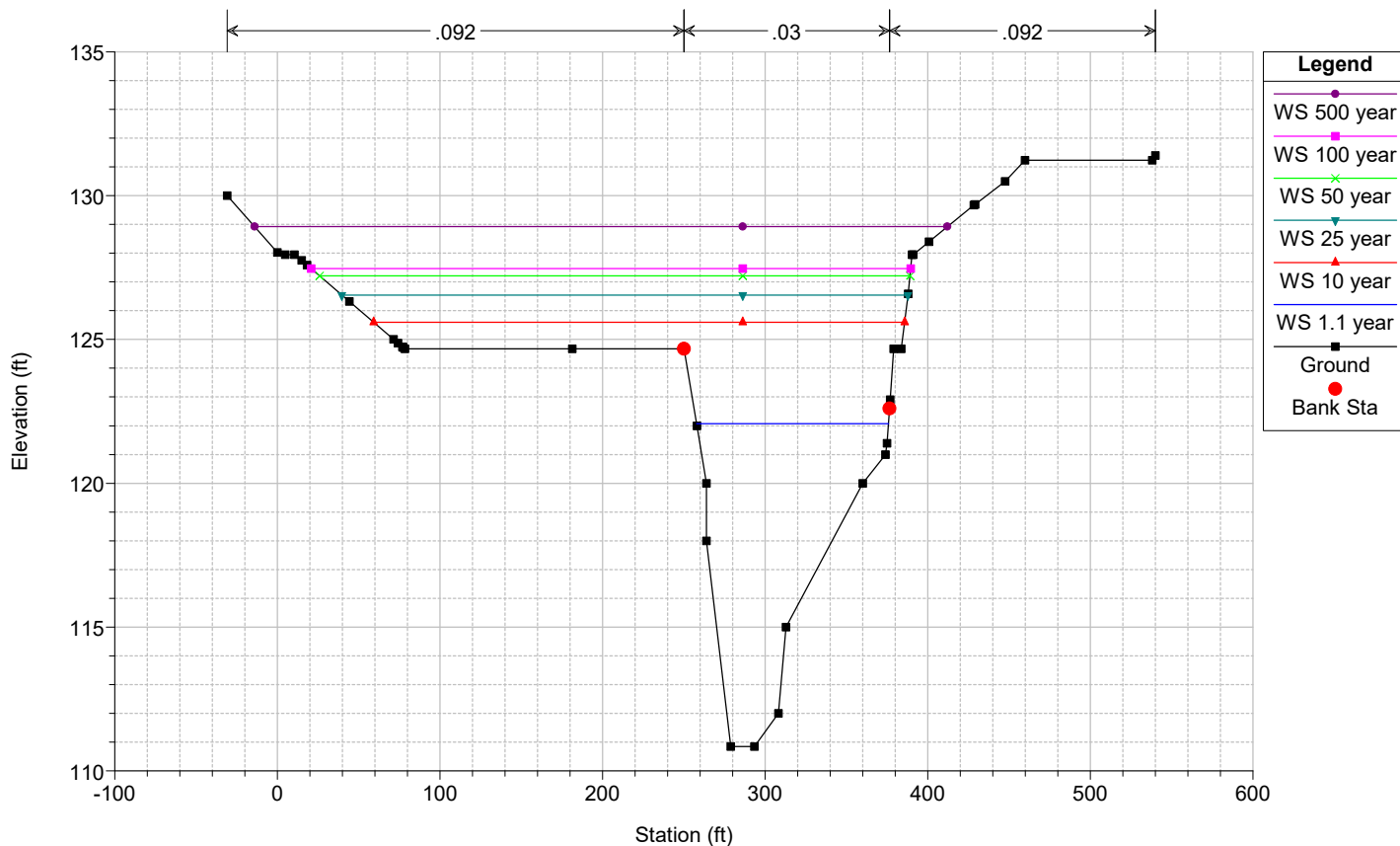
Soudabsccook Str Reach



Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

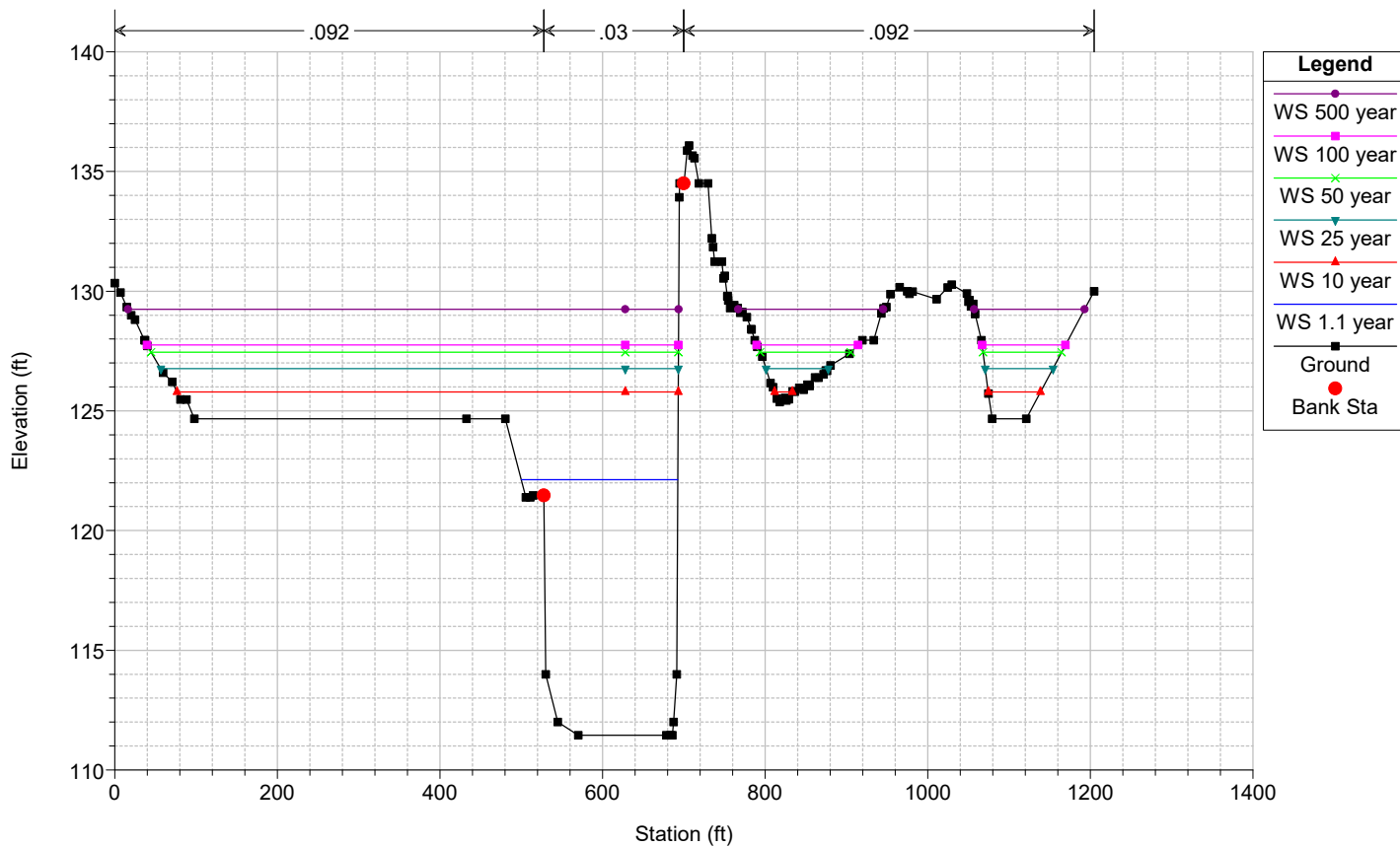
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

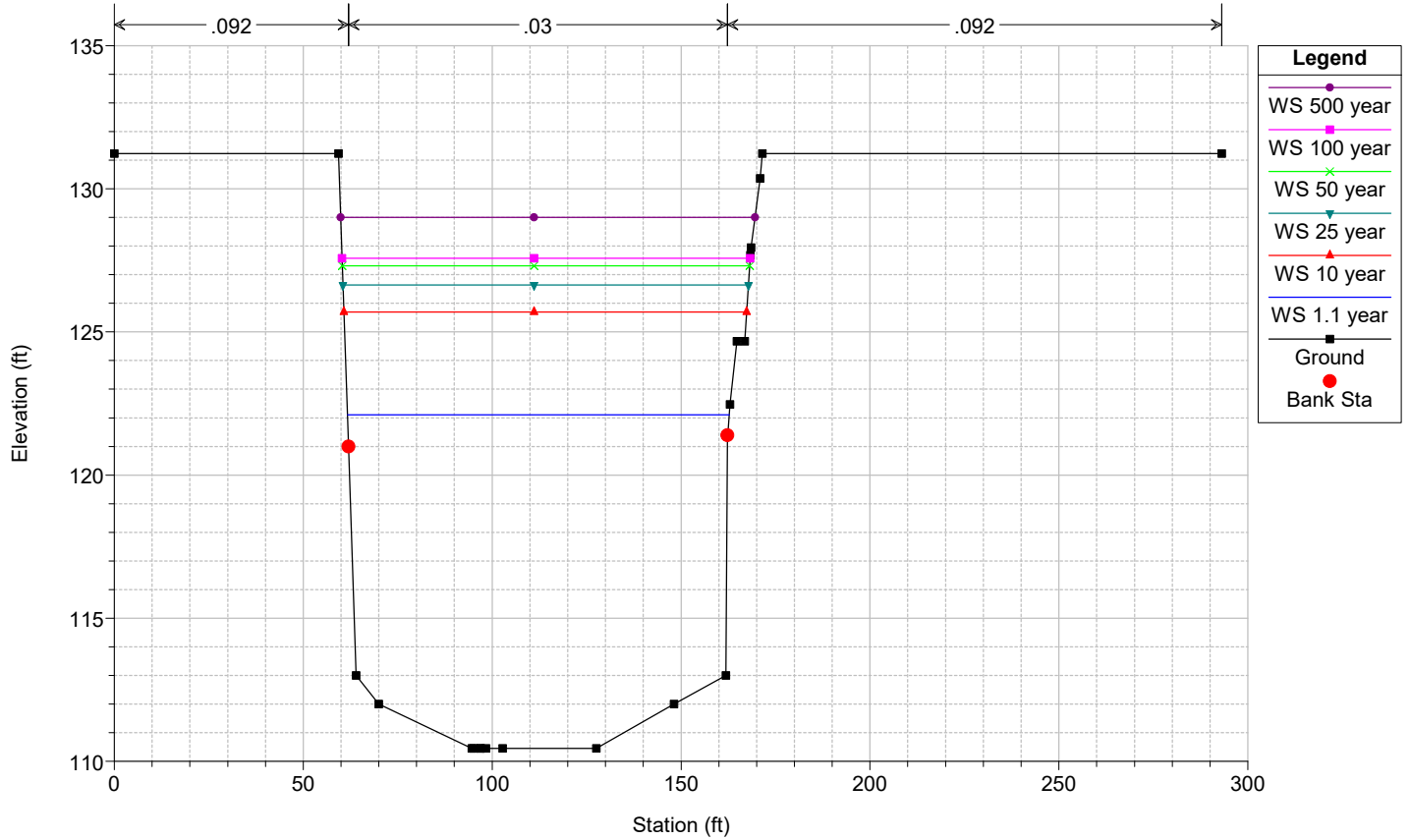
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

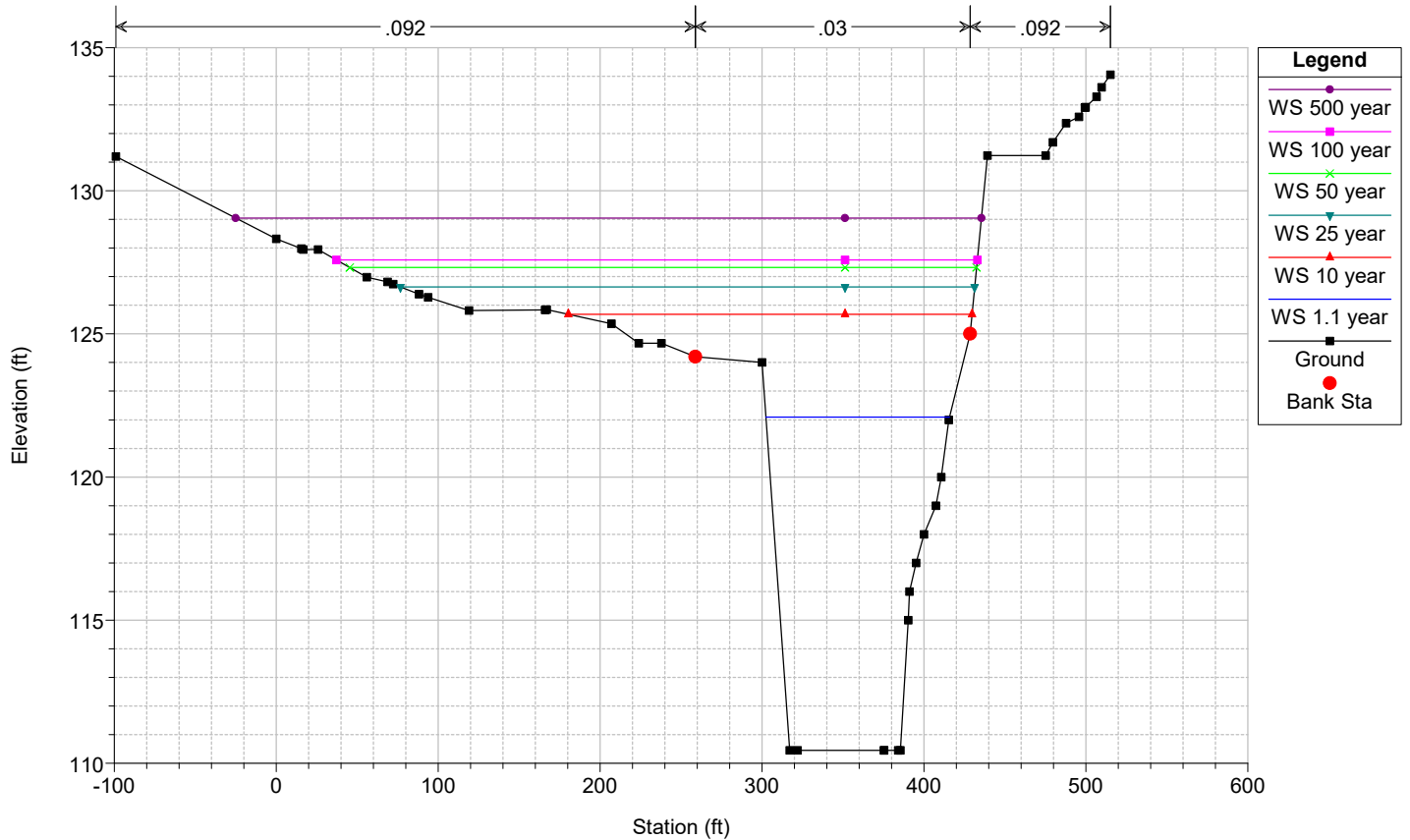
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

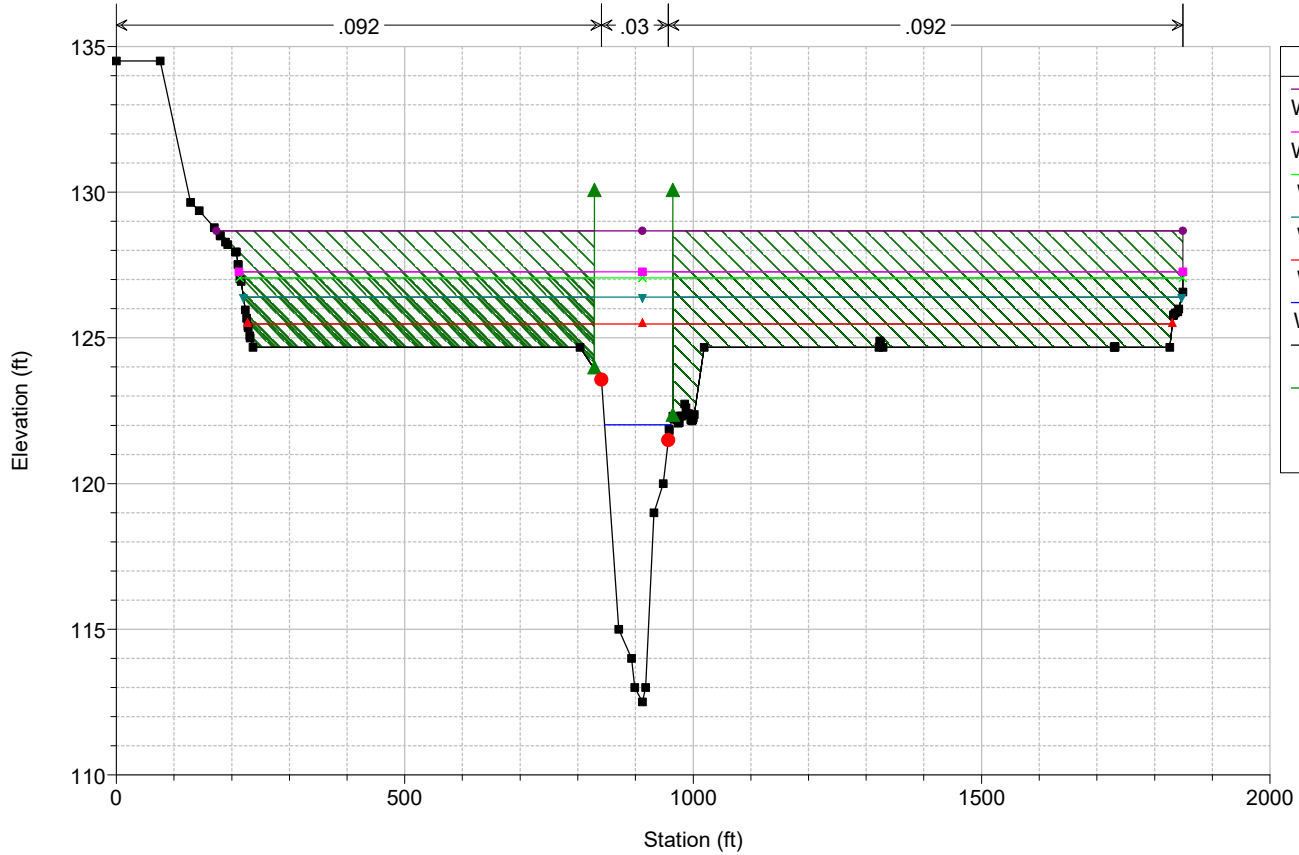
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

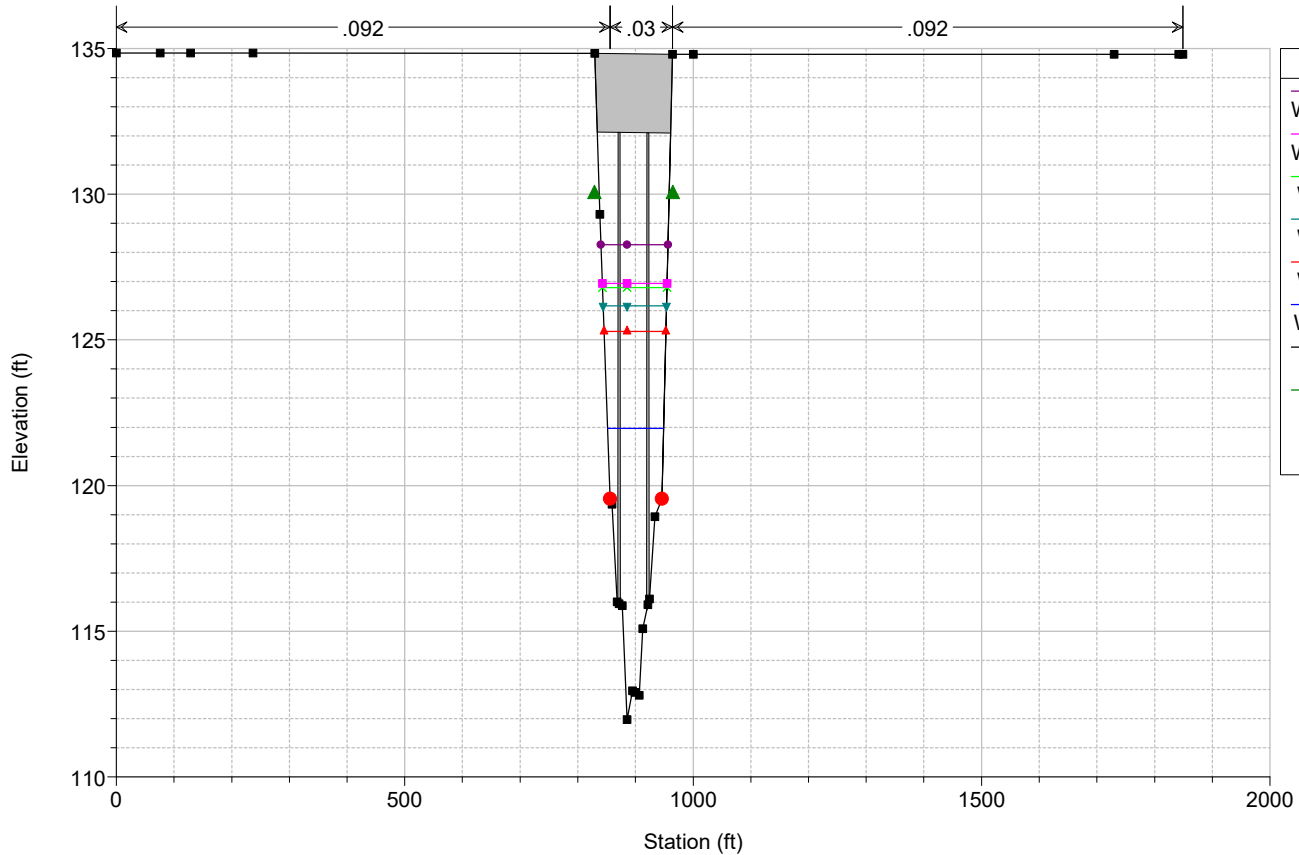
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

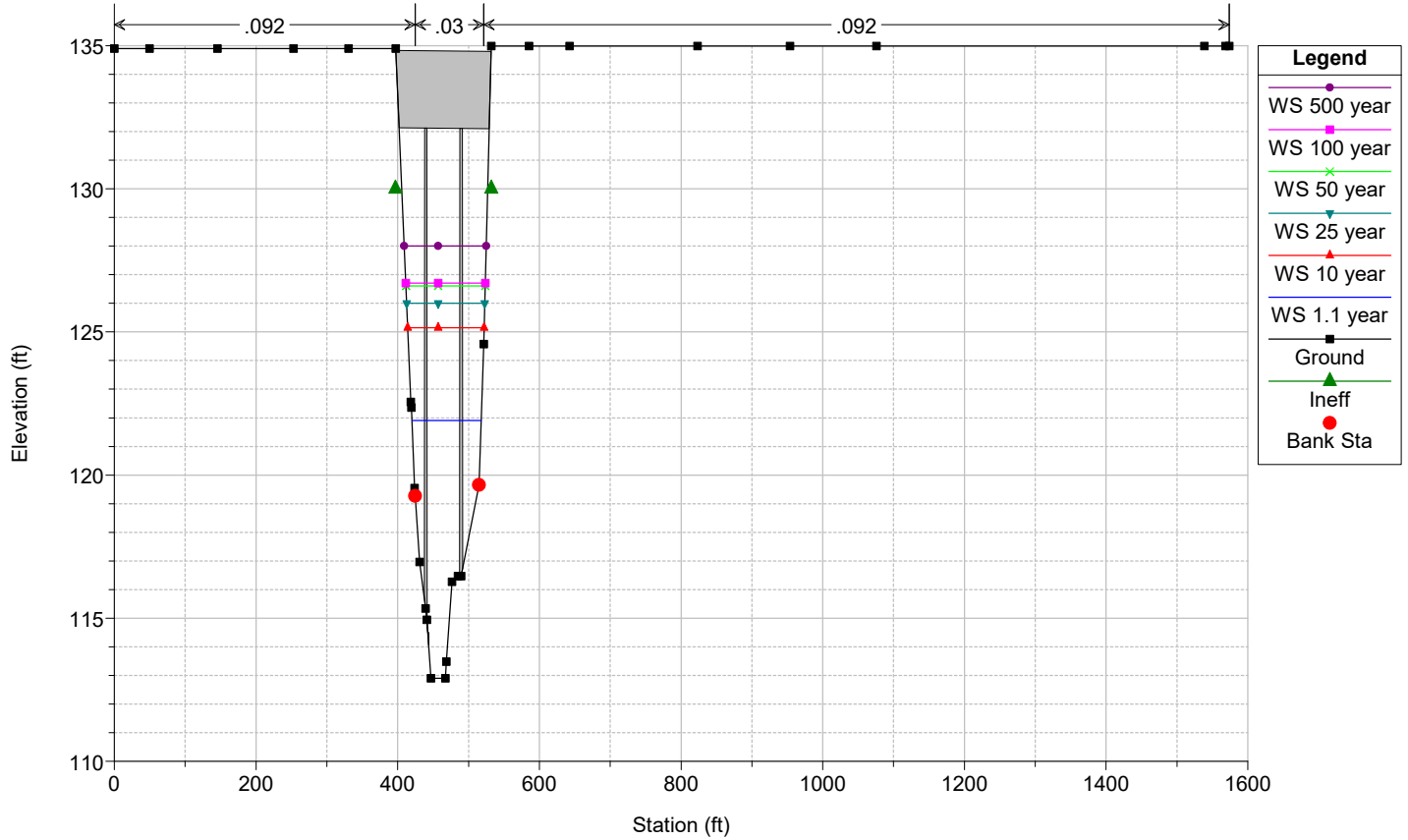
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

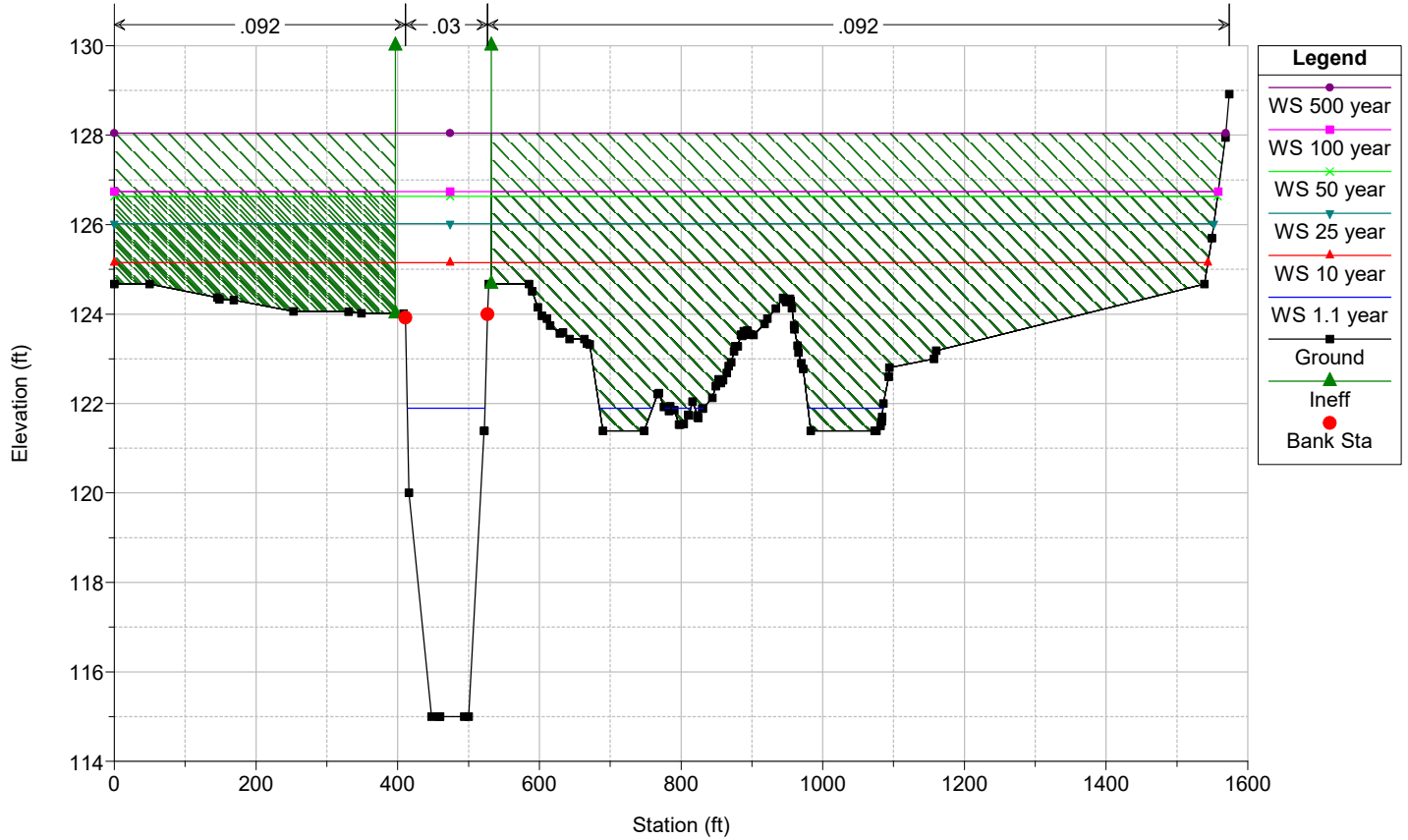
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

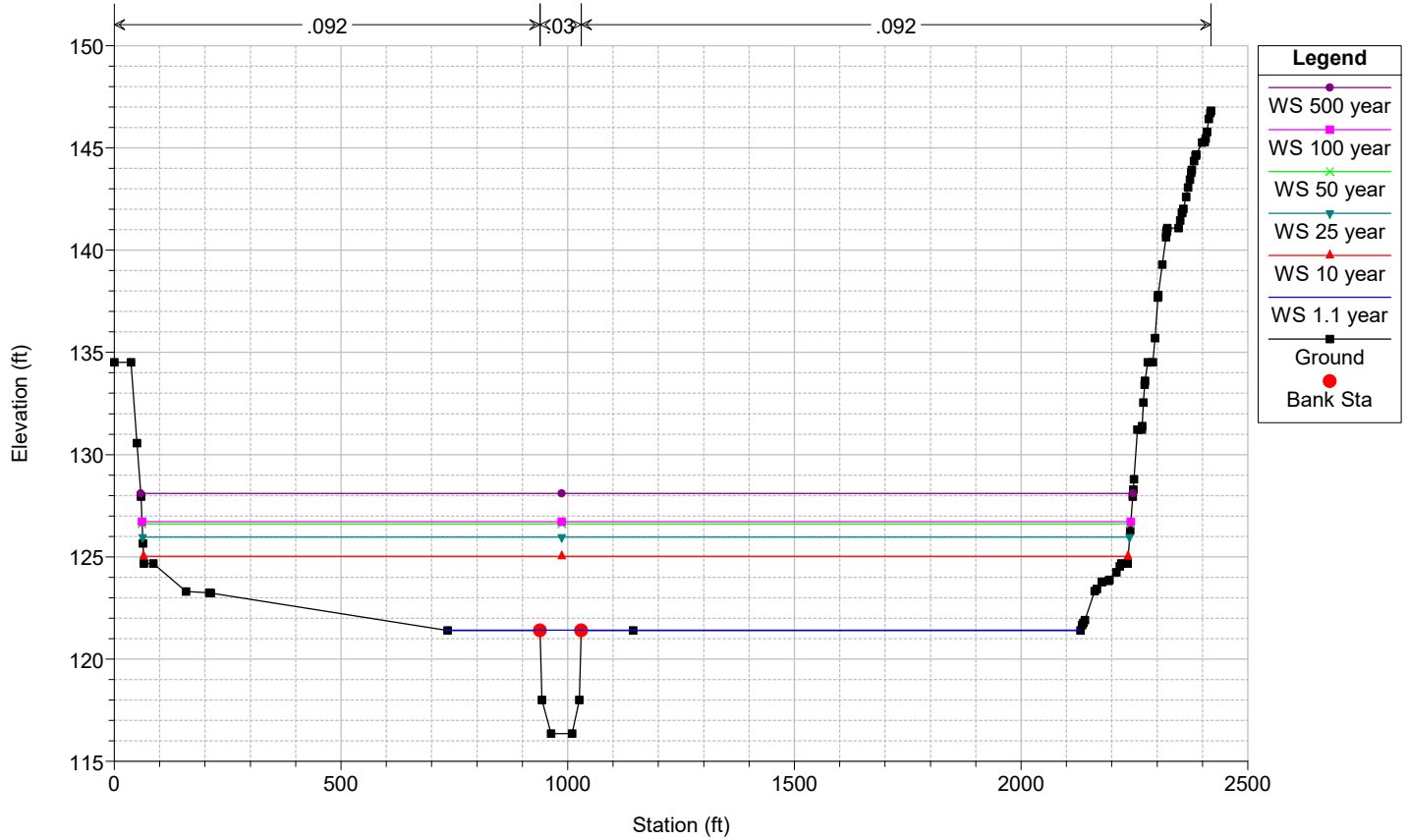
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

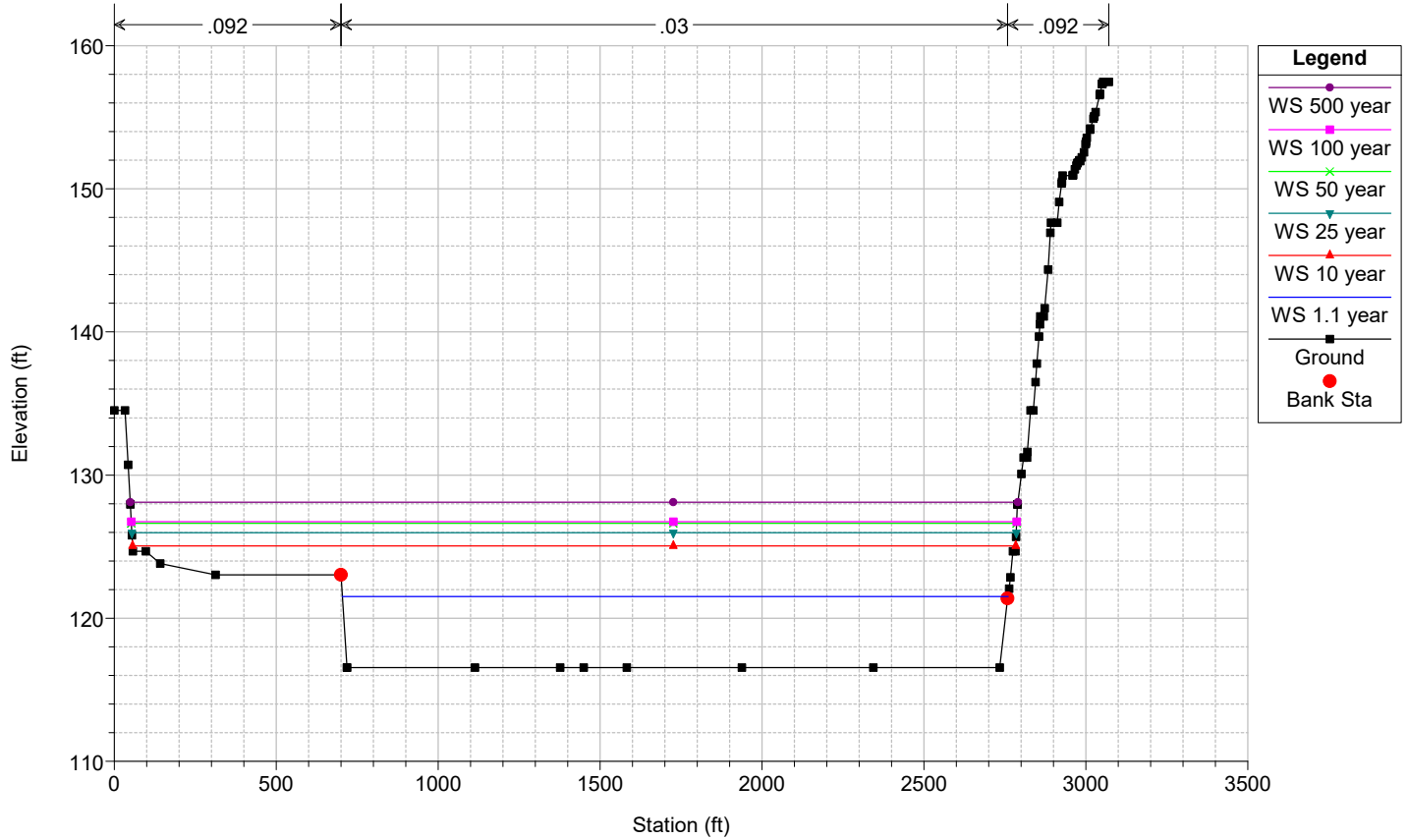
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

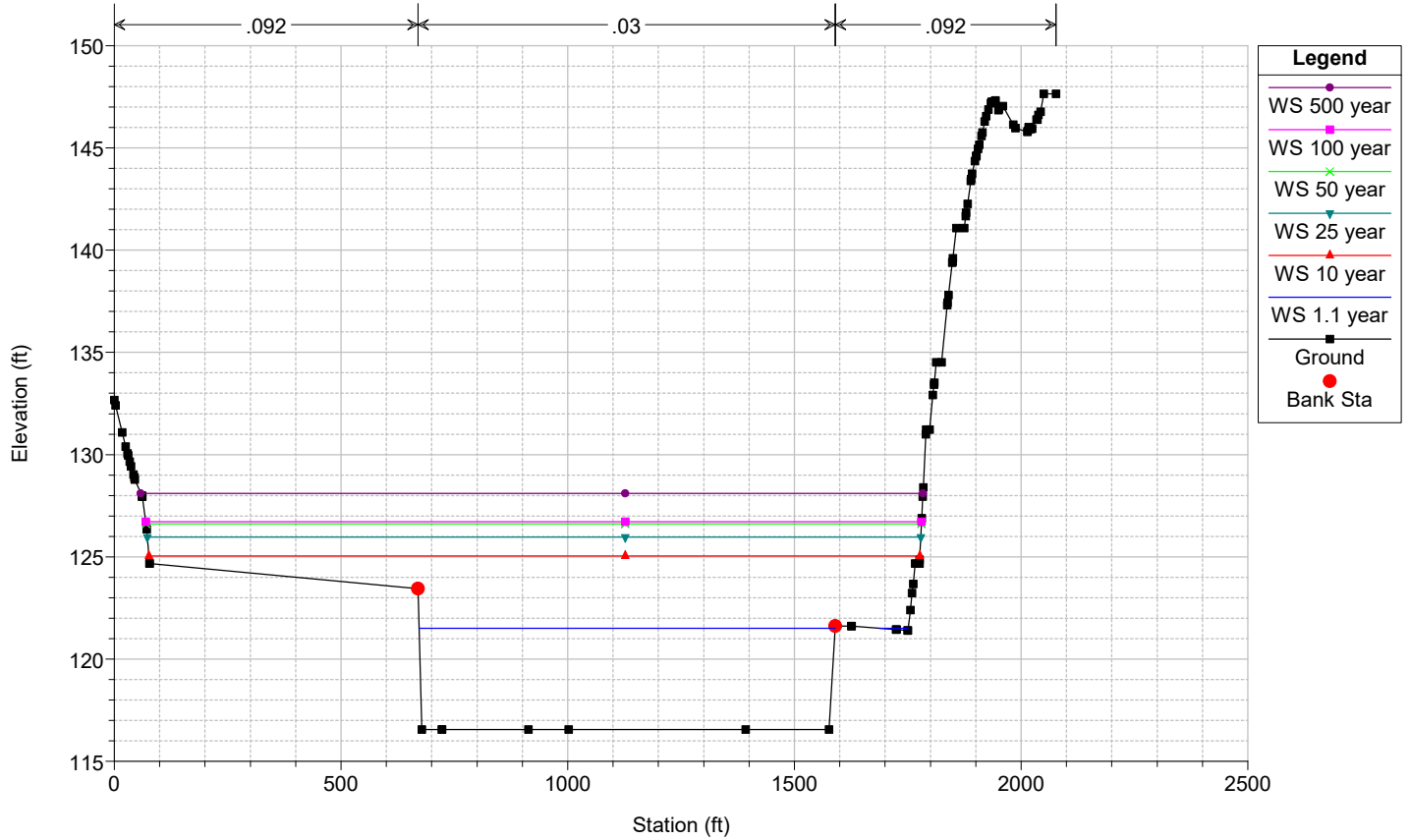
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

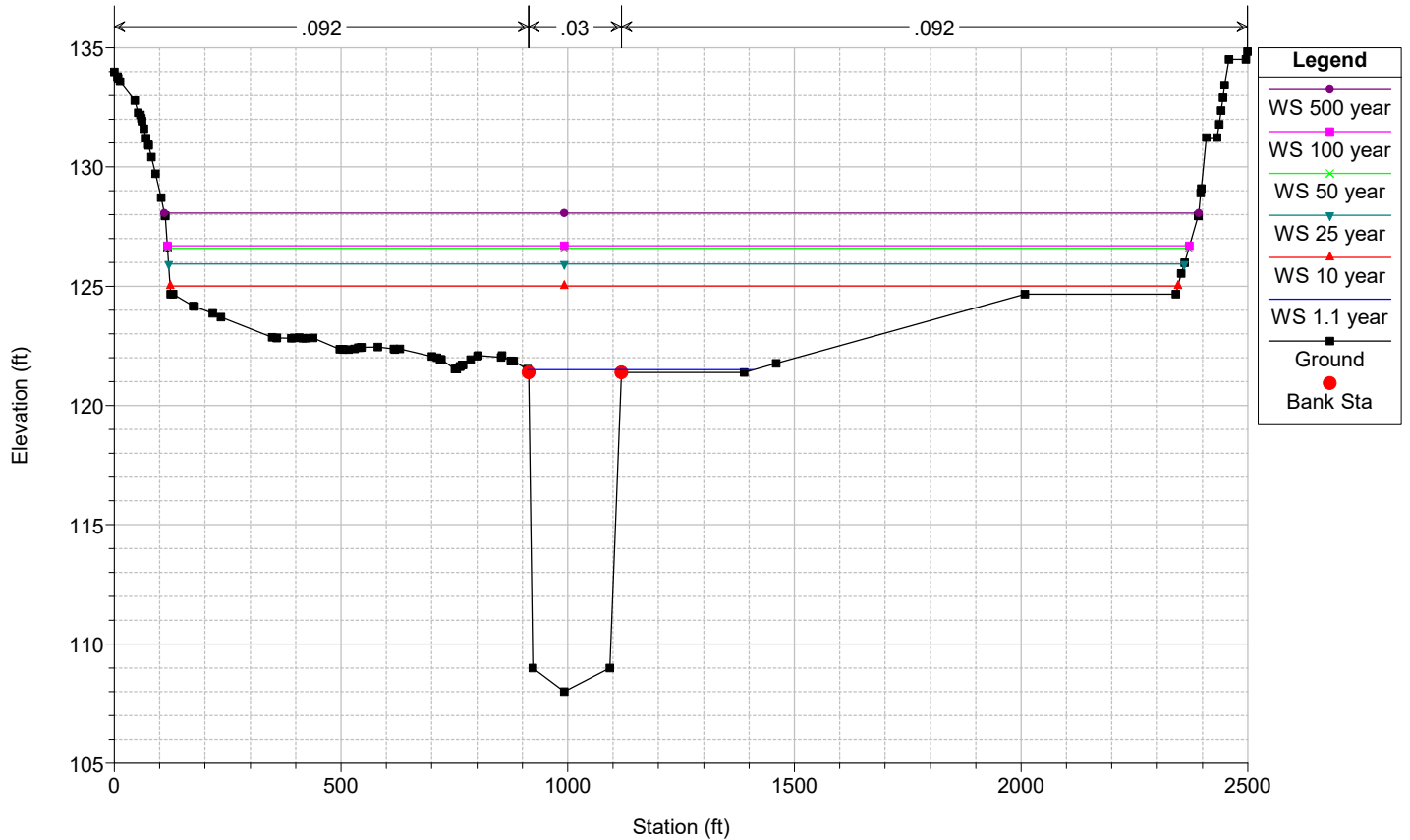
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

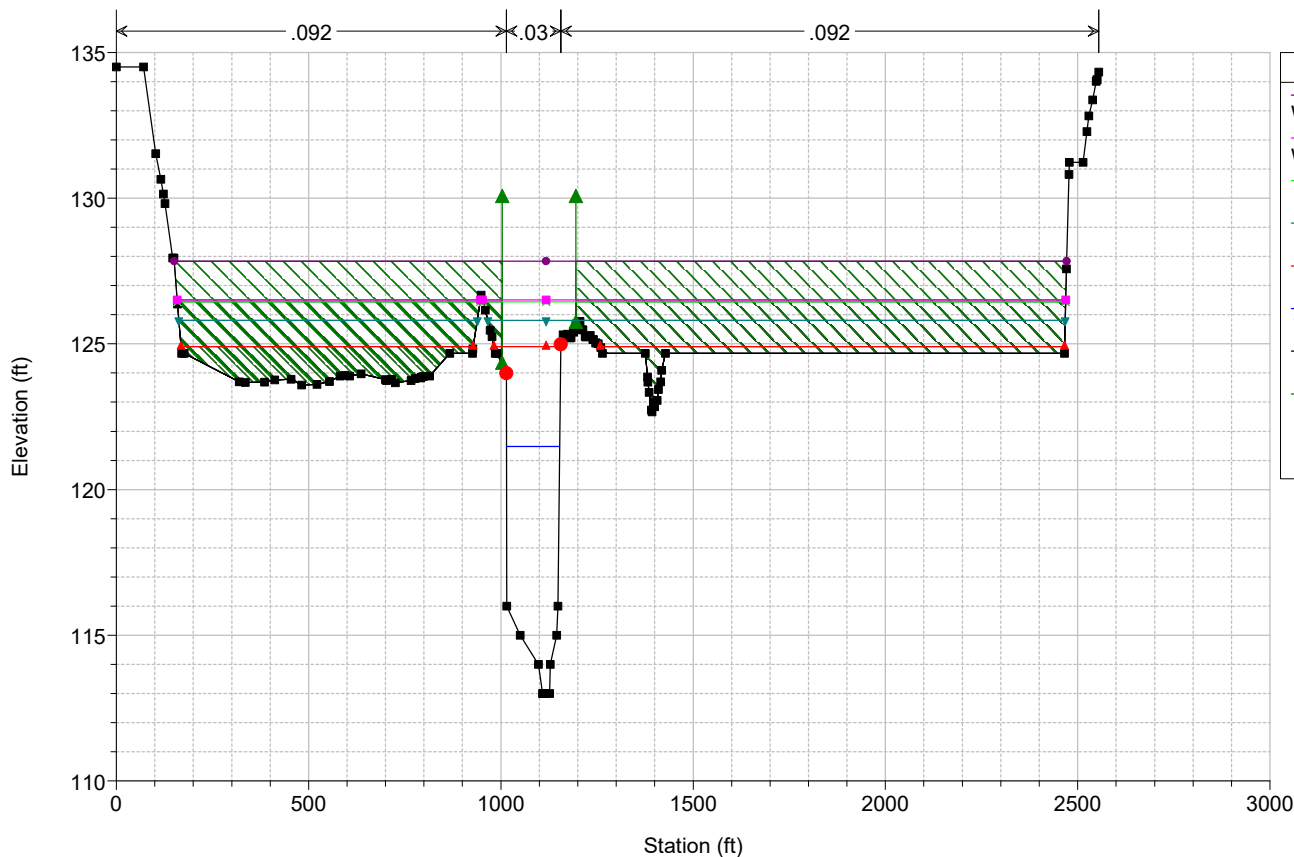
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

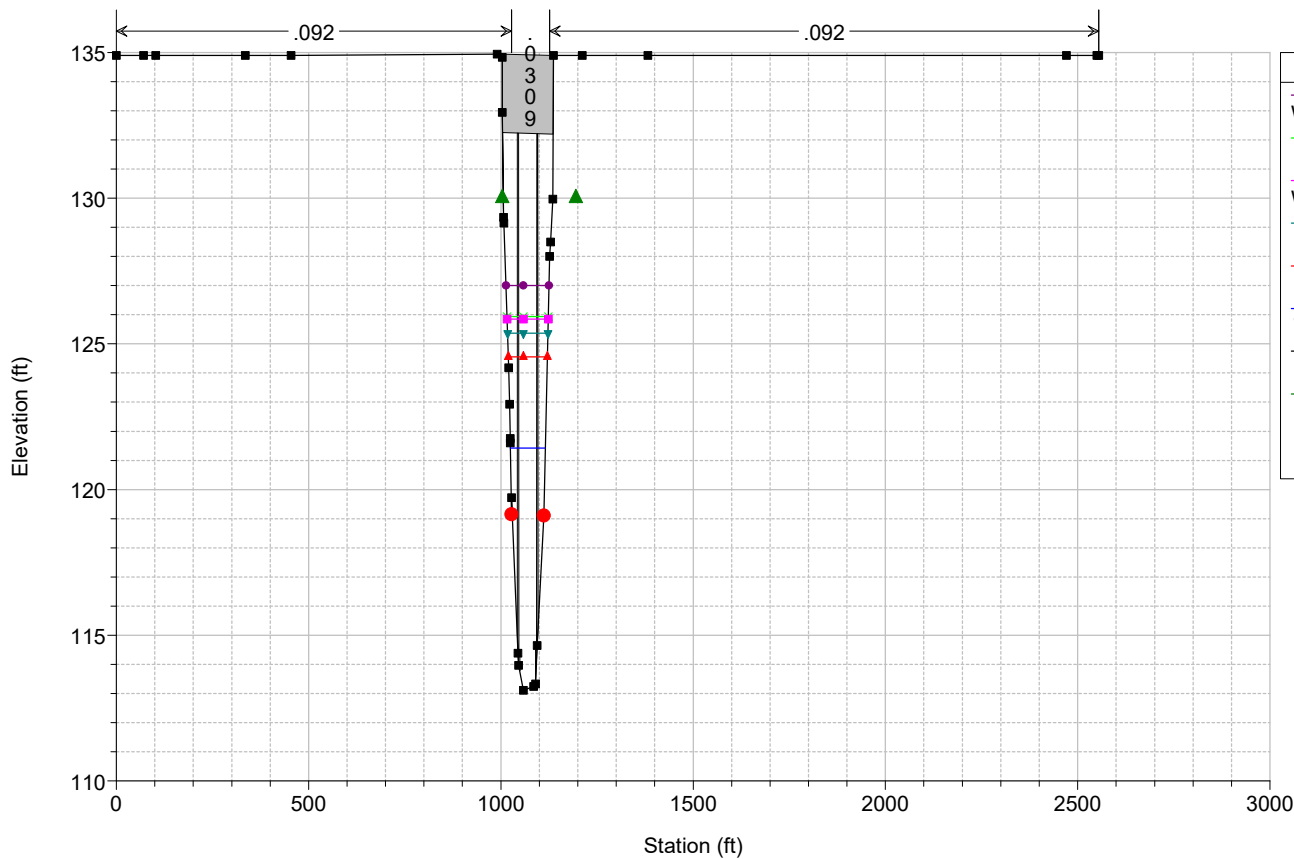
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

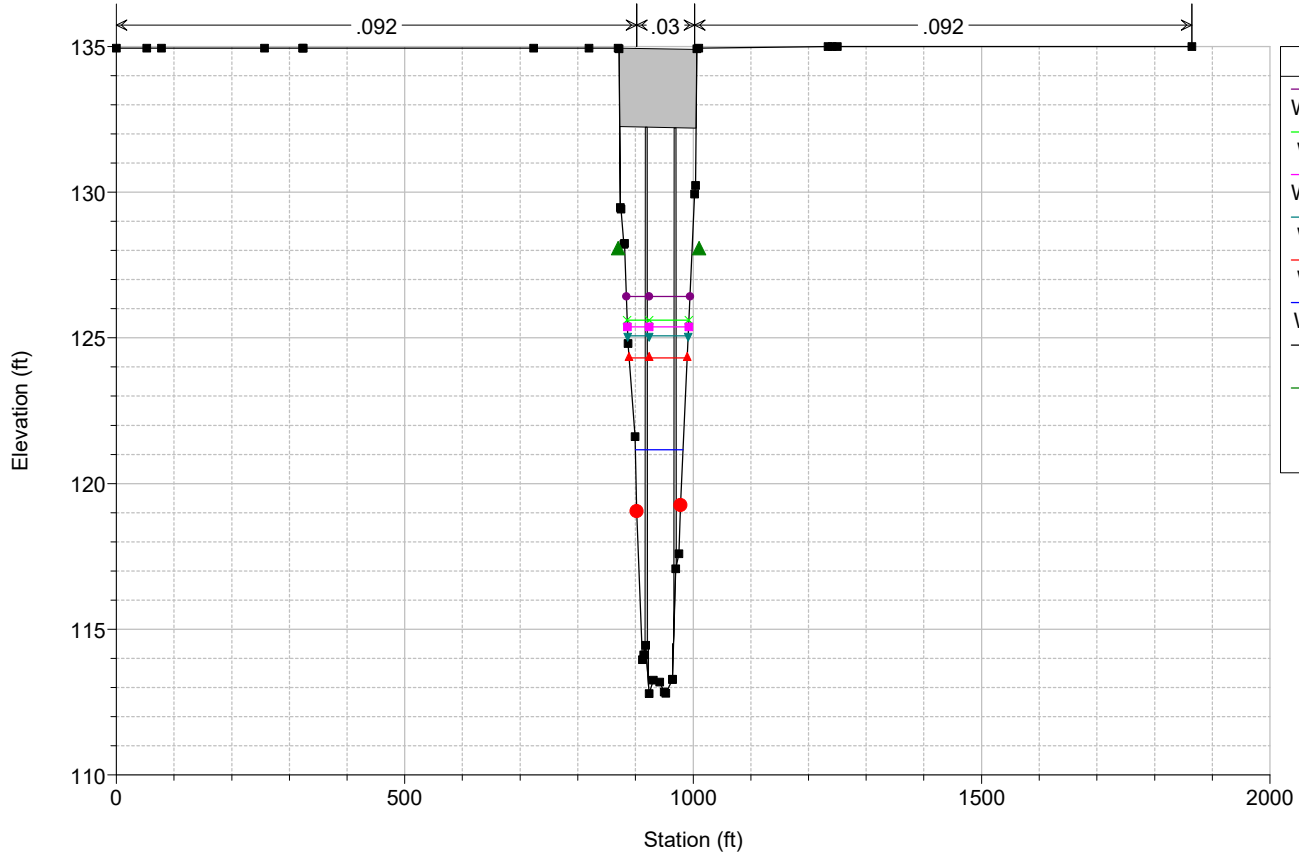
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

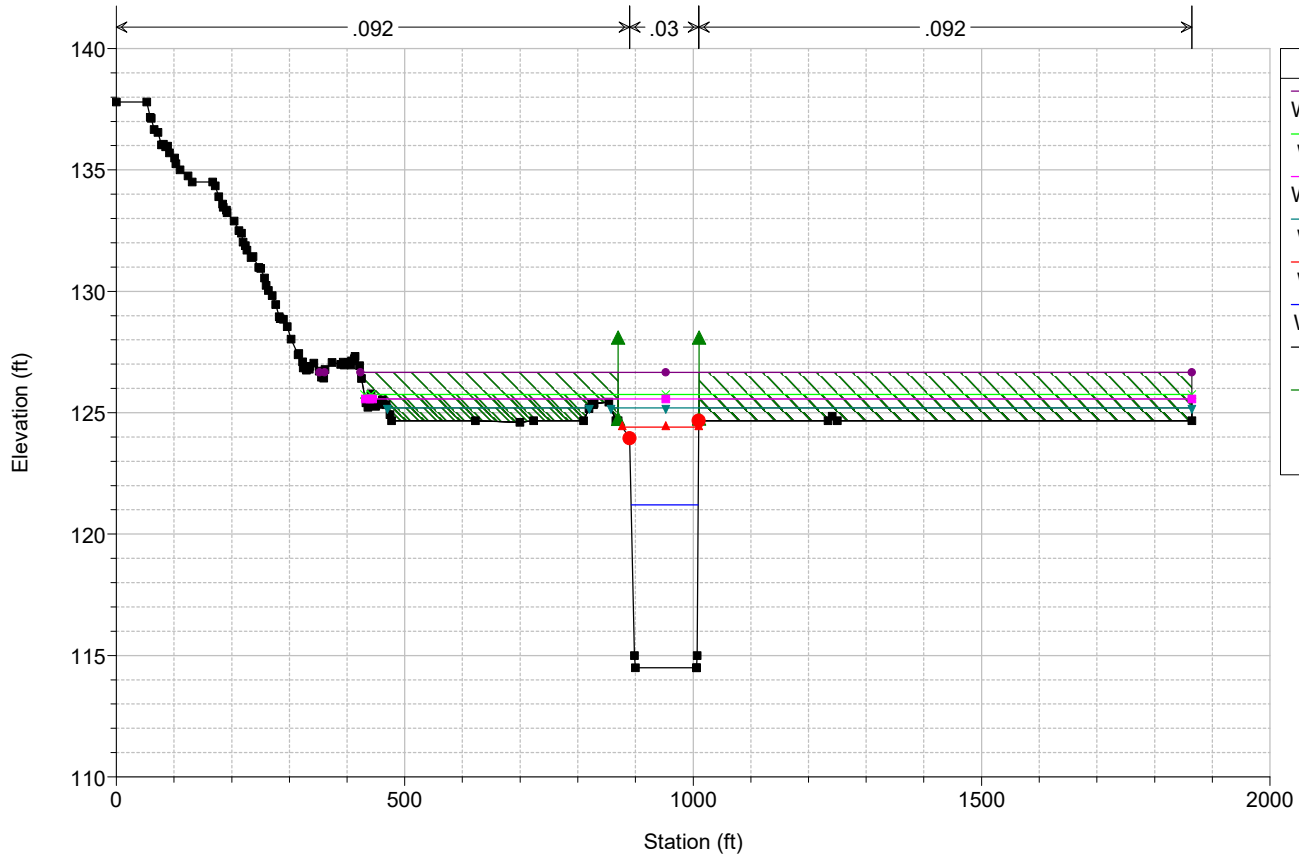
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

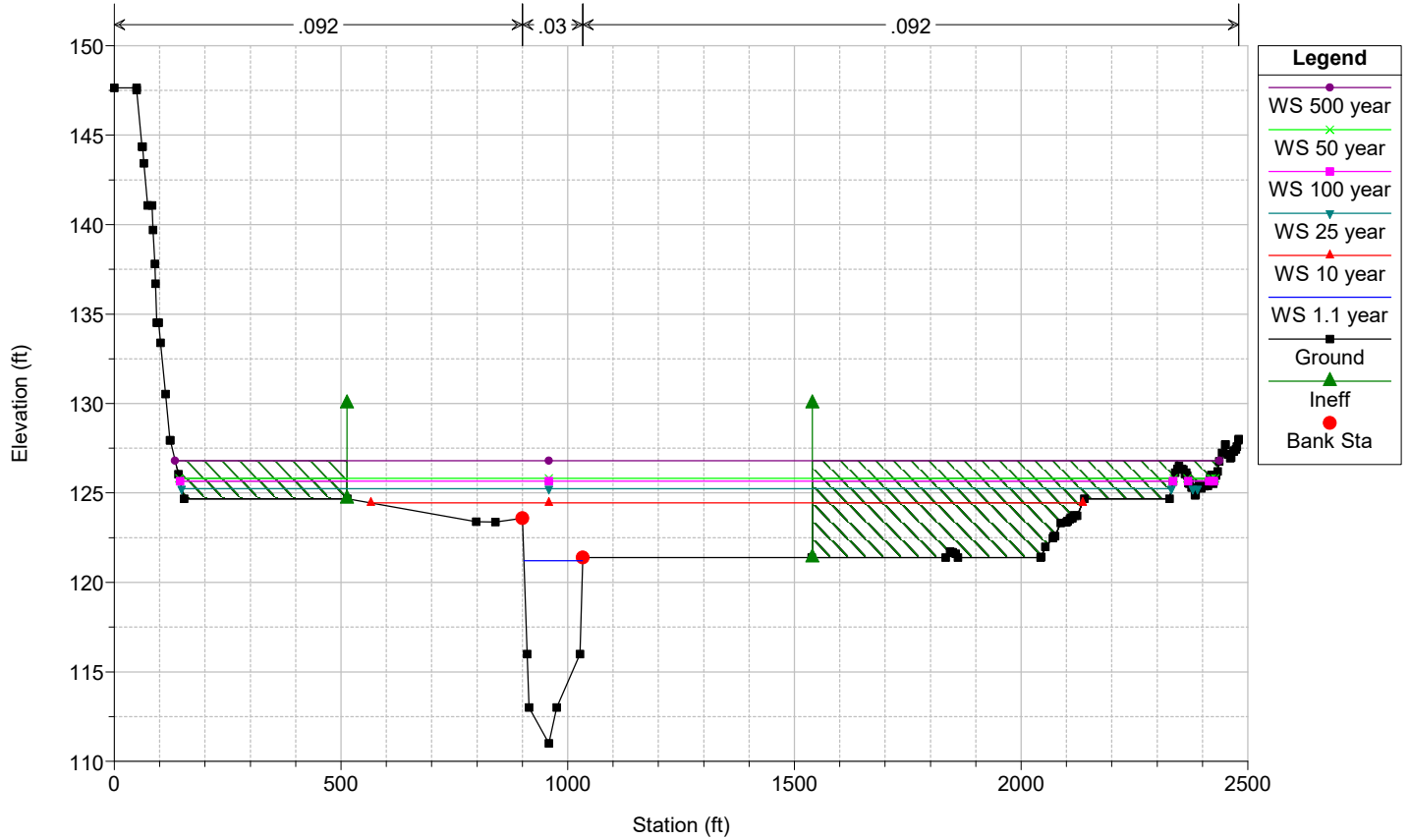
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

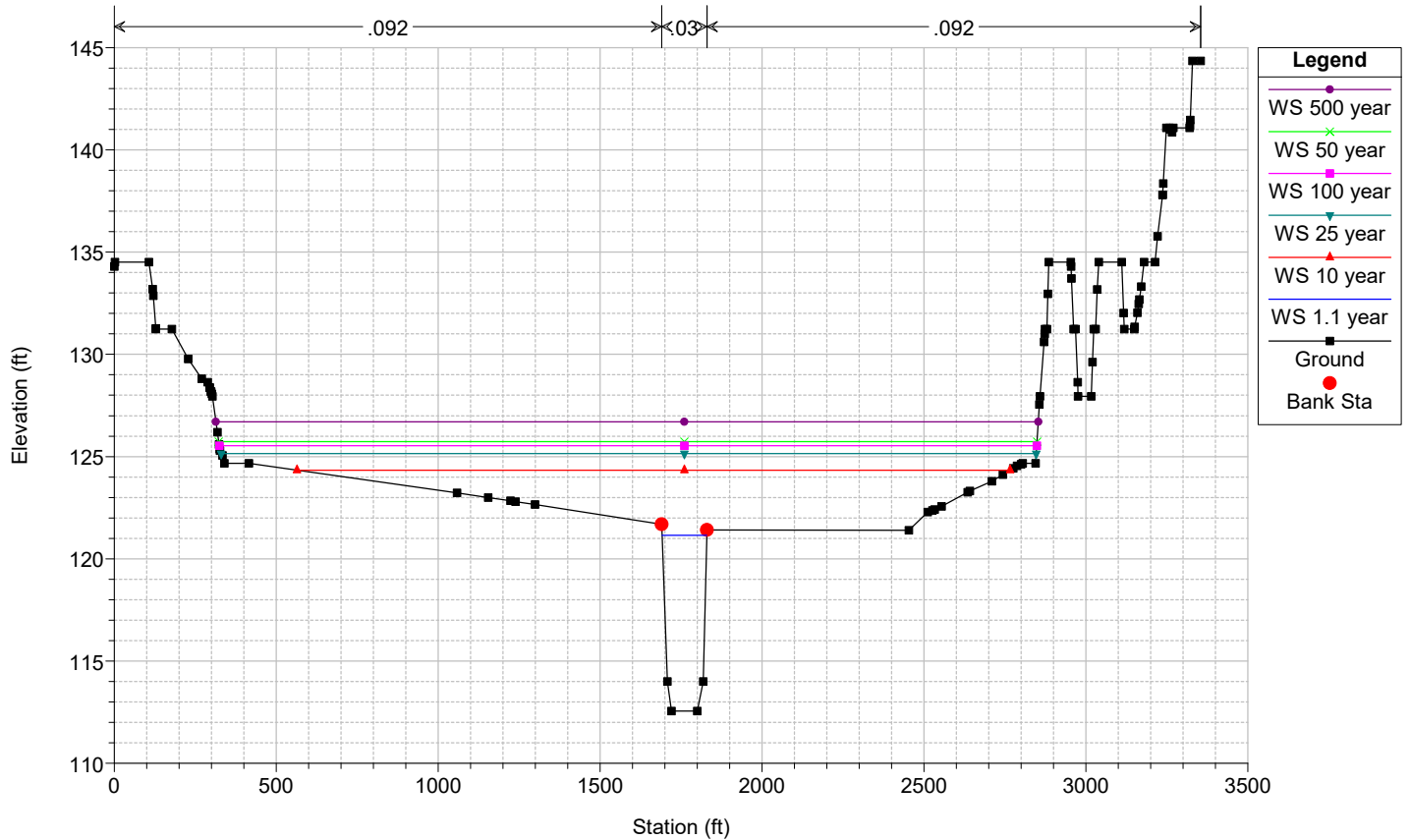
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

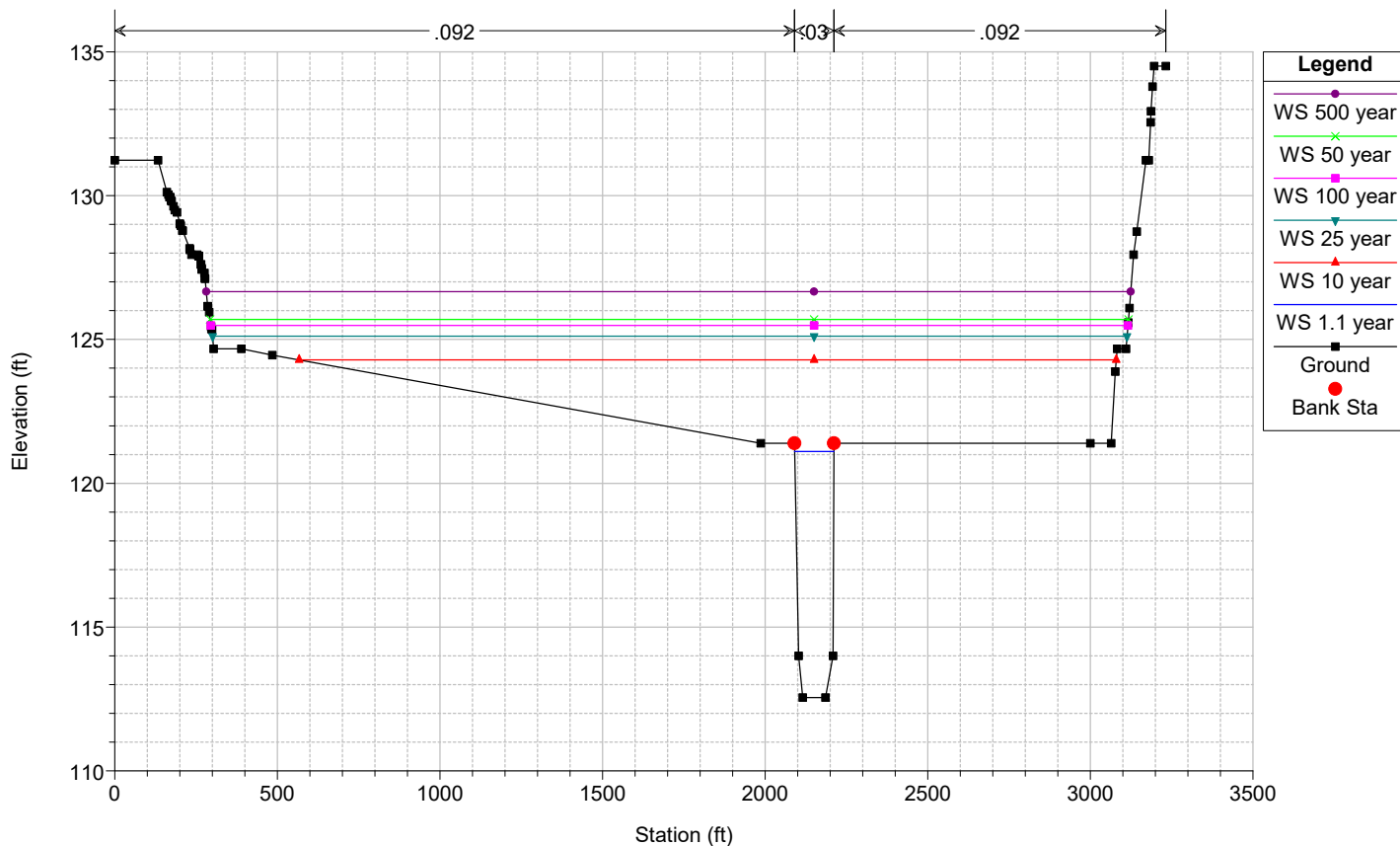
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

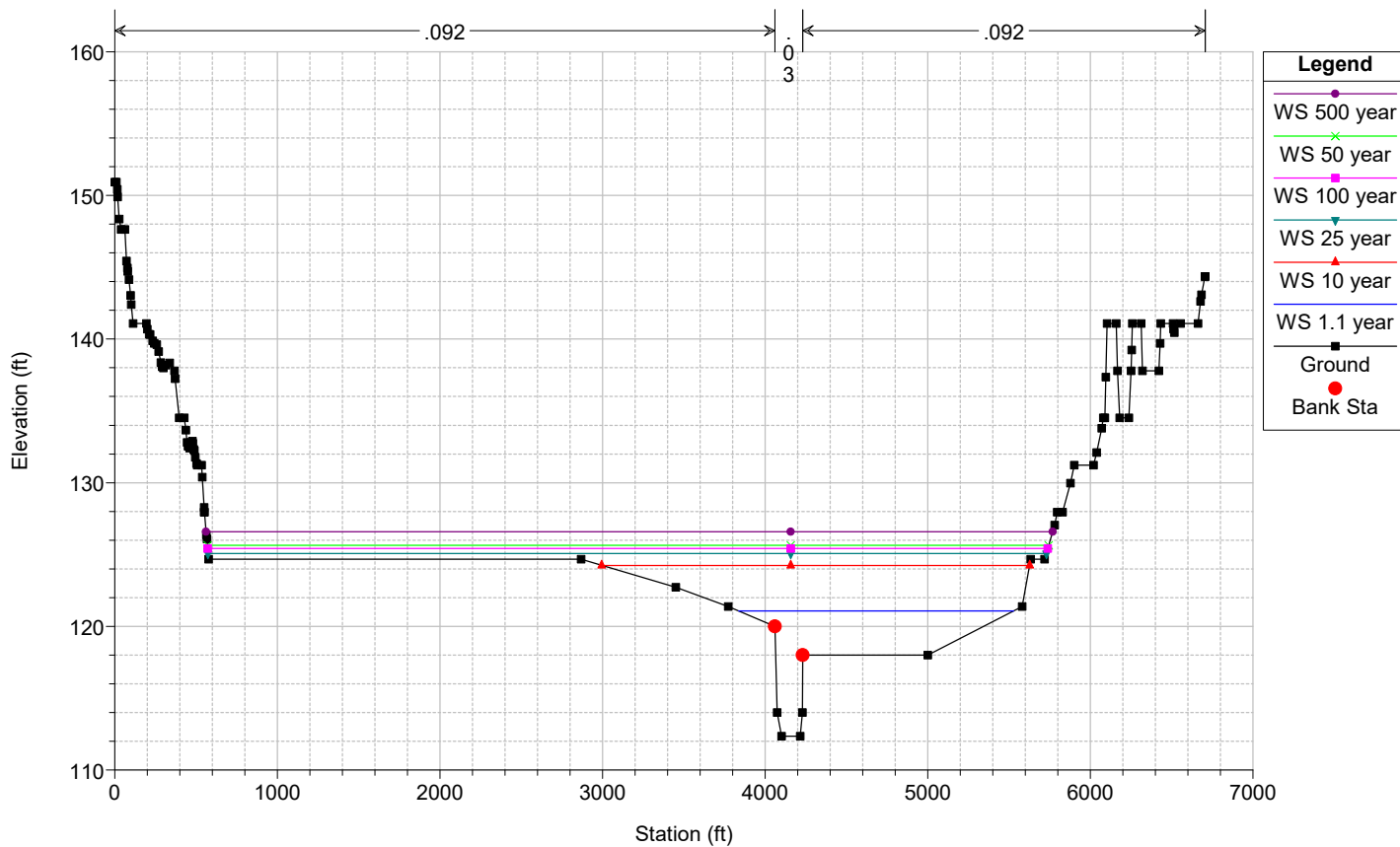
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

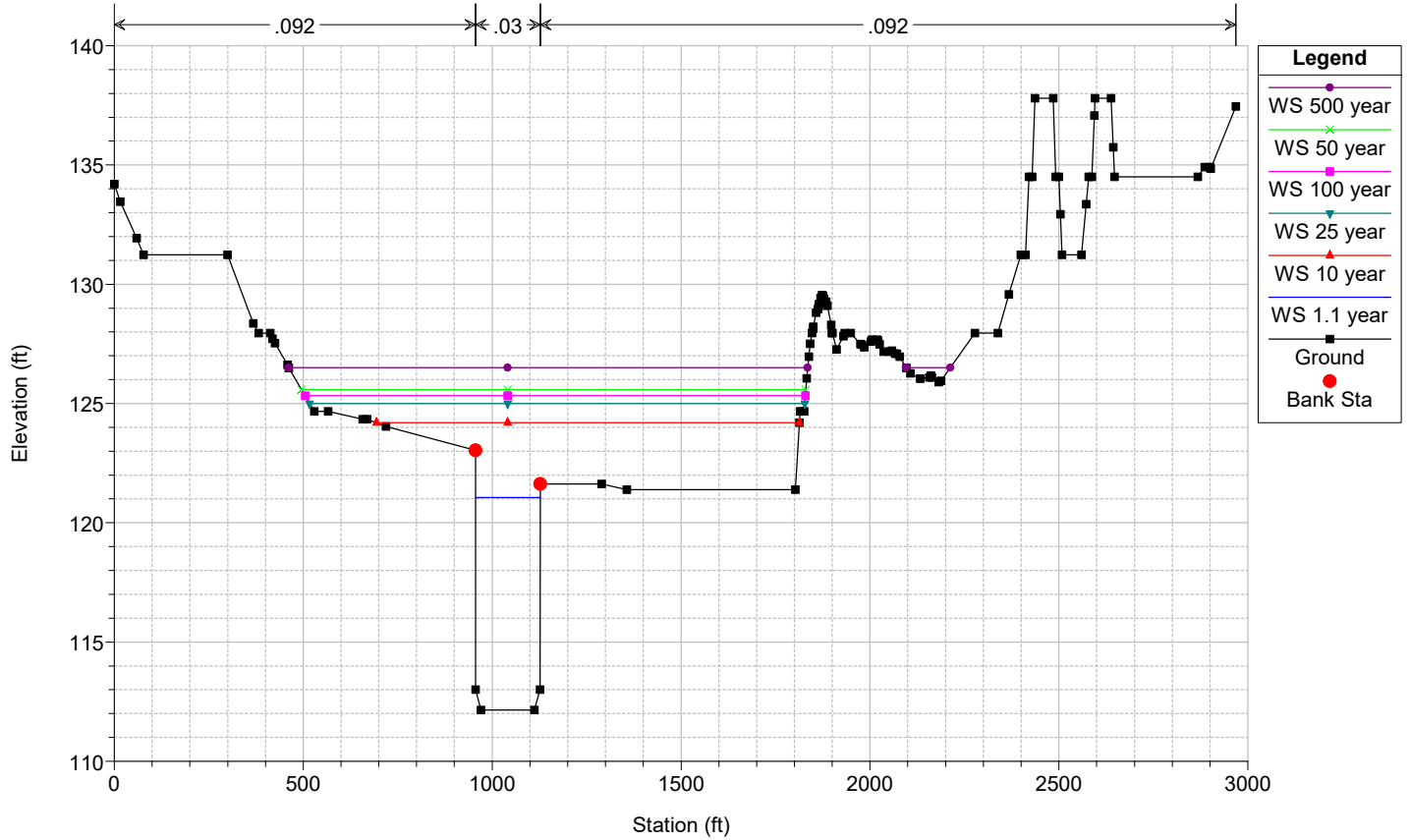
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

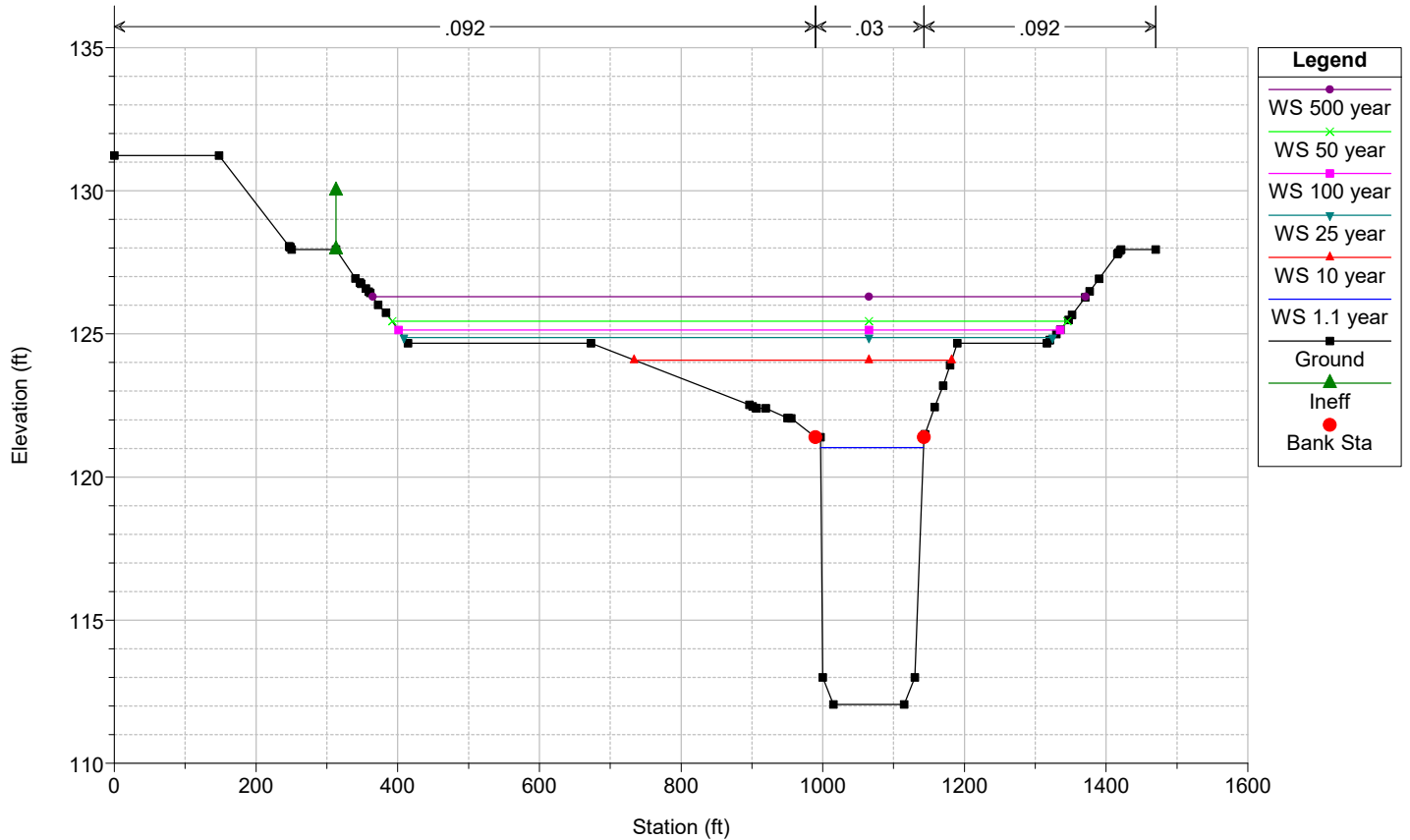
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

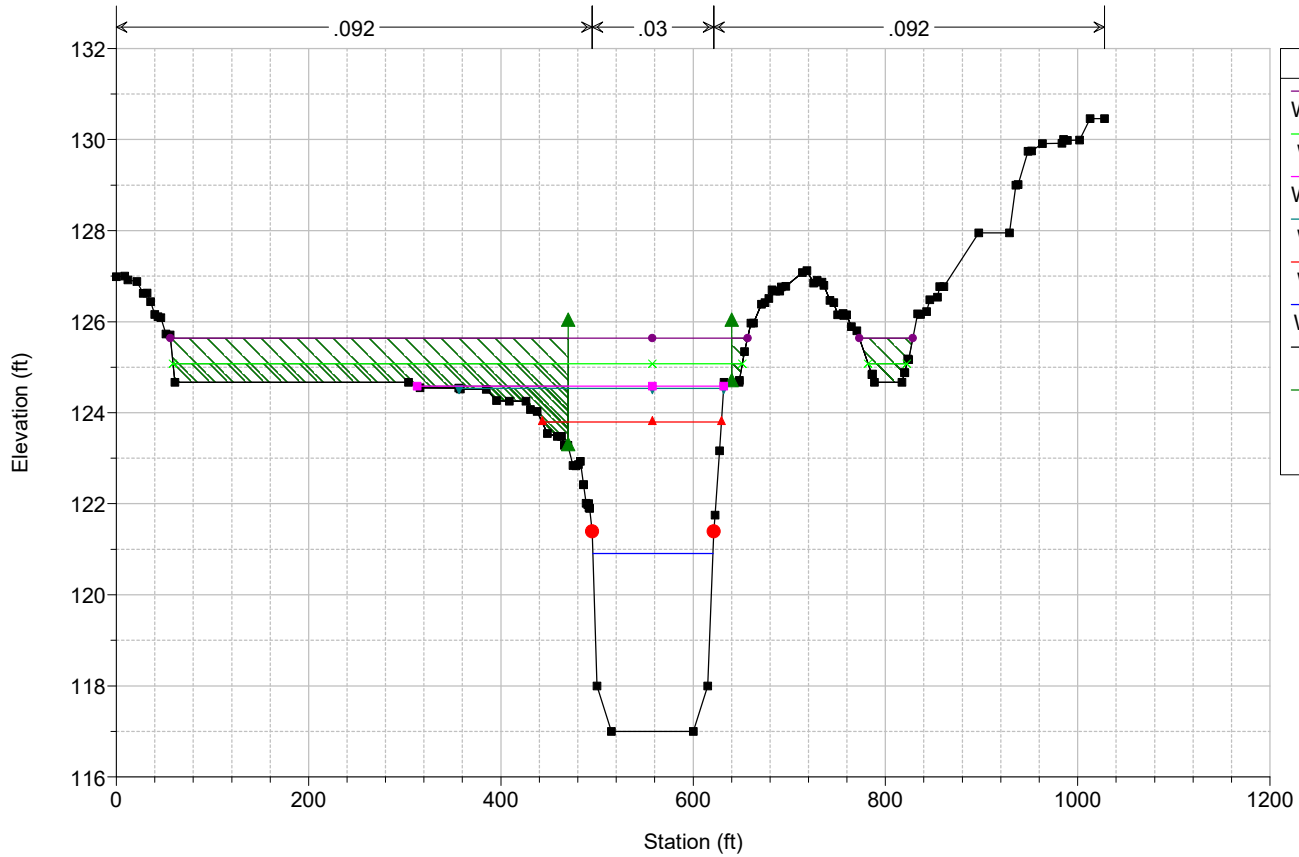
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

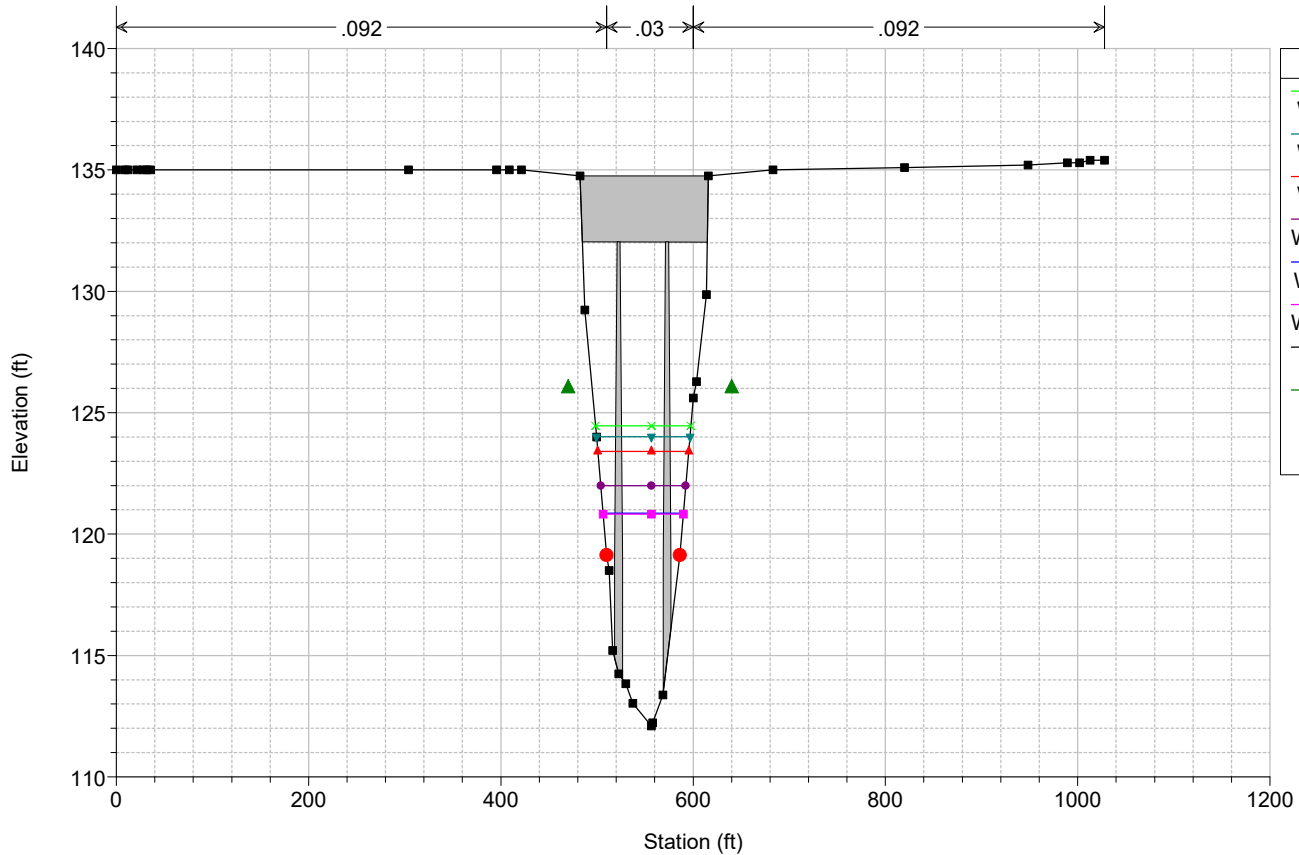
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

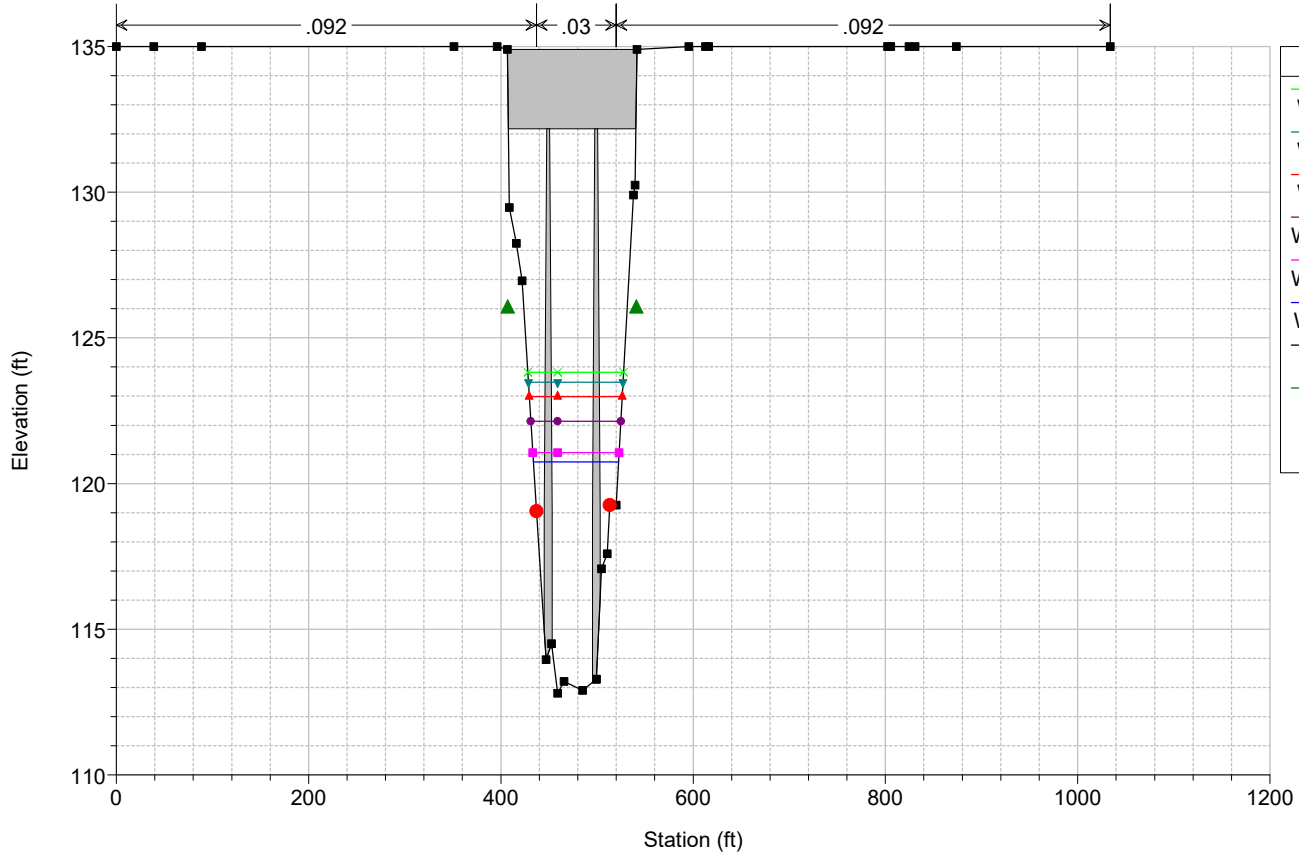
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

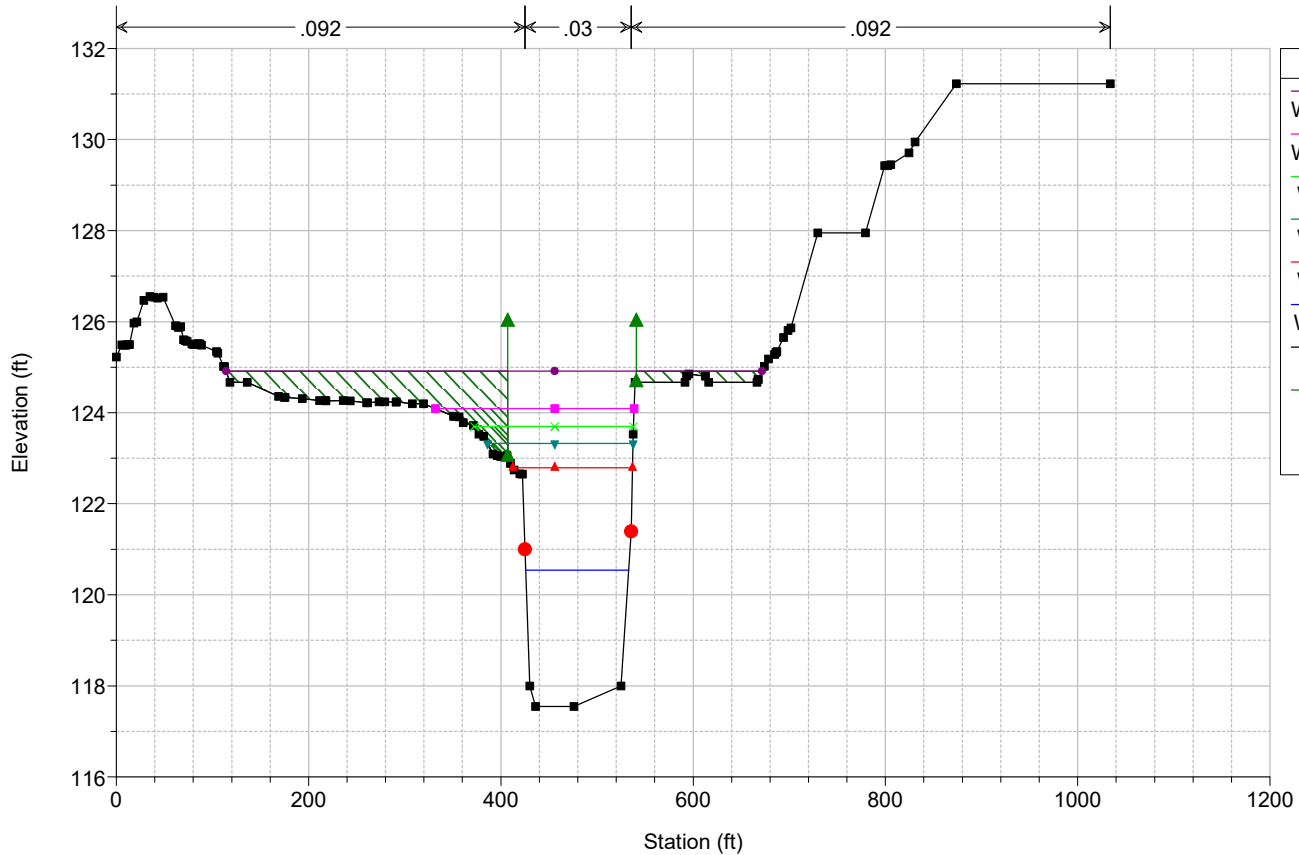
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

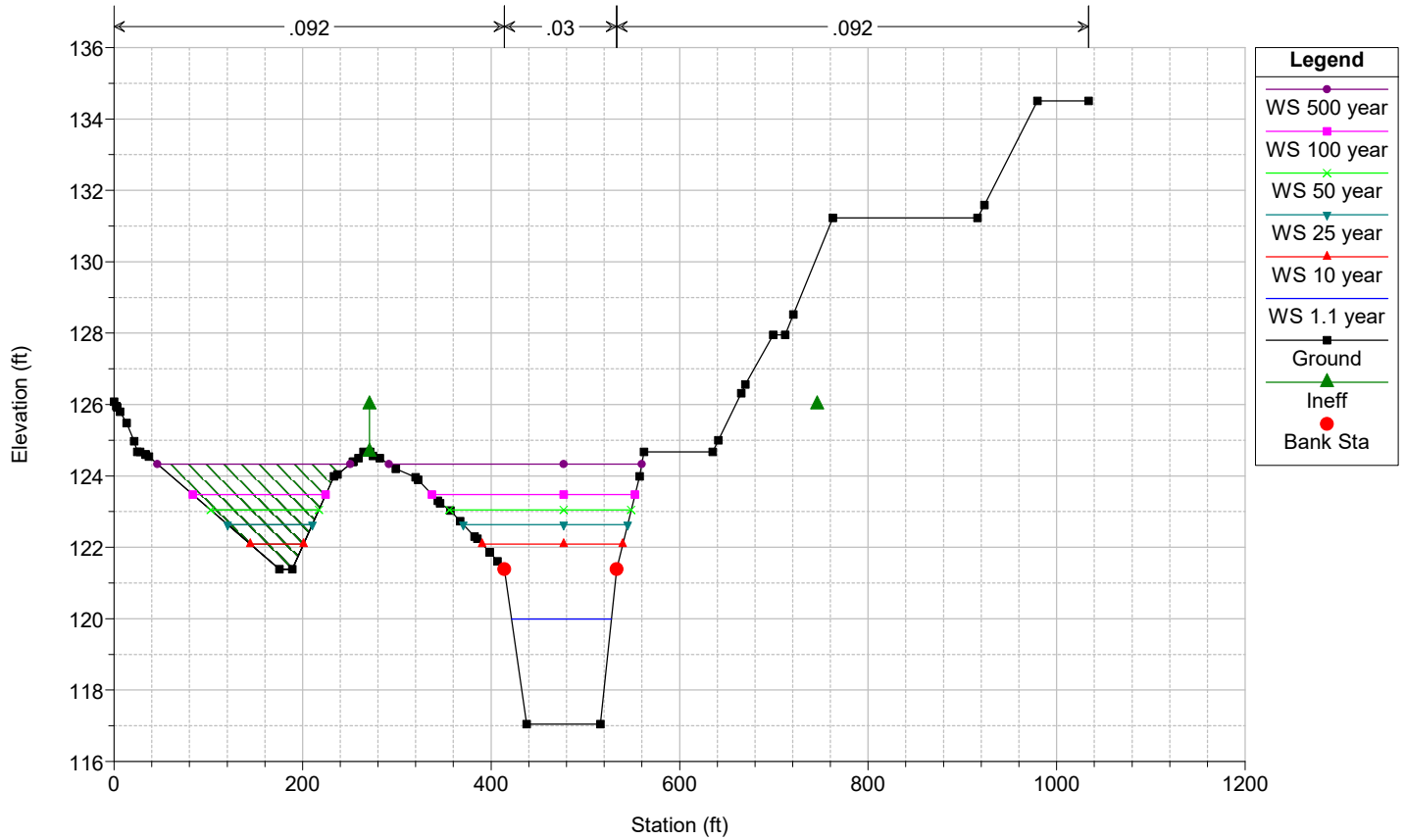
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

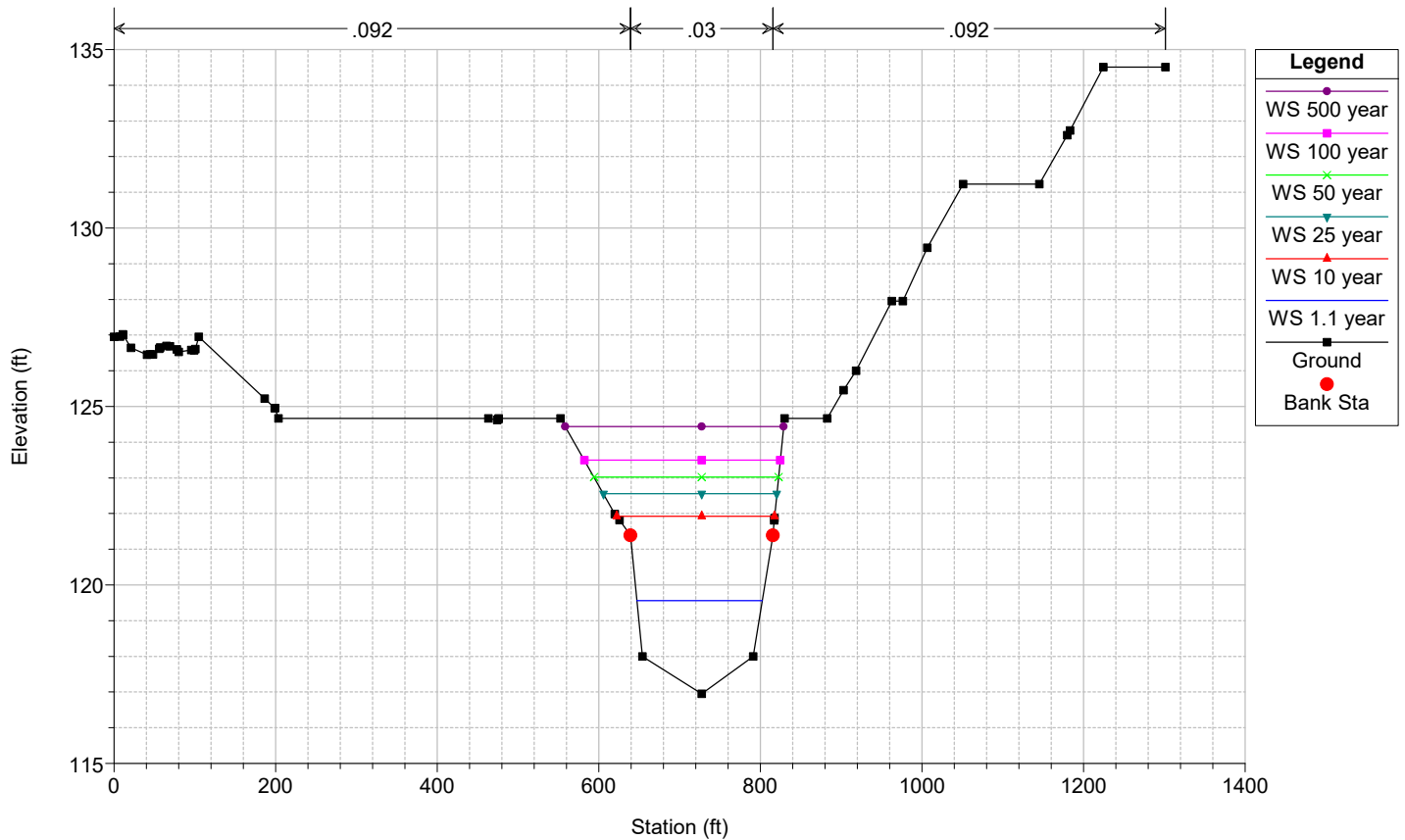
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

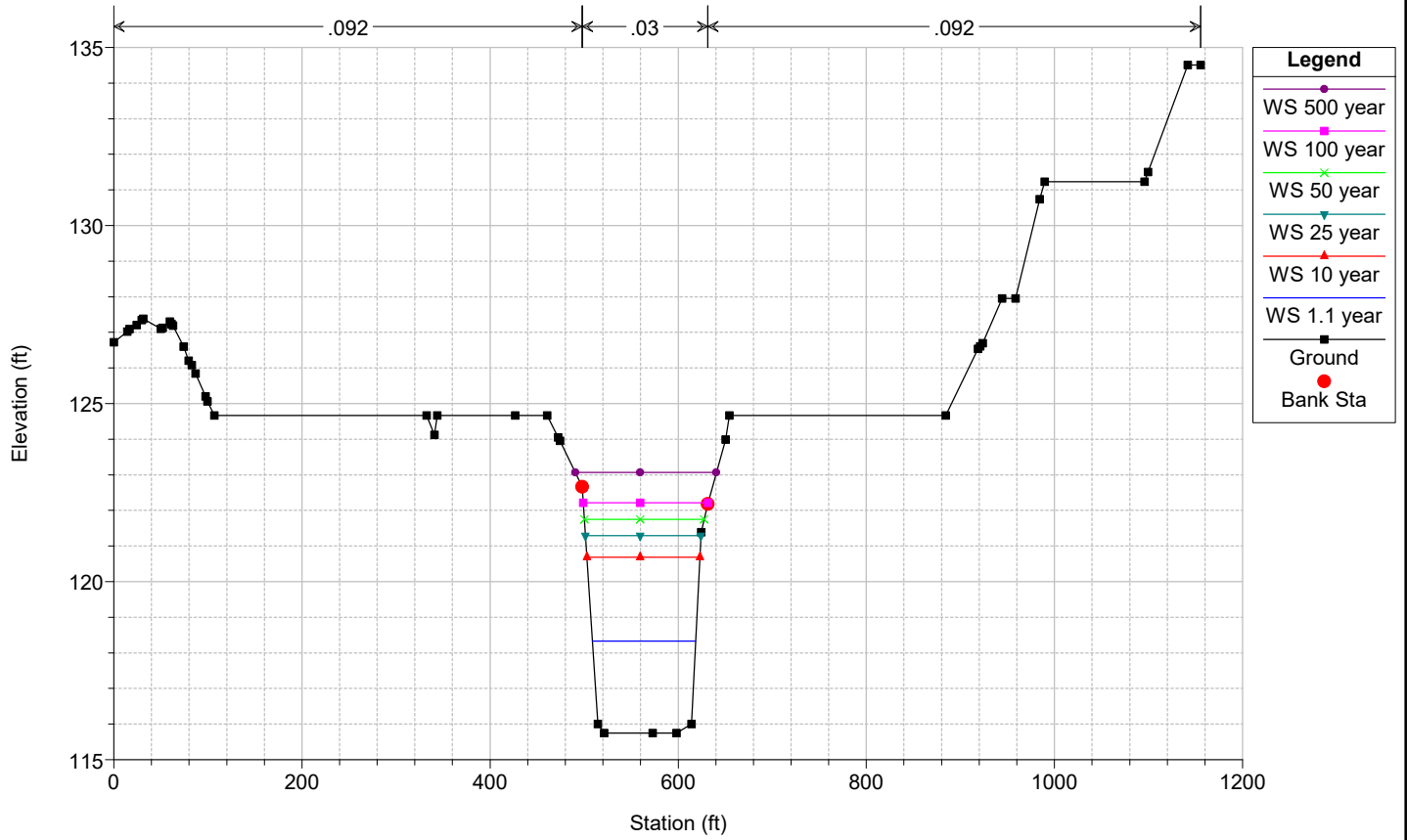
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Hampden Bridges Plan: Existing Condition MEDOT Flows

Geom: Hampden Bridges Existing

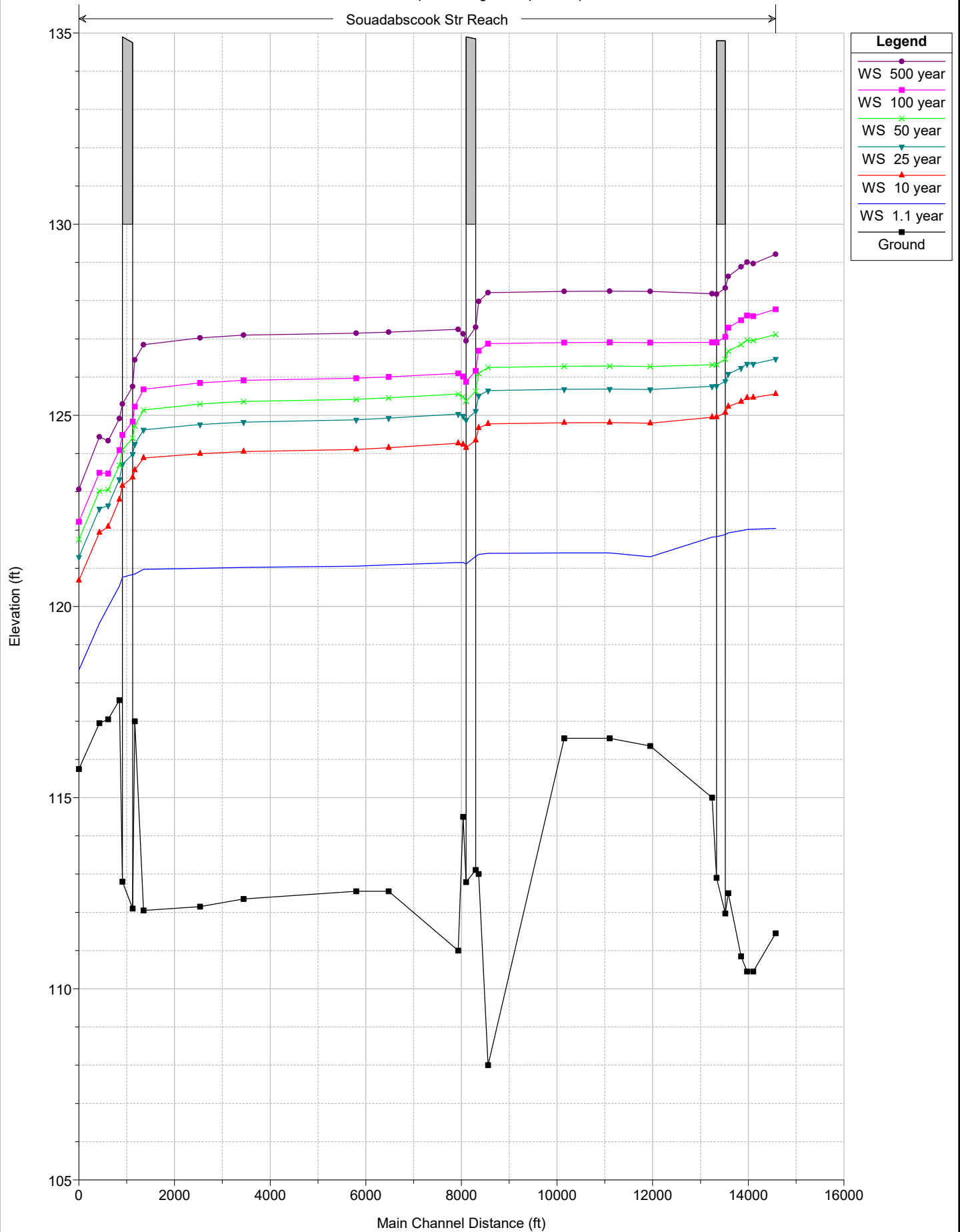
RS = 26951.26



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

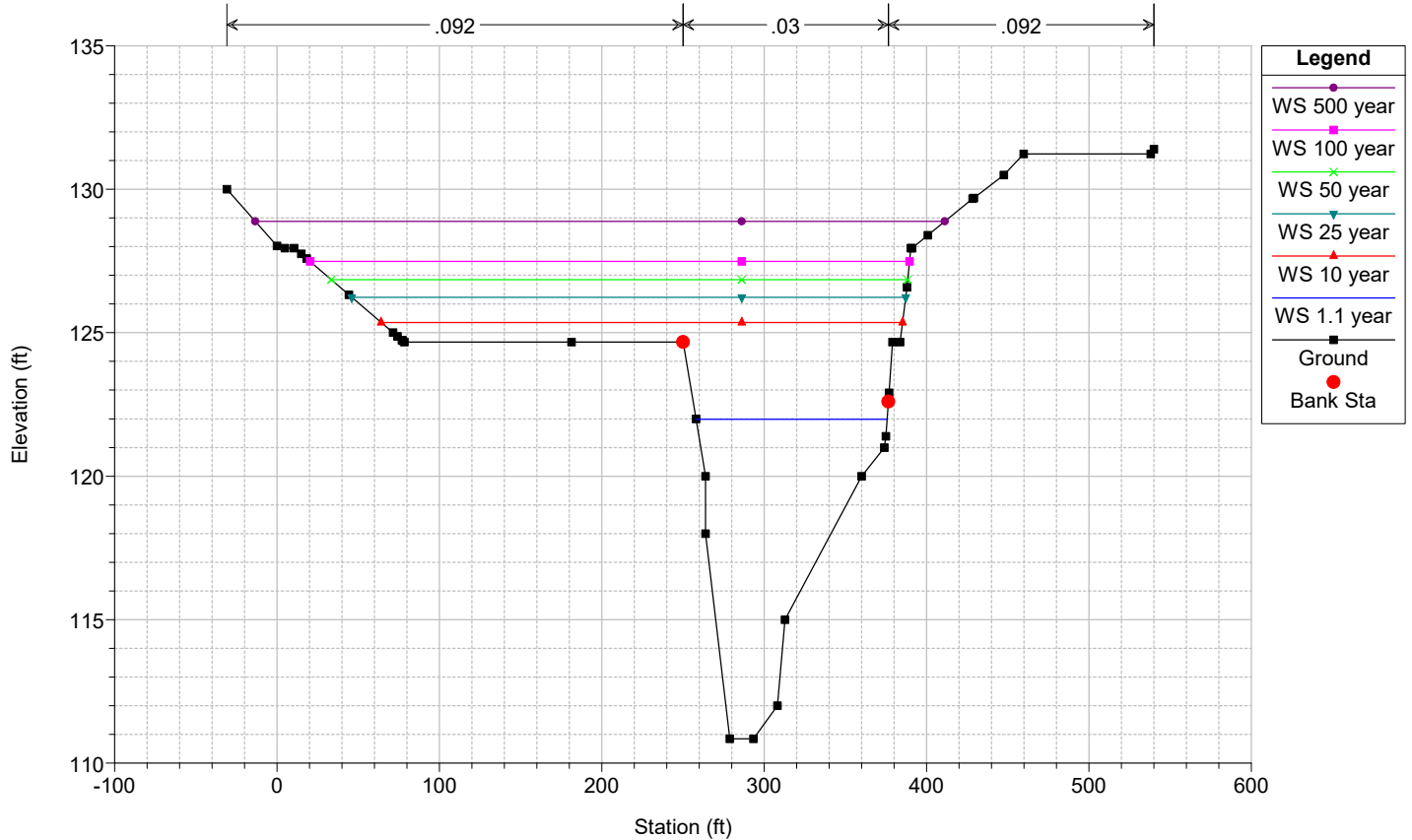
Soudabascook Str Reach



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

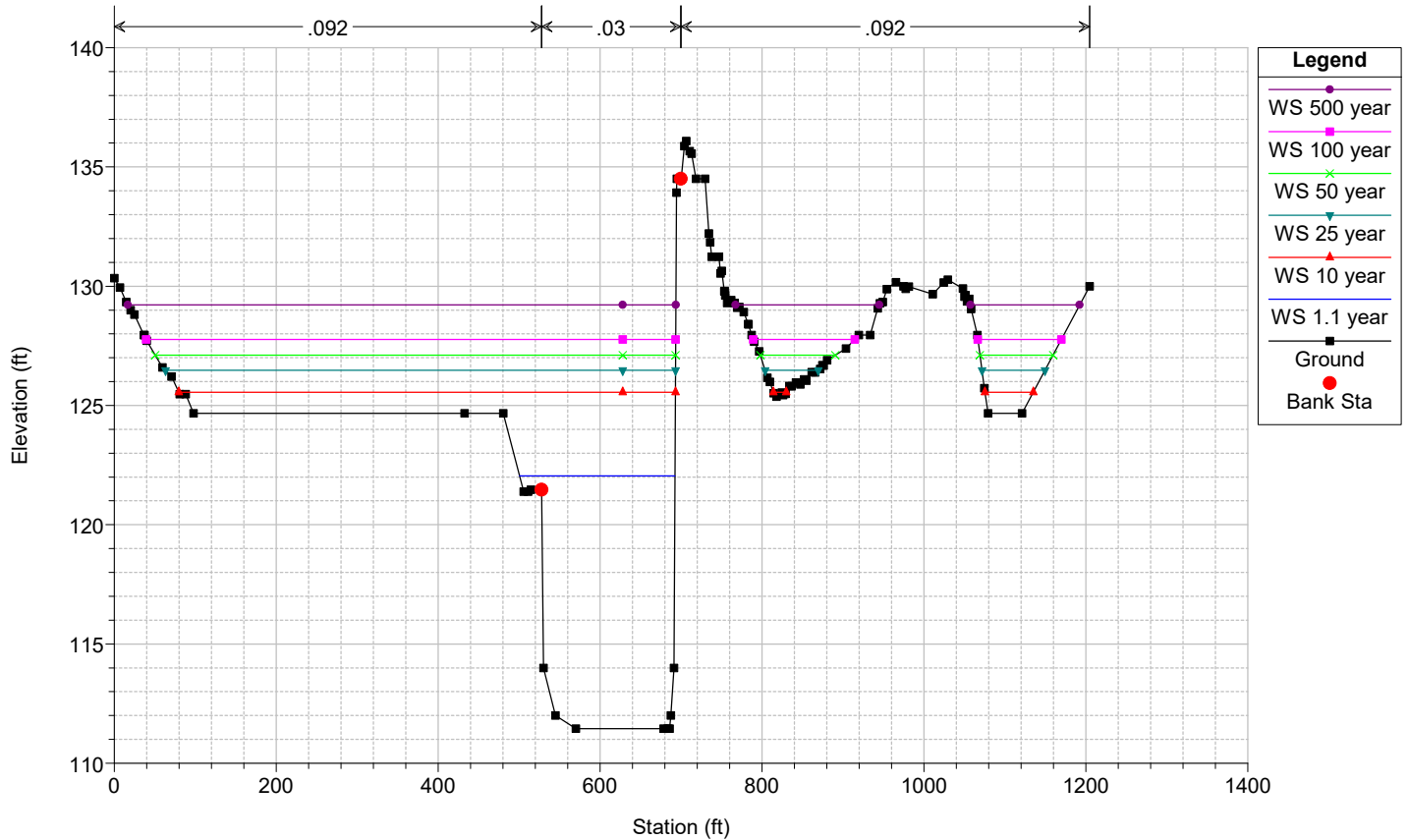
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

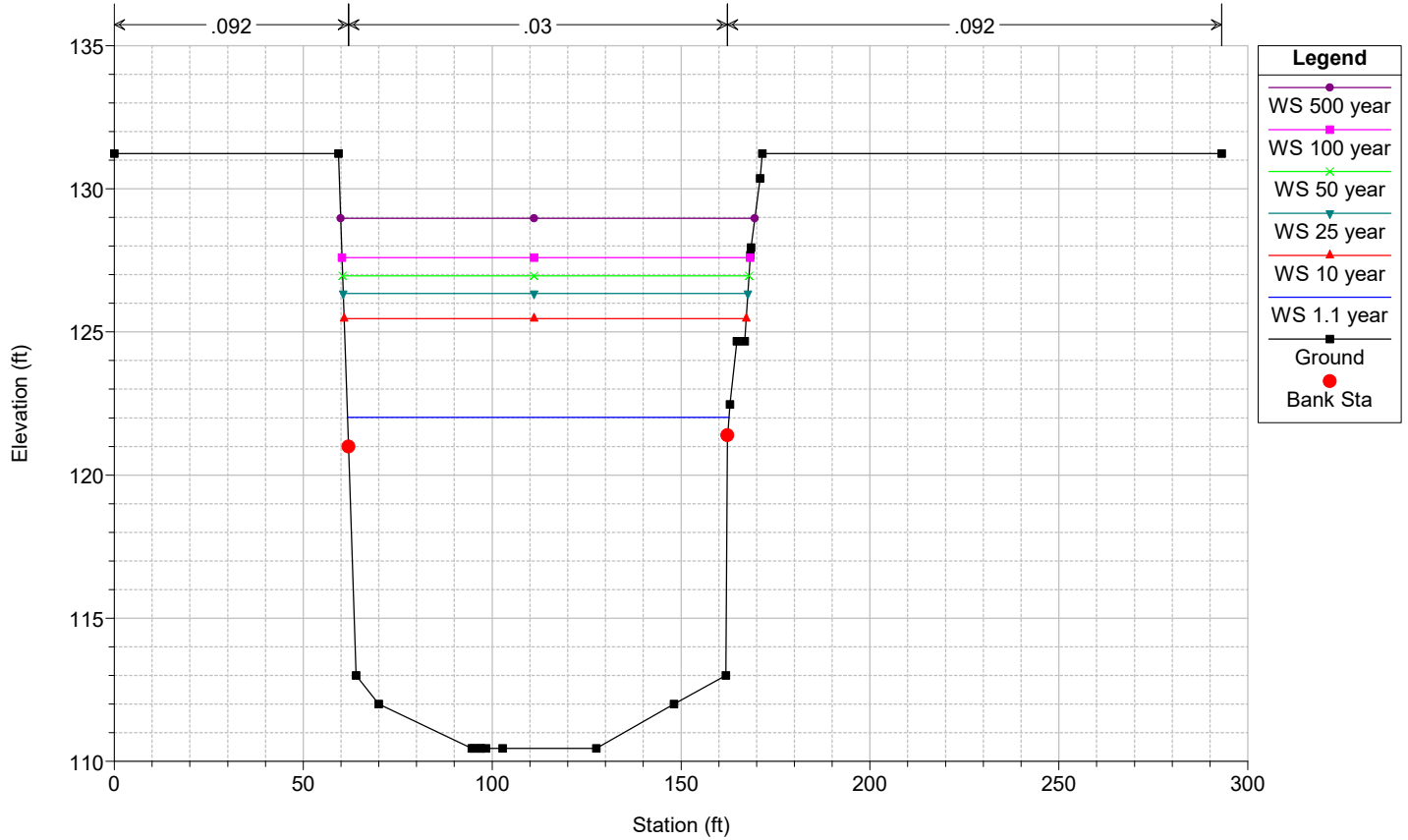
RS = 41522.56



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

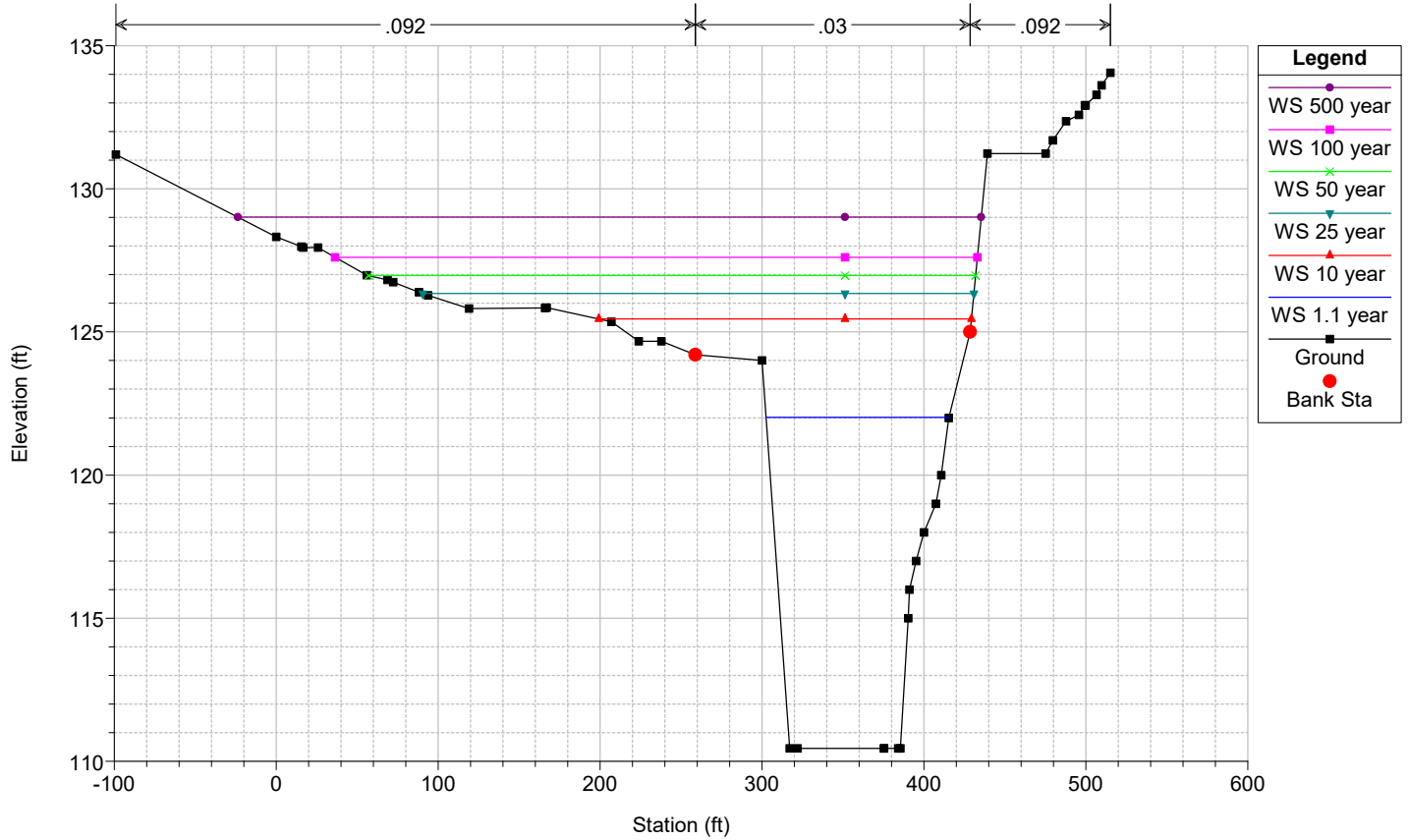
RS = 41055.75



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

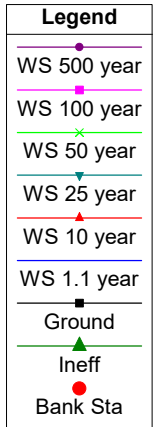
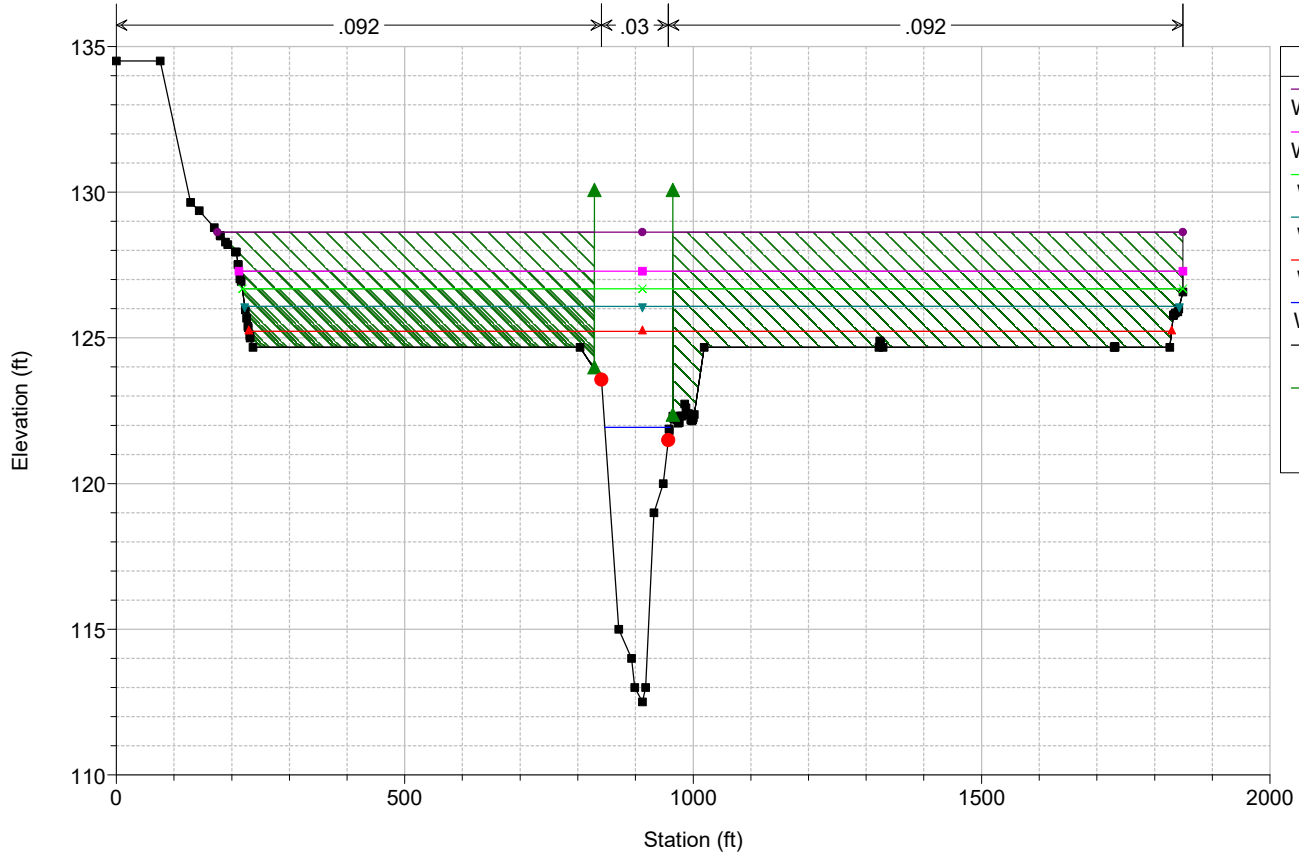
RS = 40924.49



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

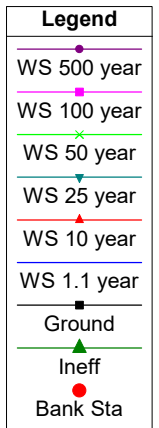
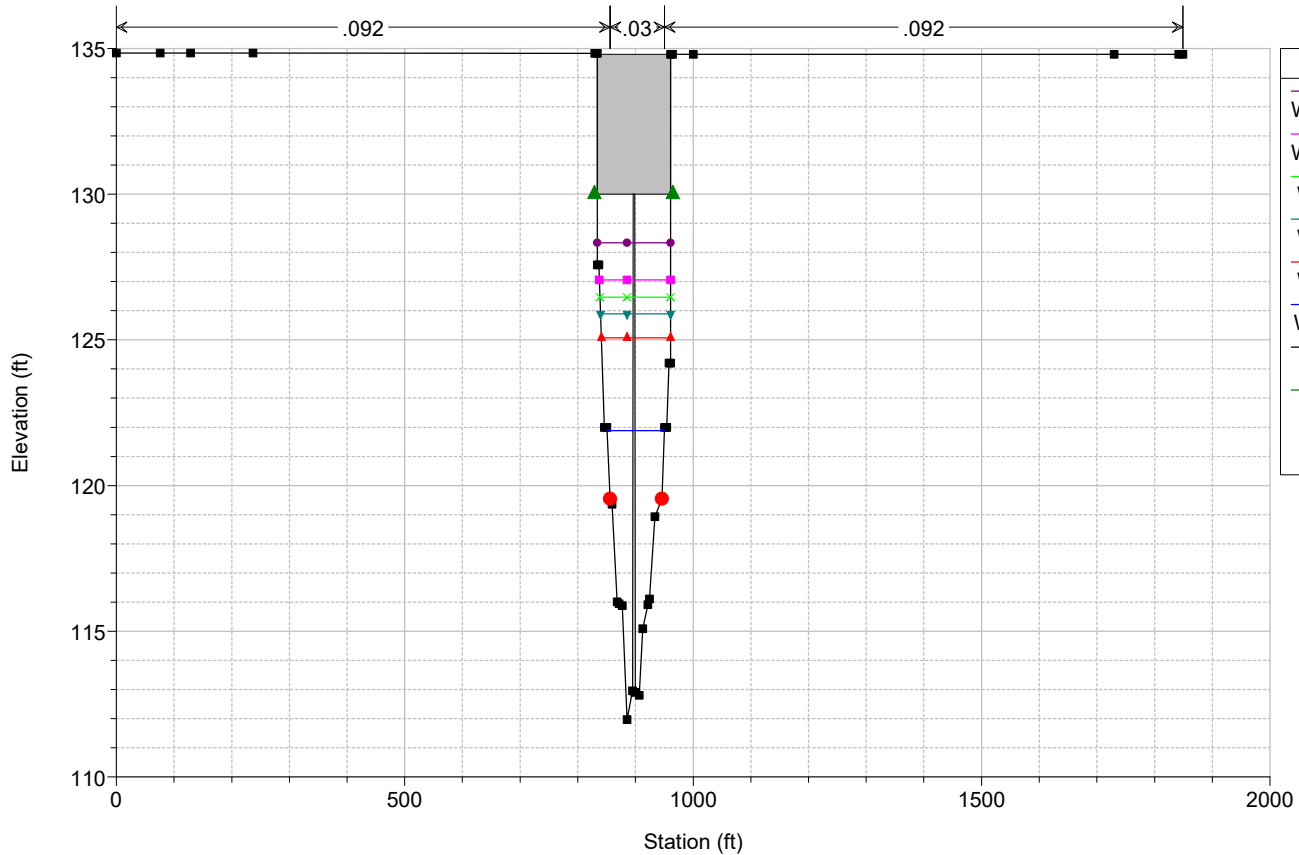
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

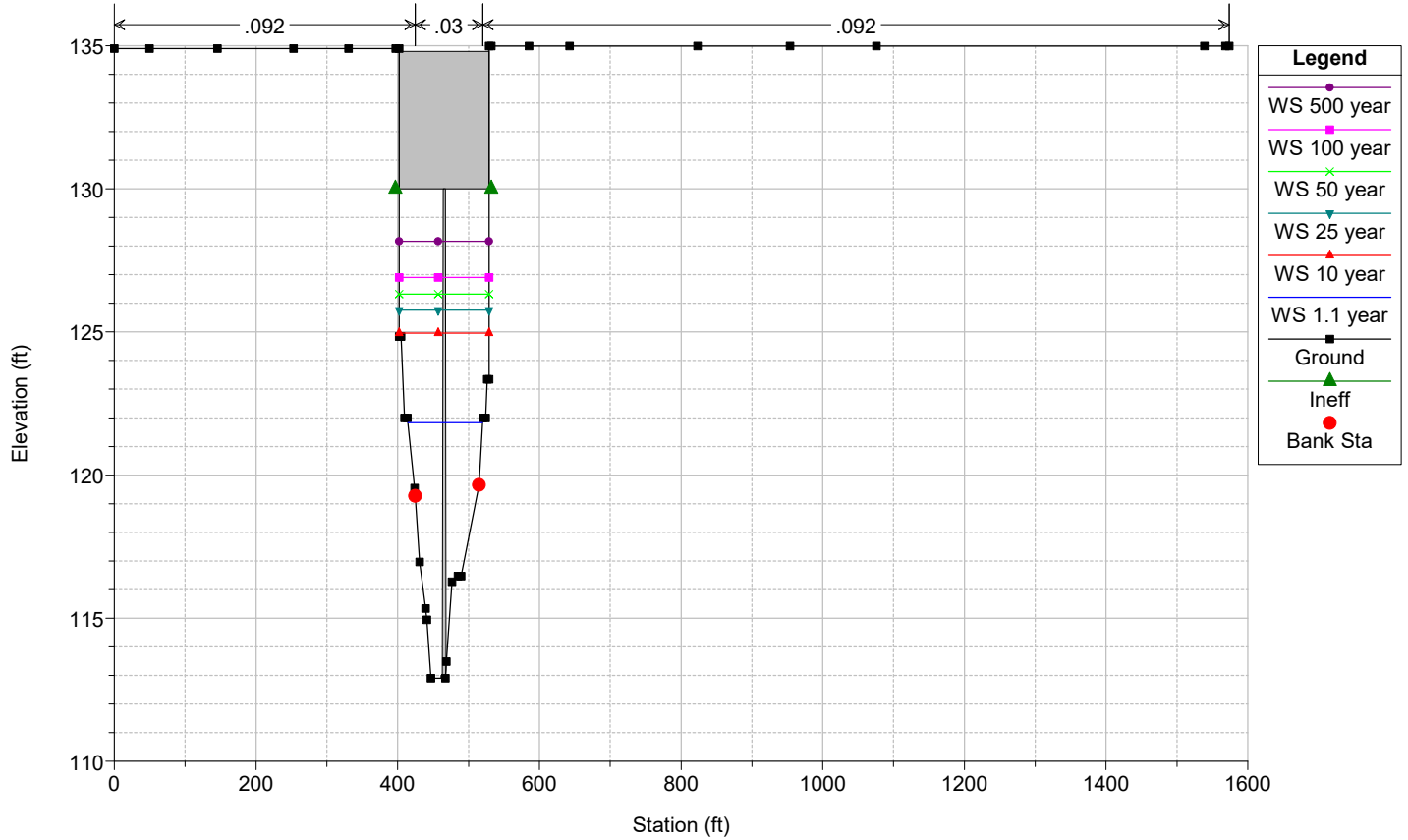
RS = 40346 BR



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

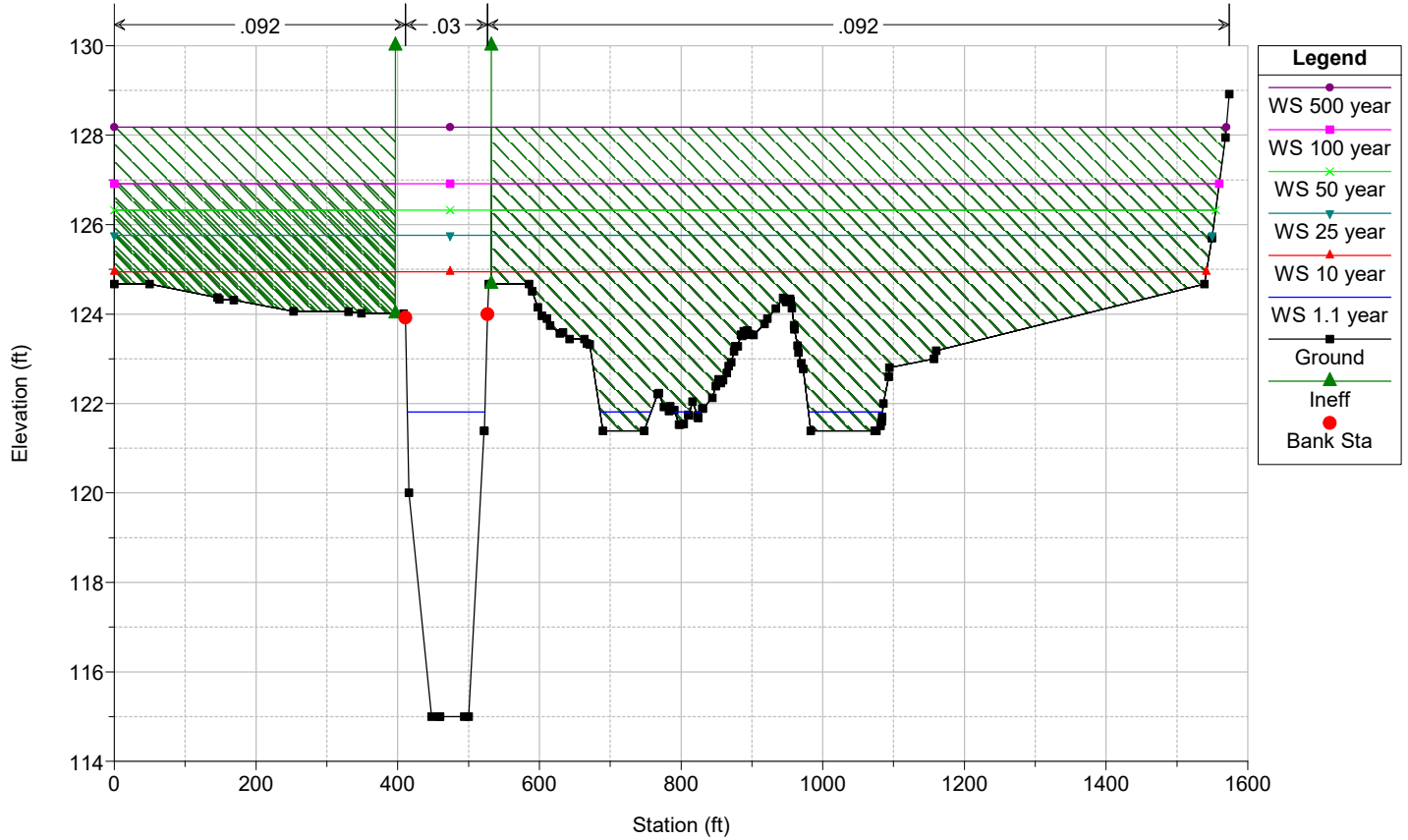
RS = 40346 BR



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

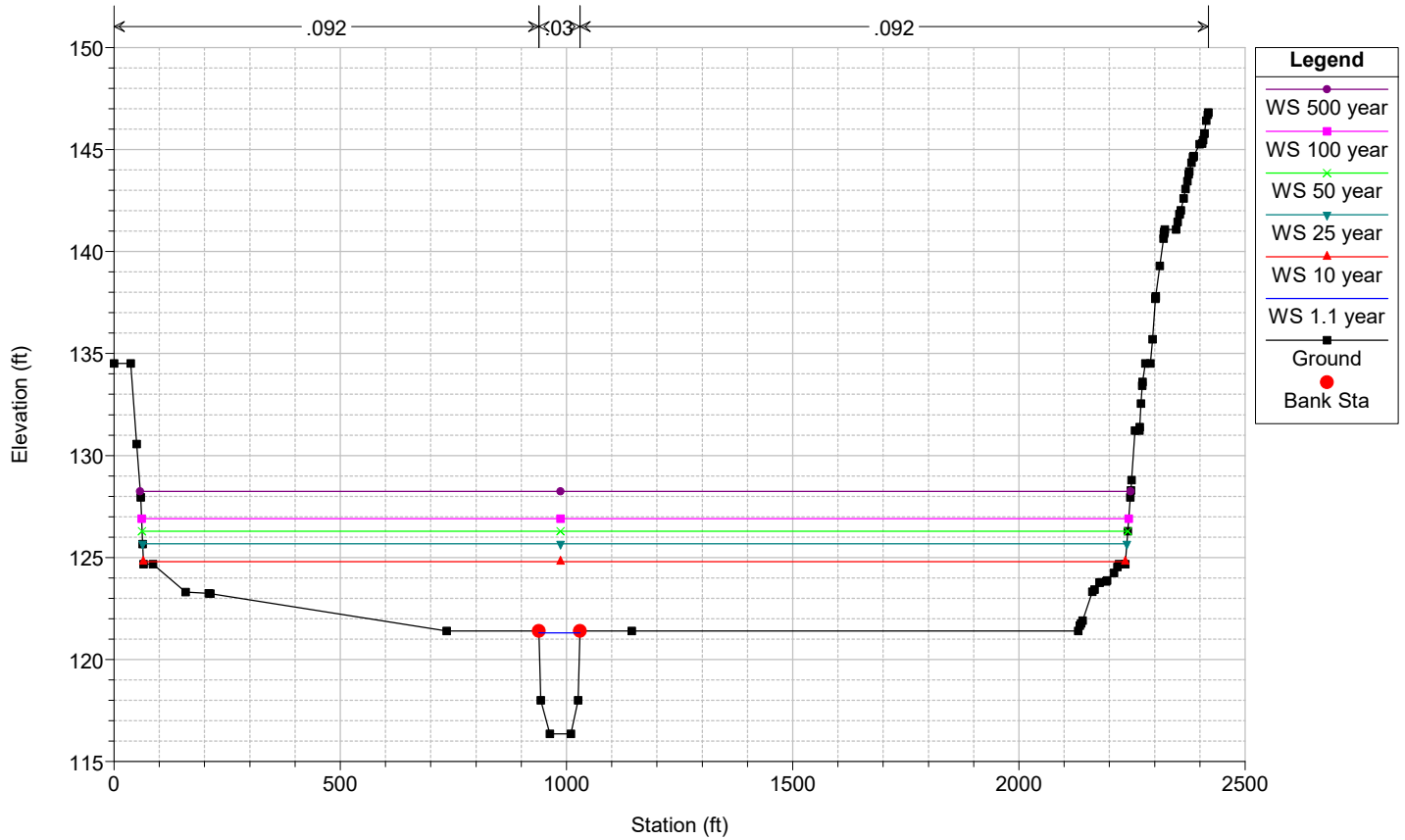
RS = 40193.72



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

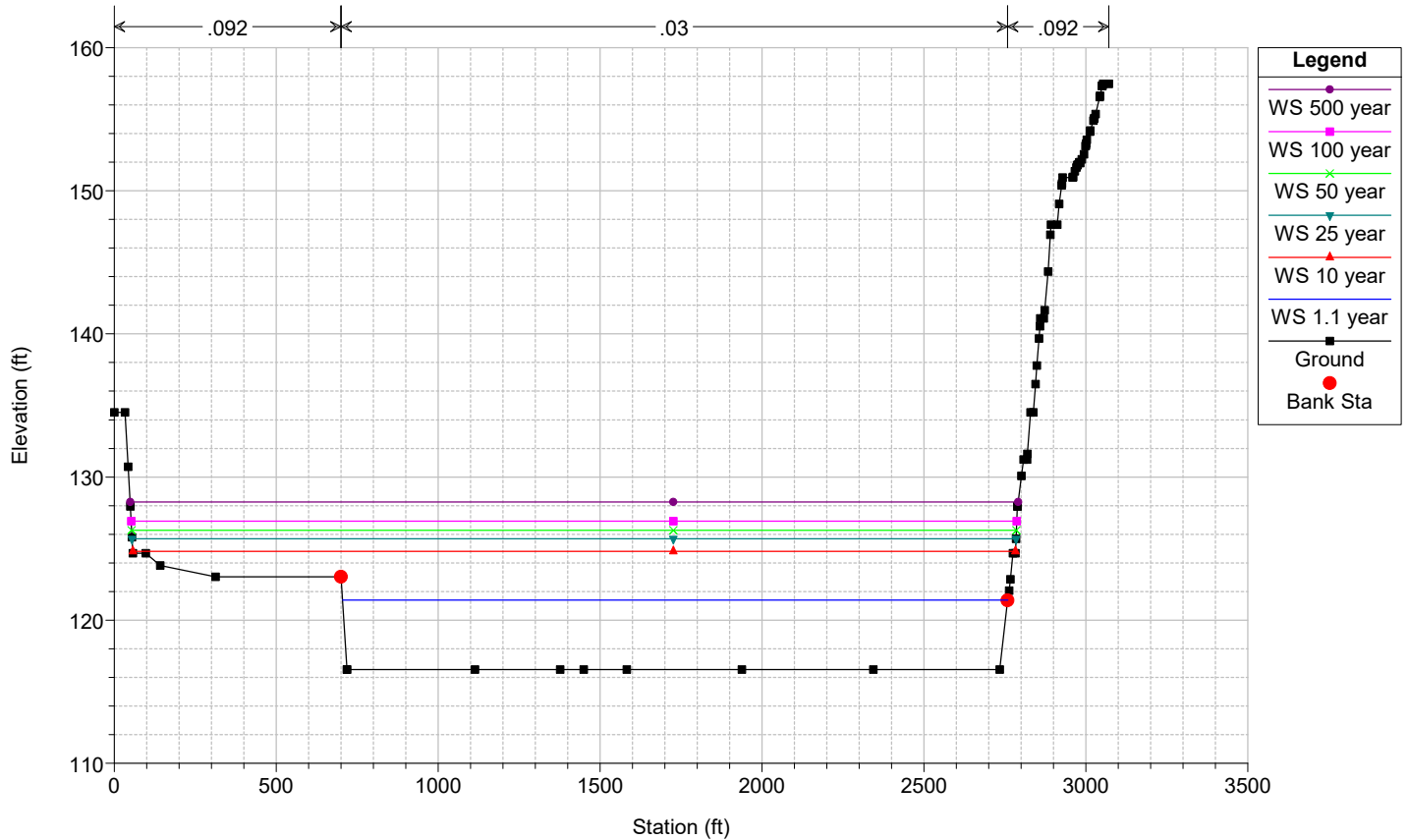
RS = 38900.00



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

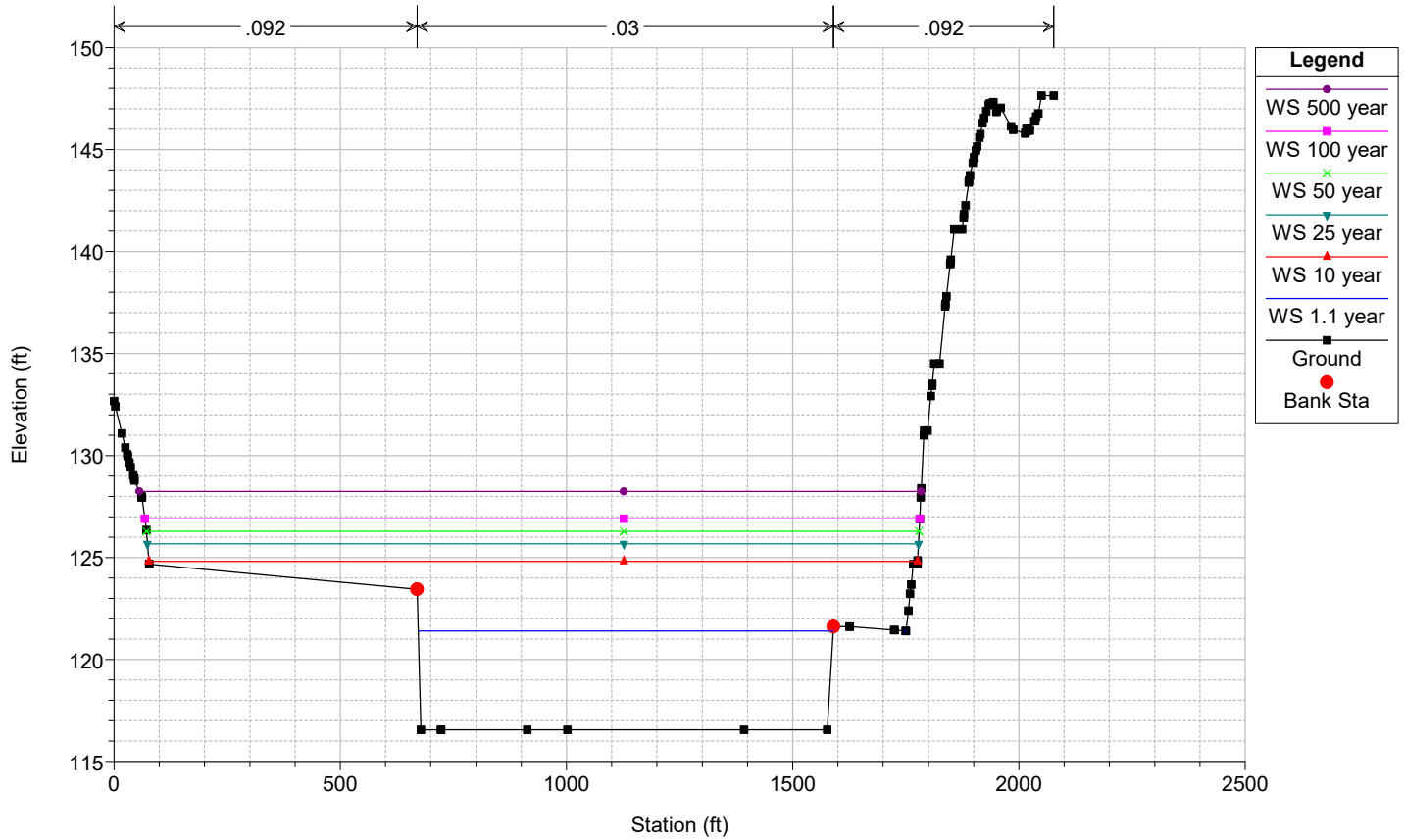
RS = 38050.00



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

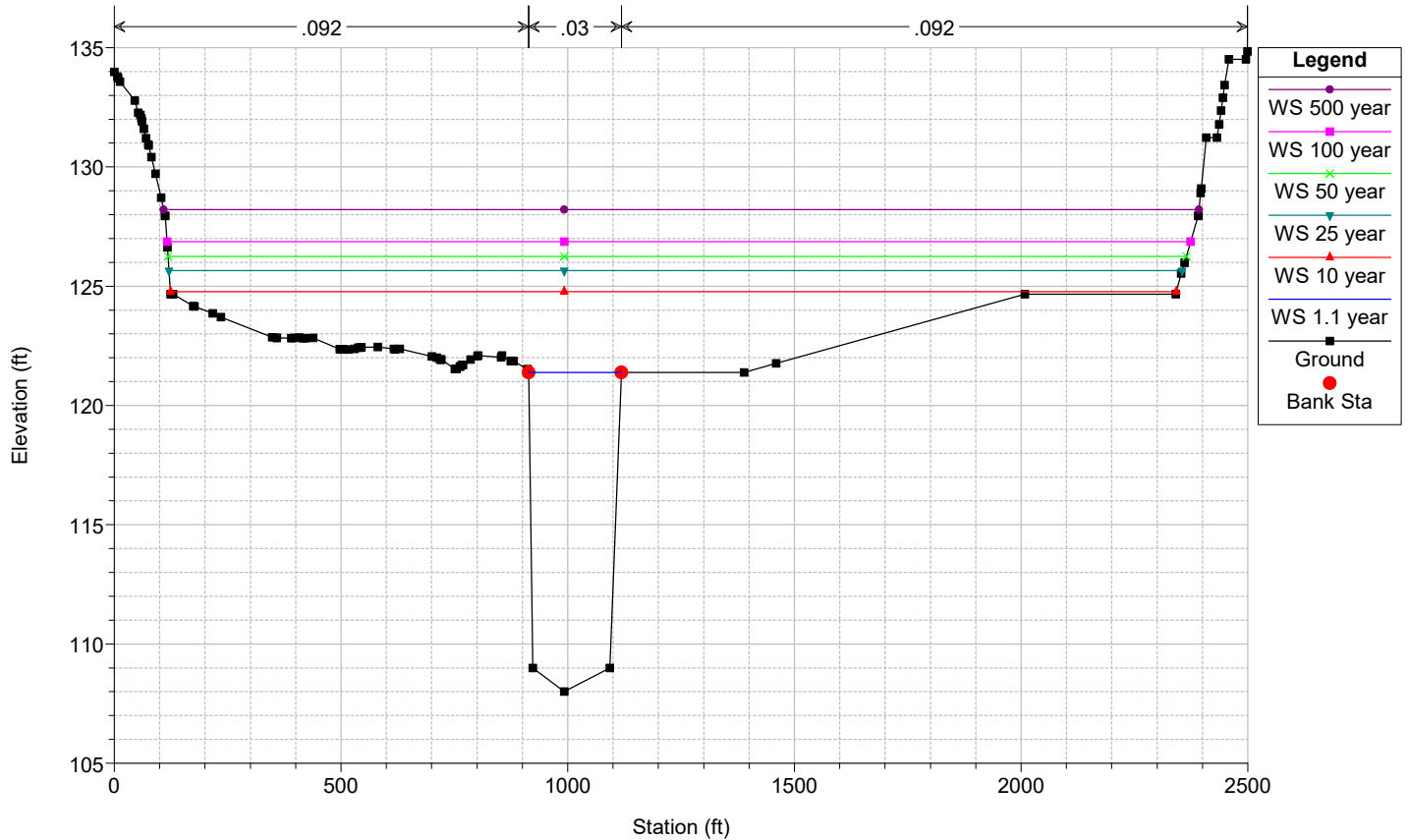
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

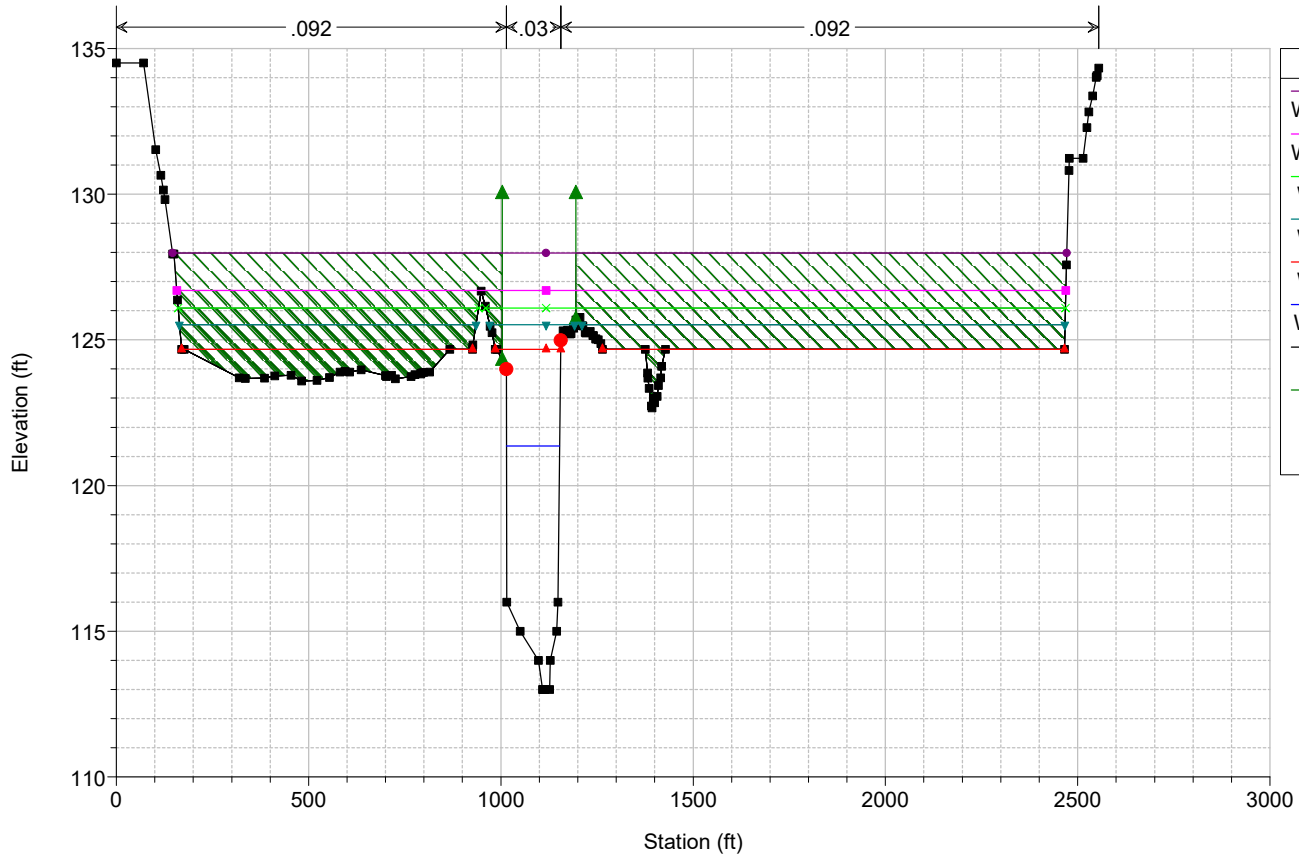
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

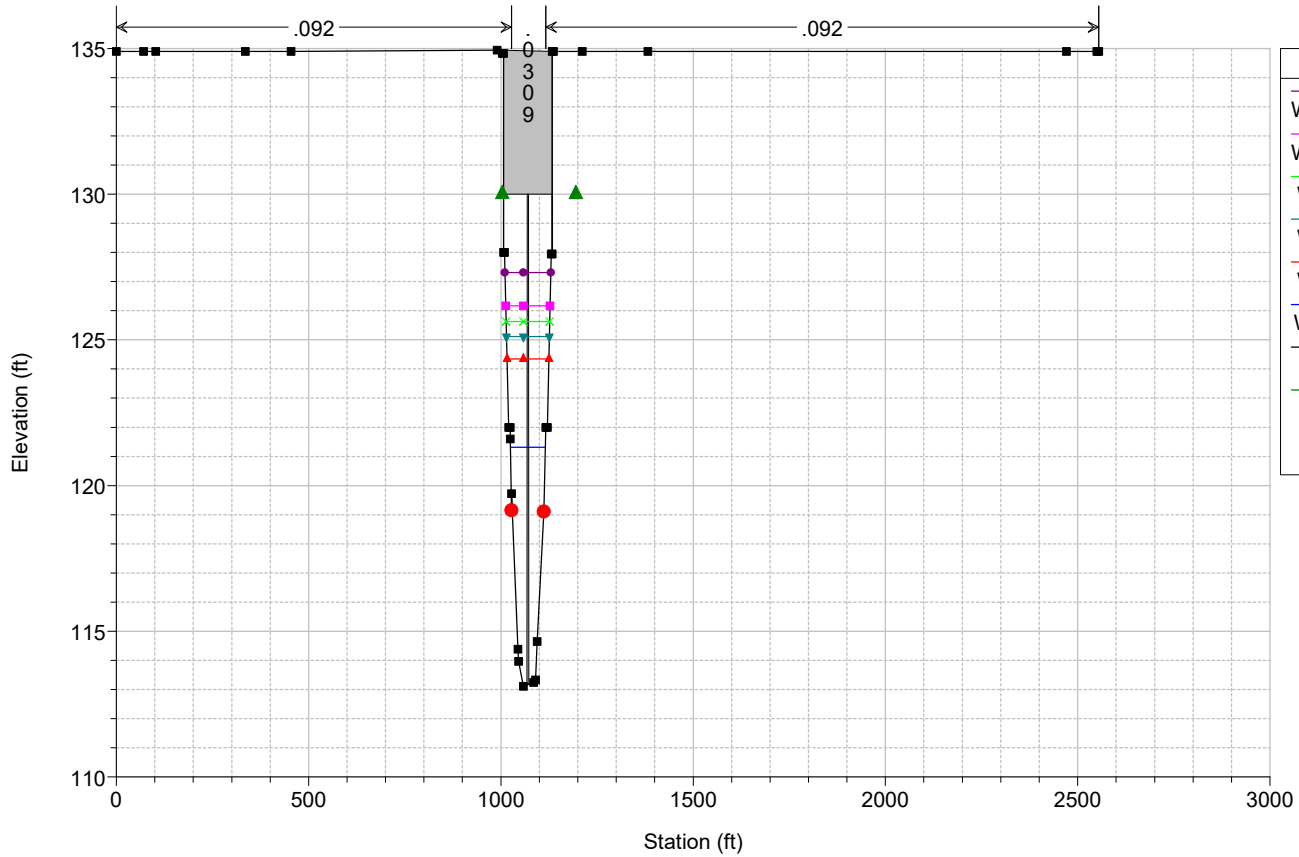
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

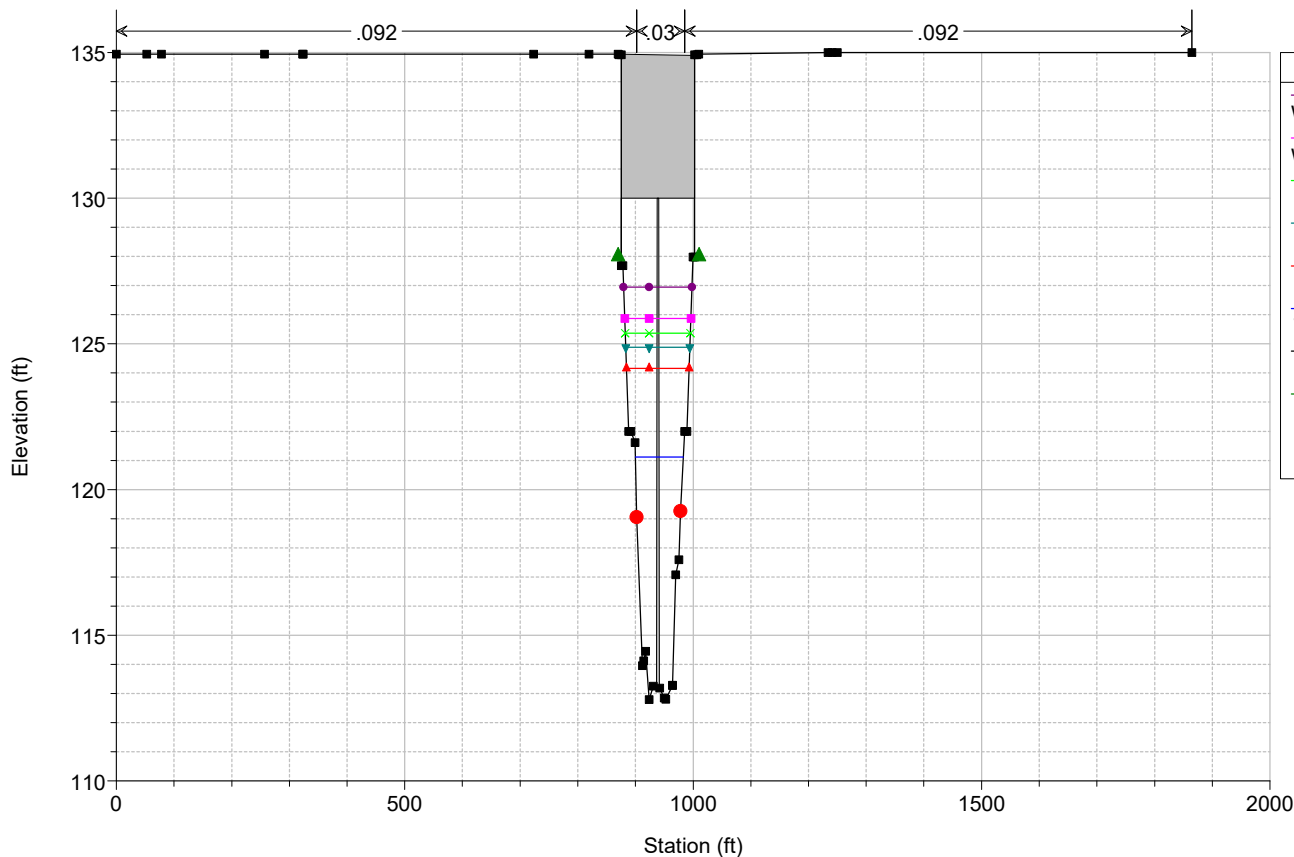
RS = 35151 BR



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

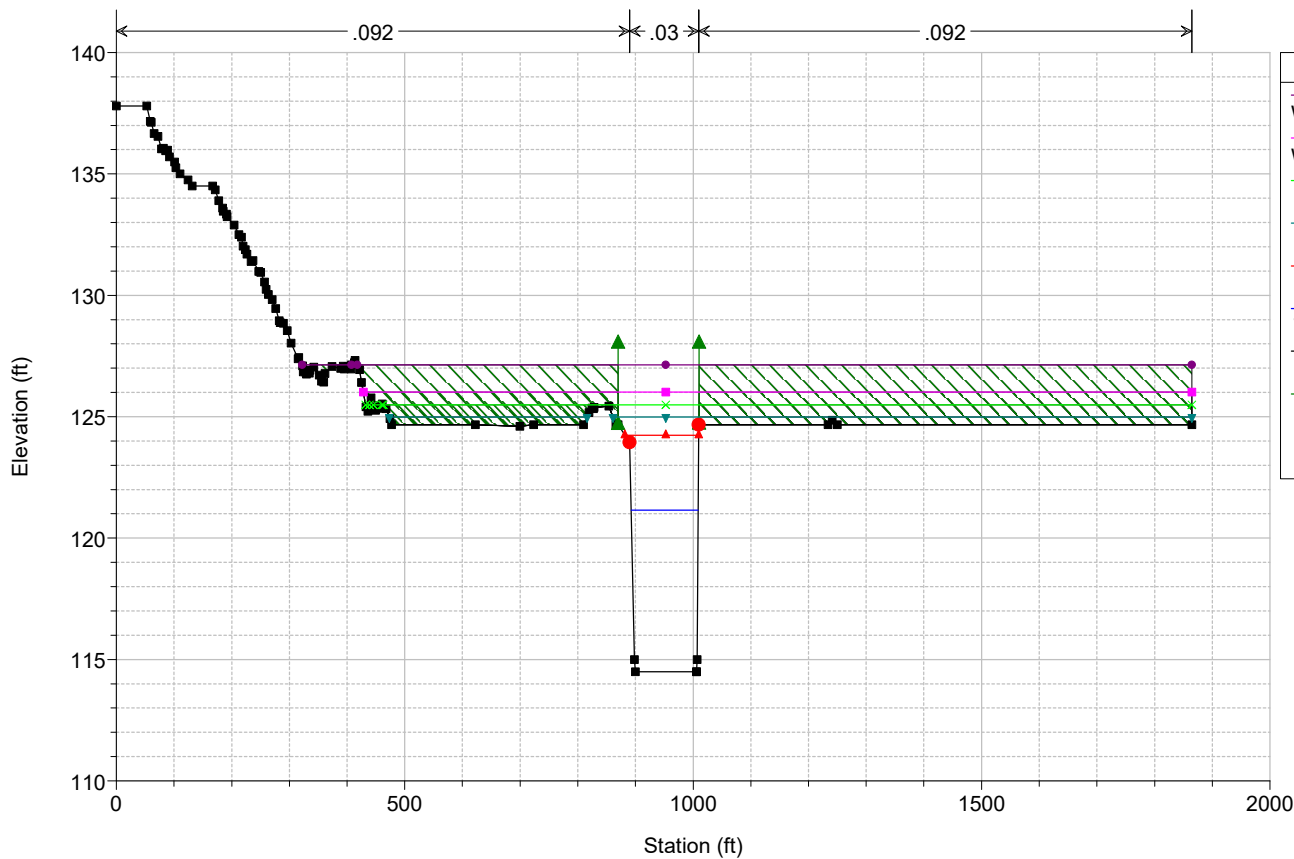
RS = 35151 BR



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

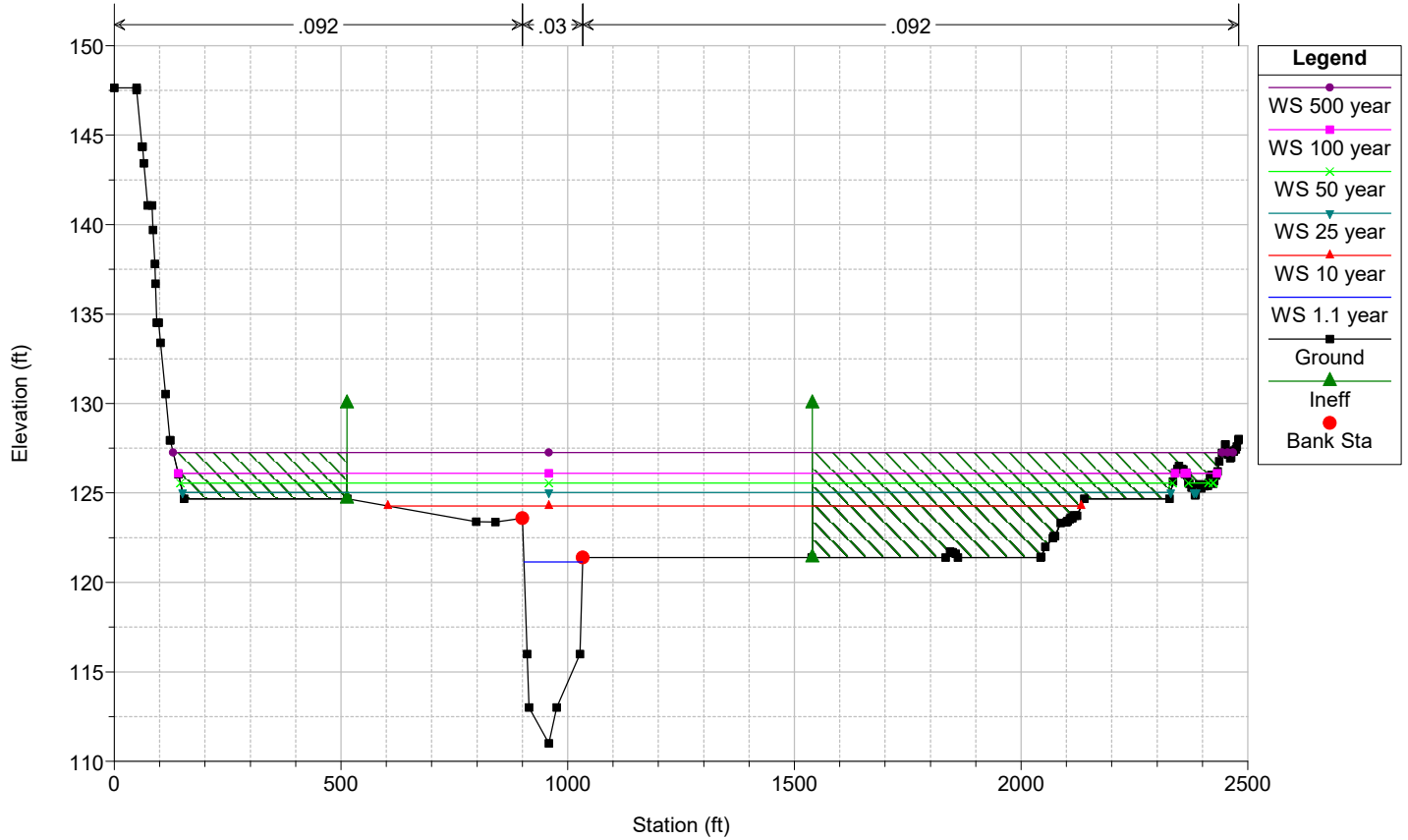
RS = 34987.11



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

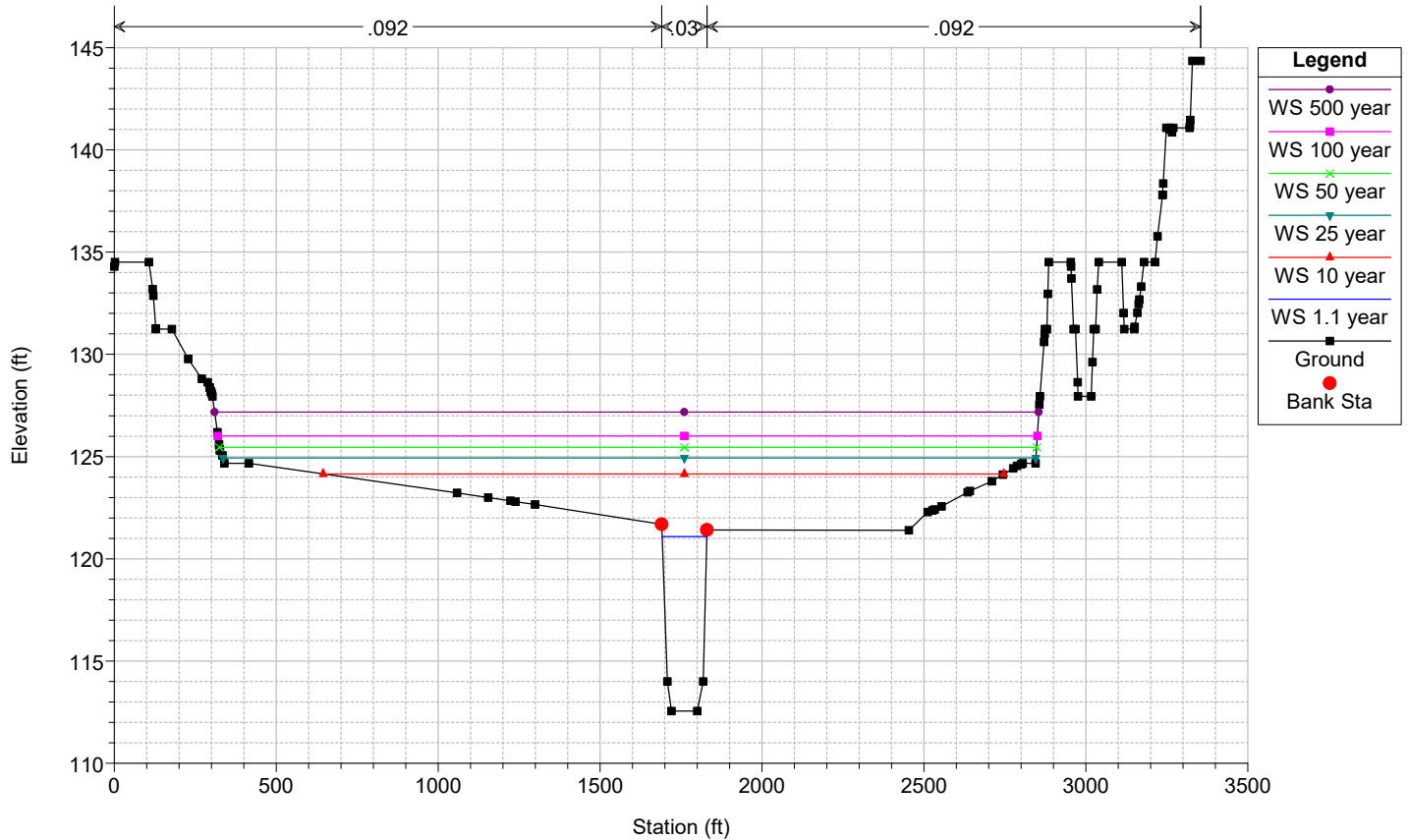
RS = 34886.44



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

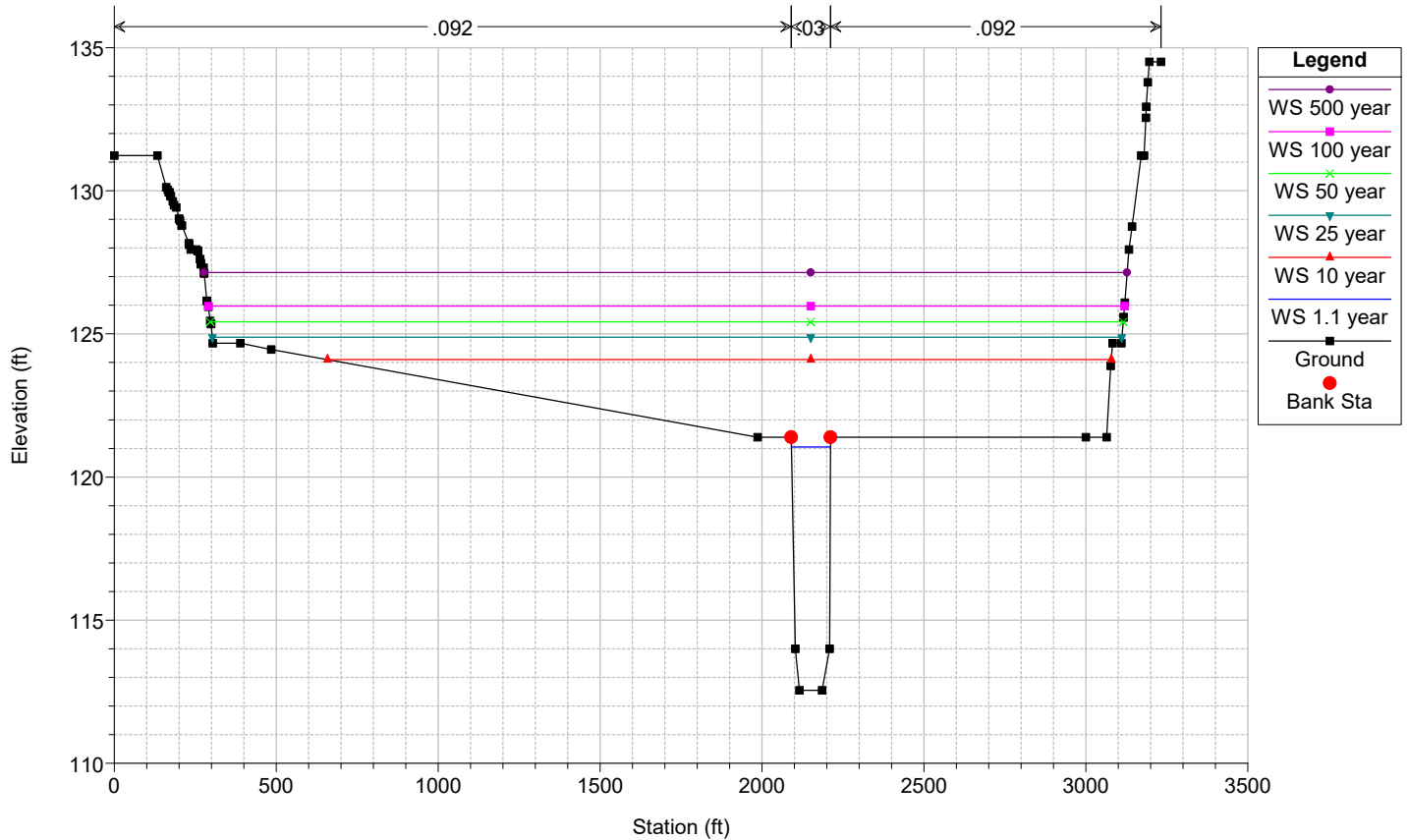
RS = 33430.00



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

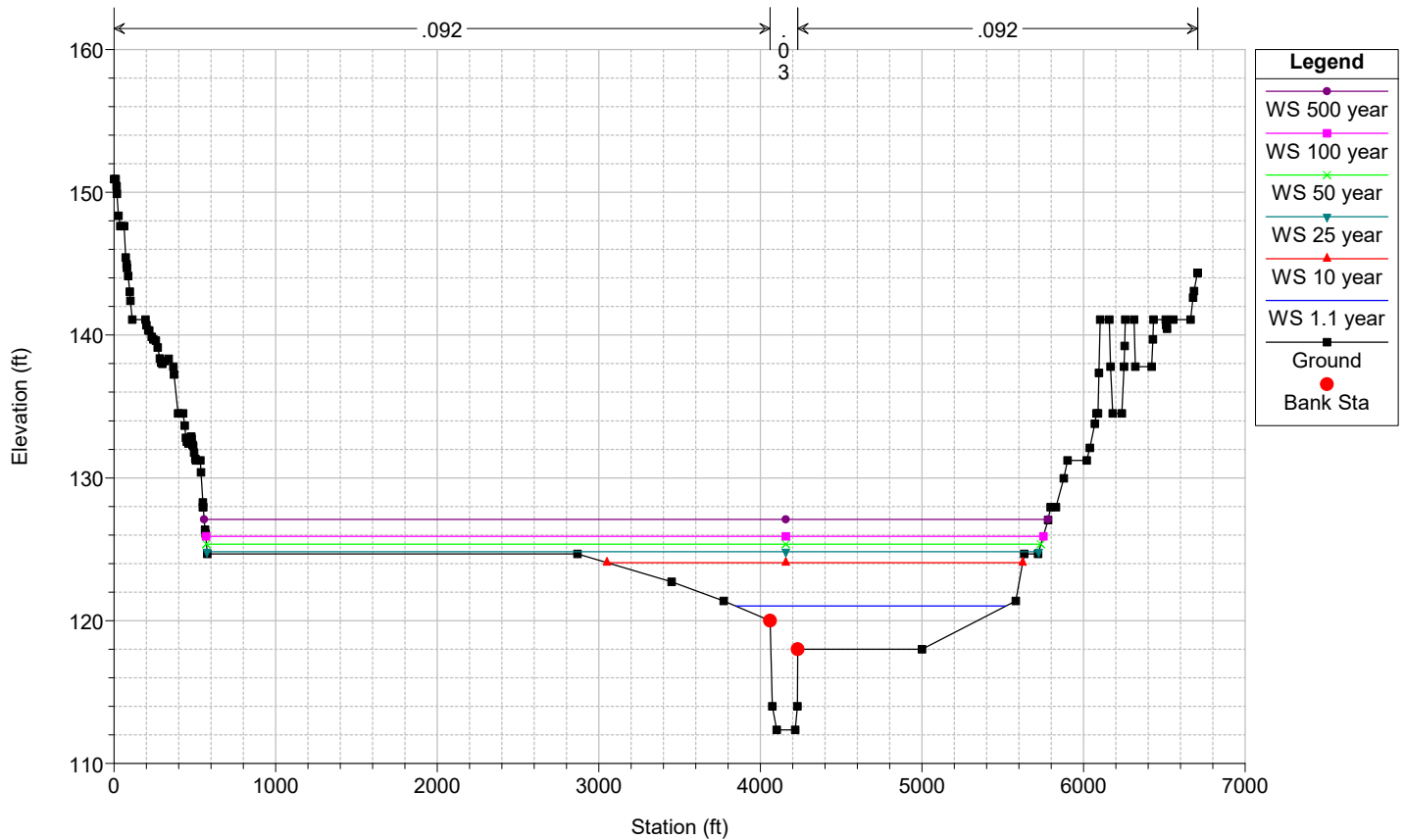
RS = 32750.00



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

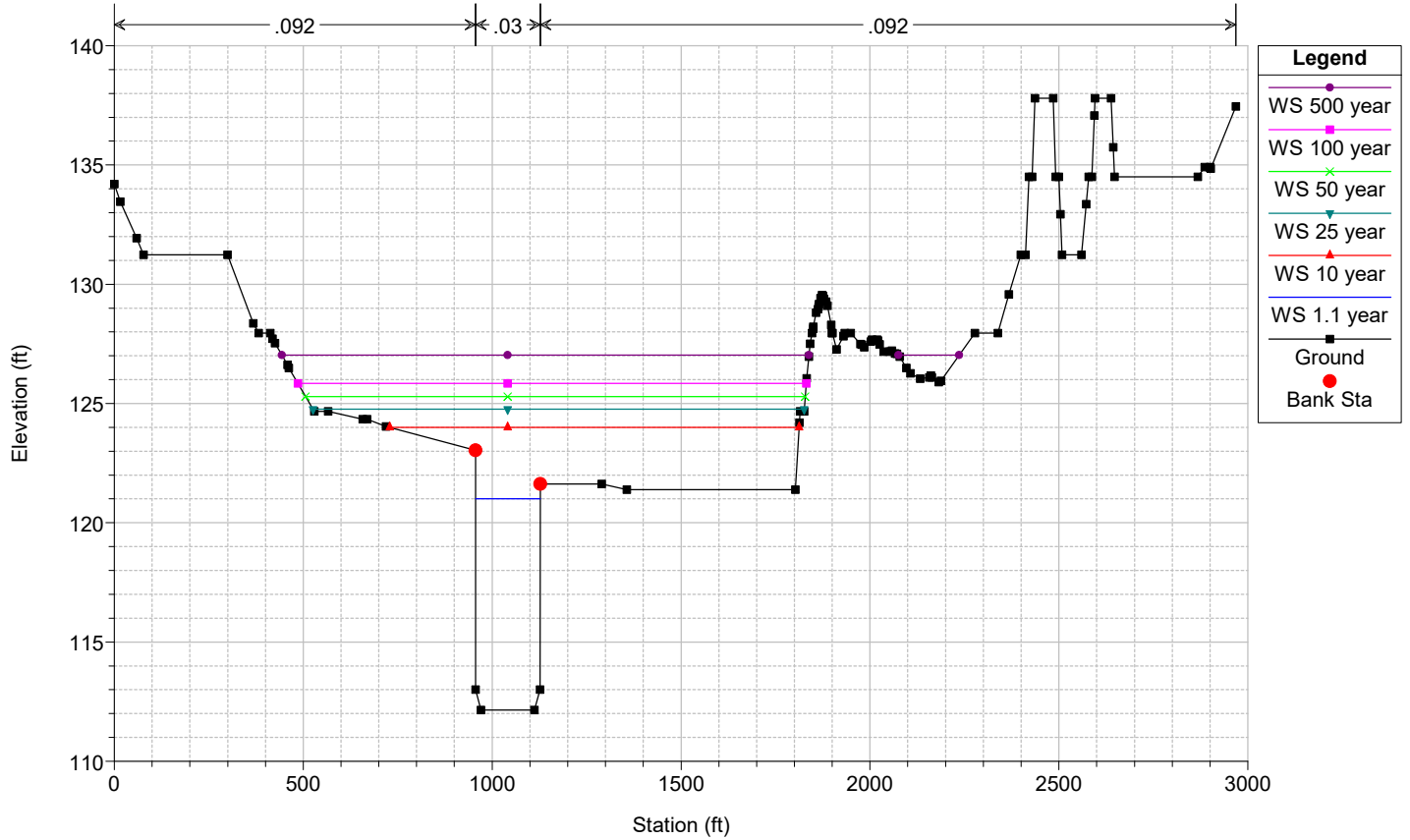
RS = 30396.70



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

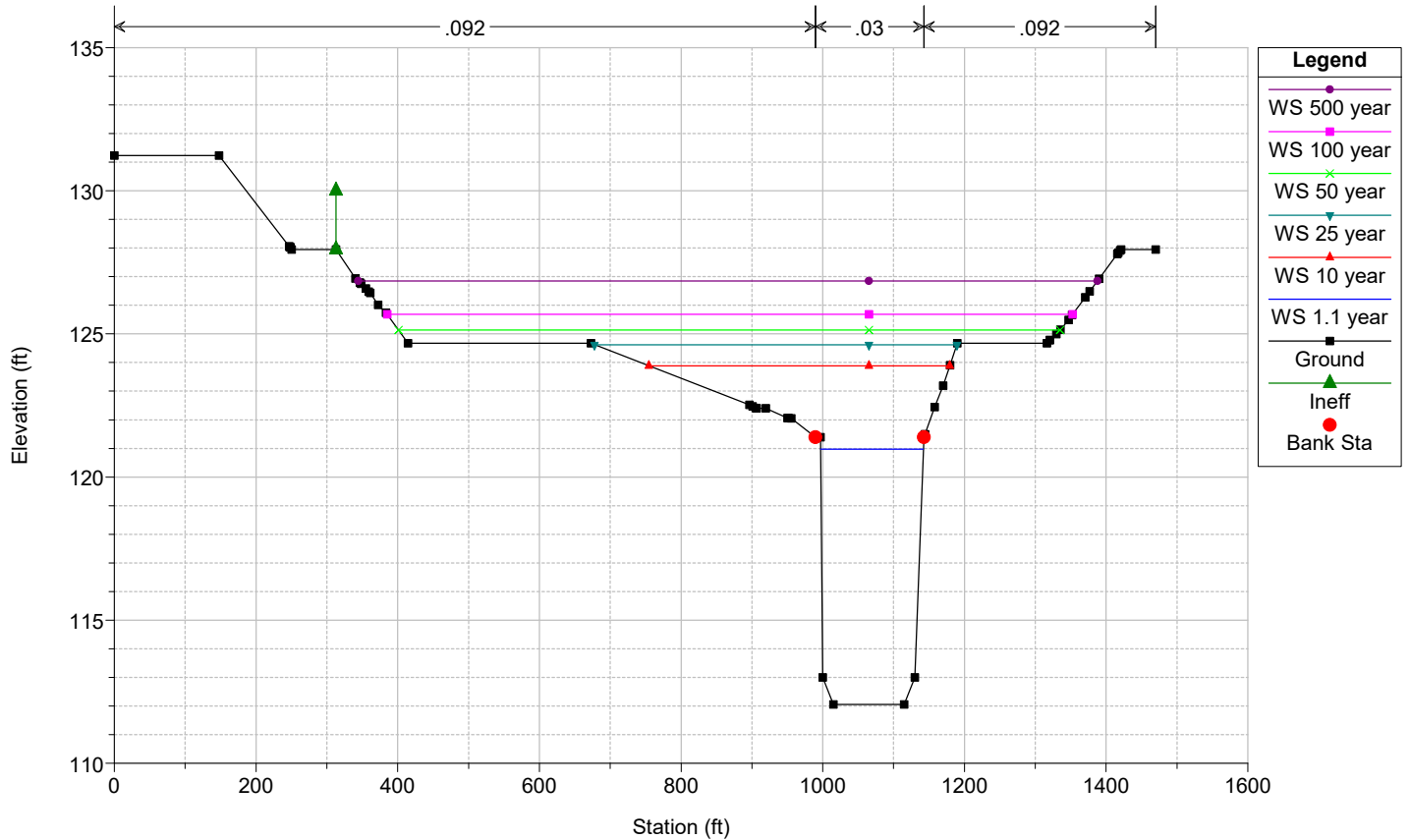
RS = 29483.97



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

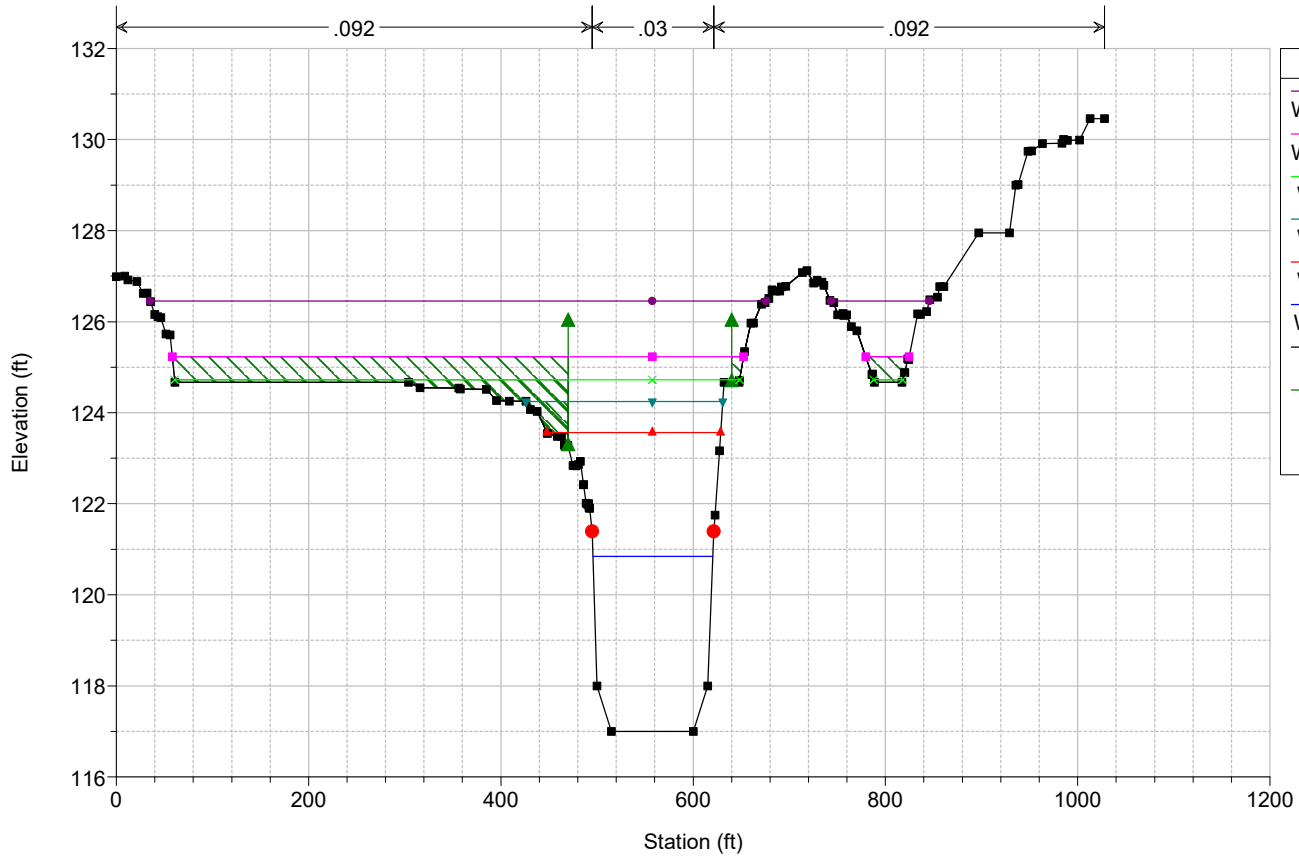
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

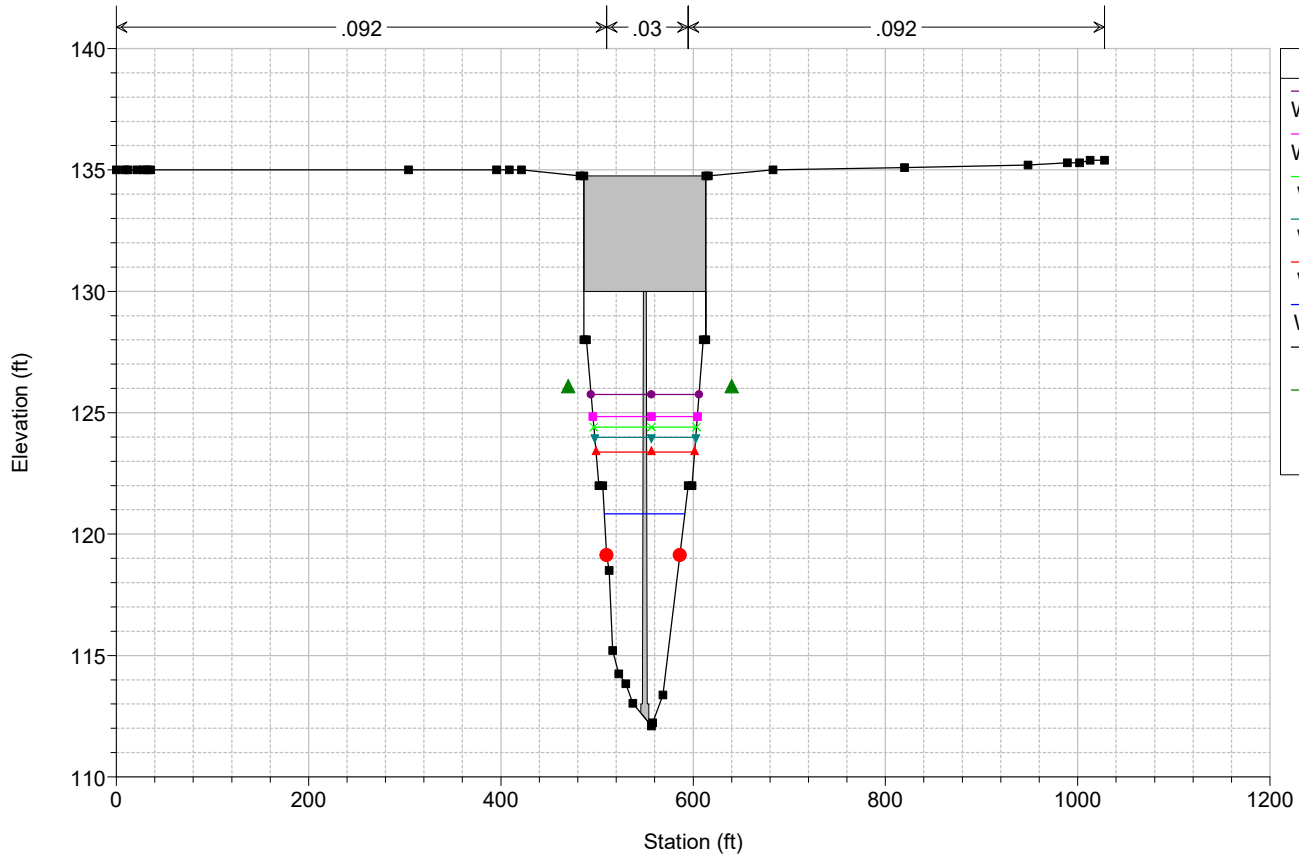
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

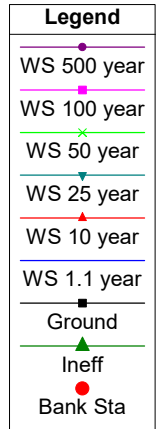
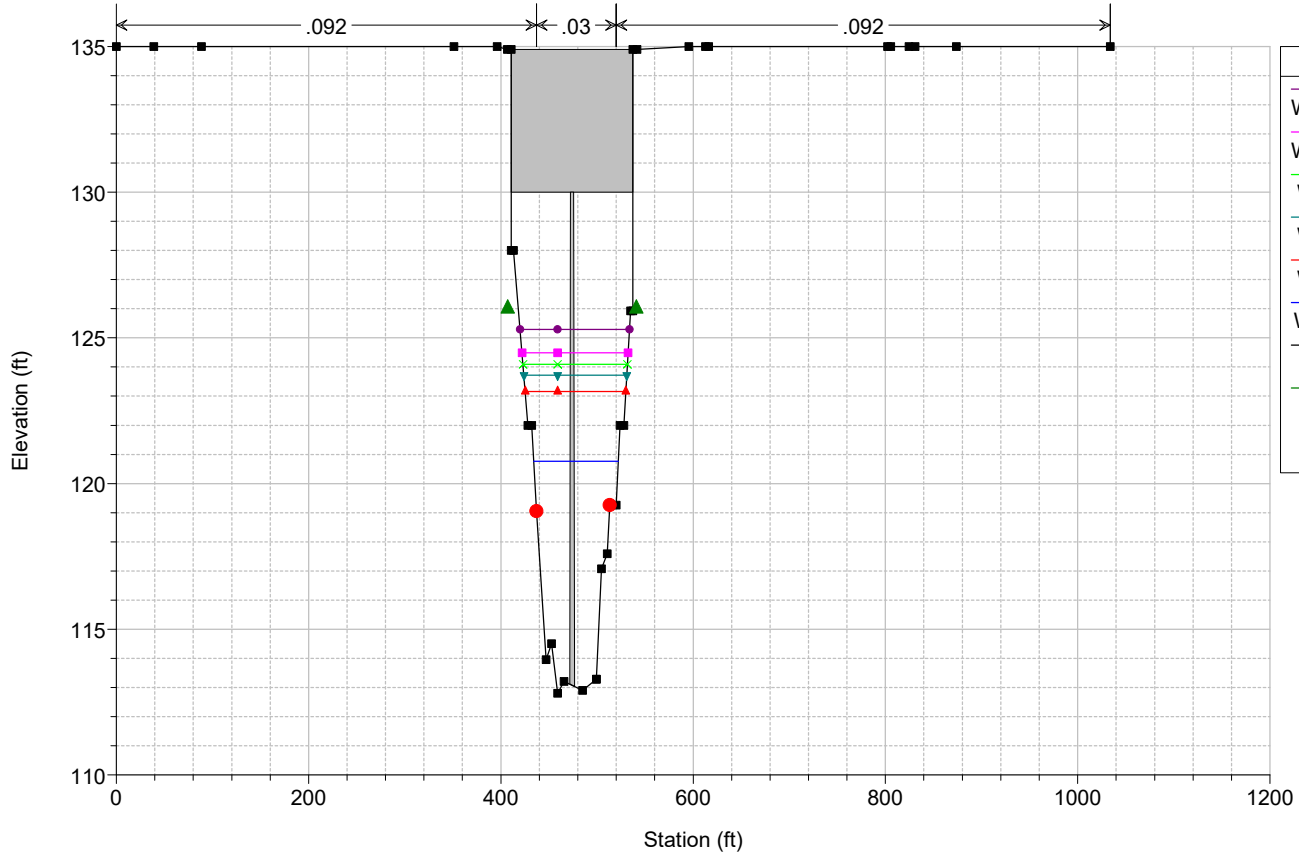
RS = 27966 BR



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

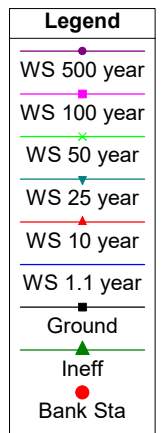
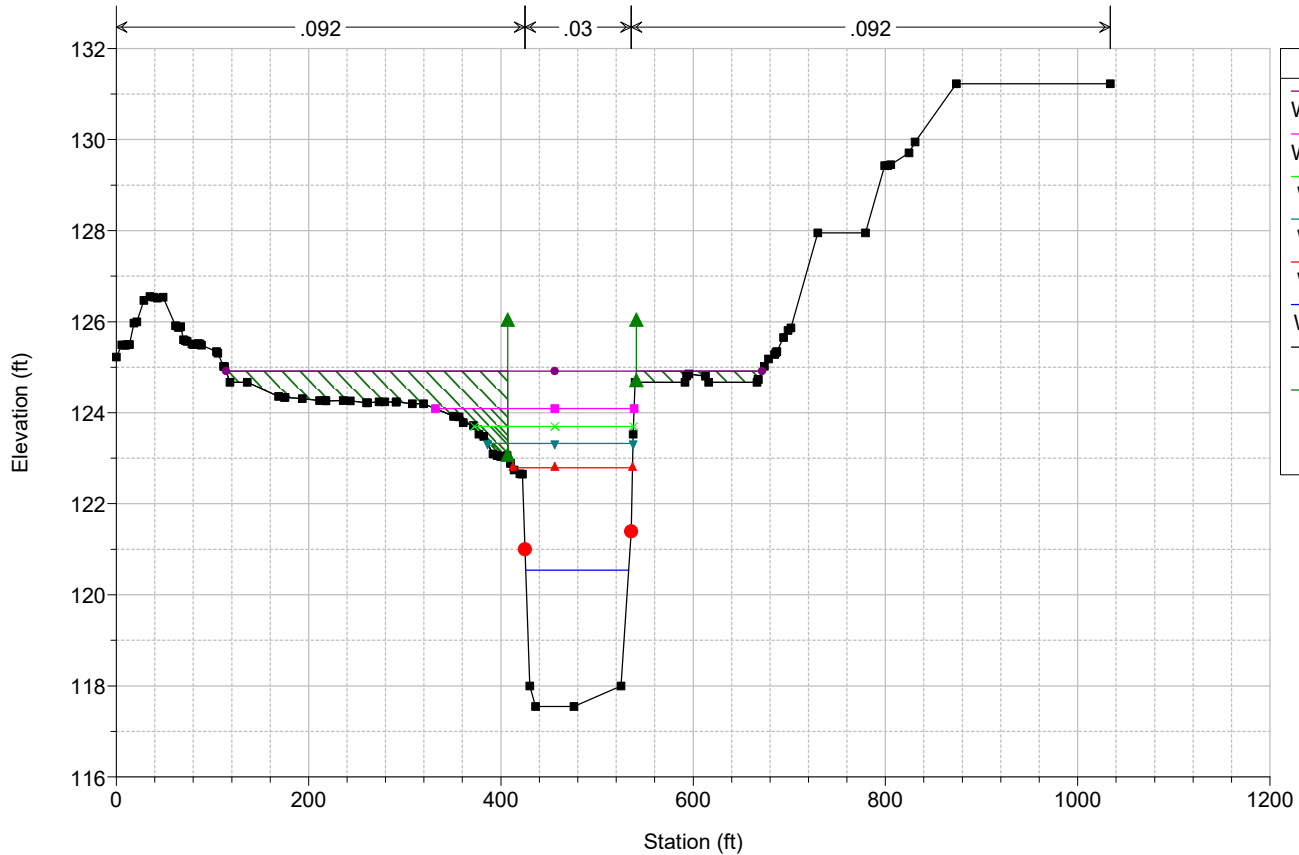
RS = 27966 BR



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

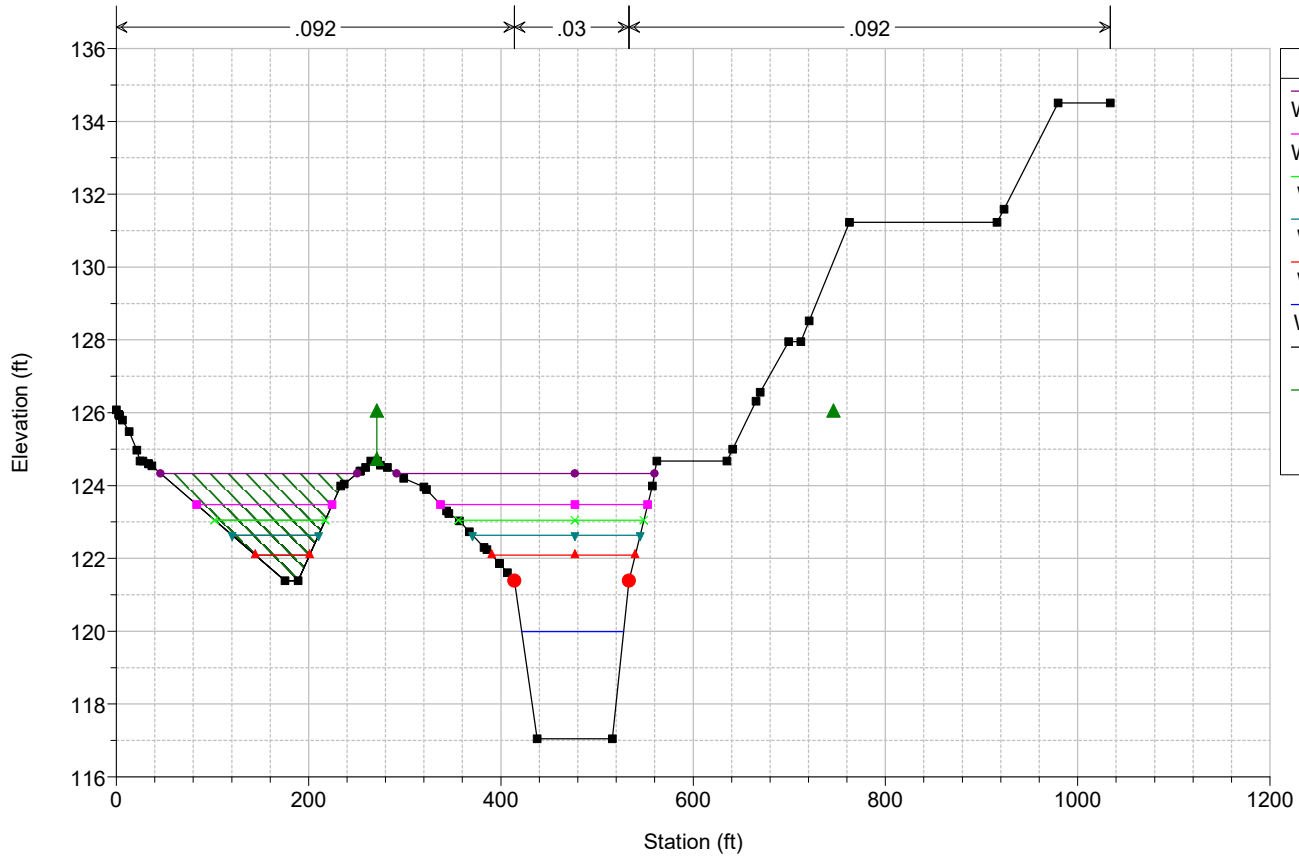
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

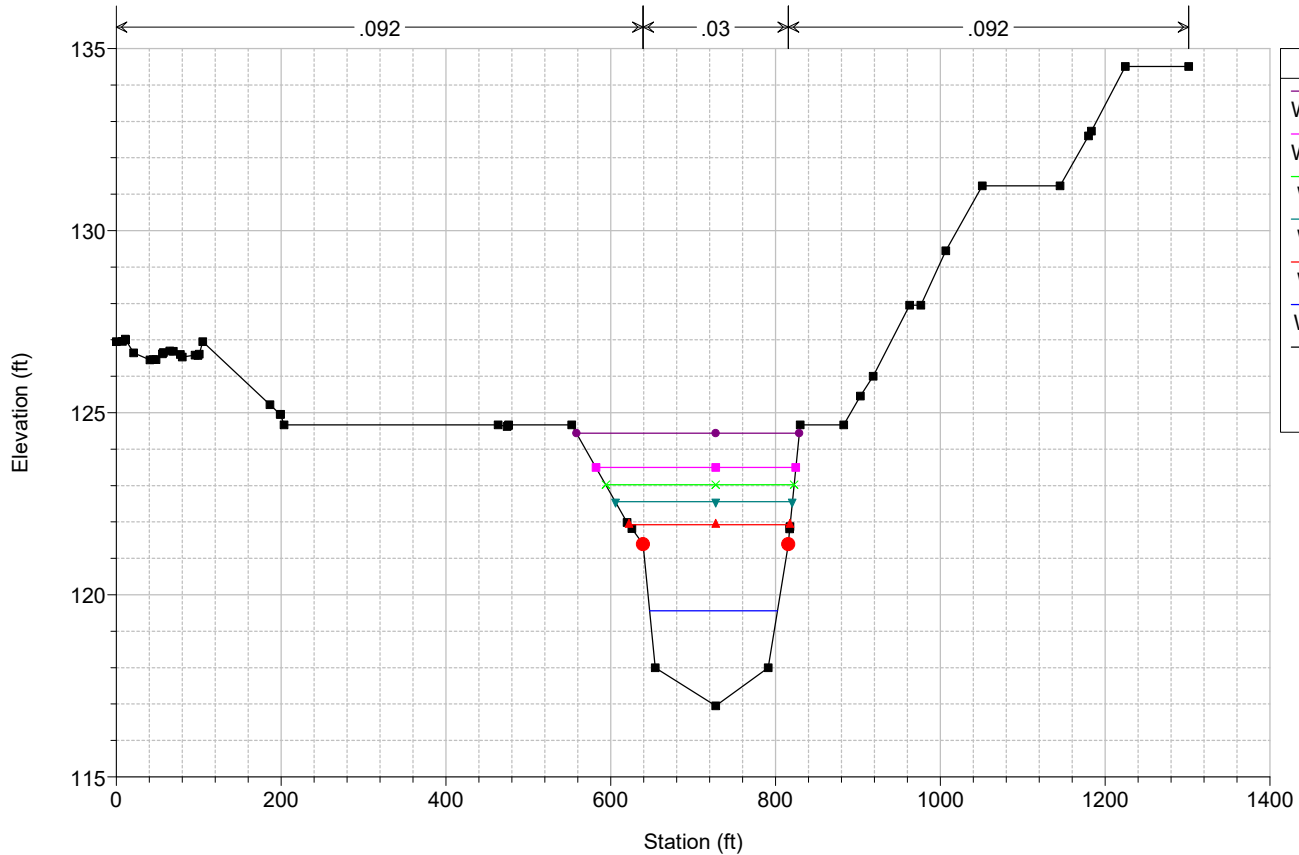
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Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

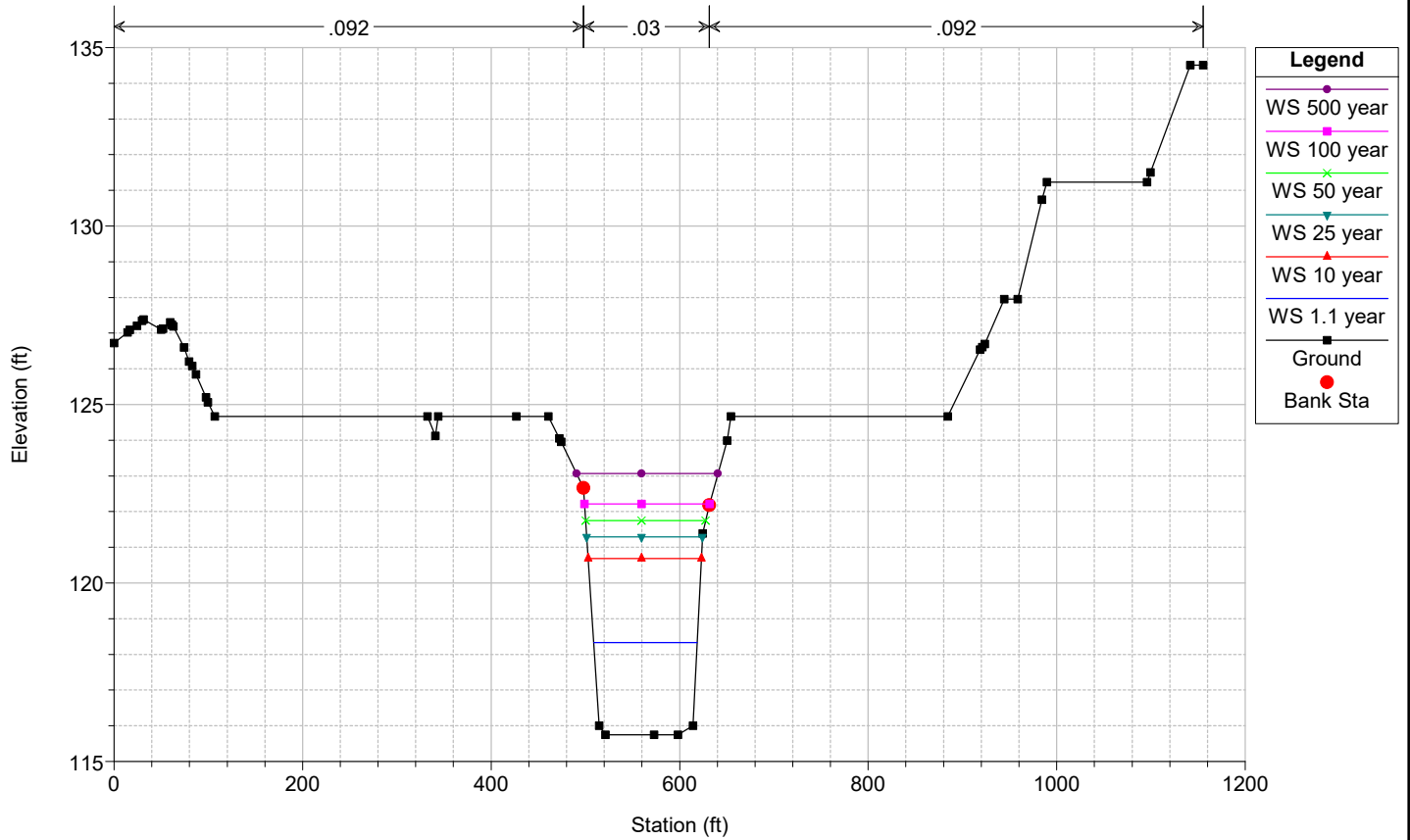
RS = 27381.56



Hampden Bridges Plan: Proposed Bridge Plan

Geom: Hampden Bridges 2-Span Proposed

RS = 26951.26



HEC-RAS River: Souadabscook Str Reach: Reach

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Reach	41522.56	1.1 year	exist MEDOT	1210.00	111.45	122.13	112.81	122.13	0.000010	0.71	1717.76	192.45	0.04
Reach	41522.56	1.1 year	PROPBRIDGE	1210.00	111.45	122.04	112.81	122.05	0.000010	0.72	1701.59	191.78	0.04
Reach	41522.56	10 year	exist MEDOT	3640.00	111.45	125.79	114.18	125.82	0.000033	1.55	2962.28	684.91	0.07
Reach	41522.56	10 year	PROPBRIDGE	3640.00	111.45	125.56	114.18	125.60	0.000035	1.58	2809.15	675.39	0.08
Reach	41522.56	25 year	exist MEDOT	4440.00	111.45	126.76	114.53	126.81	0.000038	1.72	3672.87	763.69	0.08
Reach	41522.56	25 year	PROPBRIDGE	4440.00	111.45	126.47	114.53	126.52	0.000041	1.77	3455.03	745.10	0.08
Reach	41522.56	50 year	exist MEDOT	5040.00	111.45	127.45	114.78	127.50	0.000040	1.83	4216.92	813.71	0.08
Reach	41522.56	50 year	PROPBRIDGE	5040.00	111.45	127.11	114.78	127.17	0.000044	1.89	3944.95	787.19	0.09
Reach	41522.56	100 year	exist MEDOT	5680.00	111.45	127.75	115.04	127.81	0.000047	2.00	4461.71	832.90	0.09
Reach	41522.56	100 year	PROPBRIDGE	5680.00	111.45	127.77	115.04	127.83	0.000047	2.00	4480.39	834.16	0.09
Reach	41522.56	500 year	exist MEDOT	7180.00	111.45	129.25	115.63	129.32	0.000051	2.20	5779.77	919.73	0.09
Reach	41522.56	500 year	PROPBRIDGE	7180.00	111.45	129.21	115.61	129.28	0.000051	2.21	5746.82	917.92	0.09
Reach	41055.75	1.1 year	exist MEDOT	1210.00	110.45	122.11		122.12	0.000026	1.12	1077.74	101.07	0.06
Reach	41055.75	1.1 year	PROPBRIDGE	1210.00	110.45	122.02		122.04	0.000027	1.13	1069.20	101.00	0.06
Reach	41055.75	10 year	exist MEDOT	3640.00	110.45	125.69		125.79	0.000090	2.53	1448.79	106.60	0.12
Reach	41055.75	10 year	PROPBRIDGE	3640.00	110.45	125.46		125.57	0.000095	2.57	1424.48	106.43	0.12
Reach	41055.75	25 year	exist MEDOT	4440.00	110.45	126.64		126.77	0.000108	2.90	1550.11	107.32	0.13
Reach	41055.75	25 year	PROPBRIDGE	4440.00	110.45	126.35		126.48	0.000115	2.95	1518.68	107.10	0.13
Reach	41055.75	50 year	exist MEDOT	5040.00	110.45	127.31		127.46	0.000121	3.15	1621.94	107.82	0.14
Reach	41055.75	50 year	PROPBRIDGE	5040.00	110.45	126.96		127.12	0.000130	3.22	1584.70	107.56	0.14
Reach	41055.75	100 year	exist MEDOT	5680.00	110.45	127.57		127.76	0.000145	3.49	1650.34	108.02	0.15
Reach	41055.75	100 year	PROPBRIDGE	5680.00	110.45	127.59		127.78	0.000144	3.49	1652.81	108.04	0.15
Reach	41055.75	500 year	exist MEDOT	7180.00	110.45	129.00		129.26	0.000174	4.05	1806.17	109.68	0.17
Reach	41055.75	500 year	PROPBRIDGE	7180.00	110.45	128.97		129.22	0.000176	4.06	1802.13	109.63	0.17
Reach	40924.49	1.1 year	exist MEDOT	1210.00	110.45	122.10		122.12	0.000033	1.19	1018.91	113.34	0.07
Reach	40924.49	1.1 year	PROPBRIDGE	1210.00	110.45	122.01		122.04	0.000034	1.20	1009.33	112.86	0.07
Reach	40924.49	10 year	exist MEDOT	3640.00	110.45	125.69		125.77	0.000132	2.38	1581.05	249.35	0.14
Reach	40924.49	10 year	PROPBRIDGE	3640.00	110.45	125.46		125.55	0.000144	2.45	1525.81	230.19	0.15
Reach	40924.49	25 year	exist MEDOT	4440.00	110.45	126.64		126.75	0.000138	2.61	1888.62	354.59	0.15
Reach	40924.49	25 year	PROPBRIDGE	4440.00	110.45	126.34		126.46	0.000154	2.70	1785.64	340.33	0.15
Reach	40924.49	50 year	exist MEDOT	5040.00	110.45	127.32		127.43	0.000141	2.75	2140.46	387.01	0.15
Reach	40924.49	50 year	PROPBRIDGE	5040.00	110.45	126.97		127.09	0.000159	2.86	2007.15	374.90	0.16
Reach	40924.49	100 year	exist MEDOT	5680.00	110.45	127.59		127.72	0.000163	3.01	2245.73	395.85	0.16
Reach	40924.49	100 year	PROPBRIDGE	5680.00	110.45	127.61		127.75	0.000162	3.00	2254.90	396.61	0.16
Reach	40924.49	500 year	exist MEDOT	7180.00	110.45	129.05		129.21	0.000164	3.28	2874.49	460.42	0.16
Reach	40924.49	500 year	PROPBRIDGE	7180.00	110.45	129.01		129.17	0.000166	3.29	2857.42	459.08	0.17
Reach	40799.90	1.1 year	exist MEDOT	1210.00	110.85	122.07		122.11	0.000110	1.68	719.47	118.06	0.12
Reach	40799.90	1.1 year	PROPBRIDGE	1210.00	110.85	121.98		122.03	0.000115	1.71	709.34	117.69	0.12
Reach	40799.90	10 year	exist MEDOT	3640.00	110.85	125.60		125.75	0.000221	3.12	1334.11	326.55	0.18
Reach	40799.90	10 year	PROPBRIDGE	3640.00	110.85	125.36		125.52	0.000243	3.21	1257.05	321.12	0.19
Reach	40799.90	25 year	exist MEDOT	4440.00	110.85	126.55		126.72	0.000227	3.38	1653.75	348.14	0.19
Reach	40799.90	25 year	PROPBRIDGE	4440.00	110.85	126.24		126.43	0.000255	3.51	1548.09	341.18	0.20
Reach	40799.90	50 year	exist MEDOT	5040.00	110.85	127.22		127.40	0.000229	3.54	1892.64	363.11	0.19
Reach	40799.90	50 year	PROPBRIDGE	5040.00	110.85	126.85		127.06	0.000261	3.69	1762.69	355.05	0.20
Reach	40799.90	100 year	exist MEDOT	5680.00	110.85	127.47		127.69	0.000266	3.88	1984.37	368.69	0.21
Reach	40799.90	100 year	PROPBRIDGE	5680.00	110.85	127.49		127.71	0.000264	3.87	1993.23	369.23	0.21
Reach	40799.90	500 year	exist MEDOT	7180.00	110.85	128.92		129.17	0.000262	4.18	2555.19	412.09	0.21
Reach	40799.90	500 year	PROPBRIDGE	7180.00	110.85	128.88		129.14	0.000266	4.20	2539.31	411.25	0.21
Reach	40532.46	1.1 year	exist MEDOT	1210.00	112.50	122.01	116.31	122.07	0.000167	1.97	613.73	114.72	0.15
Reach	40532.46	1.1 year	PROPBRIDGE	1210.00	112.50	121.93	116.31	121.99	0.000175	2.01	603.66	113.35	0.15
Reach	40532.46	10 year	exist MEDOT	3640.00	112.50	125.48	118.92	125.67	0.000300	3.58	1059.21	1603.59	0.21
Reach	40532.46	10 year	PROPBRIDGE	3640.00	112.50	125.23	118.92	125.44	0.000331	3.68	1025.57	1599.98	0.22
Reach	40532.46	25 year	exist MEDOT	4440.00	112.50	126.40	119.75	126.64	0.000317	3.93	1185.06	1626.77	0.22
Reach	40532.46	25 year	PROPBRIDGE	4440.00	112.50	126.08	119.75	126.34	0.000355	4.07	1141.80	1620.50	0.24
Reach	40532.46	50 year	exist MEDOT	5040.00	112.50	127.06	120.21	127.32	0.000327	4.17	1273.99	1635.26	0.23
Reach	40532.46	50 year	PROPBRIDGE	5040.00	112.50	126.68	120.21	126.97	0.000371	4.33	1222.86	1630.99	0.24
Reach	40532.46	100 year	exist MEDOT	5680.00	112.50	127.27	120.63	127.59	0.000387	4.60	1303.03	1636.65	0.25
Reach	40532.46	100 year	PROPBRIDGE	5680.00	112.50	127.29	120.63	127.62	0.000384	4.59	1306.43	1636.81	0.25
Reach	40532.46	500 year	exist MEDOT	7180.00	112.50	128.67	121.52	129.07	0.000404	5.11	1493.70	1675.45	0.26
Reach	40532.46	500 year	PROPBRIDGE	7180.00	112.50	128.63	121.52	129.03	0.000409	5.13	1488.23	1673.92	0.26
Reach	40346		Bridge										
Reach	40193.72	1.1 year	exist MEDOT	1210.00	115.00	121.90	117.37	121.96	0.000194	2.07	583.77	334.96	0.16
Reach	40193.72	1.1 year	PROPBRIDGE	1210.00	115.00	121.81	117.37	121.88	0.000203	2.11	574.64	314.06	0.16
Reach	40193.72	10 year	exist MEDOT	3640.00	115.00	125.15	119.59	125.37	0.000369	3.81	973.76	1543.61	0.23
Reach	40193.72	10 year	PROPBRIDGE	3640.00	115.00	124.95	119.59	125.18	0.000401	3.90	946.66	1541.54	0.24
Reach	40193.72	25 year	exist MEDOT	4440.00	115.00	126.02	120.13	126.29	0.000391	4.19	1091.24	1552.04	0.24
Reach	40193.72	25 year	PROPBRIDGE	4440.00	115.00	125.76	120.13	126.05	0.000431	4.31	1056.22	1549.82	0.26
Reach	40193.72	50 year	exist MEDOT	5040.00	115.00	126.63	120.49	126.94	0.000404	4.44	1174.44	1557.31	0.25
Reach	40193.72	50 year	PROPBRIDGE	5040.00	115.00	126.33	120.49	126.65	0.000451	4.59	1132.70	1554.67	0.26
Reach	40193.72	100 year	exist MEDOT	5680.00	115.00	126.74	120.87	127.12	0.000494	4.95	1188.82	1558.23	0.28
Reach	40193.72	100 year	PROPBRIDGE	5680.00	115.00	126.91	120.87	127.28	0.000466	4.87	1211.75	1559.68	0.27
Reach	40193.72	500 year	exist MEDOT	7180.00	115.00	128.05	121.68	128.52	0.000517	5.51	1365.36	1569.09	0.29
Reach	40193.72	500 year	PROPBRIDGE	7180.00	115.00	128.18	121.68	128.64	0.000496	5.44	1383.34	1569.78	0.29
Reach	38900.00	1.1 year	exist MEDOT	1210.00	116.35	121.42	118.59	121.56	0.000520	2.99	437.86	1403.65	0.25
Reach	38900.00	1.1 year	PROPBRIDGE	1210.00	116.35	121.30	118.59	121.45	0.000566	3.08	393.31	90.78	0.26
Reach	38900.00	10 year	exist MEDOT	3640.00	116.35	125.03		125.05	0.000097	1.92	7233.60	2171.83	0.12
Reach	38900.00	10 year	PROPBRIDGE	3640.00	116.35	124.79		124.82	0.000118	2.08	6724.70	2170.55	0.13
Reach	38900.00	25 year	exist MEDOT	4440.00	116.35	125.96		125.98	0.000073	1.79	9259.93	2176.91	0.11
Reach	38900.00	25 year	PROPBRIDGE	4440.00	116.35	125.67		125.70	0.000089	1.94	8636.94	2175.36	0.12
Reach	38900.00	50 year	exist MEDOT	5040.00	116.35	126.61		126.63	0.000062	1.74	10681.14	2180.45	0.10

HEC-RAS River: Souadabscook Str Reach: Reach (Continued)

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Reach	38900.00	50 year	PROPBRIDGE	5040.00	116.35	126.28		126.30	0.000076	1.88	9956.42	2178.64	0.11
Reach	38900.00	100 year	exist MEDOT	5680.00	116.35	126.72		126.74	0.000074	1.91	10917.72	2181.04	0.11
Reach	38900.00	100 year	PROPBRIDGE	5680.00	116.35	126.90		126.92	0.000067	1.84	11313.80	2182.02	0.10
Reach	38900.00	500 year	exist MEDOT	7180.00	116.35	128.11		128.12	0.000057	1.83	13945.70	2188.64	0.10
Reach	38900.00	500 year	PROPBRIDGE	7180.00	116.35	128.24		128.26	0.000054	1.79	14246.48	2189.45	0.09
Reach	38050.00	1.1 year	exist MEDOT	1210.00	116.55	121.51		121.51	0.000001	0.12	10096.28	2055.59	0.01
Reach	38050.00	1.1 year	PROPBRIDGE	1210.00	116.55	121.40		121.40	0.000001	0.12	9869.27	2054.55	0.01
Reach	38050.00	10 year	exist MEDOT	3640.00	116.55	125.04		125.04	0.000001	0.21	18508.74	2726.95	0.01
Reach	38050.00	10 year	PROPBRIDGE	3640.00	116.55	124.81		124.81	0.000001	0.21	17878.29	2725.94	0.01
Reach	38050.00	25 year	exist MEDOT	4440.00	116.55	125.97		125.97	0.000001	0.23	21040.87	2730.93	0.01
Reach	38050.00	25 year	PROPBRIDGE	4440.00	116.55	125.68		125.69	0.000001	0.24	20265.14	2729.78	0.01
Reach	38050.00	50 year	exist MEDOT	5040.00	116.55	126.62		126.62	0.000001	0.24	22818.60	2733.51	0.01
Reach	38050.00	50 year	PROPBRIDGE	5040.00	116.55	126.29		126.29	0.000001	0.25	21914.86	2732.20	0.01
Reach	38050.00	100 year	exist MEDOT	5680.00	116.55	126.73		126.73	0.000001	0.27	23118.61	2733.94	0.01
Reach	38050.00	100 year	PROPBRIDGE	5680.00	116.55	126.91		126.91	0.000001	0.26	23612.53	2734.66	0.01
Reach	38050.00	500 year	exist MEDOT	7180.00	116.55	128.11		128.11	0.000001	0.30	26904.99	2741.14	0.02
Reach	38050.00	500 year	PROPBRIDGE	7180.00	116.55	128.25		128.25	0.000001	0.29	27280.63	2742.26	0.02
Reach	37100.00	1.1 year	exist MEDOT	1210.00	116.55	121.51		121.51	0.000004	0.27	4504.98	981.96	0.02
Reach	37100.00	1.1 year	PROPBRIDGE	1210.00	116.55	121.40		121.40	0.000004	0.28	4399.77	921.68	0.02
Reach	37100.00	10 year	exist MEDOT	3640.00	116.55	125.04		125.04	0.000005	0.46	8924.89	1700.58	0.03
Reach	37100.00	10 year	PROPBRIDGE	3640.00	116.55	124.80		124.81	0.000006	0.48	8531.15	1699.23	0.03
Reach	37100.00	25 year	exist MEDOT	4440.00	116.55	125.96		125.97	0.000005	0.50	10504.36	1706.01	0.03
Reach	37100.00	25 year	PROPBRIDGE	4440.00	116.55	125.68		125.68	0.000006	0.52	10019.10	1704.34	0.03
Reach	37100.00	50 year	exist MEDOT	5040.00	116.55	126.61		126.62	0.000005	0.53	11615.08	1710.49	0.03
Reach	37100.00	50 year	PROPBRIDGE	5040.00	116.55	126.28		126.29	0.000006	0.55	11048.94	1707.88	0.03
Reach	37100.00	100 year	exist MEDOT	5680.00	116.55	126.72		126.73	0.000006	0.59	11800.58	1711.41	0.03
Reach	37100.00	100 year	PROPBRIDGE	5680.00	116.55	126.90		126.91	0.000006	0.57	12110.43	1712.93	0.03
Reach	37100.00	500 year	exist MEDOT	7180.00	116.55	128.10		128.11	0.000006	0.64	14175.00	1725.02	0.03
Reach	37100.00	500 year	PROPBRIDGE	7180.00	116.55	128.24		128.25	0.000006	0.63	14411.97	1728.02	0.03
Reach	35509.99	1.1 year	exist MEDOT	1210.00	108.00	121.50		121.50	0.000004	0.50	2458.07	498.37	0.03
Reach	35509.99	1.1 year	PROPBRIDGE	1210.00	108.00	121.39		121.39	0.000004	0.50	2404.42	204.44	0.03
Reach	35509.99	10 year	exist MEDOT	3640.00	108.00	125.01		125.03	0.000012	1.04	7310.71	2222.79	0.05
Reach	35509.99	10 year	PROPBRIDGE	3640.00	108.00	124.78		124.79	0.000013	1.07	6791.24	2218.83	0.05
Reach	35509.99	25 year	exist MEDOT	4440.00	108.00	125.94		125.95	0.000013	1.11	9376.52	2239.83	0.05
Reach	35509.99	25 year	PROPBRIDGE	4440.00	108.00	125.65		125.67	0.000014	1.16	8733.36	2233.98	0.05
Reach	35509.99	50 year	exist MEDOT	5040.00	108.00	126.59		126.60	0.000013	1.16	10836.05	2252.30	0.05
Reach	35509.99	50 year	PROPBRIDGE	5040.00	108.00	126.25		126.27	0.000015	1.21	10083.36	2245.91	0.05
Reach	35509.99	100 year	exist MEDOT	5680.00	108.00	126.69		126.71	0.000016	1.29	11066.86	2254.27	0.05
Reach	35509.99	100 year	PROPBRIDGE	5680.00	108.00	126.87		126.89	0.000015	1.26	11479.71	2257.82	0.05
Reach	35509.99	500 year	exist MEDOT	7180.00	108.00	128.07		128.09	0.000017	1.37	14202.28	2281.28	0.06
Reach	35509.99	500 year	PROPBRIDGE	7180.00	108.00	128.21		128.23	0.000016	1.35	14518.86	2283.59	0.06
Reach	35310.52	1.1 year	exist MEDOT	1210.00	113.00	121.47	115.83	121.50	0.000056	1.28	945.26	138.36	0.09
Reach	35310.52	1.1 year	PROPBRIDGE	1210.00	113.00	121.36	115.83	121.39	0.000059	1.30	929.78	138.25	0.09
Reach	35310.52	10 year	exist MEDOT	3640.00	113.00	124.91	117.34	125.01	0.000136	2.55	1434.13	2141.39	0.14
Reach	35310.52	10 year	PROPBRIDGE	3640.00	113.00	124.67	117.34	124.78	0.000147	2.61	1397.96	2128.04	0.15
Reach	35310.52	25 year	exist MEDOT	4440.00	113.00	125.81	117.75	125.94	0.000152	2.85	1590.13	2277.82	0.15
Reach	35310.52	25 year	PROPBRIDGE	4440.00	113.00	125.52	117.75	125.65	0.000166	2.93	1534.20	2247.64	0.16
Reach	35310.52	50 year	exist MEDOT	5040.00	113.00	126.44	118.03	126.58	0.000162	3.06	1710.46	2302.46	0.16
Reach	35310.52	50 year	PROPBRIDGE	5040.00	113.00	126.10	118.03	126.25	0.000179	3.15	1644.81	2288.64	0.17
Reach	35310.52	100 year	exist MEDOT	5680.00	113.00	126.50	118.32	126.69	0.000201	3.43	1722.77	2305.08	0.18
Reach	35310.52	100 year	PROPBRIDGE	5680.00	113.00	126.69	118.32	126.87	0.000191	3.37	1758.85	2311.98	0.17
Reach	35310.52	500 year	exist MEDOT	7180.00	113.00	127.83	118.97	128.06	0.000222	3.87	1976.73	2320.88	0.19
Reach	35310.52	500 year	PROPBRIDGE	7180.00	113.00	127.98	118.97	128.20	0.000214	3.82	2004.24	2325.03	0.19
Reach	35151		Bridge										
Reach	34987.11	1.1 year	exist MEDOT	1210.00	114.50	121.20	116.08	121.24	0.000095	1.61	751.51	116.26	0.11
Reach	34987.11	1.1 year	PROPBRIDGE	1210.00	114.50	121.15	116.08	121.19	0.000098	1.62	745.31	116.20	0.11
Reach	34987.11	10 year	exist MEDOT	3640.00	114.50	124.41	117.77	124.57	0.000239	3.22	1132.97	132.67	0.18
Reach	34987.11	10 year	PROPBRIDGE	3640.00	114.50	124.24	117.77	124.40	0.000253	3.28	1110.95	127.91	0.19
Reach	34987.11	25 year	exist MEDOT	4440.00	114.50	125.19	118.22	125.40	0.000272	3.62	1242.47	1356.92	0.20
Reach	34987.11	25 year	PROPBRIDGE	4440.00	114.50	124.98	118.22	125.20	0.000292	3.70	1213.08	1346.10	0.21
Reach	34987.11	50 year	exist MEDOT	5040.00	114.50	125.75	118.55	125.98	0.000293	3.90	1319.83	1433.68	0.21
Reach	34987.11	50 year	PROPBRIDGE	5040.00	114.50	125.49	118.55	125.74	0.000318	3.99	1284.31	1423.54	0.22
Reach	34987.11	100 year	exist MEDOT	5680.00	114.50	125.57	118.88	125.88	0.000394	4.47	1294.99	1428.15	0.24
Reach	34987.11	100 year	PROPBRIDGE	5680.00	114.50	126.01	118.88	126.30	0.000343	4.28	1357.37	1436.64	0.23
Reach	34987.11	500 year	exist MEDOT	7180.00	114.50	126.67	119.61	127.07	0.000451	5.10	1448.58	1449.85	0.26
Reach	34987.11	500 year	PROPBRIDGE	7180.00	114.50	127.13	119.61	127.50	0.000396	4.91	1513.43	1532.32	0.25
Reach	34886.44	1.1 year	exist MEDOT	1210.00	111.00	121.20	114.31	121.23	0.000046	1.25	967.55	129.59	0.08
Reach	34886.44	1.1 year	PROPBRIDGE	1210.00	111.00	121.15	114.31	121.18	0.000047	1.26	960.65	129.45	0.08
Reach	34886.44	10 year	exist MEDOT	3640.00	111.00	124.44	116.32	124.50	0.000093	2.23	3158.97	1570.05	0.12
Reach	34886.44	10 year	PROPBRIDGE	3640.00	111.00	124.27	116.32	124.34	0.000101	2.29	2997.27	1529.26	0.13
Reach	34886.44	25 year	exist MEDOT	4440.00	111.00	125.24	116.76	125.32	0.000097	2.38	3980.43	2193.93	0.13
Reach	34886.44	25 year	PROPBRIDGE	4440.00	111.00	125.03	116.76	125.11	0.000106	2.46	3764.94	2184.58	0.13
Reach	34886.44	50 year	exist MEDOT	5040.00	111.00	125.81	117.08	125.89	0.000097	2.47	4561.99	2249.35	0.13
Reach	34886.44	50 year	PROPBRIDGE	5040.00	111.00	125.56	117.08	125.64	0.000108	2.57	4302.37	2233.92	0.13
Reach	34886.44	100 year	exist MEDOT	5680.00	111.00	125.65	117.41	125.75	0.000132	2.85	4399.13	2239.35	0.15
Reach	34886.44	100 year	PROPBRIDGE	5680.00	111.00	126.10	117.41	126.18	0.000110	2.66	4854.70	2268.30	0.13
Reach	34886.44	500 year	exist MEDOT	7180.00	111.00	126.79	118.13	126.90	0.000132	3.04	5569.22	2303.08	0.15
Reach	34886.44	500 year	PROPBRIDGE	7180.00	111.00	127.25	118.13	127.34	0.000111	2.85	6039.67	2325.83	0.14
Reach	33430.00	1.1 year	exist MEDOT	1210.00	112.55	121.14		121.17	0.000040	1.18	1027.64	138.35	0.08

HEC-RAS River: Souadabscook Str Reach: Reach (Continued)

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Reach	33430.00	1.1 year	PROPBIDGE	1210.00	112.55	121.09		121.11	0.000041	1.19	1020.08	138.14	0.08
Reach	33430.00	10 year	exist MEDOT	3640.00	112.55	124.34		124.38	0.000069	1.94	5179.24	2201.51	0.11
Reach	33430.00	10 year	PROPBIDGE	3640.00	112.55	124.15		124.21	0.000077	2.02	4790.33	2102.73	0.11
Reach	33430.00	25 year	exist MEDOT	4440.00	112.55	125.15		125.19	0.000064	1.97	7154.23	2516.50	0.10
Reach	33430.00	25 year	PROPBIDGE	4440.00	112.55	124.93		124.98	0.000074	2.08	6589.76	2510.41	0.11
Reach	33430.00	50 year	exist MEDOT	5040.00	112.55	125.73		125.77	0.000059	1.95	8608.63	2526.83	0.10
Reach	33430.00	50 year	PROPBIDGE	5040.00	112.55	125.46		125.50	0.000069	2.07	7931.04	2523.49	0.11
Reach	33430.00	100 year	exist MEDOT	5680.00	112.55	125.53		125.59	0.000084	2.30	8115.45	2524.34	0.12
Reach	33430.00	100 year	PROPBIDGE	5680.00	112.55	126.01		126.05	0.000064	2.06	9314.78	2530.53	0.10
Reach	33430.00	500 year	exist MEDOT	7180.00	112.55	126.70		126.74	0.000071	2.25	11064.75	2539.25	0.11
Reach	33430.00	500 year	PROPBIDGE	7180.00	112.55	127.18		127.21	0.000055	2.04	12288.21	2545.22	0.10
Reach	32750.00	1.1 year	exist MEDOT	1210.00	112.55	121.11		121.13	0.000048	1.30	933.78	121.03	0.08
Reach	32750.00	1.1 year	PROPBIDGE	1210.00	112.55	121.05		121.08	0.000049	1.31	927.07	120.91	0.08
Reach	32750.00	10 year	exist MEDOT	3640.00	112.55	124.29		124.33	0.000068	1.93	6176.49	2512.65	0.10
Reach	32750.00	10 year	PROPBIDGE	3640.00	112.55	124.11		124.15	0.000077	2.02	5716.79	2420.13	0.11
Reach	32750.00	25 year	exist MEDOT	4440.00	112.55	125.11		125.15	0.000061	1.91	8405.36	2812.17	0.10
Reach	32750.00	25 year	PROPBIDGE	4440.00	112.55	124.88		124.92	0.000071	2.03	7756.30	2808.50	0.11
Reach	32750.00	50 year	exist MEDOT	5040.00	112.55	125.69		125.72	0.000054	1.87	10041.53	2824.26	0.09
Reach	32750.00	50 year	PROPBIDGE	5040.00	112.55	125.42		125.46	0.000064	2.00	9266.78	2818.65	0.10
Reach	32750.00	100 year	exist MEDOT	5680.00	112.55	125.48		125.53	0.000079	2.22	9448.24	2820.21	0.11
Reach	32750.00	100 year	PROPBIDGE	5680.00	112.55	125.97		126.00	0.000059	1.97	10823.90	2829.77	0.10
Reach	32750.00	500 year	exist MEDOT	7180.00	112.55	126.66		126.69	0.000064	2.13	12774.01	2843.05	0.10
Reach	32750.00	500 year	PROPBIDGE	7180.00	112.55	127.15		127.17	0.000050	1.92	14169.12	2850.80	0.09
Reach	30396.70	1.1 year	exist MEDOT	1210.00	112.35	121.08		121.08	0.000011	0.65	4682.26	1690.00	0.04
Reach	30396.70	1.1 year	PROPBIDGE	1210.00	112.35	121.02		121.02	0.000011	0.66	4586.89	1668.52	0.04
Reach	30396.70	10 year	exist MEDOT	3640.00	112.35	124.24		124.25	0.000016	0.99	11517.70	2632.58	0.05
Reach	30396.70	10 year	PROPBIDGE	3640.00	112.35	124.05		124.06	0.000018	1.03	11021.46	2572.92	0.05
Reach	30396.70	25 year	exist MEDOT	4440.00	112.35	125.06		125.07	0.000018	1.08	14674.44	5155.50	0.05
Reach	30396.70	25 year	PROPBIDGE	4440.00	112.35	124.82		124.83	0.000020	1.14	13446.26	5147.88	0.06
Reach	30396.70	50 year	exist MEDOT	5040.00	112.35	125.64		125.65	0.000017	1.08	17690.66	5174.14	0.05
Reach	30396.70	50 year	PROPBIDGE	5040.00	112.35	125.36		125.37	0.000019	1.15	16228.14	5165.11	0.06
Reach	30396.70	100 year	exist MEDOT	5680.00	112.35	125.41		125.42	0.000024	1.28	16489.80	5166.72	0.06
Reach	30396.70	100 year	PROPBIDGE	5680.00	112.35	125.92		125.93	0.000018	1.14	19098.55	5182.82	0.06
Reach	30396.70	500 year	exist MEDOT	7180.00	112.35	126.60		126.61	0.000020	1.25	22634.15	5207.16	0.06
Reach	30396.70	500 year	PROPBIDGE	7180.00	112.35	127.10		127.11	0.000016	1.13	25260.32	5223.33	0.05
Reach	29483.97	1.1 year	exist MEDOT	1210.00	112.15	121.06		121.07	0.000016	0.80	1510.31	171.43	0.05
Reach	29483.97	1.1 year	PROPBIDGE	1210.00	112.15	121.00		121.01	0.000016	0.81	1500.51	171.42	0.05
Reach	29483.97	10 year	exist MEDOT	3640.00	112.15	124.19		124.23	0.000043	1.59	4064.71	1119.61	0.08
Reach	29483.97	10 year	PROPBIDGE	3640.00	112.15	124.00		124.03	0.000046	1.63	3850.22	1083.28	0.08
Reach	29483.97	25 year	exist MEDOT	4440.00	112.15	125.00		125.04	0.000047	1.73	5061.15	1310.22	0.09
Reach	29483.97	25 year	PROPBIDGE	4440.00	112.15	124.76		124.80	0.000051	1.79	4742.79	1300.01	0.09
Reach	29483.97	50 year	exist MEDOT	5040.00	112.15	125.58		125.62	0.000048	1.81	5830.24	1334.56	0.09
Reach	29483.97	50 year	PROPBIDGE	5040.00	112.15	125.29		125.34	0.000054	1.88	5445.38	1322.44	0.09
Reach	29483.97	100 year	exist MEDOT	5680.00	112.15	125.33		125.38	0.000067	2.11	5489.64	1323.83	0.10
Reach	29483.97	100 year	PROPBIDGE	5680.00	112.15	125.85		125.89	0.000055	1.96	6181.90	1345.54	0.09
Reach	29483.97	500 year	exist MEDOT	7180.00	112.15	126.51		126.57	0.000069	2.27	7125.55	1491.07	0.11
Reach	29483.97	500 year	PROPBIDGE	7180.00	112.15	127.03		127.08	0.000058	2.12	7914.00	1555.85	0.10
Reach	28303.36	1.1 year	exist MEDOT	1210.00	112.05	121.03	113.55	121.04	0.000026	1.00	1214.59	145.35	0.06
Reach	28303.36	1.1 year	PROPBIDGE	1210.00	112.05	120.97	113.55	120.99	0.000026	1.00	1206.20	145.24	0.06
Reach	28303.36	10 year	exist MEDOT	3640.00	112.05	124.09	115.06	124.16	0.000081	2.13	2047.56	448.39	0.11
Reach	28303.36	10 year	PROPBIDGE	3640.00	112.05	123.89	115.06	123.96	0.000087	2.18	1959.96	424.76	0.12
Reach	28303.36	25 year	exist MEDOT	4440.00	112.05	124.87	115.47	124.96	0.000095	2.41	2513.37	915.67	0.12
Reach	28303.36	25 year	PROPBIDGE	4440.00	112.05	124.62	115.47	124.71	0.000101	2.45	2304.69	511.51	0.13
Reach	28303.36	50 year	exist MEDOT	5040.00	112.05	125.45	115.75	125.54	0.000099	2.54	3048.60	953.12	0.13
Reach	28303.36	50 year	PROPBIDGE	5040.00	112.05	125.14	115.75	125.25	0.000111	2.64	2761.73	934.12	0.13
Reach	28303.36	100 year	exist MEDOT	5680.00	112.05	125.13	116.05	125.27	0.000141	2.98	2754.18	933.58	0.15
Reach	28303.36	100 year	PROPBIDGE	5680.00	112.05	125.68	116.05	125.80	0.000115	2.78	3277.51	967.51	0.14
Reach	28303.36	500 year	exist MEDOT	7180.00	112.05	126.30	116.70	126.45	0.000148	3.25	3881.97	1006.01	0.16
Reach	28303.36	500 year	PROPBIDGE	7180.00	112.05	126.85	116.70	126.98	0.000122	3.03	4447.67	1043.33	0.14
Reach	28120.39	1.1 year	exist MEDOT	1210.00	117.00	120.91	118.65	121.02	0.000547	2.69	449.00	124.96	0.25
Reach	28120.39	1.1 year	PROPBIDGE	1210.00	117.00	120.85	118.65	120.96	0.000579	2.74	441.22	124.75	0.26
Reach	28120.39	10 year	exist MEDOT	3640.00	117.00	123.79	120.27	124.10	0.000689	4.45	854.06	186.41	0.31
Reach	28120.39	10 year	PROPBIDGE	3640.00	117.00	123.57	120.27	123.90	0.000778	4.62	818.11	180.74	0.33
Reach	28120.39	25 year	exist MEDOT	4440.00	117.00	124.53	120.71	124.90	0.000706	4.85	973.03	275.09	0.32
Reach	28120.39	25 year	PROPBIDGE	4440.00	117.00	124.25	120.71	124.64	0.000812	5.05	926.93	204.58	0.34
Reach	28120.39	50 year	exist MEDOT	5040.00	117.00	125.07	121.01	125.47	0.000711	5.10	1063.37	632.25	0.32
Reach	28120.39	50 year	PROPBIDGE	5040.00	117.00	124.73	121.01	125.17	0.000832	5.35	1004.77	617.79	0.35
Reach	28120.39	100 year	exist MEDOT	5680.00	117.00	124.58	121.33	125.16	0.001130	6.16	980.63	318.98	0.40
Reach	28120.39	100 year	PROPBIDGE	5680.00	117.00	125.23	121.33	125.71	0.000843	5.63	1089.87	639.35	0.35
Reach	28120.39	500 year	exist MEDOT	7180.00	117.00	125.64	122.00	126.33	0.001131	6.74	1159.29	655.76	0.41
Reach	28120.39	500 year	PROPBIDGE	7180.00	117.00	126.45	122.00	126.90	0.000696	5.63	2245.33	742.74	0.33
Reach	27966		Bridge										
Reach	27800.00	1.1 year	exist MEDOT	1210.00	117.55	120.54	119.38	120.81	0.001978	4.22	286.83	107.09	0.45
Reach	27800.00	1.1 year	PROPBIDGE	1210.00	117.55	120.54	119.38	120.81	0.001978	4.22	286.83	107.09	0.45
Reach	27800.00	10 year	exist MEDOT	3640.00	117.55	122.79	121.18	123.51	0.002343	6.80	539.19	124.48	0.55
Reach	27800.00	10 year	PROPBIDGE	3640.00	117.55	122.79	121.18	123.51	0.002343	6.80	539.19	124.48	0.55
Reach	27800.00	25 year	exist MEDOT	4440.00	117.55	123.32	121.65	124.19	0.002458	7.47	607.51	151.28	0.57
Reach	27800.00	25 year	PROPBIDGE	4440.00	117.55	123.32	121.65	124.19	0.002458	7.47	607.51	151.28	0.57
Reach	27800.00	50 year	exist MEDOT	5040.00	117.55	123.70	121.97	124.67	0.002527	7.92	655.99	165.53	0.58
Reach	27800.00	50 year	PROPBIDGE	5040.00	117.55	123.70	121.97	124.67	0.002527	7.92	656.02	165.54	0.58

HEC-RAS River: Souadabscook Str Reach: Reach (Continued)

Reach	River Sta	Profile	Plan	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	Crit W.S. (ft)	E.G. Elev (ft)	E.G. Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl
Reach	27800.00	100 year	exist MEDOT	5680.00	117.55	124.09	122.31	125.16	0.002562	8.33	707.87	206.70	0.59
Reach	27800.00	100 year	PROPBRIDGE	5680.00	117.55	124.09	122.31	125.16	0.002560	8.33	707.97	206.79	0.59
Reach	27800.00	500 year	exist MEDOT	7180.00	117.55	124.91	123.07	126.23	0.002670	9.25	817.02	557.64	0.62
Reach	27800.00	500 year	PROPBRIDGE	7180.00	117.55	124.91	123.07	126.23	0.002670	9.25	817.02	557.64	0.62
Reach	27564.50	1.1 year	exist MEDOT	1210.00	117.05	119.99	118.93	120.30	0.002353	4.47	270.48	105.82	0.49
Reach	27564.50	1.1 year	PROPBRIDGE	1210.00	117.05	119.99	118.93	120.30	0.002353	4.47	270.48	105.82	0.49
Reach	27564.50	10 year	exist MEDOT	3640.00	117.05	122.09	120.80	122.87	0.002977	7.11	521.97	205.70	0.60
Reach	27564.50	10 year	PROPBRIDGE	3640.00	117.05	122.09	120.80	122.87	0.002977	7.11	521.97	205.70	0.60
Reach	27564.50	25 year	exist MEDOT	4440.00	117.05	122.64	121.29	123.55	0.002949	7.66	610.61	264.12	0.61
Reach	27564.50	25 year	PROPBRIDGE	4440.00	117.05	122.64	121.29	123.55	0.002949	7.66	610.61	264.12	0.61
Reach	27564.50	50 year	exist MEDOT	5040.00	117.05	123.05	121.62	124.03	0.002870	7.98	686.25	307.79	0.61
Reach	27564.50	50 year	PROPBRIDGE	5040.00	117.05	123.05	121.62	124.03	0.002869	7.98	686.34	307.85	0.61
Reach	27564.50	100 year	exist MEDOT	5680.00	117.05	123.47	121.95	124.52	0.002782	8.28	773.37	356.14	0.61
Reach	27564.50	100 year	PROPBRIDGE	5680.00	117.05	123.48	121.95	124.52	0.002780	8.28	773.64	356.27	0.61
Reach	27564.50	500 year	exist MEDOT	7180.00	117.05	124.33	122.70	125.55	0.002703	8.96	978.39	473.26	0.62
Reach	27564.50	500 year	PROPBRIDGE	7180.00	117.05	124.33	122.70	125.55	0.002703	8.96	978.39	473.26	0.62
Reach	27381.56	1.1 year	exist MEDOT	1210.00	116.95	119.56		119.81	0.002756	4.03	300.04	155.03	0.51
Reach	27381.56	1.1 year	PROPBRIDGE	1210.00	116.95	119.56		119.81	0.002756	4.03	300.04	155.03	0.51
Reach	27381.56	10 year	exist MEDOT	3640.00	116.95	121.93		122.35	0.001778	5.22	702.70	195.56	0.46
Reach	27381.56	10 year	PROPBRIDGE	3640.00	116.95	121.93		122.35	0.001778	5.22	702.70	195.56	0.46
Reach	27381.56	25 year	exist MEDOT	4440.00	116.95	122.56		123.02	0.001613	5.48	831.66	214.62	0.45
Reach	27381.56	25 year	PROPBRIDGE	4440.00	116.95	122.56		123.02	0.001613	5.48	831.66	214.62	0.45
Reach	27381.56	50 year	exist MEDOT	5040.00	116.95	123.02		123.51	0.001498	5.63	935.04	228.43	0.44
Reach	27381.56	50 year	PROPBRIDGE	5040.00	116.95	123.02		123.51	0.001497	5.63	935.15	228.45	0.44
Reach	27381.56	100 year	exist MEDOT	5680.00	116.95	123.50		124.01	0.001403	5.79	1046.30	242.42	0.43
Reach	27381.56	100 year	PROPBRIDGE	5680.00	116.95	123.50		124.01	0.001402	5.79	1046.63	242.46	0.43
Reach	27381.56	500 year	exist MEDOT	7180.00	116.95	124.44		125.03	0.001306	6.20	1287.72	270.29	0.43
Reach	27381.56	500 year	PROPBRIDGE	7180.00	116.95	124.44		125.03	0.001306	6.20	1287.72	270.29	0.43
Reach	26951.26	1.1 year	exist MEDOT	1210.00	115.75	118.33	117.43	118.66	0.002622	4.55	265.97	109.67	0.52
Reach	26951.26	1.1 year	PROPBRIDGE	1210.00	115.75	118.33	117.43	118.66	0.002622	4.55	265.97	109.67	0.52
Reach	26951.26	10 year	exist MEDOT	3640.00	115.75	120.68	119.17	121.40	0.002623	6.80	535.61	120.09	0.57
Reach	26951.26	10 year	PROPBRIDGE	3640.00	115.75	120.68	119.17	121.40	0.002623	6.80	535.61	120.09	0.57
Reach	26951.26	25 year	exist MEDOT	4440.00	115.75	121.29	119.63	122.11	0.002619	7.28	609.49	122.79	0.58
Reach	26951.26	25 year	PROPBRIDGE	4440.00	115.75	121.29	119.63	122.11	0.002619	7.28	609.49	122.79	0.58
Reach	26951.26	50 year	exist MEDOT	5040.00	115.75	121.75	119.98	122.64	0.002622	7.56	667.01	127.27	0.58
Reach	26951.26	50 year	PROPBRIDGE	5040.00	115.75	121.75	119.98	122.64	0.002621	7.56	667.08	127.28	0.58
Reach	26951.26	100 year	exist MEDOT	5680.00	115.75	122.22	120.32	123.16	0.002625	7.81	727.30	132.53	0.59
Reach	26951.26	100 year	PROPBRIDGE	5680.00	115.75	122.22	120.30	123.16	0.002621	7.81	727.69	132.57	0.59
Reach	26951.26	500 year	exist MEDOT	7180.00	115.75	123.06	121.03	124.20	0.002622	8.54	845.82	149.96	0.60
Reach	26951.26	500 year	PROPBRIDGE	7180.00	115.75	123.06	121.03	124.20	0.002622	8.54	845.82	149.96	0.60

Plan: exist MEDOT Souadabscook Str Reach RS: 40346 Profile: 1.1 year

E.G. US. (ft)	122.07	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	122.01	E.G. Elev (ft)	122.05	122.00
Q Total (cfs)	1210.00	W.S. Elev (ft)	121.97	121.91
Q Bridge (cfs)	1210.00	Crit W.S. (ft)	116.59	117.05
Q Weir (cfs)		Max Chl Dpth (ft)	10.00	9.01
Weir Sta Lft (ft)		Vel Total (ft/s)	2.34	2.37
Weir Sta Rgt (ft)		Flow Area (sq ft)	517.97	509.61
Weir Submerg		Froude # Chl	0.17	0.17
Weir Max Depth (ft)		Specif Force (cu ft)	1950.12	1825.81
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	5.81	5.67
Min El Prs (ft)	132.13	W.P. Total (ft)	116.35	116.38
Delta EG (ft)	0.11	Conv. Total (cfs)	71364.2	69288.8
Delta WS (ft)	0.12	Top Width (ft)	89.12	89.81
BR Open Area (sq ft)	1586.19	Frctn Loss (ft)	0.05	0.02
BR Open Vel (ft/s)	2.37	C & E Loss (ft)	0.00	0.01
BR Sluice Coef		Shear Total (lb/sq ft)	0.08	0.08
BR Sel Method	Energy only	Power Total (lb/ft s)	0.19	0.20

Plan: exist MEDOT Souadabscook Str Reach RS: 40346 Profile: 10 year

E.G. US. (ft)	125.67	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.48	E.G. Elev (ft)	125.61	125.47
Q Total (cfs)	3640.00	W.S. Elev (ft)	125.29	125.14
Q Bridge (cfs)	3640.00	Crit W.S. (ft)	119.67	119.76
Q Weir (cfs)		Max Chl Dpth (ft)	13.32	12.24
Weir Sta Lft (ft)		Vel Total (ft/s)	4.38	4.45
Weir Sta Rgt (ft)		Flow Area (sq ft)	831.91	817.96
Weir Submerg		Froude # Chl	0.26	0.27
Weir Max Depth (ft)		Specif Force (cu ft)	4606.31	4393.61
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	8.34	8.15
Min El Prs (ft)	132.13	W.P. Total (ft)	141.85	141.44
Delta EG (ft)	0.30	Conv. Total (cfs)	136993.2	133145.6
Delta WS (ft)	0.33	Top Width (ft)	99.74	100.42
BR Open Area (sq ft)	1586.19	Frctn Loss (ft)	0.13	0.05
BR Open Vel (ft/s)	4.45	C & E Loss (ft)	0.00	0.05
BR Sluice Coef		Shear Total (lb/sq ft)	0.26	0.27
BR Sel Method	Energy only	Power Total (lb/ft s)	1.13	1.20

Plan: exist MEDOT Souadabscook Str Reach RS: 40346 Profile: 25 year

E.G. US. (ft)	126.64	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.40	E.G. Elev (ft)	126.56	126.41
Q Total (cfs)	4440.00	W.S. Elev (ft)	126.17	126.00
Q Bridge (cfs)	4440.00	Crit W.S. (ft)	120.24	120.32
Q Weir (cfs)		Max Chl Dpth (ft)	14.20	13.10
Weir Sta Lft (ft)		Vel Total (ft/s)	4.82	4.90
Weir Sta Rgt (ft)		Flow Area (sq ft)	921.03	905.49
Weir Submerg		Froude # Chl	0.28	0.29
Weir Max Depth (ft)		Specif Force (cu ft)	5557.47	5316.89
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	8.98	8.80
Min El Prs (ft)	132.13	W.P. Total (ft)	148.61	147.85
Delta EG (ft)	0.35	Conv. Total (cfs)	156637.1	152478.9
Delta WS (ft)	0.38	Top Width (ft)	102.55	102.92
BR Open Area (sq ft)	1586.19	Frctn Loss (ft)	0.15	0.05
BR Open Vel (ft/s)	4.90	C & E Loss (ft)	0.00	0.07
BR Sluice Coef		Shear Total (lb/sq ft)	0.31	0.32
BR Sel Method	Energy only	Power Total (lb/ft s)	1.50	1.59

Plan: exist MEDOT Souadabscook Str Reach RS: 40346 Profile: 50 year

E.G. US. (ft)	127.32	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	127.06	E.G. Elev (ft)	127.24	127.07
Q Total (cfs)	5040.00	W.S. Elev (ft)	126.79	126.61
Q Bridge (cfs)	5040.00	Crit W.S. (ft)	120.65	120.73
Q Weir (cfs)		Max Chl Dpth (ft)	14.82	13.71
Weir Sta Lft (ft)		Vel Total (ft/s)	5.11	5.20
Weir Sta Rgt (ft)		Flow Area (sq ft)	985.45	968.66
Weir Submerg		Froude # Chl	0.29	0.30
Weir Max Depth (ft)		Specif Force (cu ft)	6294.17	6032.81
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	9.43	9.25
Min El Prs (ft)	132.13	W.P. Total (ft)	153.38	152.37
Delta EG (ft)	0.38	Conv. Total (cfs)	171039.0	166649.3
Delta WS (ft)	0.42	Top Width (ft)	104.54	104.69
BR Open Area (sq ft)	1586.19	Frctn Loss (ft)	0.16	0.05
BR Open Vel (ft/s)	5.20	C & E Loss (ft)	0.00	0.08
BR Sluice Coef		Shear Total (lb/sq ft)	0.35	0.36
BR Sel Method	Energy only	Power Total (lb/ft s)	1.78	1.89

Plan: exist MEDOT Souadabscook Str Reach RS: 40346 Profile: 100 year

E.G. US. (ft)	127.59	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	127.27	E.G. Elev (ft)	127.49	127.28
Q Total (cfs)	5680.00	W.S. Elev (ft)	126.94	126.71
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	121.07	121.14
Q Weir (cfs)		Max Chl Dpth (ft)	14.97	13.81
Weir Sta Lft (ft)		Vel Total (ft/s)	5.67	5.80
Weir Sta Rgt (ft)		Flow Area (sq ft)	1000.93	979.12
Weir Submerg		Froude # Chl	0.32	0.33
Weir Max Depth (ft)		Specif Force (cu ft)	6650.50	6347.90
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	9.53	9.33
Min El Prs (ft)	132.13	W.P. Total (ft)	154.51	153.11
Delta EG (ft)	0.47	Conv. Total (cfs)	174520.4	169013.2
Delta WS (ft)	0.53	Top Width (ft)	105.01	104.98
BR Open Area (sq ft)	1586.19	Frctn Loss (ft)	0.20	0.07
BR Open Vel (ft/s)	5.80	C & E Loss (ft)	0.01	0.10
BR Sluice Coef		Shear Total (lb/sq ft)	0.43	0.45
BR Sel Method	Energy only	Power Total (lb/ft s)	2.43	2.62

Plan: exist MEDOT Souadabscook Str Reach RS: 40346 Profile: 500 year

E.G. US. (ft)	129.07	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	128.67	E.G. Elev (ft)	128.95	128.71
Q Total (cfs)	7180.00	W.S. Elev (ft)	128.26	128.00
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.99	122.05
Q Weir (cfs)		Max Chl Dpth (ft)	16.29	15.10
Weir Sta Lft (ft)		Vel Total (ft/s)	6.28	6.43
Weir Sta Rgt (ft)		Flow Area (sq ft)	1142.50	1116.64
Weir Submerg		Froude # Chl	0.34	0.35
Weir Max Depth (ft)		Specif Force (cu ft)	8492.83	8131.72
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	10.46	10.27
Min El Prs (ft)	132.13	W.P. Total (ft)	164.65	162.69
Delta EG (ft)	0.56	Conv. Total (cfs)	206728.7	200418.2
Delta WS (ft)	0.62	Top Width (ft)	109.23	108.72
BR Open Area (sq ft)	1586.19	Frctn Loss (ft)	0.23	0.07
BR Open Vel (ft/s)	6.43	C & E Loss (ft)	0.01	0.12
BR Sluice Coef		Shear Total (lb/sq ft)	0.52	0.55
BR Sel Method	Energy only	Power Total (lb/ft s)	3.28	3.54

Plan: exist MEDOT Souadabscook Str Reach RS: 35151 Profile: 1.1 year

E.G. US. (ft)	121.50	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	121.47	E.G. Elev (ft)	121.51	121.27
Q Total (cfs)	1210.00	W.S. Elev (ft)	121.42	121.16
Q Bridge (cfs)	1210.00	Crit W.S. (ft)	116.22	115.91
Q Weir (cfs)		Max Chl Dpth (ft)	8.31	8.37
Weir Sta Lft (ft)		Vel Total (ft/s)	2.43	2.55
Weir Sta Rgt (ft)		Flow Area (sq ft)	498.84	474.16
Weir Submerg		Froude # Chl	0.17	0.17
Weir Max Depth (ft)		Specif Force (cu ft)	1858.00	1825.82
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	6.03	6.35
Min El Prs (ft)	132.25	W.P. Total (ft)	112.94	103.61
Delta EG (ft)	0.26	Conv. Total (cfs)	66375.5	66861.2
Delta WS (ft)	0.27	Top Width (ft)	82.73	74.62
BR Open Area (sq ft)	1625.91	Frctn Loss (ft)		
BR Open Vel (ft/s)	2.55	C & E Loss (ft)		
BR Sluice Coef		Shear Total (lb/sq ft)	0.09	0.09
BR Sel Method	Momentum	Power Total (lb/ft s)	0.22	0.24

Plan: exist MEDOT Souadabscook Str Reach RS: 35151 Profile: 10 year

E.G. US. (ft)	125.01	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	124.91	E.G. Elev (ft)	124.92	124.72
Q Total (cfs)	3640.00	W.S. Elev (ft)	124.55	124.31
Q Bridge (cfs)	3640.00	Crit W.S. (ft)	119.02	118.71
Q Weir (cfs)		Max Chl Dpth (ft)	11.44	11.52
Weir Sta Lft (ft)		Vel Total (ft/s)	4.70	4.94
Weir Sta Rgt (ft)		Flow Area (sq ft)	775.08	736.45
Weir Submerg		Froude # Chl	0.28	0.29
Weir Max Depth (ft)		Specif Force (cu ft)	4298.45	4195.27
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	8.25	7.89
Min El Prs (ft)	132.25	W.P. Total (ft)	137.99	135.64
Delta EG (ft)	0.45	Conv. Total (cfs)	121321.3	118494.7
Delta WS (ft)	0.51	Top Width (ft)	93.95	93.33
BR Open Area (sq ft)	1625.91	Frctn Loss (ft)	0.19	0.03
BR Open Vel (ft/s)	4.94	C & E Loss (ft)	0.01	0.12
BR Sluice Coef		Shear Total (lb/sq ft)	0.32	0.32
BR Sel Method	Energy only	Power Total (lb/ft s)	1.48	1.58

Plan: exist MEDOT Souadabscook Str Reach RS: 35151 Profile: 25 year

E.G. US. (ft)	125.94	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.81	E.G. Elev (ft)	125.82	125.58
Q Total (cfs)	4440.00	W.S. Elev (ft)	125.37	125.07
Q Bridge (cfs)	4440.00	Crit W.S. (ft)	119.69	119.39
Q Weir (cfs)		Max Chl Dpth (ft)	12.26	12.28
Weir Sta Lft (ft)		Vel Total (ft/s)	5.20	5.49
Weir Sta Rgt (ft)		Flow Area (sq ft)	853.17	809.40
Weir Submerg		Froude # Chl	0.30	0.31
Weir Max Depth (ft)		Specif Force (cu ft)	5157.59	4994.92
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	8.75	8.29
Min El Prs (ft)	132.25	W.P. Total (ft)	145.03	143.17
Delta EG (ft)	0.54	Conv. Total (cfs)	137460.2	132770.9
Delta WS (ft)	0.62	Top Width (ft)	97.48	97.63
BR Open Area (sq ft)	1625.91	Frctn Loss (ft)	0.22	0.03
BR Open Vel (ft/s)	5.49	C & E Loss (ft)	0.02	0.15
BR Sluice Coef		Shear Total (lb/sq ft)	0.38	0.39
BR Sel Method	Energy only	Power Total (lb/ft s)	1.99	2.17

Plan: exist MEDOT Souadabscook Str Reach RS: 35151 Profile: 50 year

E.G. US. (ft)	126.58	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.44	E.G. Elev (ft)	126.45	126.19
Q Total (cfs)	5040.00	W.S. Elev (ft)	125.94	125.60
Q Bridge (cfs)	5040.00	Crit W.S. (ft)	120.12	119.85
Q Weir (cfs)		Max Chl Dpth (ft)	12.83	12.81
Weir Sta Lft (ft)		Vel Total (ft/s)	5.54	5.85
Weir Sta Rgt (ft)		Flow Area (sq ft)	909.30	862.08
Weir Submerg		Froude # Chl	0.31	0.33
Weir Max Depth (ft)		Specif Force (cu ft)	5816.35	5610.27
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	9.10	8.63
Min El Prs (ft)	132.25	W.P. Total (ft)	149.95	147.73
Delta EG (ft)	0.60	Conv. Total (cfs)	149156.6	143190.0
Delta WS (ft)	0.69	Top Width (ft)	99.93	99.88
BR Open Area (sq ft)	1625.91	Frctn Loss (ft)	0.24	0.03
BR Open Vel (ft/s)	5.85	C & E Loss (ft)	0.02	0.18
BR Sluice Coef		Shear Total (lb/sq ft)	0.43	0.45
BR Sel Method	Energy only	Power Total (lb/ft s)	2.40	2.64

Plan: exist MEDOT Souadabscook Str Reach RS: 35151 Profile: 100 year

E.G. US. (ft)	126.69	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.50	E.G. Elev (ft)	126.52	126.16
Q Total (cfs)	5680.00	W.S. Elev (ft)	125.85	125.38
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	120.55	120.32
Q Weir (cfs)		Max Chl Dpth (ft)	12.74	12.59
Weir Sta Lft (ft)		Vel Total (ft/s)	6.31	6.77
Weir Sta Rgt (ft)		Flow Area (sq ft)	900.34	839.51
Weir Submerg		Froude # Chl	0.36	0.38
Weir Max Depth (ft)		Specif Force (cu ft)	5988.41	5706.55
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	9.04	8.49
Min El Prs (ft)	132.25	W.P. Total (ft)	149.17	145.79
Delta EG (ft)	0.81	Conv. Total (cfs)	147285.1	138714.8
Delta WS (ft)	0.94	Top Width (ft)	99.54	98.92
BR Open Area (sq ft)	1625.91	Frctn Loss (ft)	0.32	0.05
BR Open Vel (ft/s)	6.77	C & E Loss (ft)	0.04	0.24
BR Sluice Coef		Shear Total (lb/sq ft)	0.56	0.60
BR Sel Method	Energy only	Power Total (lb/ft s)	3.54	4.08

Plan: exist MEDOT Souadabscook Str Reach RS: 35151 Profile: 500 year

E.G. US. (ft)	128.06	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	127.83	E.G. Elev (ft)	127.85	127.43
Q Total (cfs)	7180.00	W.S. Elev (ft)	127.01	126.42
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.53	121.39
Q Weir (cfs)		Max Chl Dpth (ft)	13.90	13.63
Weir Sta Lft (ft)		Vel Total (ft/s)	7.05	7.60
Weir Sta Rgt (ft)		Flow Area (sq ft)	1018.49	944.63
Weir Submerg		Froude # Chl	0.38	0.42
Weir Max Depth (ft)		Specif Force (cu ft)	7584.11	7171.04
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	9.74	9.14
Min El Prs (ft)	132.25	W.P. Total (ft)	159.17	154.67
Delta EG (ft)	0.99	Conv. Total (cfs)	172102.7	159713.9
Delta WS (ft)	1.17	Top Width (ft)	104.54	103.31
BR Open Area (sq ft)	1625.91	Frctn Loss (ft)	0.38	0.05
BR Open Vel (ft/s)	7.60	C & E Loss (ft)	0.05	0.30
BR Sluice Coef		Shear Total (lb/sq ft)	0.70	0.77
BR Sel Method	Energy only	Power Total (lb/ft s)	4.90	5.86

Plan: exist MEDOT Souadabscook Str Reach RS: 27966 Profile: 1.1 year

E.G. US. (ft)	121.02	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	120.91	E.G. Elev (ft)	121.00	120.89
Q Total (cfs)	1210.00	W.S. Elev (ft)	120.86	120.74
Q Bridge (cfs)	1210.00	Crit W.S. (ft)	115.84	116.09
Q Weir (cfs)		Max Chl Dpth (ft)	8.76	7.94
Weir Sta Lft (ft)		Vel Total (ft/s)	2.97	3.04
Weir Sta Rgt (ft)		Flow Area (sq ft)	407.20	398.09
Weir Submerg		Froude # Chl	0.21	0.22
Weir Max Depth (ft)		Specif Force (cu ft)	1592.25	1464.35
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	5.92	5.39
Min El Prs (ft)	132.04	W.P. Total (ft)	95.16	99.95
Delta EG (ft)	0.21	Conv. Total (cfs)	55154.4	51902.3
Delta WS (ft)	0.37	Top Width (ft)	68.84	73.84
BR Open Area (sq ft)	1512.98	Frctn Loss (ft)	0.11	0.06
BR Open Vel (ft/s)	3.04	C & E Loss (ft)	0.00	0.01
BR Sluice Coef		Shear Total (lb/sq ft)	0.13	0.14
BR Sel Method	Energy only	Power Total (lb/ft s)	0.38	0.41

Plan: exist MEDOT Souadabscook Str Reach RS: 27966 Profile: 10 year

E.G. US. (ft)	124.10	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	123.79	E.G. Elev (ft)	124.02	123.65
Q Total (cfs)	3640.00	W.S. Elev (ft)	123.41	122.98
Q Bridge (cfs)	3640.00	Crit W.S. (ft)	119.03	119.22
Q Weir (cfs)		Max Chl Dpth (ft)	11.31	10.18
Weir Sta Lft (ft)		Vel Total (ft/s)	6.07	6.33
Weir Sta Rgt (ft)		Flow Area (sq ft)	599.29	574.64
Weir Submerg		Froude # Chl	0.38	0.41
Weir Max Depth (ft)		Specif Force (cu ft)	3465.37	3173.50
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.32	6.88
Min El Prs (ft)	132.04	W.P. Total (ft)	117.68	118.27
Delta EG (ft)	0.59	Conv. Total (cfs)	91027.9	83953.7
Delta WS (ft)	1.00	Top Width (ft)	81.83	83.58
BR Open Area (sq ft)	1512.98	Frctn Loss (ft)	0.37	0.13
BR Open Vel (ft/s)	6.33	C & E Loss (ft)	0.01	0.01
BR Sluice Coef		Shear Total (lb/sq ft)	0.51	0.57
BR Sel Method	Energy only	Power Total (lb/ft s)	3.09	3.61

Plan: exist MEDOT Souadabscook Str Reach RS: 27966 Profile: 25 year

E.G. US. (ft)	124.90	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	124.53	E.G. Elev (ft)	124.80	124.34
Q Total (cfs)	4440.00	W.S. Elev (ft)	124.01	123.47
Q Bridge (cfs)	4440.00	Crit W.S. (ft)	119.76	120.04
Q Weir (cfs)		Max Chl Dpth (ft)	11.91	10.67
Weir Sta Lft (ft)		Vel Total (ft/s)	6.83	7.20
Weir Sta Rgt (ft)		Flow Area (sq ft)	650.07	616.28
Weir Submerg		Froude # Chl	0.41	0.45
Weir Max Depth (ft)		Specif Force (cu ft)	4114.14	3755.56
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.65	7.19
Min El Prs (ft)	132.04	W.P. Total (ft)	123.06	122.29
Delta EG (ft)	0.71	Conv. Total (cfs)	100733.9	91788.4
Delta WS (ft)	1.21	Top Width (ft)	84.93	85.72
BR Open Area (sq ft)	1512.98	Frctn Loss (ft)	0.45	0.15
BR Open Vel (ft/s)	7.20	C & E Loss (ft)	0.01	0.00
BR Sluice Coef		Shear Total (lb/sq ft)	0.64	0.74
BR Sel Method	Energy only	Power Total (lb/ft s)	4.38	5.30

Plan: exist MEDOT Souadabscook Str Reach RS: 27966 Profile: 50 year

E.G. US. (ft)	125.47	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.07	E.G. Elev (ft)	125.37	124.85
Q Total (cfs)	5040.00	W.S. Elev (ft)	124.45	123.82
Q Bridge (cfs)	5040.00	Crit W.S. (ft)	120.29	120.56
Q Weir (cfs)		Max Chl Dpth (ft)	12.35	11.02
Weir Sta Lft (ft)		Vel Total (ft/s)	7.33	7.80
Weir Sta Rgt (ft)		Flow Area (sq ft)	687.85	646.44
Weir Submerg		Froude # Chl	0.44	0.49
Weir Max Depth (ft)		Specif Force (cu ft)	4624.57	4213.20
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.88	7.41
Min El Prs (ft)	132.04	W.P. Total (ft)	126.99	125.13
Delta EG (ft)	0.81	Conv. Total (cfs)	108005.1	97510.9
Delta WS (ft)	1.38	Top Width (ft)	87.24	87.23
BR Open Area (sq ft)	1512.98	Frctn Loss (ft)	0.51	0.16
BR Open Vel (ft/s)	7.80	C & E Loss (ft)	0.01	0.02
BR Sluice Coef		Shear Total (lb/sq ft)	0.74	0.86
BR Sel Method	Energy only	Power Total (lb/ft s)	5.40	6.72

Plan: exist MEDOT Souadabscook Str Reach RS: 27966 Profile: 100 year

E.G. US. (ft)	125.16	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	124.58	E.G. Elev (ft)	123.95	123.99
Q Total (cfs)	5680.00	W.S. Elev (ft)	120.83	121.06
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	120.83	121.06
Q Weir (cfs)		Max Chl Dpth (ft)	8.73	8.26
Weir Sta Lft (ft)		Vel Total (ft/s)	14.02	13.46
Weir Sta Rgt (ft)		Flow Area (sq ft)	405.20	421.86
Weir Submerg		Froude # Chl	0.98	0.95
Weir Max Depth (ft)		Specif Force (cu ft)	3967.04	3898.27
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	5.90	5.61
Min El Prs (ft)	132.04	W.P. Total (ft)	94.91	102.56
Delta EG (ft)	-1.40	Conv. Total (cfs)	54789.3	56077.0
Delta WS (ft)	2.27	Top Width (ft)	68.69	75.22
BR Open Area (sq ft)	1512.98	Frctn Loss (ft)		
BR Open Vel (ft/s)	14.02	C & E Loss (ft)		
BR Sluice Coef		Shear Total (lb/sq ft)	2.86	2.63
BR Sel Method	Momentum	Power Total (lb/ft s)	40.16	35.47

Plan: exist MEDOT Souadabscook Str Reach RS: 27966 Profile: 500 year

E.G. US. (ft)	126.33	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.64	E.G. Elev (ft)	125.50	125.45
Q Total (cfs)	7180.00	W.S. Elev (ft)	121.99	122.14
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.99	122.14
Q Weir (cfs)		Max Chl Dpth (ft)	9.89	9.34
Weir Sta Lft (ft)		Vel Total (ft/s)	14.69	14.20
Weir Sta Rgt (ft)		Flow Area (sq ft)	488.82	505.71
Weir Submerg		Froude # Chl	0.97	0.95
Weir Max Depth (ft)		Specif Force (cu ft)	5333.81	5227.07
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	6.55	6.33
Min El Prs (ft)	132.04	W.P. Total (ft)	105.21	111.38
Delta EG (ft)	-1.62	Conv. Total (cfs)	70227.2	71184.8
Delta WS (ft)	2.57	Top Width (ft)	74.63	79.92
BR Open Area (sq ft)	1512.98	Frctn Loss (ft)		
BR Open Vel (ft/s)	14.69	C & E Loss (ft)		
BR Sluice Coef		Shear Total (lb/sq ft)	3.03	2.88
BR Sel Method	Momentum	Power Total (lb/ft s)	44.54	40.94

Plan: PROPBRIDGE Souadabscook Str Reach RS: 40346 Profile: 1.1 year

E.G. US. (ft)	121.99	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	121.93	E.G. Elev (ft)	121.97	121.91
Q Total (cfs)	1210.00	W.S. Elev (ft)	121.88	121.83
Q Bridge (cfs)	1210.00	Crit W.S. (ft)	116.90	117.31
Q Weir (cfs)		Max Chl Dpth (ft)	9.91	8.93
Weir Sta Lft (ft)		Vel Total (ft/s)	2.32	2.33
Weir Sta Rgt (ft)		Flow Area (sq ft)	522.26	519.92
Weir Submerg		Froude # Chl	0.17	0.17
Weir Max Depth (ft)		Specif Force (cu ft)	1866.35	1754.15
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	5.47	5.14
Min El Prs (ft)	130.00	W.P. Total (ft)	116.20	120.31
Delta EG (ft)	0.11	Conv. Total (cfs)	72882.3	71282.8
Delta WS (ft)	0.11	Top Width (ft)	95.56	101.17
BR Open Area (sq ft)	1467.71	Frctn Loss (ft)	0.05	0.02
BR Open Vel (ft/s)	2.33	C & E Loss (ft)	0.00	0.01
BR Sluice Coef		Shear Total (lb/sq ft)	0.08	0.08
BR Sel Method	Energy only	Power Total (lb/ft s)	0.18	0.18

Plan: PROPBRIDGE Souadabscook Str Reach RS: 40346 Profile: 10 year

E.G. US. (ft)	125.44	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.23	E.G. Elev (ft)	125.38	125.27
Q Total (cfs)	3640.00	W.S. Elev (ft)	125.07	124.96
Q Bridge (cfs)	3640.00	Crit W.S. (ft)	119.74	119.81
Q Weir (cfs)		Max Chl Dpth (ft)	13.10	12.06
Weir Sta Lft (ft)		Vel Total (ft/s)	4.17	4.13
Weir Sta Rgt (ft)		Flow Area (sq ft)	872.26	881.63
Weir Submerg		Froude # Chl	0.26	0.27
Weir Max Depth (ft)		Specif Force (cu ft)	4491.33	4347.46
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	7.51	7.17
Min El Prs (ft)	130.00	W.P. Total (ft)	145.15	150.95
Delta EG (ft)	0.26	Conv. Total (cfs)	146933.7	144729.0
Delta WS (ft)	0.28	Top Width (ft)	116.13	122.99
BR Open Area (sq ft)	1467.71	Frctn Loss (ft)	0.11	0.05
BR Open Vel (ft/s)	4.17	C & E Loss (ft)	0.00	0.04
BR Sluice Coef		Shear Total (lb/sq ft)	0.23	0.23
BR Sel Method	Energy only	Power Total (lb/ft s)	0.96	0.95

Plan: PROPBRIDGE Souadabscook Str Reach RS: 40346 Profile: 25 year

E.G. US. (ft)	126.34	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.08	E.G. Elev (ft)	126.27	126.14
Q Total (cfs)	4440.00	W.S. Elev (ft)	125.90	125.76
Q Bridge (cfs)	4440.00	Crit W.S. (ft)	120.29	120.36
Q Weir (cfs)		Max Chl Dpth (ft)	13.93	12.86
Weir Sta Lft (ft)		Vel Total (ft/s)	4.59	4.53
Weir Sta Rgt (ft)		Flow Area (sq ft)	968.13	980.99
Weir Submerg		Froude # Chl	0.28	0.28
Weir Max Depth (ft)		Specif Force (cu ft)	5420.76	5273.00
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	8.23	7.97
Min El Prs (ft)	130.00	W.P. Total (ft)	149.27	154.18
Delta EG (ft)	0.29	Conv. Total (cfs)	169086.3	166996.8
Delta WS (ft)	0.33	Top Width (ft)	117.66	123.08
BR Open Area (sq ft)	1467.71	Frctn Loss (ft)	0.13	0.05
BR Open Vel (ft/s)	4.59	C & E Loss (ft)	0.00	0.05
BR Sluice Coef		Shear Total (lb/sq ft)	0.28	0.28
BR Sel Method	Energy only	Power Total (lb/ft s)	1.28	1.27

Plan: PROPBRIDGE Souadabscook Str Reach RS: 40346 Profile: 50 year

E.G. US. (ft)	126.97	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.68	E.G. Elev (ft)	126.89	126.76
Q Total (cfs)	5040.00	W.S. Elev (ft)	126.47	126.33
Q Bridge (cfs)	5040.00	Crit W.S. (ft)	120.68	120.76
Q Weir (cfs)		Max Chl Dpth (ft)	14.50	13.43
Weir Sta Lft (ft)		Vel Total (ft/s)	4.87	4.80
Weir Sta Rgt (ft)		Flow Area (sq ft)	1035.56	1050.28
Weir Submerg		Froude # Chl	0.29	0.30
Weir Max Depth (ft)		Specif Force (cu ft)	6133.74	5984.76
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	8.72	8.53
Min El Prs (ft)	130.00	W.P. Total (ft)	152.13	156.43
Delta EG (ft)	0.32	Conv. Total (cfs)	185153.3	183173.7
Delta WS (ft)	0.35	Top Width (ft)	118.72	123.14
BR Open Area (sq ft)	1467.71	Frctn Loss (ft)	0.14	0.05
BR Open Vel (ft/s)	4.87	C & E Loss (ft)	0.00	0.05
BR Sluice Coef		Shear Total (lb/sq ft)	0.31	0.32
BR Sel Method	Energy only	Power Total (lb/ft s)	1.53	1.52

Plan: PROPBRIDGE Souadabscook Str Reach RS: 40346 Profile: 100 year

E.G. US. (ft)	127.62	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	127.29	E.G. Elev (ft)	127.54	127.39
Q Total (cfs)	5680.00	W.S. Elev (ft)	127.05	126.91
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	121.09	121.17
Q Weir (cfs)		Max Chl Dpth (ft)	15.08	14.01
Weir Sta Lft (ft)		Vel Total (ft/s)	5.14	5.06
Weir Sta Rgt (ft)		Flow Area (sq ft)	1105.75	1121.92
Weir Submerg		Froude # Chl	0.30	0.31
Weir Max Depth (ft)		Specif Force (cu ft)	6922.23	6773.30
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	9.23	9.11
Min El Prs (ft)	130.00	W.P. Total (ft)	155.09	158.76
Delta EG (ft)	0.34	Conv. Total (cfs)	202270.7	200426.7
Delta WS (ft)	0.38	Top Width (ft)	119.82	123.20
BR Open Area (sq ft)	1467.71	Frctn Loss (ft)	0.14	0.06
BR Open Vel (ft/s)	5.14	C & E Loss (ft)	0.00	0.06
BR Sluice Coef		Shear Total (lb/sq ft)	0.35	0.35
BR Sel Method	Energy only	Power Total (lb/ft s)	1.80	1.79

Plan: PROPBRIDGE Souadabscook Str Reach RS: 40346 Profile: 500 year

E.G. US. (ft)	129.03	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	128.63	E.G. Elev (ft)	128.94	128.77
Q Total (cfs)	7180.00	W.S. Elev (ft)	128.33	128.17
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.95	121.96
Q Weir (cfs)		Max Chl Dpth (ft)	16.36	15.27
Weir Sta Lft (ft)		Vel Total (ft/s)	5.69	5.62
Weir Sta Rgt (ft)		Flow Area (sq ft)	1261.67	1277.38
Weir Submerg		Froude # Chl	0.32	0.32
Weir Max Depth (ft)		Specif Force (cu ft)	8836.22	8684.61
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	10.23	10.36
Min El Prs (ft)	130.00	W.P. Total (ft)	163.22	163.81
Delta EG (ft)	0.40	Conv. Total (cfs)	241089.9	239580.5
Delta WS (ft)	0.45	Top Width (ft)	123.36	123.34
BR Open Area (sq ft)	1467.71	Frctn Loss (ft)	0.16	0.06
BR Open Vel (ft/s)	5.69	C & E Loss (ft)	0.00	0.07
BR Sluice Coef		Shear Total (lb/sq ft)	0.43	0.44
BR Sel Method	Energy only	Power Total (lb/ft s)	2.44	2.46

Plan: PROPBRIDGE Souadabscook Str Reach RS: 35151 Profile: 1.1 year

E.G. US. (ft)	121.39	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	121.36	E.G. Elev (ft)	121.40	121.21
Q Total (cfs)	1210.00	W.S. Elev (ft)	121.31	121.11
Q Bridge (cfs)	1210.00	Crit W.S. (ft)	116.22	115.94
Q Weir (cfs)		Max Chl Dpth (ft)	8.20	8.32
Weir Sta Lft (ft)		Vel Total (ft/s)	2.36	2.47
Weir Sta Rgt (ft)		Flow Area (sq ft)	513.49	489.26
Weir Submerg		Froude # Chl	0.17	0.17
Weir Max Depth (ft)		Specif Force (cu ft)	1866.55	1839.28
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	5.94	6.20
Min El Prs (ft)	130.00	W.P. Total (ft)	105.17	98.32
Delta EG (ft)	0.20	Conv. Total (cfs)	73317.6	73329.1
Delta WS (ft)	0.21	Top Width (ft)	86.38	78.94
BR Open Area (sq ft)	1457.75	Frctn Loss (ft)		
BR Open Vel (ft/s)	2.47	C & E Loss (ft)		
BR Sluice Coef		Shear Total (lb/sq ft)	0.08	0.08
BR Sel Method	Momentum	Power Total (lb/ft s)	0.20	0.21

Plan: PROPBRIDGE Souadabscook Str Reach RS: 35151 Profile: 10 year

E.G. US. (ft)	124.78	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	124.67	E.G. Elev (ft)	124.69	124.54
Q Total (cfs)	3640.00	W.S. Elev (ft)	124.35	124.15
Q Bridge (cfs)	3640.00	Crit W.S. (ft)	118.89	118.67
Q Weir (cfs)		Max Chl Dpth (ft)	11.24	11.36
Weir Sta Lft (ft)		Vel Total (ft/s)	4.50	4.67
Weir Sta Rgt (ft)		Flow Area (sq ft)	809.51	779.72
Weir Submerg		Froude # Chl	0.27	0.28
Weir Max Depth (ft)		Specif Force (cu ft)	4300.14	4210.54
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.72	7.43
Min El Prs (ft)	130.00	W.P. Total (ft)	131.18	131.63
Delta EG (ft)	0.38	Conv. Total (cfs)	137895.4	134916.6
Delta WS (ft)	0.44	Top Width (ft)	104.85	104.96
BR Open Area (sq ft)	1457.75	Frctn Loss (ft)	0.14	0.03
BR Open Vel (ft/s)	4.67	C & E Loss (ft)	0.01	0.11
BR Sluice Coef		Shear Total (lb/sq ft)	0.27	0.27
BR Sel Method	Energy only	Power Total (lb/ft s)	1.21	1.26

Plan: PROPBRIDGE Souadabscook Str Reach RS: 35151 Profile: 25 year

E.G. US. (ft)	125.65	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.52	E.G. Elev (ft)	125.54	125.36
Q Total (cfs)	4440.00	W.S. Elev (ft)	125.11	124.88
Q Bridge (cfs)	4440.00	Crit W.S. (ft)	119.53	119.32
Q Weir (cfs)		Max Chl Dpth (ft)	12.00	12.09
Weir Sta Lft (ft)		Vel Total (ft/s)	4.98	5.18
Weir Sta Rgt (ft)		Flow Area (sq ft)	890.82	856.84
Weir Submerg		Froude # Chl	0.30	0.31
Weir Max Depth (ft)		Specif Force (cu ft)	5142.16	5008.01
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	8.27	7.96
Min El Prs (ft)	130.00	W.P. Total (ft)	135.87	136.02
Delta EG (ft)	0.45	Conv. Total (cfs)	156619.3	151960.1
Delta WS (ft)	0.53	Top Width (ft)	107.69	107.59
BR Open Area (sq ft)	1457.75	Frctn Loss (ft)	0.17	0.03
BR Open Vel (ft/s)	5.18	C & E Loss (ft)	0.02	0.13
BR Sluice Coef		Shear Total (lb/sq ft)	0.33	0.34
BR Sel Method	Energy only	Power Total (lb/ft s)	1.64	1.74

Plan: PROPBRIDGE Souadabscook Str Reach RS: 35151 Profile: 50 year

E.G. US. (ft)	126.25	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.10	E.G. Elev (ft)	126.13	125.93
Q Total (cfs)	5040.00	W.S. Elev (ft)	125.63	125.37
Q Bridge (cfs)	5040.00	Crit W.S. (ft)	119.96	119.76
Q Weir (cfs)		Max Chl Dpth (ft)	12.52	12.58
Weir Sta Lft (ft)		Vel Total (ft/s)	5.32	5.54
Weir Sta Rgt (ft)		Flow Area (sq ft)	947.43	910.16
Weir Submerg		Froude # Chl	0.31	0.33
Weir Max Depth (ft)		Specif Force (cu ft)	5777.71	5609.21
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	8.64	8.32
Min El Prs (ft)	130.00	W.P. Total (ft)	139.05	138.99
Delta EG (ft)	0.51	Conv. Total (cfs)	169882.7	163960.1
Delta WS (ft)	0.60	Top Width (ft)	109.62	109.37
BR Open Area (sq ft)	1457.75	Frctn Loss (ft)	0.18	0.03
BR Open Vel (ft/s)	5.54	C & E Loss (ft)	0.02	0.15
BR Sluice Coef		Shear Total (lb/sq ft)	0.37	0.39
BR Sel Method	Energy only	Power Total (lb/ft s)	1.99	2.14

Plan: PROPBRIDGE Souadabscook Str Reach RS: 35151 Profile: 100 year

E.G. US. (ft)	126.87	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.69	E.G. Elev (ft)	126.73	126.51
Q Total (cfs)	5680.00	W.S. Elev (ft)	126.17	125.88
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	120.39	120.22
Q Weir (cfs)		Max Chl Dpth (ft)	13.06	13.08
Weir Sta Lft (ft)		Vel Total (ft/s)	5.64	5.88
Weir Sta Rgt (ft)		Flow Area (sq ft)	1006.58	965.71
Weir Submerg		Froude # Chl	0.32	0.34
Weir Max Depth (ft)		Specif Force (cu ft)	6476.63	6269.94
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	9.02	8.69
Min El Prs (ft)	130.00	W.P. Total (ft)	142.33	142.04
Delta EG (ft)	0.57	Conv. Total (cfs)	183915.1	176626.1
Delta WS (ft)	0.68	Top Width (ft)	111.61	111.19
BR Open Area (sq ft)	1457.75	Frctn Loss (ft)	0.20	0.04
BR Open Vel (ft/s)	5.88	C & E Loss (ft)	0.02	0.17
BR Sluice Coef		Shear Total (lb/sq ft)	0.42	0.44
BR Sel Method	Energy only	Power Total (lb/ft s)	2.38	2.58

Plan: PROPBRIDGE Souadabscook Str Reach RS: 35151 Profile: 500 year

E.G. US. (ft)	128.20	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	127.98	E.G. Elev (ft)	128.03	127.77
Q Total (cfs)	7180.00	W.S. Elev (ft)	127.31	126.95
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.32	121.24
Q Weir (cfs)		Max Chl Dpth (ft)	14.20	14.16
Weir Sta Lft (ft)		Vel Total (ft/s)	6.32	6.61
Weir Sta Rgt (ft)		Flow Area (sq ft)	1136.07	1087.04
Weir Submerg		Froude # Chl	0.35	0.37
Weir Max Depth (ft)		Specif Force (cu ft)	8148.81	7853.60
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	9.81	9.45
Min El Prs (ft)	130.00	W.P. Total (ft)	149.29	148.52
Delta EG (ft)	0.70	Conv. Total (cfs)	215175.1	204808.5
Delta WS (ft)	0.85	Top Width (ft)	115.83	115.08
BR Open Area (sq ft)	1457.75	Frctn Loss (ft)	0.23	0.04
BR Open Vel (ft/s)	6.61	C & E Loss (ft)	0.03	0.22
BR Sluice Coef		Shear Total (lb/sq ft)	0.53	0.56
BR Sel Method	Energy only	Power Total (lb/ft s)	3.34	3.71

Plan: PROPBRIDGE Souadabscook Str Reach RS: 27966 Profile: 1.1 year

E.G. US. (ft)	120.96	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	120.85	E.G. Elev (ft)	120.94	120.87
Q Total (cfs)	1210.00	W.S. Elev (ft)	120.83	120.77
Q Bridge (cfs)	1210.00	Crit W.S. (ft)	115.98	115.95
Q Weir (cfs)		Max Chl Dpth (ft)	8.73	7.97
Weir Sta Lft (ft)		Vel Total (ft/s)	2.60	2.57
Weir Sta Rgt (ft)		Flow Area (sq ft)	465.33	471.15
Weir Submerg		Froude # Chl	0.18	0.18
Weir Max Depth (ft)		Specif Force (cu ft)	1704.60	1680.74
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	5.85	5.62
Min El Prs (ft)	130.00	W.P. Total (ft)	98.83	102.47
Delta EG (ft)	0.15	Conv. Total (cfs)	67328.8	67657.0
Delta WS (ft)	0.31	Top Width (ft)	79.59	83.78
BR Open Area (sq ft)	1441.68	Frctn Loss (ft)	0.07	0.04
BR Open Vel (ft/s)	2.60	C & E Loss (ft)	0.00	0.02
BR Sluice Coef		Shear Total (lb/sq ft)	0.09	0.09
BR Sel Method	Energy only	Power Total (lb/ft s)	0.25	0.24

Plan: PROPBRIDGE Souadabscook Str Reach RS: 27966 Profile: 10 year

E.G. US. (ft)	123.90	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	123.57	E.G. Elev (ft)	123.84	123.63
Q Total (cfs)	3640.00	W.S. Elev (ft)	123.38	123.16
Q Bridge (cfs)	3640.00	Crit W.S. (ft)	118.67	118.68
Q Weir (cfs)		Max Chl Dpth (ft)	11.28	10.36
Weir Sta Lft (ft)		Vel Total (ft/s)	5.25	5.27
Weir Sta Rgt (ft)		Flow Area (sq ft)	693.29	690.84
Weir Submerg		Froude # Chl	0.33	0.33
Weir Max Depth (ft)		Specif Force (cu ft)	3683.25	3582.73
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.02	6.86
Min El Prs (ft)	130.00	W.P. Total (ft)	123.98	125.24
Delta EG (ft)	0.38	Conv. Total (cfs)	116228.8	114357.3
Delta WS (ft)	0.77	Top Width (ft)	98.74	100.75
BR Open Area (sq ft)	1441.68	Frctn Loss (ft)	0.21	0.09
BR Open Vel (ft/s)	5.27	C & E Loss (ft)	0.00	0.02
BR Sluice Coef		Shear Total (lb/sq ft)	0.34	0.35
BR Sel Method	Energy only	Power Total (lb/ft s)	1.80	1.84

Plan: PROPBRIDGE Souadabscook Str Reach RS: 27966 Profile: 25 year

E.G. US. (ft)	124.64	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	124.25	E.G. Elev (ft)	124.58	124.32
Q Total (cfs)	4440.00	W.S. Elev (ft)	123.98	123.71
Q Bridge (cfs)	4440.00	Crit W.S. (ft)	119.37	119.36
Q Weir (cfs)		Max Chl Dpth (ft)	11.88	10.91
Weir Sta Lft (ft)		Vel Total (ft/s)	5.89	5.94
Weir Sta Rgt (ft)		Flow Area (sq ft)	753.85	747.23
Weir Submerg		Froude # Chl	0.36	0.37
Weir Max Depth (ft)		Specif Force (cu ft)	4353.70	4218.66
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.44	7.24
Min El Prs (ft)	130.00	W.P. Total (ft)	127.97	128.97
Delta EG (ft)	0.45	Conv. Total (cfs)	129583.9	126561.9
Delta WS (ft)	0.92	Top Width (ft)	101.30	103.18
BR Open Area (sq ft)	1441.68	Frctn Loss (ft)	0.25	0.11
BR Open Vel (ft/s)	5.94	C & E Loss (ft)	0.00	0.03
BR Sluice Coef		Shear Total (lb/sq ft)	0.43	0.45
BR Sel Method	Energy only	Power Total (lb/ft s)	2.54	2.65

Plan: PROPBRIDGE Souadabscook Str Reach RS: 27966 Profile: 50 year

E.G. US. (ft)	125.17	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	124.73	E.G. Elev (ft)	125.10	124.81
Q Total (cfs)	5040.00	W.S. Elev (ft)	124.40	124.09
Q Bridge (cfs)	5040.00	Crit W.S. (ft)	119.81	119.84
Q Weir (cfs)		Max Chl Dpth (ft)	12.30	11.29
Weir Sta Lft (ft)		Vel Total (ft/s)	6.33	6.41
Weir Sta Rgt (ft)		Flow Area (sq ft)	796.77	786.76
Weir Submerg		Froude # Chl	0.38	0.39
Weir Max Depth (ft)		Specif Force (cu ft)	4869.59	4706.68
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	7.73	7.50
Min El Prs (ft)	130.00	W.P. Total (ft)	130.74	131.53
Delta EG (ft)	0.50	Conv. Total (cfs)	139194.3	135231.9
Delta WS (ft)	1.03	Top Width (ft)	103.08	104.85
BR Open Area (sq ft)	1441.68	Frctn Loss (ft)	0.29	0.12
BR Open Vel (ft/s)	6.41	C & E Loss (ft)	0.00	0.03
BR Sluice Coef		Shear Total (lb/sq ft)	0.50	0.52
BR Sel Method	Energy only	Power Total (lb/ft s)	3.16	3.32

Plan: PROPBRIDGE Souadabscook Str Reach RS: 27966 Profile: 100 year

E.G. US. (ft)	125.71	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	125.23	E.G. Elev (ft)	125.63	125.31
Q Total (cfs)	5680.00	W.S. Elev (ft)	124.84	124.49
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	120.28	120.30
Q Weir (cfs)		Max Chl Dpth (ft)	12.74	11.69
Weir Sta Lft (ft)		Vel Total (ft/s)	6.75	6.86
Weir Sta Rgt (ft)		Flow Area (sq ft)	841.94	828.31
Weir Submerg		Froude # Chl	0.40	0.41
Weir Max Depth (ft)		Specif Force (cu ft)	5440.45	5247.16
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	8.02	7.77
Min El Prs (ft)	130.00	W.P. Total (ft)	133.60	134.18
Delta EG (ft)	0.55	Conv. Total (cfs)	149424.6	144434.4
Delta WS (ft)	1.14	Top Width (ft)	104.92	106.57
BR Open Area (sq ft)	1441.68	Frctn Loss (ft)	0.32	0.12
BR Open Vel (ft/s)	6.86	C & E Loss (ft)	0.00	0.02
BR Sluice Coef		Shear Total (lb/sq ft)	0.57	0.60
BR Sel Method	Energy only	Power Total (lb/ft s)	3.84	4.09

Plan: PROPBRIDGE Souadabscook Str Reach RS: 27966 Profile: 500 year

E.G. US. (ft)	126.90	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.45	E.G. Elev (ft)	126.79	126.40
Q Total (cfs)	7180.00	W.S. Elev (ft)	125.75	125.29
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.31	121.29
Q Weir (cfs)		Max Chl Dpth (ft)	13.65	12.49
Weir Sta Lft (ft)		Vel Total (ft/s)	7.64	7.84
Weir Sta Rgt (ft)		Flow Area (sq ft)	939.47	915.83
Weir Submerg		Froude # Chl	0.44	0.46
Weir Max Depth (ft)		Specif Force (cu ft)	6809.71	6535.77
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	8.64	8.32
Min El Prs (ft)	130.00	W.P. Total (ft)	139.61	139.62
Delta EG (ft)	0.67	Conv. Total (cfs)	171862.7	164087.0
Delta WS (ft)	1.54	Top Width (ft)	108.79	110.12
BR Open Area (sq ft)	1441.68	Frctn Loss (ft)	0.39	0.14
BR Open Vel (ft/s)	7.84	C & E Loss (ft)	0.01	0.02
BR Sluice Coef		Shear Total (lb/sq ft)	0.73	0.78
BR Sel Method	Energy only	Power Total (lb/ft s)	5.60	6.15

CALCULATION COVER PAGE

PROJECT: Hampden, I-95 over Souadabscook Stream West, Center, and East Bridges (Br. Nos. 5951, 1433, 5950, 1432, 5949, 1431)	MJ JOB NO.: 18084.99
CLIENT: Maine Department of Transportation (MEDOT)	WIN NO.:
SUBJECT/ TITLE: Approximate Scour Depths for the Request for Proposals Document	FEDERAL JOB NO.:

REV. NO.	ORIGINATOR'S SIGNATURE / DATE	CHECKER'S SIGNATURE / DATE
	 5/1/2019	 5/3/2019

CALCULATION OBJECTIVE: Estimate scour depths.

CALCULATION METHODOLOGY/ LIST OF ASSUMPTIONS:

- The preliminary hydraulic (HEC-RAS) model prepared for the MEDOT Request for Proposals (RFP) (based on 2-span layout). Controls over the simple span alternative.
- Scour depths were calculations for the West, Center, and East bridges.
- Pier foundations consist of a 5-foot wide wall pier (at the base). See attached sketch.
- Estimate Contraction Scour, considering borings and particle size (mm) analyses.
- Design Discharge = Q100 (Maintain normal FOS) (BDG 2.3.9.2)
- Check Discharge = Q500 Super Flood (FOS=1.0) (BDG 2.3.9.2)
- Bottom of footing to be placed on rock, or piles designed for Extreme Event scour load case.
- Increase 5-foot pier width by 25% for local scour to account for collection of debris. (BDG 2.3.11.1)
- Incorporate CSU HEC-18 Equation 7.1. [Note: The HEC-18 alternative Florida DOT method not considered, since bridge does not include wide piers. ($y/a < 0.2$)]
- K1 = 1.0 (Round Nose Pier) (HEC-18 Table 7.1) K2=1.0 (Piers aligned with channel. 0 degree angle of attack) (HEC-18 Table 7.2) K3=1.1 (No dunes) (HEC-18 Table 7.3)

REFERENCES / DESIGN FILES:

REFERENCE TITLE:	LOCATION:	REASON FOR REFERENCE:
HEC-RAS Model	M:\18084.99 MaineDOT Hampden Bridges\Design\H&H\HEC-RAS	Hydraulic Design File
HEC 18 – Evaluating Scour at Bridges (5 th Edition) (April 2012)	http://www.fhwa.dot.gov/engineering/hydraulics/pubs/hifl2003.pdf	Primary scour reference.
MeDOT Bridge Design Guide (BDG) Complete 2003 BDG with Updates to 2018.PDF	https://www.maine.gov/mdot/bdg/	Primary client reference.

CONCLUSIONS:
Scour depths were calculated at Q100 and Q500 for the total abutment scour, local pier scour, and contraction scour. For a summary of scour depths, see attached chart.

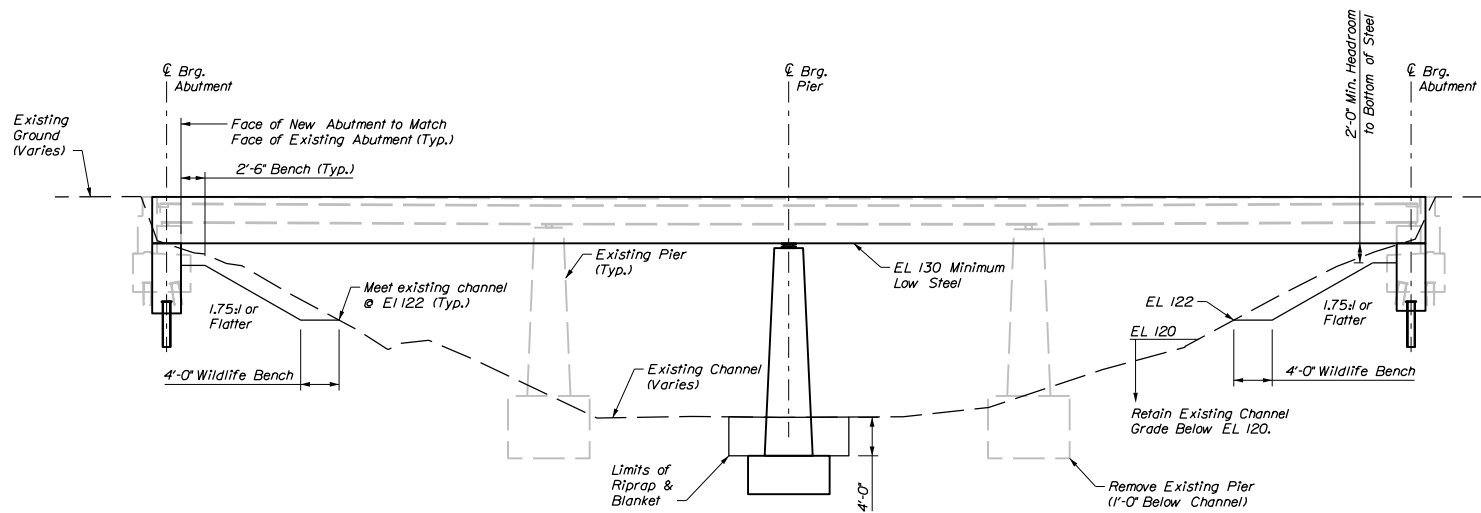


FIGURE 1: ASSUMED BRIDGE ELEVATION SCHEMATIC

Center Bridge Shown, West and East Bridges Similar.
Not to scale.

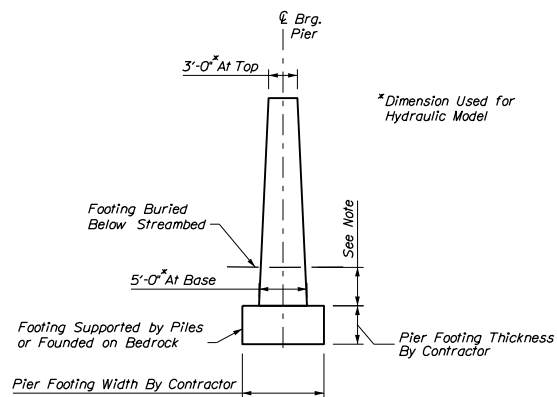


FIGURE 2: ASSUMED PIER GEOMETRY

Note:
The proposed top of footing for the pier is assumed to be placed below the MaineDOT Standard Detail riprap section.

Scour Depth Summary

Project Description: I-95 over Souadabscook Stream, West, Center, and East Bridges

Project Number: 18084.99

Calcs By: TEPA 5/1/2019

Check By:

Q100	West Bridge			
	Abutment Scour³	Local Pier Scour	Contraction Scour	Total Pier Scour
	2.15	9.12	2.30	11.42
	Center Bridge			
	Abutment Scour³	Local Pier Scour	Contraction Scour	Total Pier Scour
	5.00	7.32	3.18	10.50
	East Bridge			
	Abutment Scour³	Local Pier Scour	Contraction Scour	Total Pier Scour
	12.17	8.58	1.95	10.53

Q500	West Bridge			
	Abutment Scour³	Local Pier Scour	Contraction Scour	Total Pier Scour
	3.10	8.75	2.79	11.54
	Center Bridge			
	Abutment Scour³	Local Pier Scour	Contraction Scour	Total Pier Scour
	8.94	7.84	5.21	13.05
	East Bridge			
	Abutment Scour³	Local Pier Scour	Contraction Scour	Total Pier Scour
	17.39	8.75	1.88	10.63

Notes

- 1) Depths are given in feet.
- 2) Some of the scour depths calculated may exceed depth of bedrock. For these values, the assumed scour depth for design should be the bedrock depth.
- 3) NCHRP 24-20 was used for abutment scour. This calculation provides the total scour, and therefore includes contraction scour.
- 4) Pier scour was calculated using CSU Equations. Contraction scour was then added to this value to determine the total scour.

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, West, Center, and East Bridges	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Raw Data from Borings

West Bridge (RS 40346)

<u>Location</u>	<u>Boring ID</u>	<u>Depth (ft)</u>	<u>D50 (mm)</u>	<u>D85 (mm)</u>
W Abut	BB-HSS-101	6.5	1.0239	8.5294
W Abut	BB-HSS-102	4.5	0.2441	1.1291
Pier	BB-HSS-103	12	0.074	0.1169
Pier	BB-HSS-104	3.4	3.2307	11.1119
E Abut	BB-HSS-105	30	0.074	0.1229
E Abut	BB-HSS-106	35	0.1211	0.238

Center Bridge (RS 35151)

<u>Location</u>	<u>Sample No.</u>	<u>Depth (ft)</u>	<u>D50 (mm)</u>	<u>D85 (mm)</u>
W Abut	BB-HSS-107	18.5	2.3752	8.3426
W Abut	BB-HSS-108	5	3.3617	13.9141
Pier	BB-HSS-109	0	7.3178	23.5608
Pier	BB-HSS-110	0	6.3242	16.5421
E Abut	BB-HSS-111	8	0.425	7.523
E Abut	BB-HSS-112	15.5	2.1187	8.4443

East Bridge (RS 27966)

<u>Location</u>	<u>Sample No.</u>	<u>Depth (ft)</u>	<u>D50 (mm)</u>	<u>D85 (mm)</u>
W Abut	BB-HSS-113	10.5	0.074	0.1403
W Abut	BB-HSS-114	11	1.6168	7.5704
Pier	BB-HSS-115	4.5	0.1677	4.9308
E Abut	BB-HSS-117	16	0.6794	9.4773
E Abut	BB-HSS-118	5	0.5274	5.4272
E Abut	BB-HSS-118	15	1.7018	9.1176

<u>Design D50 (mm)</u>		
<u>West Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.10	1.65	0.63
<u>Center Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
2.87	6.82	1.27
<u>East Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.97	0.17	0.85

<u>Design D85 (mm)</u>		
<u>West Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.18	5.61	4.83
<u>Center Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
11.13	20.05	7.98
<u>East Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
8.01	4.93	3.86

<u>Design D50 (ft)</u>		
<u>West Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.000328	0.005413	0.002067
<u>Center Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.009416	0.022375	0.004167
<u>East Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.003182	0.000558	0.002789

<u>Design D85 (ft)</u>		
<u>West Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.000591	0.018406	0.015846
<u>Center Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.036516	0.065781	0.026181
<u>East Bridge</u>		
<u>LOB</u>	<u>Channel</u>	<u>ROB</u>
0.026280	0.016175	0.012664

NCHRP 24-20 Scour Calculations

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: 100 years

y_c = Flow depth including clear-water contraction scour, ft (m)

q_{2c} = unit discharge in the constricted opening accounting for non-uniform flow distribution, ft²/s (m²/s)

K_u = 11.17 (English units) or 6.19 (SI units)

D_{50} = Particle size with 50 percent finer, ft (m)

$$y_c = y_1 \left(\frac{q_{2c}}{q_1} \right)^{6/7} \quad \text{scour equation (eq. 8.5, HEC 18)}$$

y_{max} = Maximum flow depth resulting from abutment scour, ft (m)

y_c = Flow depth including live-bed or clear-water contraction scour, ft (m)

α_A = Amplification factor for live-bed conditions

α_B = Amplification factor for clear-water conditions

y_s = Abutment scour depth, ft (m)

y_0 = Flow depth prior to scour, ft (m)

$$y_{max} = \alpha_A y_c \quad \text{or} \quad y_{max} = \alpha_B y_c$$

$$y_s = y_{max} - y_0$$

The scour type for NCHRP 24-20 is determined by a ratio of L/Bf, or embankment length* over the total floodplain width. If this ratio is greater than 75%, then live-bed scour occurs. If it is less than 75% then clearwater scour occurs. Since the interstate is acting more like a causeway for this stream, L/Bf > 75% by inspection and live-bed scour

*The embankment length is equal to the total area in a cross section intercepted by the flow, minus the bridge opening.

Scour Type: Live-Bed Scour

Upstream						RS 40799.90						From HEC Ras						
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q1			
5680	366.12	1941.89	5.30	11.17	0.00541	0.48	2.36	254.61	3.93	10.89	5412.33	0.44	2.32	13.06	40.8340			

Bridge						RS 40346 BR U						From HEC Ras						
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q2c			
5680	108.43	1019.34	9.4009	11.17	0.00541	0	0	0	5.57	9.4	5680	0	0	0	52.3580			

NOTE: q1 & q2c = (Velocity x Depth) for L OB, R OB, and Ch, weighted by flow

KEY:

L OB D = Left Overbank Depth (ft)

R OB Vel = Right Overbank Velocity (ft/s)

CH Flow = Channel Flow (cfs)

$q_{2c}/q_1 = 1.28222$, use chart to calculate α_A

$\alpha_A = 1.76$ from chart.

$y_c = 6.56356$ ft (Eq. 8.5)

$y_{max} = 11.5519$ ft

CALCULATED SCOUR

$$y_s = 2.15096 \text{ ft}$$

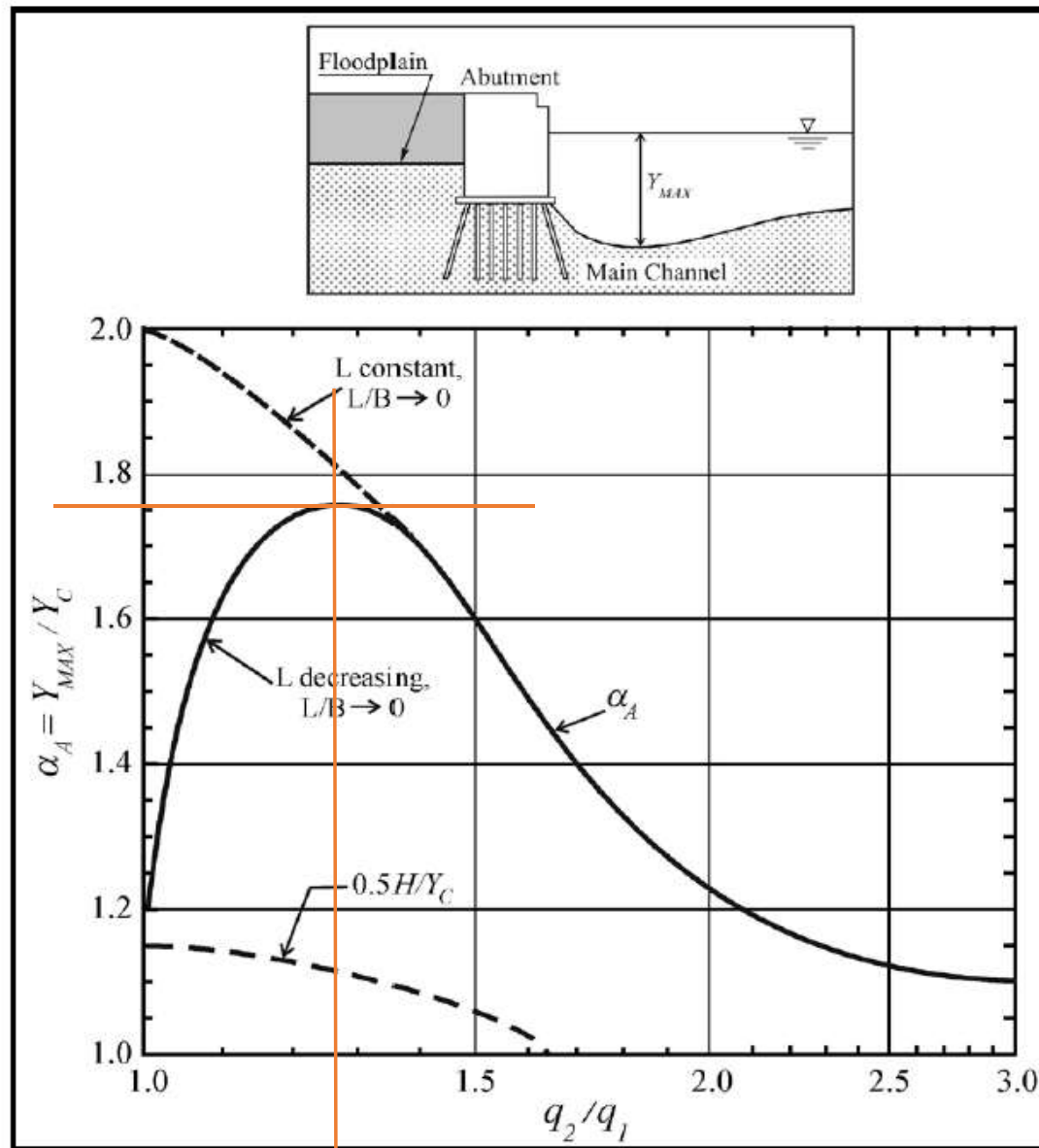


Figure 8.10. Scour amplification factor for wingwall abutments and live-bed conditions (NCHRP 2010b).

Cross Section Output

File Type Options Help

River: Souadabscook Str Profile: 100 year

Reach: Reach RS: 40799.90 Plan: SCOUR

Plan: SCOUR Souadabscook Str Reach RS: 40799.90 Profile: 100 year					
		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	127.58	Wt. n-Val.	0.092	0.030	0.092
Vel Head (ft)	0.23	Reach Len. (ft)	237.36	267.44	303.63
W.S. Elev (ft)	127.35	Flow Area (sq ft)	534.52	1377.74	29.63
Crit W.S. (ft)		Area (sq ft)	534.52	1377.74	29.63
E.G. Slope (ft/ft)	0.000277	Flow (cfs)	254.61	5412.33	13.06
Q Total (cfs)	5680.00	Top Width (ft)	226.82	126.52	12.78
Top Width (ft)	366.12	Avg. Vel. (ft/s)	0.48	3.93	0.44
Vel Total (ft/s)	2.92	Hydr. Depth (ft)	2.36	10.89	2.32
Max Chl Dpth (ft)	16.50	Conv. (cfs)	15285.3	324924.2	783.9
Conv. Total (cfs)	340993.4	Wetted Per. (ft)	226.88	132.60	14.13
Length Wtd. (ft)	266.85	Shear (lb/sq ft)	0.04	0.18	0.04
Min Ch El (ft)	110.85	Stream Power (lb/ft s)	0.02	0.71	0.02
Alpha	1.72	Cum Volume (acre-ft)	1020.73	1141.90	1087.30
Frctn Loss (ft)	0.09	Cum SA (acres)	415.26	106.67	248.03
C & E Loss (ft)	0.01				

Bridge Output

File Type Options Help

River: Souadabscook Str Profile: 100 year

Reach: Reach RS: 40346 Plan: SCOUR

Plan: SCOUR Souadabscook Str Reach RS: 40346 Profile: 100 year				
		Element	Inside BR US	Inside BR DS
E.G. US. (ft)	127.48	E.G. Elev (ft)	127.39	127.22
W.S. US. (ft)	127.15	W.S. Elev (ft)	126.86	126.67
Q Total (cfs)	5680.00	Crit W.S. (ft)	121.08	121.15
Q Bridge (cfs)	5680.00	Max Chl Dpth (ft)	14.89	13.77
Q Weir (cfs)		Vel Total (ft/s)	5.57	5.67
Weir Sta Lft (ft)		Flow Area (sq ft)	1019.34	1002.14
Weir Sta Rgt (ft)		Froude # Chl	0.32	0.32
Weir Submerg		Specif Force (cu ft)	6595.87	6338.01
Weir Max Depth (ft)		Hydr Depth (ft)	9.40	9.23
Min El Weir Flow (ft)	134.81	W.P. Total (ft)	141.93	140.57
Min El Prs (ft)	130.00	Conv. Total (cfs)	192944.1	188465.7
Delta EG (ft)	0.41	Top Width (ft)	108.43	108.56
Delta WS (ft)	0.46	Frctn Loss (ft)	0.16	0.06
BR Open Area (sq ft)	1375.71	C & E Loss (ft)	0.01	0.08
BR Open Vel (ft/s)	5.67	Shear Total (lb/sq ft)	0.39	0.40
BR Sluice Coef		Power Total (lb/ft s)	2.17	2.29
BR Sel Method	Energy only			

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **100 Years** **RS 40532.46**
 Units: **English**

Description of Streambed Material :

D_{50} of Streambed Material: **0.005413** ft Particle size in a mixture of which 50% are smaller.
 D_{95} of Streambed Material: ft Particle size in a mixture of which 95% are smaller.

Determine Critical Velocity

$$V_c = K_u y^{1/6} D_{50}^{1/3}$$

Required User Inputs:

$y =$ **10.38** ft Average depth of flow upstream of the bridge.
 $V =$ **4.66** ft/s Upstream Velocity (from HEC-RAS)

Calculated Inputs:

$D_{50} =$ 0.00541339 ft Particle size in a mixture of which 50% are smaller.
 $K_u =$ 11.17 Equation constant based on units.
 $V_c =$ 2.90 ft/s

Type of Scour = **Live-Bed Scour**

Plan: SCOUR Souadabscook Str Reach RS: 40532.46 Profile: 100 year					
E.G. Elev (ft)	127.48	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.33	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	127.15	Reach Len. (ft)	62.50	62.50	62.50
Crit W.S. (ft)	120.63	Flow Area (sq ft)	40.92	1204.66	41.04
E.G. Slope (ft/ft)	0.000402	Area (sq ft)	1549.27	1204.66	2312.14
Q Total (cfs)	5680.00	Flow (cfs)	30.03	5610.67	39.30
Top Width (ft)	1635.86	Top Width (ft)	627.54	116.02	892.30
Vel Total (ft/s)	4.41	Avg. Vel. (ft/s)	0.73	4.66	0.96
Max Chl Dpth (ft)	14.65	Hydr. Depth (ft)	3.41	10.38	5.14
Conv. Total (cfs)	283155.6	Conv. (cfs)	1497.1	279699.2	1959.2
Length Wtd. (ft)	62.50	Wetted Per. (ft)	12.01	118.69	8.08
Min Ch El (ft)	112.50	Shear (lb/sq ft)	0.09	0.25	0.13
Alpha	1.10	Stream Power (lb/ft s)	0.06	1.19	0.12
Frctn Loss (ft)	0.04	Cum Volume (acre-ft)	1015.05	1133.97	1079.14
C & E Loss (ft)	0.06	Cum SA (acres)	412.94	105.92	244.87

Pier Scour - Colorado State University (CSU) Equation**Imperial Units**

Enter Pier Description ==> West Bridge, Center Pier

Correction for Pier Nose Shape:

Enter Storm Event and Total Flow ==> Q100 - 5680 CFS

K1 = Pier Nose Shape Coefficient (HEC-18 Table 2)

Type of Pier	K1	Type
Square Nose	1.10	Type 1
Round Nose	1.00	Type 2
Circular Cylinder	1.00	Type 3
Sharp Nose	0.90	Type 4
Group of Cylinders	1.00	Type 5

Enter Type of Pier (1, 2, 3, 4 or 5) ==> 2

K1 = 1.00

Correction for Piers Skewed to Flow

Enter Pier Width (a) ==> 5.00 feet at base of wall

Design Pier Width (a) ==> 6.25 feet increase by 25%, MEDOT BDG 2.3.11.1

K2 = Coefficient Factor for Angle of Attack of the Flow (HEC-18 Table 3)

Enter Attack Angle (0, 15, 30, 45 or 90) ==> 0 Degrees

Enter (Pier Length / Pier Width) Ratio (4, 8, or 12) ==> 12

K2 = 1.00

Correction Factor for Bed Condition

K3 = Coefficient Factor for Bed Condition (HEC-18 Table 1) ==> Assume Clear-Water Scour / Antidune Flow

K3 = 1.10

Depth of Flow at Pier

y1 = Flow Depth Directly Upstream of the Pier

Enter y1 ==> 10.38 ft

Reference ==> HEC-RAS

y1 = 10.38 feet

Velocity of Flow Directly Upstream of Pier

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second)

Enter V1 ==> 4.66 fps

Reference ==> HEC-RAS

Ve = 4.66 ft per sec

Froude Number $Fr1 = (V1) / \{[(g)(y1)]^{0.5}\} = \text{Froude}$

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second) - Entered Above

g = 32.2 feet / sec²

y1 = Flow Depth Directly Upstream of the Pier - Entered Above

Fr = 0.25

CALCULATE TOTAL LOCAL PIER SCOUR $ys / y1 = (2.0)(K1)(K2)(K3)[(a / y1)^{0.65}](Fr^{0.43})$

y1 = 10.38 feet

ys / y1 = 0.88

K1 = 1.00

K2 = 1.00

K3 = 1.10

a = 6.25 feet

ys = 0.88 X 10.38

Fr = 0.25

ys = Pier Scour Depth = 9.1 feet

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA
		Checked By:	5/1/2019

Live Bed Contraction Scour

Flood Event: 100 Years

$$\frac{y_2}{y_1} = \left(\frac{Q_2}{Q_1} \right)^{6/7} \left(\frac{W_1}{W_2} \right)^{k_1} \quad y_s = y_2 - y_o = (\text{average contraction scour depth})$$

Required User Inputs:

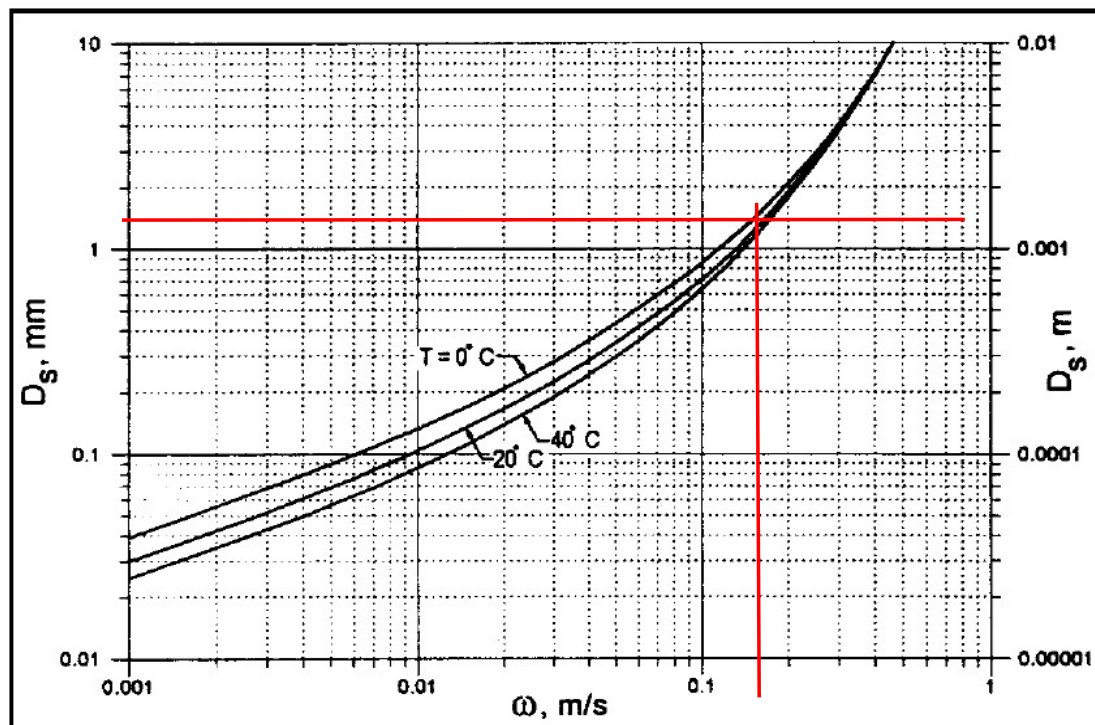
y1 =	10.38	ft	Average depth of mainstream channel
D50 =	1.65	mm	
Q1 =	5610.67	CFS	flow in upstream channel transporting sediment
Q2 =	5680	CFS	flow in contracted channel
W1 =	116.02	ft	Top width of upstream main channel that is transporting bed material
W2 =	81.1	ft	Top width of main channel in contracted section less pier widths
y _o =	10.89	ft	Average existing depth in the contracted section.
EGL Slope =	0.000867	ft/ft	slope of energy grade line (from bridge cross section)
T =	0.5904	ft/s	fall velocity of bed material (from chart below)

Calculated Inputs:

g =	32.2	ft/s ²	constant
V* =	0.538315	ft/s ²	shear velocity in upstream section
k1 =	0.64		

y₂ = 13.19 ft Average equilibrium depth in the contracted section after contraction scour.

Calculated Scour Depth: 2.30 ft Live Bed Contraction Scour



Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	100 year		
Reach	Reach	RS:	40532.46	↓	↑
Plan: SCOUR Souadabscook Str Reach RS: 40532.46 Profile: 100 year					
E.G. Elev (ft)		Element	Left OB	Channel	Right OB
Vel Head (ft)	0.33	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	127.15	Reach Len. (ft)	62.50	62.50	62.50
Crit W.S. (ft)	120.63	Flow Area (sq ft)	40.92	1204.66	41.04
E.G. Slope (ft/ft)	0.000402	Area (sq ft)	1549.27	1204.66	2312.14
Q Total (cfs)	5680.00	Flow (cfs)	30.03	5610.67	39.30
Top Width (ft)	1635.86	Top Width (ft)	627.54	116.02	892.30
Vel Total (ft/s)	4.41	Avg. Vel. (ft/s)	0.73	4.66	0.96
Max Chl Dpth (ft)	14.65	Hydr. Depth (ft)	3.41	10.38	5.14
Conv. Total (cfs)	283155.6	Conv. (cfs)	1497.1	279699.2	1959.2
Length Wtd. (ft)	62.50	Wetted Per. (ft)	12.01	118.69	8.08
Min Ch El (ft)	112.50	Shear (lb/sq ft)	0.09	0.25	0.13
Alpha	1.10	Stream Power (lb/ft s)	0.06	1.19	0.12
Frctn Loss (ft)	0.04	Cum Volume (acre-ft)	1015.05	1133.97	1079.14
C & E Loss (ft)	0.06	Cum SA (acres)	412.94	105.92	244.87

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	100 year		
Reach	Reach	RS:	40346 BR U	↓	↑
Plan: SCOUR Souadabscook Str Reach RS: 40346 BR U Profile: 100 year					
E.G. Elev (ft)		Element	Left OB	Channel	Right OB
Vel Head (ft)	0.53	Wt. n-Val.	0.092	0.030	0.030
W.S. Elev (ft)	126.86	Reach Len. (ft)	182.00	182.00	182.00
Crit W.S. (ft)	121.08	Flow Area (sq ft)	49.51	937.64	32.19
E.G. Slope (ft/ft)	0.000867	Area (sq ft)	49.51	937.64	32.19
Q Total (cfs)	5680.00	Flow (cfs)	51.31	5535.16	93.53
Top Width (ft)	108.43	Top Width (ft)	13.53	86.10	8.80
Vel Total (ft/s)	5.57	Avg. Vel. (ft/s)	1.04	5.90	2.91
Max Chl Dpth (ft)	14.89	Hydr. Depth (ft)	3.66	10.89	3.66
Conv. Total (cfs)	192944.1	Conv. (cfs)	1743.1	188023.9	3177.1
Length Wtd. (ft)	182.00	Wetted Per. (ft)	15.38	115.10	11.44
Min Ch El (ft)	111.97	Shear (lb/sq ft)	0.17	0.44	0.15
Alpha	1.10	Stream Power (lb/ft s)	0.18	2.60	0.44
Frctn Loss (ft)	0.16	Cum Volume (acre-ft)	1013.91	1132.43	1077.46
C & E Loss (ft)	0.01	Cum SA (acres)	412.48	105.78	244.23

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **500 Years** **RS 40532.46**
 Units: **English**

Description of Streambed Material :

D₅₀ of Streambed Material: **0.005413** ft Particle size in a mixture of which 50% are smaller.
D₉₅ of Streambed Material: ft Particle size in a mixture of which 95% are smaller.

Determine Critical Velocity

$$V_c = K_u y^{1/6} D_{50}^{1/3}$$

Required User Inputs:

y = **11.70** ft Average depth of flow upstream of the bridge.
 V = **5.21** ft/s Upstream Velocity (from HEC-RAS)

Calculated Inputs:

D50 = 0.00541339 ft Particle size in a mixture of which 50% are smaller.
 Ku = 11.17 Equation constant based on units.
 Vc = 2.96 ft/s

Type of Scour = **Live-Bed Scour**

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	500 year		
Reach	Reach	RS:	40532.46	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 40532.46 Profile: 500 year					
		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	128.88	Wt. n-Val.	0.092	0.030	0.092
Vel Head (ft)	0.41	Reach Len. (ft)	62.50	62.50	62.50
W.S. Elev (ft)	128.47	Flow Area (sq ft)	56.75	1357.68	51.57
Crit W.S. (ft)	121.52	Area (sq ft)	2389.48	1357.68	3489.00
E.G. Slope (ft/ft)	0.000429	Flow (cfs)	53.45	7067.22	59.34
Q Total (cfs)	7180.00	Top Width (ft)	659.15	116.02	892.30
Top Width (ft)	1667.47	Avg. Vel. (ft/s)	0.94	5.21	1.15
Vel Total (ft/s)	4.90	Hydr. Depth (ft)	4.73	11.70	6.46
Max Chl Dpth (ft)	15.97	Conv. (cfs)	2581.8	341386.6	2866.2
Conv. Total (cfs)	346834.6	Wetted Per. (ft)	12.01	118.69	8.08
Length Wtd. (ft)	62.50	Shear (lb/sq ft)	0.13	0.31	0.17
Min Ch El (ft)	112.50	Stream Power (lb/ft s)	0.12	1.59	0.20
Alpha	1.11	Cum Volume (acre-ft)	1506.80	1266.16	1368.89
Frctn Loss (ft)	0.04	Cum SA (acres)	418.35	105.93	252.63
C & E Loss (ft)	0.08				

NCHRP 24-20 Scour Calculations

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **500 years**

y_c = Flow depth including clear-water contraction scour, ft (m)

q_{2c} = unit discharge in the constricted opening accounting for non-uniform flow distribution, ft²/s (m²/s)

K_u = 11.17 (English units) or 6.19 (SI units)

D_{50} = Particle size with 50 percent finer, ft (m)

$$y_c = y_1 \left(\frac{q_{2c}}{q_1} \right)^{6/7} \quad \text{scour equation (eq. 8.5, HEC 18)}$$

y_{max} = Maximum flow depth resulting from abutment scour, ft (m)

y_c = Flow depth including live-bed or clear-water contraction scour, ft (m)

α_A = Amplification factor for live-bed conditions

α_B = Amplification factor for clear-water conditions

y_s = Abutment scour depth, ft (m)

y_0 = Flow depth prior to scour, ft (m)

$$y_{max} = \alpha_A y_c \quad \text{or} \quad y_{max} = \alpha_B y_c$$

$$y_s = y_{max} - y_0$$

The scour type for NCHRP 24-20 is determined by a ratio of L/Bf, or embankment length* over the total floodplain width. If this ratio is greater than 75%, then live-bed scour occurs. If it is less than 75% then clearwater scour occurs. Since the interstate is acting more like a causeway for this stream, L/Bf > 75% by inspection and live-bed scour

*The embankment length is equal to the total area in a cross section intercepted by the flow, minus the bridge opening.

Scour Type: Live-Bed Scour

Upstream			RS 40799.90			From HEC Ras									
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q1
7180	407.83	2475.11	6.07	11.17	0.00541	0.62	3.47	536.25	4.27	12.26	6622.57	0.38	1.77	21.18	48.4486

Bridge RS 40346 BR U						From HEC Ras									
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q2c
7180	112.36	1156.38	10.2917	11.17	0.00541	0	0	0	6.21	10.29	7180	0	0	0	63.9009

NOTE: q1 & q2c = (Velocity x Depth) for L OB, R OB, and Ch, weighted by flow

KEY:

L OB D = Left Overbank Depth (ft)

R OB Vel = Right Overbank Velocity (ft/s)

CH Flow = Channel Flow (cfs)

$q_{2c}/q_1 = 1.31894$, use chart to calculate α_A

$\alpha_A = 1.74$ from chart.

$y_c = 7.69425$ ft (Eq. 8.5)

$y_{max} = 13.388$ ft

CALCULATED SCOUR

$$y_s = 3.09625 \text{ ft}$$

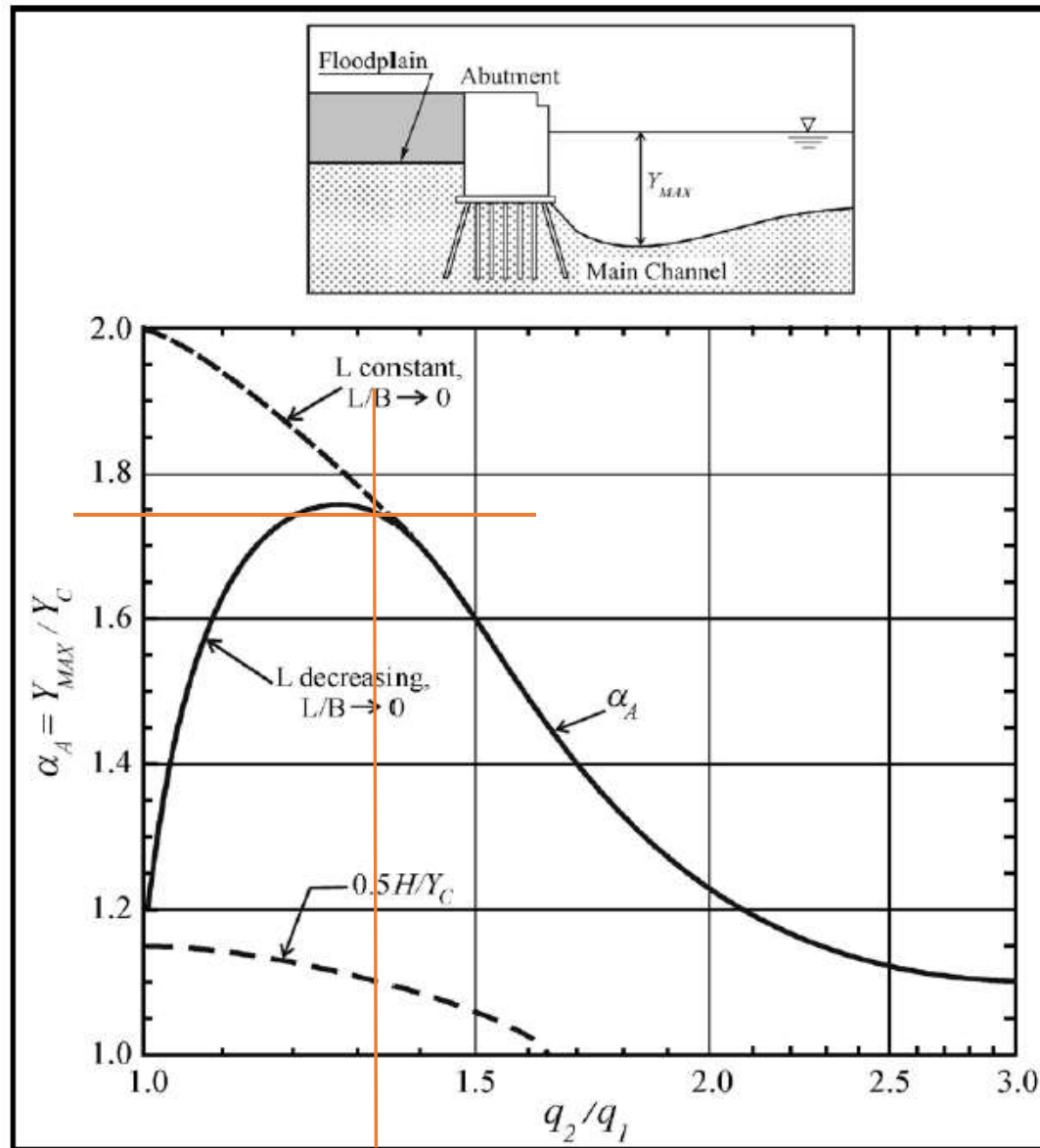


Figure 8.10. Scour amplification factor for wingwall abutments and live-bed conditions (NCHRP 2010b).

Cross Section Output

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 40799.90 Profile: 500 year

		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	128.99				
Vel Head (ft)	0.26	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	128.73	Reach Len. (ft)	237.36	267.44	303.63
Crit W.S. (ft)		Flow Area (sq ft)	867.99	1551.74	55.38
E.G. Slope (ft/ft)	0.000279	Area (sq ft)	867.99	1551.74	55.38
Q Total (cfs)	7180.00	Flow (cfs)	536.25	6622.57	21.18
Top Width (ft)	407.83	Top Width (ft)	250.00	126.52	31.31
Vel Total (ft/s)	2.90	Avg. Vel. (ft/s)	0.62	4.27	0.38
Max Chl Dpth (ft)	17.88	Hydr. Depth (ft)	3.47	12.26	1.77
Conv. Total (cfs)	429504.9	Conv. (cfs)	32078.2	396159.5	1267.2
Length Wtd. (ft)	266.41	Wetted Per. (ft)	250.78	132.60	32.83
Min Ch El (ft)	110.85	Shear (lb/sq ft)	0.06	0.20	0.03
Alpha	2.00	Stream Power (lb/ft s)	0.04	0.87	0.01
Frctn Loss (ft)	0.09	Cum Volume (acre-ft)	1515.68	1275.09	1381.24
C & E Loss (ft)	0.02	Cum SA (acres)	420.82	106.67	255.85

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 40346 Profile: 500 year

		Element	Inside BR US	Inside BR DS
E.G. US. (ft)	128.88			
W.S. US. (ft)	128.47	E.G. Elev (ft)	128.77	128.58
Q Total (cfs)	7180.00	W.S. Elev (ft)	128.10	127.89
Q Bridge (cfs)	7180.00	Crit W.S. (ft)	121.97	122.03
Q Weir (cfs)		Max Chl Dpth (ft)	16.13	14.99
Weir Sta Lft (ft)		Vel Total (ft/s)	6.21	6.32
Weir Sta Rgt (ft)		Flow Area (sq ft)	1156.38	1136.17
Weir Submerg		Froude # Chl	0.34	0.35
Weir Max Depth (ft)		Specif Force (cu ft)	8374.90	8072.63
Min El Weir Flow (ft)	134.81	Hydr Depth (ft)	10.29	10.14
Min El Prs (ft)	130.00	W.P. Total (ft)	148.97	147.17
Delta EG (ft)	0.48	Conv. Total (cfs)	229403.7	224271.3
Delta WS (ft)	0.54	Top Width (ft)	112.36	112.05
BR Open Area (sq ft)	1375.71	Frctn Loss (ft)	0.18	0.07
BR Open Vel (ft/s)	6.32	C & E Loss (ft)	0.01	0.11
BR Sluice Coef		Shear Total (lb/sq ft)	0.47	0.49
BR Sel Method	Energy only	Power Total (lb/ft s)	2.95	3.12

Pier Scour - Colorado State University (CSU) Equation**Imperial Units****Correction for Pier Nose Shape:**

Enter Pier Description ==> West Bridge, Center Pier

Enter Storm Event and Total Flow ==> Q500 - 7180 CFS

K1 = Pier Nose Shape Coefficient (HEC-18 Table 2)

Type of Pier	K1	Type
Square Nose	1.10	Type 1
Round Nose	1.00	Type 2
Circular Cylinder	1.00	Type 3
Sharp Nose	0.90	Type 4
Group of Cylinders	1.00	Type 5

Enter Type of Pier (1, 2, 3, 4 or 5) ==> 4

K1 = 0.90

Correction for Piers Skewed to Flow

Enter Pier Width (a) ==> 5.00 feet at base of wall

Design Pier Width (a) ==> 6.25 feet increase by 25%, MEDOT BDG 2.3.11.1

K2 = Coefficient Factor for Angle of Attack of the Flow (HEC-18 Table 3)

Enter Attack Angle (0, 15, 30, 45 or 90) ==> 0 Degrees

Enter (Pier Length / Pier Width) Ratio (4, 8, or 12) ==> 12

K2 = 1.00

Correction Factor for Bed Condition

K3 = Coefficient Factor for Bed Condition (HEC-18 Table 1) ==> Assume Clear-Water Scour / Antidune Flow

K3 = 1.10

Depth of Flow at Pier

y1 = Flow Depth Directly Upstream of the Pier

Enter y1 ==> 11.7 ft Reference ==> HEC-RAS

y1 = 11.70 feet

Velocity of Flow Directly Upstream of Pier

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second)

Enter V1 ==> 5.21 fps Reference ==> HEC-RAS

Ve = 5.21 ft per sec

Froude Number $Fr1 = (V1) / \{[(g)(y1)]^{0.5}\} = \text{Froude}$

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second) - Entered Above

g = 32.2 feet / sec²

y1 = Flow Depth Directly Upstream of the Pier - Entered Above

Fr = 0.27

CALCULATE TOTAL LOCAL PIER SCOUR $ys / y1 = (2.0)(K1)(K2)(K3)[(a / y1)^{0.65}](Fr^{0.43})$

y1 = 11.70 feet

ys / y1 = 0.75

K1 = 0.90

K2 = 1.00

K3 = 1.10

a = 6.25 feet

ys = 0.75 X 11.70

Fr = 0.27

ys = Pier Scour Depth = 8.8 feet

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA
		Checked By:	5/1/2019

Live Bed Contraction Scour

Flood Event: 500 Years

$$\frac{y_2}{y_1} = \left(\frac{Q_2}{Q_1} \right)^{6/7} \left(\frac{W_1}{W_2} \right)^{k_1} \quad y_s = y_2 - y_o = (\text{average contraction scour depth})$$

Required User Inputs:

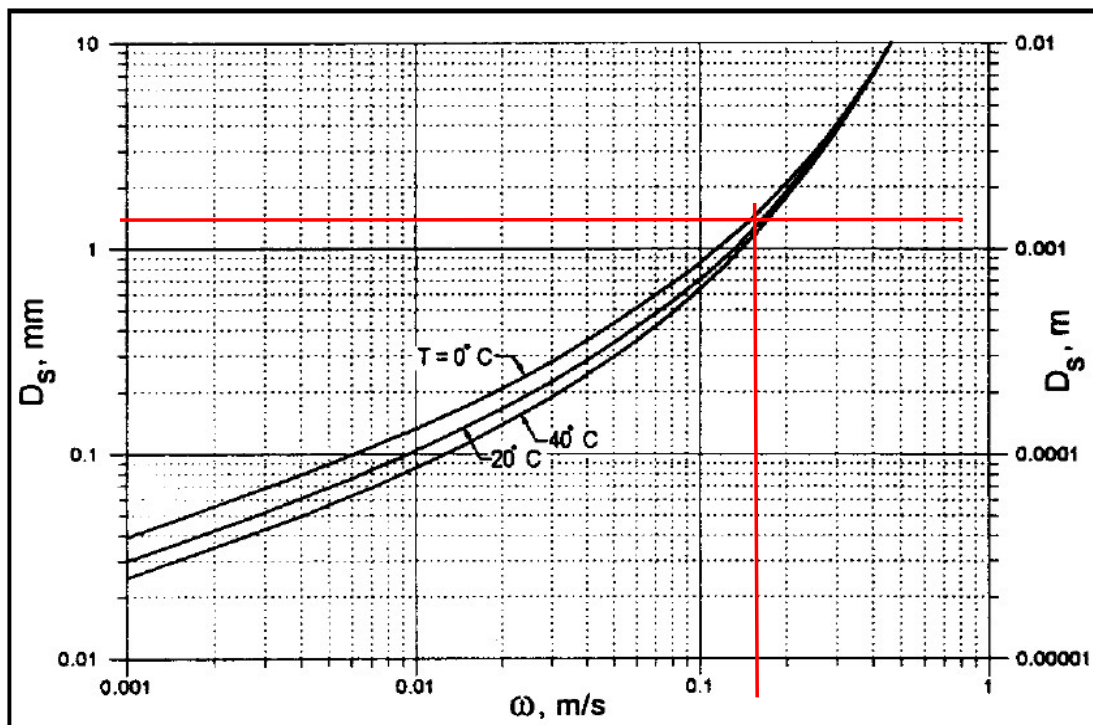
y1 =	11.7	ft	Average depth of mainstream channel
D50 =	1.65	mm	
Q1 =	7067.22	CFS	flow in upstream channel transporting sediment
Q2 =	7180	CFS	flow in contracted channel
W1 =	116.02	ft	Top width of upstream main channel that is transporting bed material
W2 =	81.24	ft	Top width of main channel in contracted section less pier widths
y _o =	12.11	ft	Average existing depth in the contracted section.
EGL Slope =	0.00098	ft/ft	slope of energy grade line (from bridge cross section)
T =	0.5904	ft/s	fall velocity of bed material (from chart below)

Calculated Inputs:

g =	32.2	ft/s ²	constant
V* =	0.607623	ft/s ²	shear velocity in upstream section
k1 =	0.64		

y₂ = 14.90 ft Average equilibrium depth in the contracted section after contraction scour.

Calculated Scour Depth: 2.79 ft Live Bed Contraction Scour



Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	500 year		
Reach	Reach	RS:	40532.46	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 40532.46 Profile: 500 year					
E.G. Elev (ft)	128.88	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.41	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	128.47	Reach Len. (ft)	62.50	62.50	62.50
Crit W.S. (ft)	121.52	Flow Area (sq ft)	56.75	1357.68	51.57
E.G. Slope (ft/ft)	0.000429	Area (sq ft)	2389.48	1357.68	3489.00
Q Total (cfs)	7180.00	Flow (cfs)	53.45	7067.22	59.34
Top Width (ft)	1667.47	Top Width (ft)	659.15	116.02	892.30
Vel Total (ft/s)	4.90	Avg. Vel. (ft/s)	0.94	5.21	1.15
Max Chl Dpth (ft)	15.97	Hydr. Depth (ft)	4.73	11.70	6.46
Conv. Total (cfs)	346834.6	Conv. (cfs)	2581.8	341386.8	2866.2
Length Wtd. (ft)	62.50	Wetted Per. (ft)	12.01	118.69	8.08
Min Ch El (ft)	112.50	Shear (lb/sq ft)	0.13	0.31	0.17
Alpha	1.11	Stream Power (lb/ft s)	0.12	1.59	0.20
Frctn Loss (ft)	0.04	Cum Volume (acre-ft)	1506.80	1266.16	1368.89
C & E Loss (ft)	0.08	Cum SA (acres)	418.35	105.93	252.63

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	500 year		
Reach	Reach	RS:	40346 BR U	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 40346 BR U Profile: 500 year					
E.G. Elev (ft)	128.77	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.67	Wt. n-Val.	0.092	0.030	0.030
W.S. Elev (ft)	128.10	Reach Len. (ft)	182.00	182.00	182.00
Crit W.S. (ft)	121.97	Flow Area (sq ft)	67.73	1044.60	44.04
E.G. Slope (ft/ft)	0.000980	Area (sq ft)	67.73	1044.60	44.04
Q Total (cfs)	7180.00	Flow (cfs)	82.86	6946.12	151.02
Top Width (ft)	112.36	Top Width (ft)	15.83	86.24	10.29
Vel Total (ft/s)	6.21	Avg. Vel. (ft/s)	1.22	6.65	3.43
Max Chl Dpth (ft)	16.13	Hydr. Depth (ft)	4.28	12.11	4.28
Conv. Total (cfs)	229403.7	Conv. (cfs)	2647.3	221931.3	4825.1
Length Wtd. (ft)	182.00	Wetted Per. (ft)	17.99	117.59	13.38
Min Ch El (ft)	111.97	Shear (lb/sq ft)	0.23	0.54	0.20
Alpha	1.12	Stream Power (lb/ft s)	0.28	3.61	0.69
Frctn Loss (ft)	0.18	Cum Volume (acre-ft)	1505.04	1264.44	1366.36
C & E Loss (ft)	0.01	Cum SA (acres)	417.86	105.78	251.98

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, Center Bridge	Project Number:	18084.99
		Calculated By:	TEPA
		Checked By:	5/1/2019

Flood Event: **100 Years** **RS 35310.52**
 Units: **English**

Description of Streambed Material :

D₅₀ of Streambed Material: **0.022375** ft Particle size in a mixture of which 50% are smaller.
D₉₅ of Streambed Material: ft Particle size in a mixture of which 95% are smaller.

Determine Critical Velocity

$$V_c = K_u y^{1/6} D_{50}^{1/3}$$

Required User Inputs:

y = **11.62** ft Average depth of flow upstream of the bridge.
 V = **3.44** ft/s Upstream Velocity (from HEC-RAS)

Calculated Inputs:

D50 = 0.02237533 ft Particle size in a mixture of which 50% are smaller.
 K_u = 11.17 Equation constant based on units.
 V_c = 4.74 ft/s

Type of Scour = **Clear-Water Scour**

Plan: SCOUR Souadabscook Str Reach RS: 35310.52 Profile: 100 year					
E.G. Elev (ft)	126.63	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.18	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	126.45	Reach Len. (ft)	59.00	59.00	59.00
Crit W.S. (ft)	118.32	Flow Area (sq ft)	23.77	1644.02	44.68
E.G. Slope (ft/ft)	0.000205	Area (sq ft)	1999.24	1644.02	2327.47
Q Total (cfs)	5680.00	Flow (cfs)	9.61	5659.14	11.25
Top Width (ft)	2302.89	Top Width (ft)	848.51	141.50	1312.88
Vel Total (ft/s)	3.32	Avg. Vel. (ft/s)	0.40	3.44	0.25
Max Chl Dpth (ft)	13.45	Hydr. Depth (ft)	2.31	11.62	1.14
Conv. Total (cfs)	397011.7	Conv. (cfs)	671.7	395553.4	786.6
Length Wtd. (ft)	59.00	Wetted Per. (ft)	10.27	153.56	39.25
Min Ch El (ft)	113.00	Shear (lb/sq ft)	0.03	0.14	0.01
Alpha	1.07	Stream Power (lb/ft s)	0.01	0.47	0.00
Frctn Loss (ft)	0.02	Cum Volume (acre-ft)	493.97	314.77	764.02
C & E Loss (ft)	0.13	Cum SA (acres)	258.22	27.37	167.17

NCHRP 24-20 Scour Calculations

Project Description :	I-95 over Souadabscook Stream, Center Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **100 years**

y_c = Flow depth including clear-water contraction scour, ft (m)

q_{2c} = unit discharge in the constricted opening accounting for non-uniform flow distribution, ft²/s (m²/s)

K_u = 11.17 (English units) or 6.19 (SI units)

D_{50} = Particle size with 50 percent finer, ft (m)

$$y_c = y_1 \left(\frac{q_{2c}}{q_1} \right)^{6/7} \quad \text{scour equation (eq. 8.5, HEC 18)}$$

y_{max} = Maximum flow depth resulting from abutment scour, ft (m)

y_c = Flow depth including live-bed or clear-water contraction scour, ft (m)

α_A = Amplification factor for live-bed conditions

α_B = Amplification factor for clear-water conditions

y_s = Abutment scour depth, ft (m)

y_0 = Flow depth prior to scour, ft (m)

$$y_{max} = \alpha_A y_c \text{ OR } y_{max} = \alpha_B y_c$$

$$y_s = y_{max} - y_0$$

The scour type for NCHRP 24-20 is determined by a ratio of L/Bf, or embankment length over the total floodplain width. If this ratio is greater than 75%, then live-bed scour occurs. If it is less than 75% then clearwater scour occurs. Since the interstate is acting more like a causeway for this stream, L/Bf > 75% by inspection and live-bed scour

*The embankment length is equal to the total area in a cross section intercepted by the flow, minus the bridge opening.

Scour Type: Live-Bed Scour

Upstream						From HEC Ras									
RS 35509.99															
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q1
5680	2253.26	10949.2	4.86	11.17	0.02238	0.16	3.93	514.58	1.3	17.01	4511.29	0.15	3.46	654.13	17.6798

Bridge RS 35151 BR U						From HEC Ras									
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q2c
5680	103.39	943.68	9.12738	11.17	0.02238	0	0	0	6.02	9.13	5680	0	0	0	54.9626

NOTE: q1 & q2c = (Velocity x Depth) for L OB, R OB, and Ch, weighted by flow

$q_{2c}/q_1 = \frac{3.10878}{1.1}$, use chart to calculate α_A
 $\alpha_B = 1.1$ from chart.
 $y_c = 12.8466$ ft (Eq. 8.6)
 $y_{max} = 14.1313$ ft

Designers Note: $q_{2c}/q_1 > 3$, therefore conservatively use lowest value on chart

KEY:

L OB D = Left Overbank Depth (ft)
R OB Vel = Right Overbank Velocity (ft/s)
CH Flow = Channel Flow (cfs)

CALCULATED SCOUR

$$y_s = 5.00131 \text{ ft}$$

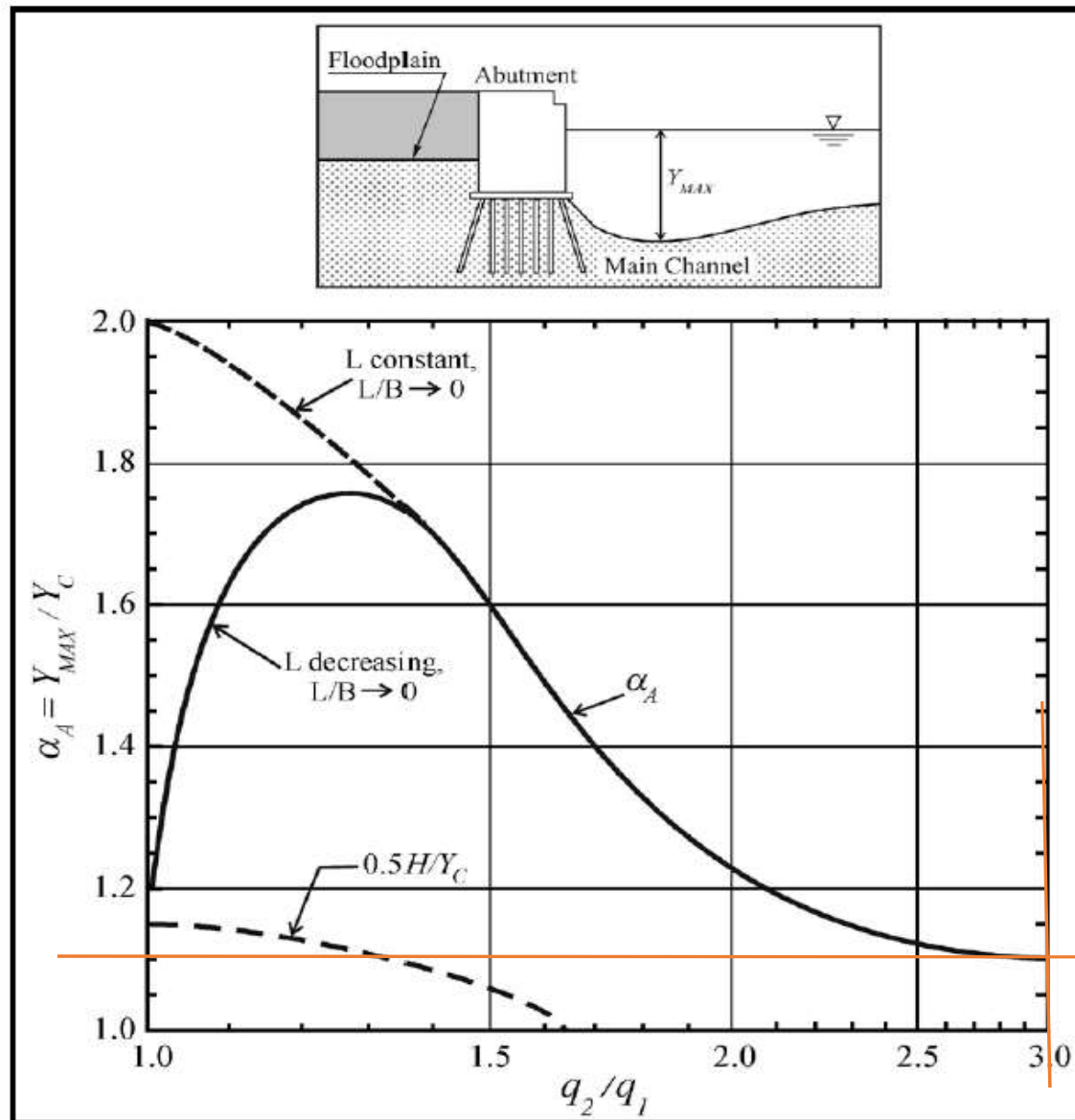


Figure 8.10. Scour amplification factor for wingwall abutments and live-bed conditions (NCHRP 2010b).

Cross Section Output

File Type **Options** Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 35509.99 Profile: 100 year

E.G. Elev (ft)	126.66	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.02	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	126.64	Reach Len. (ft)	238.86	199.47	180.10
Crit W.S. (ft)		Flow Area (sq ft)	3135.30	3477.44	4336.42
E.G. Slope (ft/ft)	0.000017	Area (sq ft)	3135.30	3477.44	4336.42
Q Total (cfs)	5680.00	Flow (cfs)	514.58	4511.29	654.13
Top Width (ft)	2253.26	Top Width (ft)	797.15	204.44	1251.67
Vel Total (ft/s)	0.52	Avg. Vel. (ft/s)	0.16	1.30	0.15
Max Chl Dpth (ft)	18.64	Hydr. Depth (ft)	3.93	17.01	3.46
Conv. Total (cfs)	1392418.0	Conv. (cfs)	126146.6	1105917.0	160355.1
Length Wtd. (ft)	200.15	Wetted Per. (ft)	797.44	213.73	1251.75
Min Ch El (ft)	108.00	Shear (lb/sq ft)	0.00	0.02	0.00
Alpha	4.99	Stream Power (lb/ft s)	0.00	0.02	0.00
Frctn Loss (ft)	0.01	Cum Volume (acre-ft)	508.04	326.49	777.80
C & E Loss (ft)	0.02	Cum SA (acres)	262.74	28.16	172.47

Bridge Output

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 35151 Profile: 100 year

E.G. US. (ft)	126.63	Element	Inside BR US	Inside BR DS
W.S. US. (ft)	126.45	E.G. Elev (ft)	126.48	126.23
Q Total (cfs)	5680.00	W.S. Elev (ft)	125.87	125.53
Q Bridge (cfs)	5680.00	Crit W.S. (ft)	120.39	120.22
Q Weir (cfs)		Max Chl Dpth (ft)	12.76	12.74
Weir Sta Lft (ft)		Vel Total (ft/s)	6.02	6.39
Weir Sta Rgt (ft)		Flow Area (sq ft)	943.68	889.50
Weir Submerg		Froude # Chl	0.34	0.36
Weir Max Depth (ft)		Specif Force (cu ft)	6171.89	5925.20
Min El Weir Flow (ft)	134.91	Hydr Depth (ft)	9.13	8.61
Min El Prs (ft)	130.00	W.P. Total (ft)	133.25	132.81
Delta EG (ft)	0.64	Conv. Total (cfs)	175002.3	165912.2
Delta WS (ft)	0.76	Top Width (ft)	103.39	103.31
BR Open Area (sq ft)	1399.21	Frctn Loss (ft)	0.22	0.04
BR Open Vel (ft/s)	6.39	C & E Loss (ft)	0.03	0.20
BR Sluice Coef		Shear Total (lb/sq ft)	0.47	0.49
BR Sel Method	Energy only	Power Total (lb/ft s)	2.80	3.13

Pier Scour - Colorado State University (CSU) Equation**Imperial Units****Correction for Pier Nose Shape:**

Enter Pier Description ==> Center Bridge, Center Pier

Enter Storm Event and Total Flow ==> Q100 - 5680 CFS

K1 = Pier Nose Shape Coefficient (HEC-18 Table 2)

Type of Pier	K1	Type
Square Nose	1.10	Type 1
Round Nose	1.00	Type 2
Circular Cylinder	1.00	Type 3
Sharp Nose	0.90	Type 4
Group of Cylinders	1.00	Type 5

Enter Type of Pier (1, 2, 3, 4 or 5) ==> 4

K1 = 0.90

Correction for Piers Skewed to Flow

Enter Pier Width (a) ==> 5.00 feet at base of wall

Design Pier Width (a) ==> 6.25 feet increase by 25%, MEDOT BDG 2.3.11.1

K2 = Coefficient Factor for Angle of Attack of the Flow (HEC-18 Table 3)

Enter Attack Angle (0, 15, 30, 45 or 90) ==> 0 Degrees

Enter (Pier Length / Pier Width) Ratio (4, 8, or 12) ==> 12

K2 = 1.00

Correction Factor for Bed Condition

K3 = Coefficient Factor for Bed Condition (HEC-18 Table 1) ==> Assume Clear-Water Scour / Antidune Flow

K3 = 1.10

Depth of Flow at Pier

y1 = Flow Depth Directly Upstream of the Pier

Enter y1 ==> 11.62 ft Reference ==> HEC-RAS

y1 = 11.62 feet

Velocity of Flow Directly Upstream of Pier

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second)

Enter V1 ==> 3.44 fps Reference ==> HEC-RAS

Ve = 3.44 ft per sec

Froude Number $Fr1 = (V1) / \{[(g)(y1)]^{0.5}\} = \text{Froude}$

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second) - Entered Above

g = 32.2 feet / sec²

y1 = Flow Depth Directly Upstream of the Pier - Entered Above

Fr = 0.18

CALCULATE TOTAL LOCAL PIER SCOUR $ys / y1 = (2.0)(K1)(K2)(K3)[(a / y1)^{0.65}](Fr^{0.43})$

y1 = 11.62 feet

ys / y1 = 0.63

K1 = 0.90

K2 = 1.00

K3 = 1.10

a = 6.25 feet

ys = 0.63 X 11.62

Fr = 0.18

ys = Pier Scour Depth = 7.3 feet

BRIDGE SCOUR CALCULATIONS

Project Description :	Farmington, Maine. Hamlin Br No. 3286	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Clear-Water Contraction Scour

Flood Event: **100 Years** Units: English

Laursen's Equation:

$$y_2 = [(K_u * Q^2) / (D_m^{2/3} * W^2)]^{3/7}$$

Required User Inputs:

Q = 5680 CFS Discharge through the bridge or on the set-back overbank area associated with W.
W = 75.34 ft Top width of the contracted section less pier width(s).
y_o = 10.85 ft Average existing depth in the contracted section.

Calculated Inputs:

D_m = 0.02797 ft Diameter of the smallest nontransportable particle (1.25xD50).
D₅₀ = 0.02238 ft Median diameter of bed material. Assumed 6mm for scour design.
K_u = 0.0077 Equation constant base on units.
y₂ = 14.03 ft Average equilibrium depth in the contracted section after contraction scour.

Calculated Scour Depth: **3.18 ft** *Clear-Water Contraction Scour*

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	100 year		
Reach:	Reach	RS:	35151 BR U	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 35151 BR U Profile: 100 year					
E.G. Elev (ft)	126.48	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.61	Wt. n-Val.	0.092	0.031	0.031
W.S. Elev (ft)	125.87	Reach Len. (ft)	201.00	201.00	201.00
Crit W.S. (ft)	120.39	Flow Area (sq ft)	32.91	871.63	39.14
E.G. Slope (ft/ft)	0.001053	Area (sq ft)	32.91	871.63	39.14
Q Total (cfs)	5680.00	Flow (cfs)	31.38	5523.91	124.71
Top Width (ft)	103.39	Top Width (ft)	11.47	80.34	11.58
Vel Total (ft/s)	6.02	Avg. Vel. (ft/s)	0.95	6.34	3.19
Max Chl Dpth (ft)	12.76	Hydr. Depth (ft)	2.87	10.85	3.38
Conv. Total (cfs)	175002.3	Conv. (cfs)	966.9	170193.3	3842.2
Length Wtd. (ft)	201.00	Wetted Per. (ft)	13.42	106.43	13.41
Min Ch El (ft)	113.11	Shear (lb/sq ft)	0.16	0.54	0.19
Alpha	1.08	Stream Power (lb/ft s)	0.15	3.41	0.61
Frctn Loss (ft)	0.22	Cum Volume (acre-ft)	492.59	313.06	762.42
C & E Loss (ft)	0.03	Cum SA (acres)	257.64	27.22	166.27

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, Center Bridge	Project Number:	18084.99
		Calculated By:	TEPA
		Checked By:	5/1/2019

Flood Event: **500 Years** **RS 35310.52**
 Units: **English**

Description of Streambed Material :

D₅₀ of Streambed Material: **0.022375** ft Particle size in a mixture of which 50% are smaller.
D₉₅ of Streambed Material: ft Particle size in a mixture of which 95% are smaller.

Determine Critical Velocity

$$V_c = K_u y^{1/6} D_{50}^{1/3}$$

Required User Inputs:

y = **12.87** ft Average depth of flow upstream of the bridge.
 V = **3.91** ft/s Upstream Velocity (from HEC-RAS)

Calculated Inputs:

D50 = 0.02237533 ft Particle size in a mixture of which 50% are smaller.
 Ku = 11.17 Equation constant based on units.
 Vc = 4.82 ft/s

Type of Scour = **Clear-Water Scour**

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	500 year		
Reach:	Reach	RS:	35310.52	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 35310.52 Profile: 500 year					
E.G. Elev (ft)	127.94	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.24	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	127.70	Reach Len. (ft)	59.00	59.00	59.00
Crit W.S. (ft)	118.97	Flow Area (sq ft)	36.61	1820.95	93.73
E.G. Slope (ft/ft)	0.000230	Area (sq ft)	3073.07	1820.95	3970.42
Q Total (cfs)	7180.00	Flow (cfs)	20.94	7118.02	41.04
Top Width (ft)	2319.82	Top Width (ft)	863.19	141.50	1315.13
Vel Total (ft/s)	3.68	Avg. Vel. (ft/s)	0.57	3.91	0.44
Max Chl Dpth (ft)	14.70	Hydr. Depth (ft)	3.57	12.87	2.39
Conv. Total (cfs)	473100.1	Conv. (cfs)	1379.7	469016.1	2704.4
Length Wtd. (ft)	59.00	Wetted Per. (ft)	10.27	153.56	39.25
Min Ch El (ft)	113.00	Shear (lb/sq ft)	0.05	0.17	0.03
Alpha	1.12	Stream Power (lb/ft s)	0.03	0.67	0.02
Frctn Loss (ft)	0.03	Cum Volume (acre-ft)	783.19	344.40	952.94
C & E Loss (ft)	0.17	Cum SA (acres)	262.50	27.38	174.10

NCHRP 24-20 Scour Calculations

Project Description :	I-95 over Souadabscook Stream, Center Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **500 years**

y_c = Flow depth including clear-water contraction scour, ft (m)

q_{2c} = unit discharge in the constricted opening accounting for non-uniform flow distribution, ft²/s (m²/s)

K_u = 11.17 (English units) or 6.19 (SI units)

D_{50} = Particle size with 50 percent finer, ft (m)

$$y_c = y_1 \left(\frac{q_{2c}}{q_1} \right)^{6/7} \quad \text{scour equation (eq. 8.5, HEC 18)}$$

y_{max} = Maximum flow depth resulting from abutment scour, ft (m)

y_c = Flow depth including live-bed or clear-water contraction scour, ft (m)

α_A = Amplification factor for live-bed conditions

α_B = Amplification factor for clear-water conditions

y_s = Abutment scour depth, ft (m)

y_0 = Flow depth prior to scour, ft (m)

$$y_{max} = \alpha_A y_c \text{ OR } y_{max} = \alpha_B y_c$$

$$y_s = y_{max} - y_0$$

The scour type for NCHRP 24-20 is determined by a ratio of L/Bf, or embankment length over the total floodplain width. If this ratio is greater than 75%, then live-bed scour occurs. If it is less than 75% then clearwater scour occurs. Since the interstate is acting more like a causeway for this stream, L/Bf > 75% by inspection and live-bed scour

*The embankment length is equal to the total area in a cross section intercepted by the flow, minus the bridge opening.

Scour Type: Live-Bed Scour

Upstream						RS 35509.99						From HEC Ras						
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q1			
7180	2278.58	13910.3	6.10	11.17	0.02238	0.2	5.21	844.11	1.39	18.32	5206.27	0.19	4.71	1129.62	18.7280			

Bridge RS 35151 BR U						From HEC Ras									
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q2c
7180	112.36	1156.38	10.2917	11.17	0.02238	0	0	0	6.21	10.29	7180	0	0	0	63.9009

NOTE: q1 & q2c = (Velocity x Depth) for L OB, R OB, and Ch, weighted by flow

$q_{2c}/q_1 = \frac{3.41205}{1.1}$, use chart to calculate α_A
 $\alpha_B = 1.1$ from chart.
 $y_c = 17.48$ ft (Eq. 8.6)
 $y_{max} = 19.228$ ft

Designers Note: $q_{2c}/q_1 > 3$, therefore conservatively use lowest value on chart

KEY:

L OB D = Left Overbank Depth (ft)
R OB Vel = Right Overbank Velocity (ft/s)
CH Flow = Channel Flow (cfs)

CALCULATED SCOUR

$$y_s = 8.93798 \text{ ft}$$

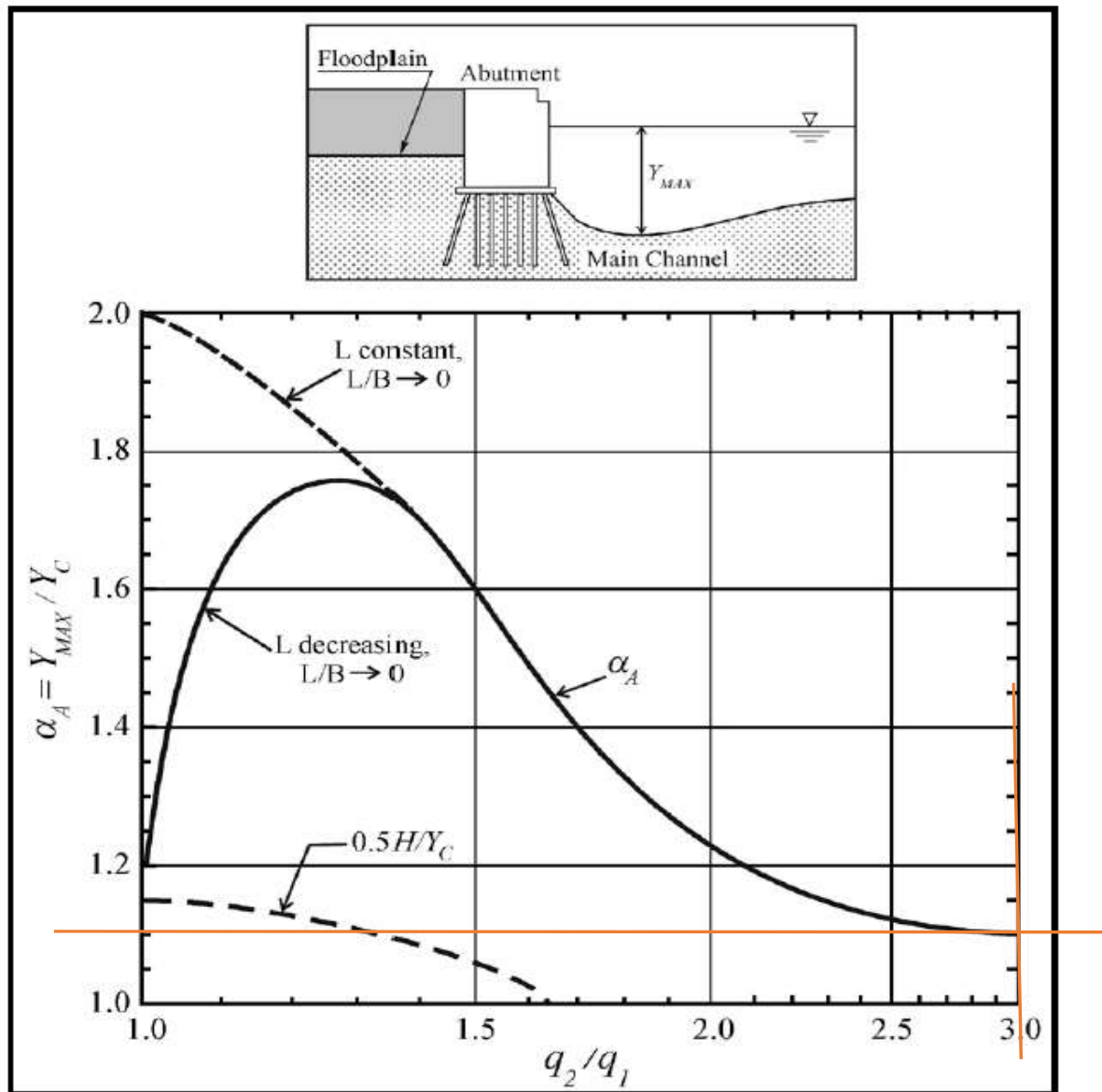


Figure 8.10. Scour amplification factor for wingwall abutments and live-bed conditions (NCHRP 2010b).

Cross Section Output

File Type Options Help

River: Souadabscook Str Profile: 500 year

Reach: Reach RS: 35509.99 Plan: SCOUR

Plan: SCOUR Souadabscook Str Reach RS: 35509.99 Profile: 500 year

		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	127.97	Wt. n-Val.	0.092	0.030	0.092
Vel Head (ft)	0.02	Reach Len. (ft)	238.86	199.47	180.10
W.S. Elev (ft)	127.94	Flow Area (sq ft)	4180.39	3744.60	5985.26
Crit W.S. (ft)		Area (sq ft)	4180.39	3744.60	5985.26
E.G. Slope (ft/ft)	0.000017	Flow (cfs)	844.11	5206.27	1129.62
Q Total (cfs)	7180.00	Top Width (ft)	802.33	204.44	1271.81
Top Width (ft)	2278.58	Avg. Vel. (ft/s)	0.20	1.39	0.19
Vel Total (ft/s)	0.52	Hydr. Depth (ft)	5.21	18.32	4.71
Max Chl Dpth (ft)	19.94	Conv. (cfs)	202849.0	1251120.0	271458.8
Conv. Total (cfs)	1725428.0	Wetted Per. (ft)	802.78	213.73	1271.93
Length Wtd. (ft)	200.26	Shear (lb/sq ft)	0.01	0.02	0.01
Min Ch El (ft)	108.00	Stream Power (lb/ft s)	0.00	0.03	0.00
Alpha	5.30	Cum Volume (acre-ft)	803.08	357.14	973.52
Frctn Loss (ft)	0.01	Cum SA (acres)	267.06	28.17	179.45
C & E Loss (ft)	0.02				

File Type Options Help

River: Souadabscook Str Profile: 500 year

Reach: Reach RS: 40346 Plan: SCOUR

Plan: SCOUR Souadabscook Str Reach RS: 40346 Profile: 500 year

		Element	Inside BR US	Inside BR DS
E.G. US. (ft)	128.88	E.G. Elev (ft)	128.77	128.58
W.S. US. (ft)	128.47	W.S. Elev (ft)	128.10	127.89
Q Total (cfs)	7180.00	Crit W.S. (ft)	121.97	122.03
Q Bridge (cfs)	7180.00	Max Chl Dpth (ft)	16.13	14.99
Q Weir (cfs)		Vel Total (ft/s)	6.21	6.32
Weir Sta Lft (ft)		Flow Area (sq ft)	1156.38	1136.17
Weir Sta Rgt (ft)		Froude # Chl	0.34	0.35
Weir Submerg		Specif Force (cu ft)	8374.90	8072.63
Weir Max Depth (ft)		Hydr Depth (ft)	10.29	10.14
Min El Weir Flow (ft)	134.81	W.P. Total (ft)	148.97	147.17
Min El Prs (ft)	130.00	Conv. Total (cfs)	229403.7	224271.3
Delta EG (ft)	0.48	Top Width (ft)	112.36	112.05
Delta WS (ft)	0.54	Frctn Loss (ft)	0.18	0.07
BR Open Area (sq ft)	1375.71	C & E Loss (ft)	0.01	0.11
BR Open Vel (ft/s)	6.32	Shear Total (lb/sq ft)	0.47	0.49
BR Sluice Coef		Power Total (lb/ft s)	2.95	3.12
BR Sel Method	Energy only			

Pier Scour - Colorado State University (CSU) Equation**Imperial Units**

Enter Pier Description ==> Center Bridge, Center Pier

Correction for Pier Nose Shape:

Enter Storm Event and Total Flow ==> Q500 - 7180 CFS

K1 = Pier Nose Shape Coefficient (HEC-18 Table 2)

Type of Pier	K1	Type
Square Nose	1.10	Type 1
Round Nose	1.00	Type 2
Circular Cylinder	1.00	Type 3
Sharp Nose	0.90	Type 4
Group of Cylinders	1.00	Type 5

Enter Type of Pier (1, 2, 3, 4 or 5) ==> 4

K1 = 0.90

Correction for Piers Skewed to Flow

Enter Pier Width (a) ==> 5.00 feet at base of wall

Design Pier Width (a) ==> 6.25 feet increase by 25%, MEDOT BDG 2.3.11.1

K2 = Coefficient Factor for Angle of Attack of the Flow (HEC-18 Table 3)

Enter Attack Angle (0, 15, 30, 45 or 90) ==> 0 Degrees

Enter (Pier Length / Pier Width) Ratio (4, 8, or 12) ==> 12

K2 = 1.00

Correction Factor for Bed Condition

K3 = Coefficient Factor for Bed Condition (HEC-18 Table 1) ==> Assume Clear-Water Scour / Antidune Flow

K3 = 1.10

Depth of Flow at Pier

y1 = Flow Depth Directly Upstream of the Pier

Enter y1 ==> 12.87 ft Reference ==> HEC-RAS

y1 = 12.87 feet

Velocity of Flow Directly Upstream of Pier

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second)

Enter V1 ==> 3.91 fps Reference ==> HEC-RAS

Ve = 3.91 ft per sec

Froude Number $Fr1 = (V1) / \{[(g)(y1)]^{0.5}\} = \text{Froude}$

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second) - Entered Above

g = 32.2 feet / sec²

y1 = Flow Depth Directly Upstream of the Pier - Entered Above

Fr = 0.19

CALCULATE TOTAL LOCAL PIER SCOUR $ys / y1 = (2.0)(K1)(K2)(K3)[(a / y1)^{0.65}](Fr^{0.43})$

y1 = 12.87 feet

ys / y1 = 0.61

K1 = 0.90

K2 = 1.00

K3 = 1.10

a = 6.25 feet

ys = 0.61 X 12.87

Fr = 0.19

ys = Pier Scour Depth = 7.8 feet

BRIDGE SCOUR CALCULATIONS

Project Description :	Farmington, Maine. Hamlin Br No. 3286	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Clear-Water Contraction Scour

Flood Event: **500 Years** Units: English

Laursen's Equation:

$$y_2 = [(K_u * Q^2) / (D_m^{2/3} * W^2)]^{3/7}$$

Required User Inputs:

Q = 7180 CFS Discharge through the bridge or on the set-back overbank area associated with W.
W = 75.46 ft Top width of the contracted section less pier width(s).
y_o = 11.92 ft Average existing depth in the contracted section.

Calculated Inputs:

D_m = 0.02797 ft Diameter of the smallest nontransportable particle (1.25xD50).
D₅₀ = 0.02238 ft Median diameter of bed material. Assumed 6mm for scour design.
K_u = 0.0077 Equation constant base on units.
y₂ = 17.13 ft Average equilibrium depth in the contracted section after contraction scour.

Calculated Scour Depth: **5.21 ft** *Clear-Water Contraction Scour*

Cross Section Output					
File Type Options Help					
River:	Soudabscook Str	Profile:	500 year		
Reach:	Reach	RS:	35151 BR U	Plan:	SCOUR
Plan: SCOUR Soudabscook Str Reach RS: 35151 BR U Profile: 500 year					
E.G. Elev (ft)	127.74	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.79	Wt. n-Val.	0.092	0.031	0.031
W.S. Elev (ft)	126.96	Reach Len. (ft)	201.00	201.00	201.00
Crit W.S. (ft)	121.32	Flow Area (sq ft)	46.77	958.71	52.68
E.G. Slope (ft/ft)	0.001238	Area (sq ft)	46.77	958.71	52.68
Q Total (cfs)	7180.00	Flow (cfs)	53.71	6925.36	200.94
Top Width (ft)	108.02	Top Width (ft)	14.13	80.46	13.43
Vel Total (ft/s)	6.79	Avg. Vel. (ft/s)	1.15	7.22	3.81
Max Chl Dpth (ft)	13.85	Hydr. Depth (ft)	3.31	11.92	3.92
Conv. Total (cfs)	204037.5	Conv. (cfs)	1526.2	196801.2	5710.2
Length Wtd. (ft)	201.00	Wetted Per. (ft)	16.29	108.60	15.55
Min Ch El (ft)	113.11	Shear (lb/sq ft)	0.22	0.68	0.26
Alpha	1.10	Stream Power (lb/ft s)	0.25	4.93	1.00
Frctn Loss (ft)	0.27	Cum Volume (acre-ft)	781.08	342.51	950.21
C & E Loss (ft)	0.04	Cum SA (acres)	261.90	27.23	173.20

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, East Bridge	Project Number:	18084.99
		Calculated By:	TEPA
		Checked By:	5/1/2019

Flood Event: **100 Years** **RS 28120.39**
 Units: **English**

Description of Streambed Material :

D₅₀ of Streambed Material: **0.000558** ft Particle size in a mixture of which 50% are smaller.
D₉₅ of Streambed Material: ft Particle size in a mixture of which 95% are smaller.

Determine Critical Velocity

$$V_c = K_u y^{1/6} D_{50}^{1/3}$$

Required User Inputs:

y = **7.86** ft Average depth of flow upstream of the bridge.
 V = **5.63** ft/s Upstream Velocity (from HEC-RAS)

Calculated Inputs:

D₅₀ = 0.00055774 ft Particle size in a mixture of which 50% are smaller.
 K_u = 11.17 Equation constant based on units.
 V_c = 1.30 ft/s

Type of Scour = **Live-Bed Scour**

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	100 year		
Reach:	Reach	RS:	28120.39	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 28120.39 Profile: 100 year					
E.G. Elev (ft)	125.71	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.49	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	125.23	Reach Len. (ft)	45.00	45.00	45.00
Crit W.S. (ft)	121.33	Flow Area (sq ft)	66.95	995.46	27.45
E.G. Slope (ft/ft)	0.000843	Area (sq ft)	364.59	995.46	53.52
Q Total (cfs)	5680.00	Flow (cfs)	60.31	5603.18	16.51
Top Width (ft)	639.35	Top Width (ft)	436.74	126.61	76.00
Vel Total (ft/s)	5.21	Avg. Vel. (ft/s)	0.90	5.63	0.60
Max Chl Dpth (ft)	8.23	Hydr. Depth (ft)	2.68	7.86	1.49
Conv. Total (cfs)	195651.2	Conv. (cfs)	2077.5	193005.0	568.7
Length Wtd. (ft)	45.00	Wetted Per. (ft)	25.14	128.53	18.90
Min Ch El (ft)	117.00	Shear (lb/sq ft)	0.14	0.41	0.08
Alpha	1.15	Stream Power (lb/ft s)	0.13	2.29	0.05
Frctn Loss (ft)	0.05	Cum Volume (acre-ft)	2.22	21.04	0.58
C & E Loss (ft)	0.03	Cum SA (acres)	2.08	3.35	0.33

NCHRP 24-20 Scour Calculations

Project Description :	I-95 over Souadabscook Stream, East Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **100 years**

y_c = Flow depth including clear-water contraction scour, ft (m)

q_{2c} = unit discharge in the constricted opening accounting for non-uniform flow distribution, ft²/s (m²/s)

K_u = 11.17 (English units) or 6.19 (SI units)

D_{50} = Particle size with 50 percent finer, ft (m)

$$y_c = y_1 \left(\frac{q_{2c}}{q_1} \right)^{6/7} \quad \text{scour equation (eq. 8.5, HEC 18)}$$

y_{max} = Maximum flow depth resulting from abutment scour, ft (m)

y_c = Flow depth including live-bed or clear-water contraction scour, ft (m)

α_A = Amplification factor for live-bed conditions

α_B = Amplification factor for clear-water conditions

y_s = Abutment scour depth, ft (m)

y_0 = Flow depth prior to scour, ft (m)

$$y_{max} = \alpha_A y_c \text{ OR } y_{max} = \alpha_B y_c$$

$$y_s = y_{max} - y_0$$

The scour type for NCHRP 24-20 is determined by a ratio of L/Bf, or embankment length over the total floodplain width. If this ratio is greater than 75%, then live-bed scour occurs. If it is less than 75% then clearwater scour occurs. Since the interstate is acting more like a causeway for this stream, L/Bf > 75% by inspection and live-bed scour

*The embankment length is equal to the total area in a cross section intercepted by the flow, minus the bridge opening.

Scour Type: Live-Bed Scour

Upstream						From HEC Ras									
RS 29483.97															
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q1
5680	1345.54	6181.9	4.59	11.17	0.00056	0.18	1.78	838.85	1.96	13.59	2331.28	0.32	4.28	3011.77	10.7557

Bridge RS 27966 BR U						From HEC Ras									
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q2c
5680	104.92	841.94	8.02459	11.17	0.00056	0	0	0	6.75	8.02	5680	0	0	0	54.1350

NOTE: q1 & q2c = (Velocity x Depth) for L OB, R OB, and Ch, weighted by flow

$q_{2c}/q_1 = \frac{5.03315}{10.7557}$, use chart to calculate α_B

$\alpha_B = 1.1$ from chart.

$y_c = 18.357$ ft (Eq. 8.6)

$y_{max} = 20.1927$ ft

Designers Note: $q_{2c}/q_1 > 3$, therefore conservatively use lowest value on chart

CALCULATED SCOUR

$$y_s = 12.1727 \text{ ft}$$

KEY:

L OB D = Left Overbank Depth (ft)

R OB Vel = Right Overbank Velocity (ft/s)

CH Flow = Channel Flow (cfs)

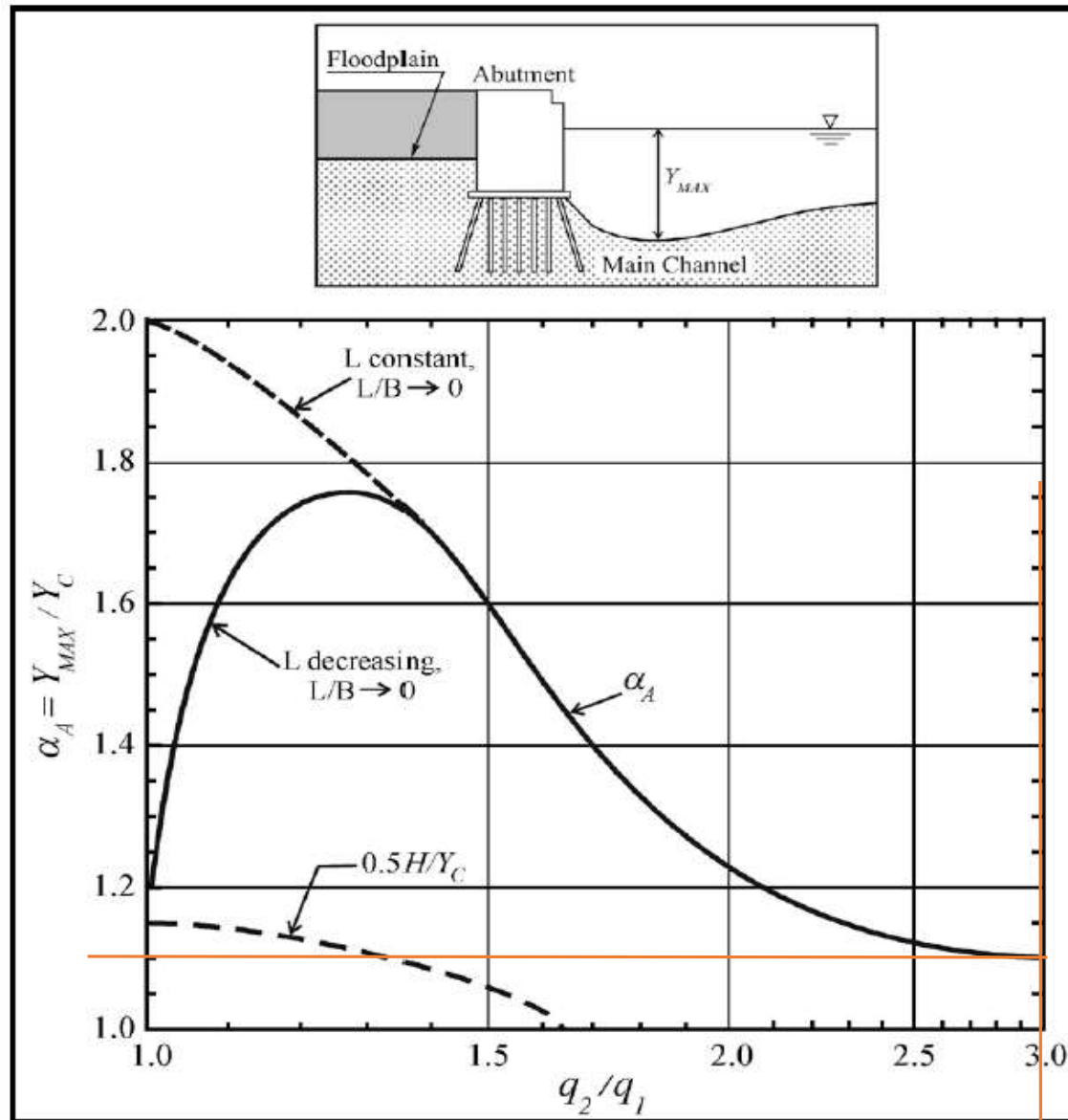


Figure 8.10. Scour amplification factor for wingwall abutments and live-bed conditions (NCHRP 2010b).

Cross Section Output

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 29483.97 Profile: 100 year

		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	125.89	Wt. n-Val.	0.092	0.030	0.092
Vel Head (ft)	0.05	Reach Len. (ft)	1179.44	1180.61	1189.53
W.S. Elev (ft)	125.85	Flow Area (sq ft)	838.85	2331.28	3011.77
Crit W.S. (ft)		Area (sq ft)	838.85	2331.28	3011.77
E.G. Slope (ft/ft)	0.000055	Flow (cfs)	148.04	4578.86	953.11
Q Total (cfs)	5680.00	Top Width (ft)	470.74	171.50	703.30
Top Width (ft)	1345.54	Avg. Vel. (ft/s)	0.18	1.96	0.32
Vel Total (ft/s)	0.92	Hydr. Depth (ft)	1.78	13.59	4.28
Max Chl Dpth (ft)	13.70	Conv. (cfs)	19913.7	615942.3	128210.8
Conv. Total (cfs)	764066.8	Wetted Per. (ft)	470.76	189.23	703.85
Length Wtd. (ft)	1181.36	Shear (lb/sq ft)	0.01	0.04	0.01
Min Ch El (ft)	112.15	Stream Power (lb/ft s)	0.00	0.08	0.00
Alpha	3.70	Cum Volume (acre-ft)	31.46	84.84	46.19
Frctn Loss (ft)	0.09	Cum SA (acres)	19.00	8.34	13.44
C & E Loss (ft)	0.01				

Bridge Output

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 27966 Profile: 100 year

		Element	Inside BR US	Inside BR DS
E.G. US. (ft)	125.71	E.G. Elev (ft)	125.63	125.31
W.S. US. (ft)	125.23	W.S. Elev (ft)	124.84	124.49
Q Total (cfs)	5680.00	Crit W.S. (ft)	120.28	120.30
Q Bridge (cfs)	5680.00	Max Chl Dpth (ft)	12.74	11.69
Q Weir (cfs)		Vel Total (ft/s)	6.75	6.86
Weir Sta Lft (ft)		Flow Area (sq ft)	841.94	828.31
Weir Sta Rgt (ft)		Froude # Chl	0.40	0.41
Weir Submerg		Specif Force (cu ft)	5440.45	5247.16
Weir Max Depth (ft)		Hydr Depth (ft)	8.02	7.77
Min El Weir Flow (ft)	134.91	W.P. Total (ft)	133.60	134.18
Min El Prs (ft)	130.00	Conv. Total (cfs)	149424.6	144434.4
Delta EG (ft)	0.55	Top Width (ft)	104.92	106.57
Delta WS (ft)	1.14	Frctn Loss (ft)	0.32	0.12
BR Open Area (sq ft)	1441.68	C & E Loss (ft)	0.00	0.02
BR Open Vel (ft/s)	6.86	Shear Total (lb/sq ft)	0.57	0.60
BR Sluice Coef		Power Total (lb/ft s)	3.84	4.09
BR Sel Method	Energy only			

Pier Scour - Colorado State University (CSU) Equation**Imperial Units****Correction for Pier Nose Shape:**

Enter Pier Description ==> East Bridge, Center Pier

Enter Storm Event and Total Flow ==> Q100 - 5680 CFS

K1 = Pier Nose Shape Coefficient (HEC-18 Table 2)

Type of Pier	K1	Type
Square Nose	1.10	Type 1
Round Nose	1.00	Type 2
Circular Cylinder	1.00	Type 3
Sharp Nose	0.90	Type 4
Group of Cylinders	1.00	Type 5

Enter Type of Pier (1, 2, 3, 4 or 5) ==> 4

K1 = 0.90

Correction for Piers Skewed to Flow

Enter Pier Width (a) ==> 5.00 feet at base of wall

Design Pier Width (a) ==> 6.25 feet increase by 25%, MEDOT BDG 2.3.11.1

K2 = Coefficient Factor for Angle of Attack of the Flow (HEC-18 Table 3)

Enter Attack Angle (0, 15, 30, 45 or 90) ==> 0 Degrees

Enter (Pier Length / Pier Width) Ratio (4, 8, or 12) ==> 12

K2 = 1.00

Correction Factor for Bed Condition

K3 = Coefficient Factor for Bed Condition (HEC-18 Table 1) ==> Assume Clear-Water Scour / Antidune Flow

K3 = 1.10

Depth of Flow at Pier

y1 = Flow Depth Directly Upstream of the Pier

Enter y1 ==> 7.86 ft Reference ==> HEC-RAS

y1 = 7.86 feet

Velocity of Flow Directly Upstream of Pier

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second)

Enter V1 ==> 5.63 fps Reference ==> HEC-RAS

Ve = 5.63 ft per sec

Froude Number $Fr1 = (V1) / \{[(g)(y1)]^{0.5}\} = \text{Froude}$

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second) - Entered Above

g = 32.2 feet / sec²

y1 = Flow Depth Directly Upstream of the Pier - Entered Above

Fr = 0.35

CALCULATE TOTAL LOCAL PIER SCOUR $ys / y1 = (2.0)(K1)(K2)(K3)[(a / y1)^{0.65}](Fr^{0.43})$

y1 = 7.86 feet

ys / y1 = 1.09

K1 = 0.90

K2 = 1.00

K3 = 1.10

a = 6.25 feet

ys = 1.09 X 7.86

Fr = 0.35

ys = Pier Scour Depth = 8.6 feet

BRIDGE SCOUR CALCULATIONS

Project Description :	Farmington, Maine. Hamlin Br No. 3286	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Live Bed Contraction Scour

Flood Event: 100 Years

$$\frac{y_2}{y_1} = \left(\frac{Q_2}{Q_1} \right)^{6/7} \left(\frac{W_1}{W_2} \right)^{k_1} \quad y_s = y_2 - y_o = (\text{average contraction scour depth})$$

Required User Inputs:

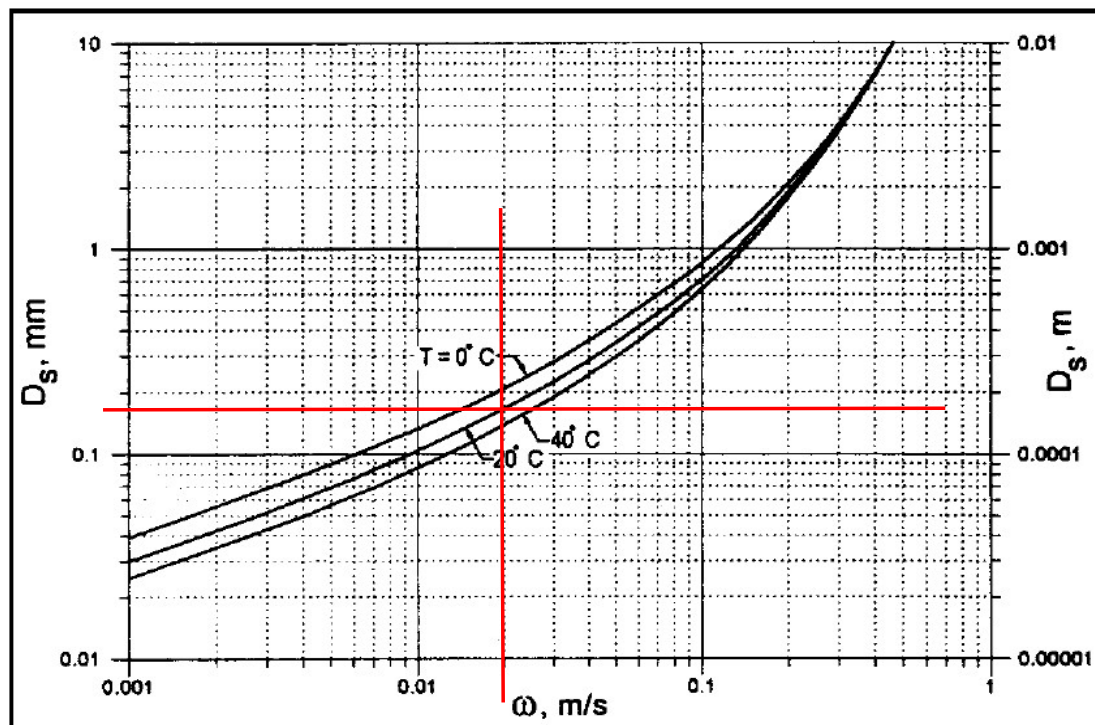
y1 =	7.86	ft	Average depth of mainstream channel
D50 =	0.17	mm	
Q1 =	5603.18	CFS	flow in upstream channel transporting sediment
Q2 =	5680	CFS	flow in contracted channel
W1 =	126.61	ft	Top width of upstream main channel that is transporting bed material
W2 =	67.45	ft	Top width of main channel in contracted section less pier widths
y _o =	10.33	ft	Average existing depth in the contracted section.
EGL Slope =	0.001445	ft/ft	slope of energy grade line (from bridge cross section)
T =	0.0656	ft/s	fall velocity of bed material (from chart below)

Calculated Inputs:

g =	32.2	ft/s ²	constant
V* =	0.604746	ft/s ²	shear velocity in upstream section
k1 =	0.69		

y₂ = 12.28 ft Average equilibrium depth in the contracted section after contraction scour.

Calculated Scour Depth: 1.95 ft *Live Bed Contraction Scour*



Plan: SCOUR Souadabscook Str Reach RS: 28120.39 Profile: 100 year					
Element		Left OB	Channel	Right OB	
E.G. Elev (ft)	125.71				
Vel Head (ft)	0.49	0.092	0.030	0.092	
W.S. Elev (ft)	125.23	45.00	45.00	45.00	
Crit W.S. (ft)	121.33	66.95	995.46	27.45	
E.G. Slope (ft/ft)	0.000843	364.59	995.46	53.52	
Q Total (cfs)	5680.00	60.31	5603.18	16.51	
Top Width (ft)	639.35	436.74	126.61	76.00	
Vel Total (ft/s)	5.21	0.90	5.63	0.60	
Max Chl Dpth (ft)	8.23	2.68	7.86	1.49	
Conv. Total (cfs)	195651.2	2077.5	195003.0	568.7	
Length Wtd. (ft)	45.00	25.14	128.53	18.90	
Min Ch El (ft)	117.00	0.14	0.41	0.08	
Alpha	1.15	0.13	2.29	0.05	
Frctn Loss (ft)	0.05	2.22	21.04	0.58	
C & E Loss (ft)	0.03	2.08	3.35	0.33	

Plan: SCOUR Souadabscook Str Reach RS: 27966 BR U Profile: 100 year					
Element		Left OB	Channel	Right OB	
E.G. Elev (ft)	125.63				
Vel Head (ft)	0.80	0.092	0.030	0.036	
W.S. Elev (ft)	124.84	212.00	212.00	212.00	
Crit W.S. (ft)	120.28	37.61	748.06	56.26	
E.G. Slope (ft/ft)	0.001445	37.61	748.06	56.26	
Q Total (cfs)	5680.00	41.21	5443.52	195.27	
Top Width (ft)	104.92	14.25	72.45	18.22	
Vel Total (ft/s)	6.75	1.10	7.28	3.47	
Max Chl Dpth (ft)	12.74	2.64	10.33	3.09	
Conv. Total (cfs)	149424.6	1084.0	143203.6	5137.0	
Length Wtd. (ft)	212.00	15.78	98.45	19.37	
Min Ch El (ft)	112.10	0.22	0.69	0.26	
Alpha	1.12	0.24	4.99	0.91	
Frctn Loss (ft)	0.32	2.01	20.14	0.52	
C & E Loss (ft)	0.00	1.85	3.25	0.28	

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, East Bridge	Project Number:	18084.99
		Calculated By:	TEPA
		Checked By:	5/1/2019

Flood Event: **500 Years** **RS 28120.39**
 Units: **English**

Description of Streambed Material :

D₅₀ of Streambed Material: **0.000558** ft Particle size in a mixture of which 50% are smaller.
D₉₅ of Streambed Material: ft Particle size in a mixture of which 95% are smaller.

Determine Critical Velocity

$$V_c = K_u y^{1/6} D_{50}^{1/3}$$

Required User Inputs:

y = **9.09** ft Average depth of flow upstream of the bridge.
 V = **5.63** ft/s Upstream Velocity (from HEC-RAS)

Calculated Inputs:

D50 = 0.00055774 ft Particle size in a mixture of which 50% are smaller.
 Ku = 11.17 Equation constant based on units.
 Vc = 1.33 ft/s

Type of Scour = **Live-Bed Scour**

Plan: SCOUR Souadabscook Str Reach RS: 28120.39 Profile: 500 year					
E.G. Elev (ft)	126.90	Element	Left OB	Channel	Right OB
Vel Head (ft)	0.45	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	126.45	Reach Len. (ft)	45.00	45.00	45.00
Crit W.S. (ft)	122.00	Flow Area (sq ft)	910.62	1150.54	184.17
E.G. Slope (ft/ft)	0.000696	Area (sq ft)	910.62	1150.54	184.17
Q Total (cfs)	7180.00	Flow (cfs)	611.61	6479.48	88.90
Top Width (ft)	742.74	Top Width (ft)	459.63	126.61	156.51
Vel Total (ft/s)	3.20	Avg. Vel. (ft/s)	0.67	5.63	0.48
Max Chl Dpth (ft)	9.45	Hydr. Depth (ft)	1.98	9.09	1.18
Conv. Total (cfs)	272238.7	Conv. (cfs)	23190.1	245677.7	3370.9
Length Wtd. (ft)	45.00	Wetted Per. (ft)	459.94	128.53	157.24
Min Ch El (ft)	117.00	Shear (lb/sq ft)	0.09	0.39	0.05
Alpha	2.80	Stream Power (lb/ft s)	0.06	2.19	0.02
Frctn Loss (ft)	0.05	Cum Volume (acre-ft)	4.84	24.02	1.05
C & E Loss (ft)	0.06	Cum SA (acres)	3.58	3.36	0.94

NCHRP 24-20 Scour Calculations

Project Description :	I-95 over Souadabscook Stream, East Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Flood Event: **500 years**

y_c = Flow depth including clear-water contraction scour, ft (m)

q_{2c} = unit discharge in the constricted opening accounting for non-uniform flow distribution, ft²/s (m²/s)

K_u = 11.17 (English units) or 6.19 (SI units)

D_{50} = Particle size with 50 percent finer, ft (m)

$$y_c = y_1 \left(\frac{q_{2c}}{q_1} \right)^{6/7} \quad \text{scour equation (eq. 8.5, HEC 18)}$$

y_{max} = Maximum flow depth resulting from abutment scour, ft (m)

y_c = Flow depth including live-bed or clear-water contraction scour, ft (m)

α_A = Amplification factor for live-bed conditions

α_B = Amplification factor for clear-water conditions

y_s = Abutment scour depth, ft (m)

y_0 = Flow depth prior to scour, ft (m)

$$y_{max} = \alpha_A y_c \text{ OR } y_{max} = \alpha_B y_c$$

$$y_s = y_{max} - y_0$$

The scour type for NCHRP 24-20 is determined by a ratio of L/Bf, or embankment length over the total floodplain width. If this ratio is greater than 75%, then live-bed scour occurs. If it is less than 75% then clearwater scour occurs. Since the interstate is acting more like a causeway for this stream, L/Bf > 75% by inspection and live-bed scour

*The embankment length is equal to the total area in a cross section intercepted by the flow, minus the bridge opening.

Scour Type: Live-Bed Scour

Upstream						From HEC Ras										
RS 29483.97																
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q1	
7180	1555.85	7914	5.09	11.17	0.00056	0.24	2.77	1419.33	2.12	14.77	2533.65	0.37	4.54	3961.02	10.9846	

Bridge RS 27966 BR U						From HEC Ras									
Q	W	Area	yo	Ku	D50	L OB Vel	L OB D	L OB Flow	Ch Vel	CH D	CH Flow	R OB Vel	R OB D	R OB Flow	q2c
7180	108.79	939.47	8.63563	11.17	0.00056	0	0	0	7.64	8.64	7180	0	0	0	66.0096

NOTE: q_1 & q_{2c} = (Velocity x Depth) for L OB, R OB, and Ch, weighted by flow

$q_{2c}/q_1 = \frac{6.0093}{10.9846}$, use chart to calculate α_B
 $\alpha_B = 1.1$ from chart.
 $y_c = 23.6587$ ft (Eq. 8.6)
 $y_{max} = 26.0246$ ft

Designers Note: $q_{2c}/q_1 > 3$, therefore conservatively use lowest value on chart

KEY:

L OB D = Left Overbank Depth (ft)
R OB Vel = Right Overbank Velocity (ft/s)
CH Flow = Channel Flow (cfs)

CALCULATED SCOUR

$$y_s = 17.389 \text{ ft}$$

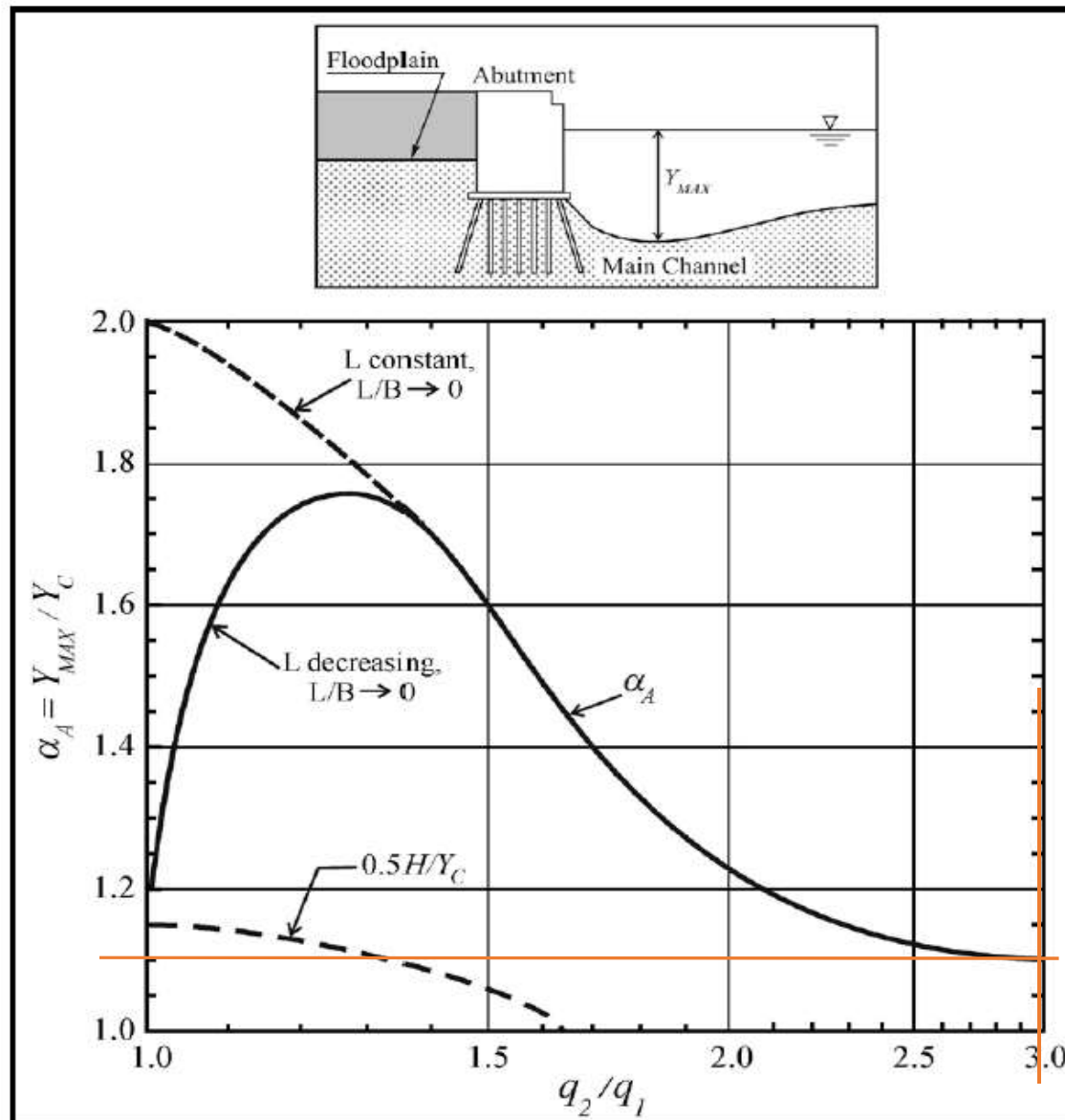


Figure 8.10. Scour amplification factor for wingwall abutments and live-bed conditions (NCHRP 2010b).

Cross Section Output

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 29483.97 Profile: 500 year

		Element	Left OB	Channel	Right OB
E.G. Elev (ft)	127.08	Wt. n-Val.	0.092	0.030	0.092
Vel Head (ft)	0.05	Reach Len. (ft)	1179.44	1180.61	1189.53
W.S. Elev (ft)	127.03	Flow Area (sq ft)	1419.33	2533.65	3961.02
Crit W.S. (ft)		Area (sq ft)	1419.33	2533.65	3961.02
E.G. Slope (ft/ft)	0.000058	Flow (cfs)	343.14	5372.67	1464.20
Q Total (cfs)	7180.00	Top Width (ft)	512.72	171.50	871.63
Top Width (ft)	1555.85	Avg. Vel. (ft/s)	0.24	2.12	0.37
Vel Total (ft/s)	0.91	Hydr. Depth (ft)	2.77	14.77	4.54
Max Chl Dpth (ft)	14.88	Conv. (cfs)	45193.3	707610.1	192842.8
Conv. Total (cfs)	945646.1	Wetted Per. (ft)	512.75	189.23	872.30
Length Wtd. (ft)	1181.54	Shear (lb/sq ft)	0.01	0.05	0.02
Min Ch El (ft)	112.15	Stream Power (lb/ft s)	0.00	0.10	0.01
Alpha	4.13	Cum Volume (acre-ft)	54.67	93.69	64.13
Frcn Loss (ft)	0.10	Cum SA (acres)	21.77	8.34	17.10
C & E Loss (ft)	0.01				

File Type Options Help

River: Profile:

Reach: RS: Plan:

Plan: SCOUR Souadabscook Str Reach RS: 27966 Profile: 500 year

		Element	Inside BR US	Inside BR DS
E.G. US. (ft)	126.90	E.G. Elev (ft)	126.79	126.40
W.S. US. (ft)	126.45	W.S. Elev (ft)	125.75	125.29
Q Total (cfs)	7180.00	Crit W.S. (ft)	121.31	121.29
Q Bridge (cfs)	7180.00	Max Chl Dpth (ft)	13.65	12.49
Q Weir (cfs)		Vel Total (ft/s)	7.64	7.84
Weir Sta Lft (ft)		Flow Area (sq ft)	939.47	915.83
Weir Sta Rgt (ft)		Froude # Chl	0.44	0.46
Weir Submerg		Specif Force (cu ft)	6809.71	6535.77
Weir Max Depth (ft)		Hydr Depth (ft)	8.64	8.32
Min El Weir Flow (ft)	134.91	W.P. Total (ft)	139.61	139.62
Min El Prs (ft)	130.00	Conv. Total (cfs)	171862.7	164087.0
Delta EG (ft)	0.67	Top Width (ft)	108.79	110.12
Delta WS (ft)	1.54	Frcn Loss (ft)	0.39	0.14
BR Open Area (sq ft)	1441.68	C & E Loss (ft)	0.01	0.02
BR Open Vel (ft/s)	7.84	Shear Total (lb/sq ft)	0.73	0.78
BR Sluice Coef		Power Total (lb/ft s)	5.60	6.15
BR Sel Method	Energy only			

Pier Scour - Colorado State University (CSU) Equation**Imperial Units**

Enter Pier Description ==> East Bridge, Center Pier

Correction for Pier Nose Shape:

Enter Storm Event and Total Flow ==> Q500 - 7180 CFS

K1 = Pier Nose Shape Coefficient (HEC-18 Table 2)

Type of Pier	K1	Type
Square Nose	1.10	Type 1
Round Nose	1.00	Type 2
Circular Cylinder	1.00	Type 3
Sharp Nose	0.90	Type 4
Group of Cylinders	1.00	Type 5

Enter Type of Pier (1, 2, 3, 4 or 5) ==> 4

K1 = 0.90

Correction for Piers Skewed to Flow

Enter Pier Width (a) ==> 5.00 feet at base of wall

Design Pier Width (a) ==> 6.25 feet increase by 25%, MEDOT BDG 2.3.11.1

K2 = Coefficient Factor for Angle of Attack of the Flow (HEC-18 Table 3)

Enter Attack Angle (0, 15, 30, 45 or 90) ==> 0 Degrees

Enter (Pier Length / Pier Width) Ratio (4, 8, or 12) ==> 12

K2 = 1.00

Correction Factor for Bed Condition

K3 = Coefficient Factor for Bed Condition (HEC-18 Table 1) ==> Assume Clear-Water Scour / Antidune Flow

K3 = 1.10

Depth of Flow at Pier

y1 = Flow Depth Directly Upstream of the Pier

Enter y1 ==> 9.09 ft Reference ==> HEC-RAS

y1 = 9.09 feet

Velocity of Flow Directly Upstream of Pier

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second)

Enter V1 ==> 5.63 fps Reference ==> HEC-RAS

Ve = 5.63 ft per sec

Froude Number $Fr1 = (V1) / \{[(g)(y1)]^{0.5}\} = \text{Froude}$

V1 = Mean Velocity of Flow Directly Upstream of the Pier (feet per second) - Entered Above

g = 32.2 feet / sec²

y1 = Flow Depth Directly Upstream of the Pier - Entered Above

Fr = 0.33

CALCULATE TOTAL LOCAL PIER SCOUR $ys / y1 = (2.0)(K1)(K2)(K3)[(a / y1)^{0.65}](Fr^{0.43})$

y1 = 9.09 feet

ys / y1 = 0.96

K1 = 0.90

K2 = 1.00

K3 = 1.10

a = 6.25 feet

ys = 0.96 X 9.09

Fr = 0.33

ys = Pier Scour Depth = 8.7 feet

BRIDGE SCOUR CALCULATIONS

Project Description :	I-95 over Souadabscook Stream, West Bridge	Project Number:	18084.99
		Calculated By:	TEPA 5/1/2019
		Checked By:	

Live Bed Contraction Scour

Flood Event: 500 Years

$$\frac{y_2}{y_1} = \left(\frac{Q_2}{Q_1} \right)^{6/7} \left(\frac{W_1}{W_2} \right)^{k_1} \quad y_s = y_2 - y_o = (\text{average contraction scour depth})$$

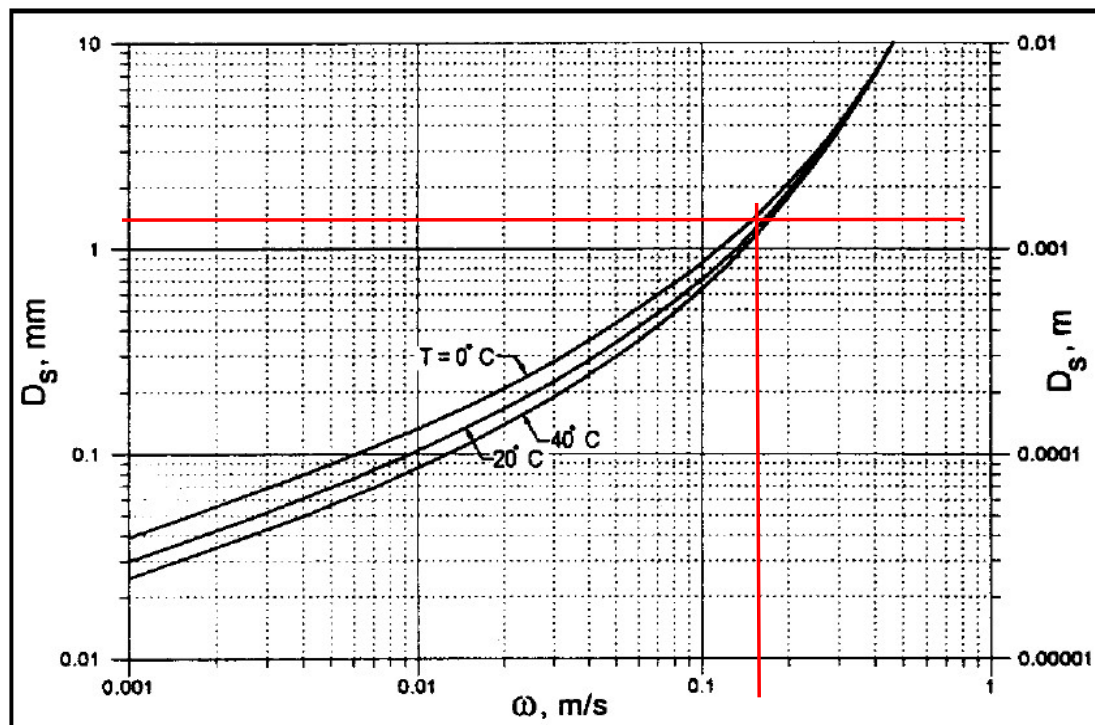
Required User Inputs:

y1 =	8.37	ft	Average depth of mainstream channel
D50 =	0.17	mm	
Q1 =	7058.15	CFS	flow in upstream channel transporting sediment
Q2 =	7180	CFS	flow in contracted channel
W1 =	126.61	ft	Top width of upstream main channel that is transporting bed material
W2 =	67.55	ft	Top width of main channel in contracted section less pier widths
y _o =	11.22	ft	Average existing depth in the contracted section.
EGL Slope =	0.001745	ft/ft	slope of energy grade line (from bridge cross section)
T =	0.0656	ft/s	fall velocity of bed material (from chart below)

Calculated Inputs:

g =	32.2	ft/s ²	constant
V* =	0.685786	ft/s ²	shear velocity in upstream section
k1 =	0.69		
y ₂ =	13.10	ft	Average equilibrium depth in the contracted section after contraction scour.

Calculated Scour Depth: 1.88 ft *Live Bed Contraction Scour*



Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	500 year		
Reach	Reach	RS:	28120.39	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 28120.39 Profile: 500 year					
E.G. Elev (ft)		Element	Left OB	Channel	Right OB
Vel Head (ft)	0.68	Wt. n-Val.	0.092	0.030	0.092
W.S. Elev (ft)	125.73	Reach Len. (ft)	45.00	45.00	45.00
Crit W.S. (ft)	122.00	Flow Area (sq ft)	79.59	1059.52	36.77
E.G. Slope (ft/ft)	0.001086	Area (sq ft)	586.20	1059.52	96.50
Q Total (cfs)	7180.00	Flow (cfs)	91.35	7058.15	30.49
Top Width (ft)	664.08	Top Width (ft)	443.36	126.61	94.11
Vel Total (ft/s)	6.11	Avg. Vel. (ft/s)	1.15	6.66	0.83
Max Chl Dpth (ft)	8.73	Hydr. Depth (ft)	3.19	8.37	2.00
Conv. Total (cfs)	217843.3	Conv. (cfs)	2771.7	214146.4	925.2
Length Wtd. (ft)	45.00	Wetted Per. (ft)	25.14	128.53	18.90
Min Ch El (ft)	117.00	Shear (lb/sq ft)	0.21	0.56	0.13
Alpha	1.17	Stream Power (lb/ft s)	0.25	3.72	0.11
Frctn Loss (ft)		Cum Volume (acre-ft)	4.45	22.65	0.65
C & E Loss (ft)		Cum SA (acres)	3.52	3.35	0.85

Cross Section Output					
File Type Options Help					
River:	Souadabscook Str	Profile:	500 year		
Reach	Reach	RS:	27966 BR U	Plan:	SCOUR
Plan: SCOUR Souadabscook Str Reach RS: 27966 BR U Profile: 500 year					
E.G. Elev (ft)		Element	Left OB	Channel	Right OB
Vel Head (ft)	1.04	Wt. n-Val.	0.092	0.030	0.037
W.S. Elev (ft)	125.75	Reach Len. (ft)	212.00	212.00	212.00
Crit W.S. (ft)	121.31	Flow Area (sq ft)	51.53	814.23	73.71
E.G. Slope (ft/ft)	0.001745	Area (sq ft)	51.53	814.23	73.71
Q Total (cfs)	7180.00	Flow (cfs)	70.20	6806.45	303.35
Top Width (ft)	108.79	Top Width (ft)	16.23	72.55	20.01
Vel Total (ft/s)	7.64	Avg. Vel. (ft/s)	1.36	8.36	4.12
Max Chl Dpth (ft)	13.65	Hydr. Depth (ft)	3.17	11.22	3.68
Conv. Total (cfs)	171862.7	Conv. (cfs)	1680.3	162921.2	7261.2
Length Wtd. (ft)	212.00	Wetted Per. (ft)	17.96	100.28	21.37
Min Ch El (ft)	112.10	Shear (lb/sq ft)	0.31	0.88	0.38
Alpha	1.15	Stream Power (lb/ft s)	0.43	7.40	1.55
Frctn Loss (ft)	0.39	Cum Volume (acre-ft)	4.34	23.01	0.92
C & E Loss (ft)	0.01	Cum SA (acres)	3.34	3.25	0.85

TABLE I**Summary of D₅₀ Laboratory Results**

Interstate 95 over Souadabscook Stream West

Bridge Nos. 5951 and 1433

Hampden, Maine

MaineDOT WIN 21730.00 and 21730.10

Boring Location	Boring No.	Sample No.	Depth	D ₅₀ (mm)	Deposit
West Abutment	BB-HSS-101	4D	6.5 - 8.5	1.0239	Fill
	BB-HSS-102	3D	4.5 - 6.5	0.2441	Fill
Pier(s)	BB-HSS-103	3D	12.0 - 14.0	< #200 SIEVE	Marine Clay
	BB-HSS-104	2D	3.4-3.9	3.2307	Alluvial Deposit
East Abutment	BB-HSS-105	12D	30.0 - 32.0	< #200 SIEVE	Marine Silt
	BB-HSS-106	10D	35.0 - 37.0	0.1211	Marine Sand

TABLE II**Summary of D₅₀ Laboratory Results**

Interstate 95 over Souadabscook Stream Center

Bridge Nos. 5950 and 1432

Hampden, Maine

MaineDOT WIN 21728.00 and WIN 21728.10

Boring Location	Boring No.	Sample No.	Depth	D ₅₀ (mm)	Deposit
West Abutment	BB-HSS-107	10D	18.5 - 20.5	2.3752	Fill
	BB-HSS-108	3D	5.0 - 7.0	3.3617	Fill
Pier(s)	BB-HSS-109	1D	0.0 - 1.5	7.3178	Alluvial Deposit
	BB-HSS-110	1D	0.0 - 2.0	6.3242	Alluvial Deposit
East Abutment	BB-HSS-111	4D	8.0 - 10.0	0.4250	Fill
	BB-HSS-112	8D	15.5 - 17.5	2.1187	Fill

TABLE III**Summary of D₅₀ Laboratory Results**

Interstate 95 over Souadabscook Stream East

Bridge Nos. 5949 and 1431

Hampden, Maine

MaineDOT WIN 21729.00 and WIN 21729.10

Boring Location	Boring No.	Sample No.	Depth	D ₅₀ (mm)	Deposit
West Abutment	BB-HSS-113	6DA	10.5 - 12.3	< #200 SIEVE	Fill
	BB-HSS-114	6D	11.0 - 12.5	1.6168	Fill
Pier(s)	BB-HSS-115	2DA	4.5 - 6.2	0.1677	Alluvial Deposit
East Abutment	BB-HSS-117	8D	16.0 - 18.0	0.6794	Fill
	BB-HSS-118	2D	5.0 - 7.0	0.5274	Fill
	BB-HSS-118	7D	15.0 - 17.0	1.7018	Alluvial Deposit

Riprap Design Calculations

Project Description: I-95 over Souadabscook Stream, West Bridge

Project Number: 18084.99

Calcs By: TEPA 5/3/2019

Check By:

Purpose: To calculate the required riprap size for the design flow event.

References: HEC 23, Vol II, DG 14.

If $Fr > 0.8$, this sheet uses Eq. 14.2, otherwise this sheet uses Eq 14.1

Note: The set-back ratio is $\ll 5$. Use the average velocity based on the entire contracted area through the bridge.

Constants

$S_s =$	2.65 assumed Riprap specific gravity
$g =$	32.2 ft/s
Is it a vertical wall abutment? =	Y (Y or N)
$K =$	1.02 for $Fr \leq 0.8$
$K =$	0.69 for $Fr > 0.8$

Hydraulic Data from HEC-RAS

<u>Upstream:</u>	Storm Event	Q100
	Channel Velocity =	5.14 fps
	Channel Depth =	9.23 ft
	Froude # =	0.3

$$\frac{D_{50}}{y} = \frac{K}{(S_s - 1)} \left[\frac{V^2}{gy} \right]$$

Eq 14.1, HEC 23 Vol II

<u>Downstream:</u>	Storm Event	Q100
	Channel Velocity =	5.06 fps
	Channel Depth =	9.11 ft
	Froude # =	0.31

$$\frac{D_{50}}{y} = \frac{K}{(S_s - 1)} \left[\frac{V^2}{gy} \right]^{0.14}$$

Eq 14.2, HEC 23 Vol II

Output

Upstream $d_{50} =$	0.51 ft
Downstream $d_{50} =$	0.49 ft
Average $d_{50} =$	5.99 in

Plan: SCOUR Souadabscook Str Reach RS: 40346 Profile: 100 year				
Element	Inside BR US	Inside BR DS		
E.G. US. (ft)	127.62		E.G. Elev (ft)	127.54
W.S. US. (ft)	127.29		W.S. Elev (ft)	127.05
Q Total (cfs)	5680.00		Crit W.S. (ft)	121.09
Q Bridge (cfs)	5680.00		Max Chl Dpth (ft)	15.08
Q Weir (cfs)			Vel Total (ft/s)	5.14
Weir Sta Lft (ft)			Flow Area (sq ft)	1105.75
Weir Sta Rgt (ft)			Froude # Chl	0.30
Weir Submerg			Specif Force (cu ft)	6922.23
Weir Max Depth (ft)			Hydr Depth (ft)	9.23
Min El Weir Flow (ft)	134.81		W.P. Total (ft)	155.09
Min El Prs (ft)	130.00		Conv. Total (cfs)	202270.7
Delta EG (ft)	0.34		Top Width (ft)	119.82
Delta WS (ft)	0.38		Frctn Loss (ft)	0.14
BR Open Area (sq ft)	1467.71		C & E Loss (ft)	0.00
BR Open Vel (ft/s)	5.14		Shear Total (lb/sq ft)	0.35
BR Sluice Coef			Power Total (lb/ft s)	1.80
BR Sel Method	Energy only			

Riprap Design Calculations

Project Description: I-95 over Souadabscook Stream, Center Bridge

Project Number: 18084.99

Calcs By: TEPA 5/3/2019

Check By:

Purpose: To calculate the required riprap size for the design flow event.

References: HEC 23, Vol II, DG 14.

If $Fr > 0.8$, sheet uses Eq. 14.2, otherwise the sheet uses Eq 14.1

Note: The set-back ratio is $\ll 5$. Use the average velocity based on the entire contracted area through the bridge.

Constants

$S_s =$	2.65 assumed Riprap specific gravity
$g =$	32.2 ft/s
Is it a vertical wall abutment? =	Y (Y or N)
$K =$	1.02 for $Fr \leq 0.8$
$K =$	0.69 for $Fr > 0.8$

Hydraulic Data from HEC-RAS

<u>Upstream:</u>	Storm Event	Q100
	Channel Velocity =	5.64 fps
	Channel Depth =	9.02 ft
	Froude # =	0.32

$$\frac{D_{50}}{y} = \frac{K}{(S_s - 1)} \left[\frac{V^2}{gy} \right]$$

Eq 14.1, HEC 23 Vol II

<u>Downstream:</u>	Storm Event	Q100
	Channel Velocity =	5.88 fps
	Channel Depth =	8.69 ft
	Froude # =	0.34

$$\frac{D_{50}}{y} = \frac{K}{(S_s - 1)} \left[\frac{V^2}{gy} \right]^{0.14}$$

Eq 14.2, HEC 23 Vol II

Output

Upstream $d_{50} =$	0.61 ft
Downstream $d_{50} =$	0.66 ft
Average $d_{50} =$	7.65 in

Plan: SCOUR Souadabscook Str Reach RS: 35151 Profile: 100 year				
Element	Inside BR US	Inside BR DS		
E.G. US. (ft)	126.87		E.G. Elev (ft)	126.73
W.S. US. (ft)	126.69		W.S. Elev (ft)	126.17
Q Total (cfs)	5680.00		Crit W.S. (ft)	120.39
Q Bridge (cfs)	5680.00		Max Chl Dpth (ft)	13.06
Q Weir (cfs)			Vel Total (ft/s)	5.64
Weir Sta Lft (ft)			Flow Area (sq ft)	1006.58
Weir Sta Rgt (ft)			Froude # Chl	0.32
Weir Submerg			Specif Force (cu ft)	6476.63
Weir Max Depth (ft)			Hydr Depth (ft)	9.02
Min El Weir Flow (ft)	134.91		W.P. Total (ft)	142.33
Min El Prs (ft)	130.00		Conv. Total (cfs)	183915.1
Delta EG (ft)	0.57		Top Width (ft)	111.61
Delta WS (ft)	0.68		Frctn Loss (ft)	0.20
BR Open Area (sq ft)	1457.75		C & E Loss (ft)	0.02
BR Open Vel (ft/s)	5.88		Shear Total (lb/sq ft)	0.42
BR Sluice Coef			Power Total (lb/ft s)	2.38
BR Sel Method	Energy only			