



REPORT

Preliminary Geotechnical Data Report REV01

*Interstate 95 Bridges 1427 and 5800 over Stillwater Avenue, Bangor, Maine
(WIN 027176.00)*

Submitted to:

Maine Department of Transportation

Submitted by:

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WIN 027176.00 / WSP US0025840.3905

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1.0 INTRODUCTION

This Preliminary Geotechnical Data Report (PGDR) summarizes the results of the geotechnical subsurface investigation and laboratory testing program of site soils and rock that WSP USA Inc. (WSP) performed to support the replacement of Bridge No. 1427 & No. 5800 that carries Interstate 95 (I-95) over Stillwater Avenue in Bangor, Maine. Figure 1 shows the site location.

2.0 PROJECT UNDERSTANDING

WSP reviewed the historical drawings¹ for the two existing I-95 bridges over Stillwater Avenue including historical boring logs provided by MaineDOT. The existing structures were constructed in 1960 and consist of two (2) three-span bridges with two (2) piers and two (2) abutments each.

3.0 GEOLOGIC SETTING

Available site geology information, consisting of surficial² geologic maps of the area indicate subsurface conditions consist of road embankment fills overlying Pleistocene Presumpscot Formation glaciomarine deposits generally consisting predominantly of silt and fine sand.

Available site geology information, consisting of bedrock³ geologic maps of the area indicate bedrock in the region is mapped as the Medium bedded facies of the Penobscot River Member of the Silurian-aged Bangor Formation of the Vassalboro Group, consisting of medium to dark gray, fine-grained to very fine-grained, metawacke; a metamorphosed impure, poorly sorted sandstone with appreciable clay minerals. The 1958 historical Kenduskeag Avenue boring logs¹ characterize bedrock as phyllite (a general term for metamorphosed clay-rich rocks).

4.0 SUBSURFACE INVESTIGATIONS

4.1 Geotechnical Borings

WSP completed six (6) borings (BB-BSA-102, BB-BSA-103, BB-BSA-108, BB-BSA-109, BB-BSA-109A, and BB-BSA-110) within the paved roadway of Stillwater Avenue beyond the extents of the existing bridges in May 2024 and seven (7) borings (BB-BSA-101, BB-BSA-104, BB-BSA-104A, BB-BSA-105, BB-BSA-106, BB-BSA-107, and BB-BSA-111) within the paved roadway of I-95 beyond the existing bridge abutments in July 2024. The as-drilled boring locations and elevations are summarized in Table 1 and boring locations with respect to existing site features are illustrated in the Boring Location Plan in Figure 2.

The field program included Standard Penetration Testing (SPT) of predominantly coarse-grained soils and recovery of rock core from the bedrock. A WSP geotechnical engineer monitored drilling activities, selected sampling intervals, logged subsurface conditions encountered, and obtained soil samples for use in visual descriptions and subsequent laboratory testing and classification.

WSP subcontracted Seaboard Drilling, LLC (Seaboard) of Bangor, Maine, who completed the borings using a Diedrich D-50 drill rig for all borings. Borings were advanced using solid stem augers (SSA) followed by 4-inch or

¹ Maine State Highway Commission, 1960 Final As Built Plans, Project No. I-95-8(6)180, Interstate #95 over Stillwater Ave. in the City of Bangor, Penobscot County, Plans and Profiles, 41 sheets, Received from HNTB, Filename: 1427 & 5800 Bangor 1958 As-Built.pdf.

² Syverson, K.M., Thompson, A.M., and Johnston, R.A., (2011). Surficial Geology, Bangor Quadrangle, Maine. Open-File No. 11-6, Maine Geological Survey, 1 sheet, scale 1:24,000.

³ Pollock, S.G., Johnston, R.A., (2011). Bedrock Geology of the Bangor Quadrangle, Maine, Open-File No. 11-57, Maine Geological Survey, 1 sheet, scale 1:240,000.

3-inch casing and drive and wash methods to refusal; rock coring was performed in either 4-inch or 3-inch casing seated in rock, depending on the drilling conditions.

SPT was performed using a calibrated automatic hammer system and standard 2-inch split spoon sampler in general accordance with American Society for Testing and Materials (ASTM) D1586. Sampling was conducted at approximately 5-foot intervals, where split spoons were advanced 24 inches with a 140-pound hammer dropped 30 inches. WSP recorded the number of hammer blows required to advance the sampler through each 6-inch increment. Measured, uncorrected N-values, calculated as the sum of the hammer blows to advance the sampler during the 6-inch to 18-inch intervals. Seaboard provided WSP with a copy of the automatic hammer calibration report from November 2023⁴ for both drill rigs used. WSP used a calibrated hammer energy transfer ratio of 106.6% for the May borings and 108.7% for the July borings provided by in the report convert the measured N-values to N_{60} values. Uncorrected N-values and N_{60} are shown on the boring logs (Appendix A). WSP collected and stored soil samples in sealed glass jars for later evaluation and laboratory testing.

Up to 10 feet of rock core was collected in each boring using NX size (1-7/8-inch diameter) diamond tipped core barrels following either refusal of casing or failure to advance the split spoon sampler or roller bit. Rock core samples were placed in wooden boxes and transported to the WSP office. WSP recorded the lithology, Total Core Recovery (TCR), Rock Quality Designation (RQD), and coring rates for each core run which are provided in the boring logs in Appendix A. Photographs of all collected rock core are presented in Appendix B.

The boring logs provided in Appendix A present details of the sampling methods used, field data obtained, and soil and rock conditions encountered during the investigation. A description of the boring log symbols and terms used for the soil and rock descriptions precedes the boring logs. A WSP geotechnical engineer monitored drilling activities, selected sampling intervals, logged subsurface conditions encountered, and obtained soil samples for use in visual descriptions and subsequent laboratory testing and classification WSP field characterized the soils in accordance with ASTM D2488. WSP field characterized the bedrock lithology.

4.2 Geologic Evaluation of Exposed Rock Cuts

On April 23, 2024, WSP visited the Stillwater Avenue site to collect geological data from the exposed rock cuts along Stillwater Avenue beneath the I-95 existing bridge foundations. The general locations of the exposed rock cuts are shown in plan view in Appendix D. During the site visit, WSP measured 37 geologic discontinuities and photographed existing rock cut conditions. Photographs of the existing rock cut conditions and discontinuities evaluated are presented in Appendix E. Our discontinuity measurements and observations are summarized in Table 2 (attached) and include discontinuity type, orientation, persistence, aperture, infilling materials, estimated strength, surface roughness, shape, spacing, and groundwater conditions. Our measured discontinuity orientations are plotted in Appendix D.1.

5.0 LABORATORY TESTING PROGRAM

After reviewing the collected samples in the office, WSP transferred select samples to GeoTesting Express (GTX) of Acton, Massachusetts for geotechnical laboratory testing in accordance with applicable AASHTO and ASTM testing procedures. The types and numbers of each of the laboratory tests conducted on soil samples and rock

⁴ GRL Engineers, Inc., SPT Energy Calibration on November 2, 2023, Submitted to Eric Baron of S.W. Cole Explorations, LLC (now known as Seaboard Drilling LLC) on November 10, 2023.

core are presented in Table 5-1. Soil testing results are included on the boring logs in Appendix A. Complete soil and rock laboratory testing results are provided in Appendix C.

Table 5-1: Number and Type of Laboratory Tests Performed

Laboratory Test	Test Standard	No. Tests Completed
Moisture content	AASHTO T267, ASTM D2216	18
Grain size analysis (coarse)	AASHTO T88, ASTM D6913	37
Grain size (fine)	AASHTO T88, ASTM D7928	12
Atterberg limits	AASHTO T89 / T90, ASTM D4318	11
Chlorides	AASHTO T291, ASTM D512	2
pH	AASHTO T289, ASTM D4972	2
Sulfates	AASHTO T290	2
Electric Resistivity	ASTM G57	1
Elastic Moduli of Rock in Uniaxial Compression - Rock	ASTM D7012 Method D	6

6.0 SUBSURFACE CONDITIONS

The boring logs in Appendix A provide detailed descriptions of the soil, bedrock, and measured groundwater conditions encountered in the borings.

Soils: The soils encountered in the borings generally consist of fill materials placed during construction of the bridge and roadway and naturally occurring sand deposits, clay deposits, sand and gravel interpreted as glacial till. Table 6-1 summarizes the major stratigraphic units, the range of thicknesses, and generalized material descriptions for soils encountered.

Table 6-1: Summary of Subsurface Fill and Soil Encountered

Stratigraphic Unit	Approximate Range in Encountered Thickness (feet)	Generalized Description
Asphalt	0.5 to 0.8	Asphalt pavement approximately 5-inch to 10-inch thick (<i>Encountered in all borings</i>)
Fill	2.6 to 20	The fill consists of olive brown to brown or grey to brown, dry to moist, medium dense to very dense, hard, fine to coarse Sand or SILT, with trace to little fine to coarse gravel, and non-plastic to slightly plastic. USCS: SM, ML, GM. AASHTO: A-1-b (0), A-4 (0), A-2-4 (0) (<i>Encountered in all borings</i>)
Sand, Silt, Gravel	1.3 to 22	Olive to brown to grey, moist to wet, medium dense to very dense, very stiff to hard, fine to coarse SAND or SILT with varying amounts of fine to coarse GRAVEL, and non-plastic to slightly

Stratigraphic Unit	Approximate Range in Encountered Thickness (feet)	Generalized Description
		plastic. USCS: SM, ML, GM, SC. AASHTO: A-2-4 (0), A-4 (0) (Encountered in BB-BSA-101, -102, -105, -106, -107, -108, and -109)
Clay	3 to 14.5	Grey with brown and olive, wet, very soft to hard, CLAY, trace to little fine sand, trace gravel, medium plasticity with interbedded silt or sand lenses. USCS: CL. AASHTO: A-6 (9, 10, 11, 15, 18, 19, 37) (Encountered in BB-BSA-104, -106, -107, and -111))
Glacial Till	3 to 10.3	Grey with brown to olive, wet, very dense to hard, fine to coarse SAND and fine to coarse GRAVEL, with varying amounts of silt and gravel, non-plastic, and weathered rock fragments. USCS: SM, GM, ML. AASHTO: A-1-b (0), A-4 (0) (Encountered in BB-BSA-104, -106, -107, and -111))

Notes: USCS classification from laboratory testing in accordance with ASTM D2487. AASHTO classification from laboratory testing and includes Group Classification and Group Index in parentheses in accordance with AASHTO M145.

Bedrock: Bedrock was cored for each boring location. Bedrock cores for BB-BSA-104 and BB-BSA-109 were taken at the offset borings BB-BSA-104A and BB-BSA-109A respectively. For the borings performed from Stillwater Avenue, top of bedrock surface ranged from 3.5 feet bgs (EL. 123.5 feet NAVD88) to 12.2 feet bgs (EL. 121.3 feet NAVD88). For the borings performed from I-95, top of bedrock ranged from 17.8 feet bgs (130.5 feet NAVD88) to 63.8 feet bgs (EL. 79.8 feet NAVD88). The bedrock was described as grey, very fine to fine grained, very thinly to thinly bedded, Metawacke [metasandstone] with calcite veins, medium strong to very strong, slightly to moderately weathered.

Rock quality designation (RQD) is a common parameter that is used to help assess the competency of sampled bedrock. RQD is defined as the sum of pieces of recovered bedrock greater than 4 inches in length divided by the total length of the core run. RQD values for bedrock encountered at the site ranges between 0 and 88 percent, which generally correlates to Rock Mass Quality ratings of very poor to good.

Groundwater: Groundwater levels were measured in all borings except BB-BSA-104, BB-BSA-104A, and BB-BSA-109. Groundwater was measured before the casing was withdrawn and at the end of the drilling day. Groundwater elevations vary from approximately EL. 123.1 feet to EL. 135.1 feet (NAVD88), ground water levels encountered at the time of drilling may have been influenced by the drilling methods used. Groundwater levels will fluctuate due to soil conditions and topography and seasonal variations in precipitation. Groundwater levels encountered during construction may differ from those recorded from the borings.

7.0 CONDITIONS OF EXPOSED ROCK CUTS

Rock Mass Rating (RMR) and Geological Strength Index (GSI) values were calculated for the existing rock cut exposures along Stillwater Avenue and for the rock core collected in each boring for comparison. The RMR system⁵ assigns numerical ratings to six parameters, including strength of the intact rock, RQD, discontinuity spacing, discontinuity surface conditions, groundwater conditions, and orientation of discontinuities. These ratings are summed to provide the RMR value. The GSI system⁶ assigns a numerical rating to qualitative estimates of the lithology, discontinuity structure, and discontinuity surface conditions in a rock mass.

To determine the RMR, WSP used the discontinuities described in each rock cut exposure or core run and the RQD measured in each core run to assign ratings. We used the discontinuity orientations measured in the rock cuts to assign rating adjustments for the discontinuity sets that we identified as having unfavorable orientations relative to the existing foundation orientation (i.e., kinematically susceptible to sliding or toppling failure). The proposed foundation orientation may allow for a different rating adjustment for discontinuity orientation, and thus a modification to the RMR value. Our calculated RMR values are summarized in Table 2 (attached) for the measured rock cut exposures and Table 3 (attached) for the boring rock core runs. Full RMR calculations including the individual parameter ratings are provided in Appendix D.2. Photographs of the rock cuts evaluated are presented in Appendix E. Based on our field observations and measurements at the Stillwater Avenue bridge site, we estimate that:

- RMR values range from 40 to 79 and average 63 for the exposed rock cuts from 37 discontinuities evaluated.
- RMR values range from 26 to 72 and average 44 for the rock core runs from 30 runs.

To determine the GSI, WSP used the discontinuity structure observed in the existing rock cuts and the discontinuity surface conditions described in the rock cuts and core runs to assign a rating. We selected the GSI value from the range established by Marinos and Hoek⁶ for typical sandstone lithologies. The GSI chart is presented in Appendix D.3. Based on our field observations and measurements, we estimate a GSI value of 55 for the exposed rock cuts at the Stillwater Avenue bridge site.

8.0 REPORT AND EXPLORATION LIMITATIONS

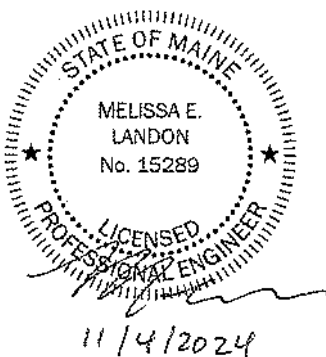
This Preliminary Geotechnical Data Report (PGDR) was prepared for the replacement of I-95 Bridge No. 1427 & Bridge No. 5800 over Stillwater Ave in Bangor, Maine. The professional services provided by WSP for this project include only the geotechnical aspects of the subsurface conditions at this site. The presence or implications of possible surface and/or subsurface contamination resulting from previous activities or uses of the site and/or resulting from the introduction onto the site of materials from off-site sources are outside the terms of reference for this report and have not been investigated or addressed.

⁵ Bieniawski, Z.T. 1989. Engineering Rock Mass Classifications: A Complete Manual for Engineers and Geologists in Mining, Civil, and Petroleum Engineering. John Wiley & Sons.

⁶ Marinos, Paul and Hoek, Evert. November 2000. GSI: a geologically friendly tool for rock mass strength estimation. ISRM International Symposium, Melbourne, Australia, paper number ISRM-IS-2000-035,

Signature Page

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TABLES

Table 1: Summary of Subsurface Explorations
Geotechnical Data Report
MaineDOT I-95 Bridge Over Stillwater Avenue, Bangor, Maine
MaineDOT WIN 027176.00

	As-Drilled Locations ⁴				Approximate Strata Thickness (feet)						Approximate	Approximate	Approximate	Approximate
	Test Boring No. ^{1,2,3}	Northing	Easting	Ground Surface Elevation ⁴ (feet NAVD88)	Asphalt	Fill	Sand, Silt, Gravel ⁶	Clay	Glacial Till	Weathered Bedrock	Top of Bedrock Depth (feet bgs ⁵)	Elevation of Top of Bedrock (feet NAVD88)	Bottom of Exploration Depth (ft) (feet bgs ⁵)	Elevation of Bottom of Exploration (feet NAVD88)
South bound Bridge #1427	BB-BSA-101	482856.27	1735264.27	150.5	0.6	12.9	15.0	NE ⁵	3.0	NE ⁵	31.5	119.0	41.5	109.0
	BB-BSA-102	482969.08	1735451.57	133.5	0.6	4.4	7.2	NE ⁵	NE ⁵	NE ⁵	12.2	121.3	22.2	111.3
	BB-BSA-103	482888.01	1735425.94	132.1	0.6	2.5	NE ⁵	NE ⁵	NE ⁵	4.1	7.2	124.9	17.2	114.9
	BB-BSA-104	483018.96	1735602.84	151.9	0.8	14.7	NE ⁵	3.0	4.5	NE ⁵	23.0	128.9	23.5	128.4
	BB-BSA-104A	483017.59	1735600.99	152.0	0.7	NE ⁵	NE ⁵	NE ⁵	NE ⁵	NE ⁵	20.4	131.6	31.0	121.0
	BB-BSA-105	482984.90	1735593.56	152.1	0.8	12.3	11.9	NE ⁵	NE ⁵	1.4	26.4	125.7	36.2	115.9
North bound Bridge #5800	BB-BSA-106	482611.20	1735095.82	143.6	0.8	18.2	22.0	12.5	10.3	NE ⁵	63.8	79.8	74.1	69.5
	BB-BSA-107	482578.95	1735092.78	143.1	0.5	20.0	18.5	14.5	9.9	NE ⁵	63.4	79.7	77.2	65.9
	BB-BSA-108	482749.52	1735322.13	129.5	0.6	2.6	3.5	NE ⁵	NE ⁵	NE ⁵	6.7	122.8	16.7	112.8
	BB-BSA-109	482636.37	1735255.48	127.0	0.7	8	1.3	NE ⁵	NE ⁵	0.1	NE ⁵	NE ⁵	10.1	116.9
	BB-BSA-109A	482637.93	1735257.73	127.0	NE ⁵	NE ⁵	NE ⁵	NE ⁵	NE ⁵	NE ⁵	3.5	123.5	14.0	113.0
	BB-BSA-110	482660.73	1735292.34	127.5	0.6	4.7	NE ⁵	NE ⁵	NE ⁵	NE ⁵	5.3	122.2	15.3	112.2
	BB-BSA-111	482728.68	1735418.07	148.3	0.6	8.9	NE ⁵	4.0	4.3	NE ⁶	17.8	130.5	29.0	119.3

Notes:

- Boring locations are shown in Figure 2 - Boring Location Plan of the Preliminary Geotechnical Data Report.
- Borings BB-BSA-102, BB-BSA-103, BB-BSA-108, BB-BSA-109, BB-BSA-109A, and BB-BSA-110 were performed by Seaboard Drilling, LLC in May, 2024. Borings BB-BSA-101, BB-BSA-104, BB-BSA-104A, BB-BSA-105, BB-BSA-106, BB-BSA-107, and BB-BSA-111 were performed by Seaboard Drilling, LLC in July, 2024.
- Boring logs are presented in Appendix A of the Preliminary Geotechnical Data Report.
- As drilled Boring Locations Derived from the Electronic file "Ground.dgn" Provided to WSP by HNTB on August 12, 2024.
- bgs = below ground surface, NE = not encountered
- This layer mainly consists of silty Sand or sandy Silt, but includes Gravel with some sand in borings BB-BSA-102 and BB-BSA-108 strata layers.

Prepared By: RJN

Checked By: LMP

Reviewed By: MEL

Table 2: Summary of Rock Cut Discontinuities
Preliminary Geotechnical Design Report
Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine
MaineDOT WIN 027176.00

Outcrop Area	Discontinuity		Dip [degrees]	Uncorrected Dip Direction State Plane Grid North [degrees]	Corrected Dip Direction State Plane Grid North ⁽¹⁾ [degrees]	Set ⁽²⁾	Persistence [ft]	Aperture [in]	Infilling	Infilling Shear Strength ⁽³⁾	Surface Roughness	Discontinuity Shape	Water	Discontinuity Spacing [ft]	Notes/Comments ⁽⁴⁾	RMR
	ID	Type														
Stillwater Ave Northbound	1	bedding	32	348	333	5	10	0.13	none	-	rough	undulating to stepped	dry	0.2	Quartz veins 0.25" thick in vicinity	40
	2	joint	84	229	214	3	15	0.25	lichen	low	slightly rough	planar	dry	1.5		64
	3	joint	88	245	230	3	3	0.50	none	-	slightly rough	planar	dry	2.8		78
	4	joint	85	265	250	2	8	0.25	lichen	low	smooth	planar	dry	0.9		46
	5	joint	11	243	228	1	5	0.13	none	-	smooth	undulating	dry	5.9		78
	6	joint	83	186	171	4	10	0.06	none	-	slightly rough	planar	dry	1.6		72
	7	bedding	25	335	320	5	10	tight	none	-	rough	stepped	dry	0.3		49
	8	joint	8	100	85	1	3	0.50	sandy soil	medium	smooth	planar	dry	5.9		73
	9	joint	75	50	35	3	15	0.06	none	-	slightly rough	planar	dry	1.1		58
	10	joint	10	58	43	1	20	0.75	quartz	high	slightly rough	planar	dry	1.0		52
	11	joint	64	4	349	-	4	0.75	quartz	high	rough	irregular	dry	3.7		64
	12	joint	83	41	26	3	12	0.06	none	-	slightly rough	planar	dry	4.5		66
	13	joint	65	278	263	2	6	0.13	none	-	slightly rough	stepped	dry	5.4		54
	14	joint	4	48	33	1	10	0.50	quartz	high	slightly rough	undulating	dry	0.9		63
	15	joint	83	133	118	2	5	tight	none	-	smooth	planar	dry	5.1		68
	16	joint	8	124	109	1	10	0.38	broken rock	high	rough	undulating	dry	1.3		67
	17	joint	89	357	342	4	15	0.06	roots	low	slightly rough	undulating	dry	2.5		71
	18	joint	67	213	198	-	15	tight	none	-	smooth	undulating	dry	2.5		78
	19	joint	87	20	5	4	15	0.06	none	-	rough	stepped	dry	1.8		71
	20	joint	88	124	109	2	15	0.25	topsoil	low	slightly rough	planar	dry	1.7		47
	21	bedding	21	26	11	5	6	0.06	none	-	smooth	stepped	dry	0.4		42
	22	joint	80	278	263	2	10	0.13	none	-	slightly rough	planar	dry	1.8	Shotcrete and dowel repair 2 ft north	54
	23	joint	10	111	96	1	22.5	0.25	quartz	high	smooth	planar	dry	2.0		64
	24	joint	18	65	50	1	20	tight	none	-	slightly rough	undulating	dry	1.4		72
	25	joint	85	190	175	4	15	tight	none	-	slightly rough	planar	dry	2.3	Blast fragmentation to south	79
	26	joint	59	212	197	-	15	1.50	quartz	high	smooth	planar	dry	2.2		67
	27	joint	31	106	91	1	10	0.50	roots, topsoil	low	smooth	planar	dry	4.0		68
	28	joint	25	5	350	5	10	0.50	quartz, broken rock	high	rough	undulating	dry	1.8		69
	29	joint	81	10	355	4	10	0.13	broken rock	high	rough	planar	dry	2.2		74
	30	joint	10	220	205	1	24.8	0.50	broken rock	high	slightly rough	planar	dry	1.6		67
	31	joint	84	55	40	3	4.5	0.50	roots, sandy soil	low	slightly rough	planar	dry	2.3		69

Table 2: **Summary of Rock Cut Discontinuities**
 Preliminary Geotechnical Design Report
 Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine
 MaineDOT WIN 027176.00

Outcrop Area	Discontinuity		Dip [degrees]	Uncorrected Dip Direction State Plane Grid North [degrees]	Corrected Dip Direction State Plane Grid North ⁽¹⁾ [degrees]	Set ⁽²⁾	Persistence [ft]	Aperture [in]	Infilling	Infilling Shear Strength ⁽³⁾	Surface Roughness	Discontinuity Shape	Water	Discontinuity Spacing [ft]	Notes/Comments ⁽⁴⁾	RMR
	ID	Type														
Stillwater Ave Southbound	32	joint	76	329	314	-	3.9	0.25	sandy soil	medium	very rough	undulating	dry	0.9		66
	33	joint	72	183	168	4	3.5	0.13	sandy soil	medium	rough	planar to stepped	dry	0.2		53
	34	joint	66	278	263	2	-	0.13	sandy soil	medium	very rough	planar	dry	0.3		40
	35	joint	17	62	47	1	9.7	0.50	none	-	rough	undulating	dry	2.0		74
	36	joint	88	219	204	3	2.9	0.13	sandy soil	medium	smooth	planar	dry	0.6		60
	37	joint	89	262	247	2	3.4	0.25	none	-	smooth	stepped	dry	0.4		41

(1) Dip direction data corrected for magnetic declination (15 degrees west).

(2) See Appendix E for stereonets.

(3) Shear strength of infilling materials as follows:
 Low = friction angle < 20 degrees
 Medium = 20 degrees < friction angle < 30 degrees
 High = 30 degrees < friction angle

(4) Discontinuity measurements were collected on April 23, 2024.

Prepared by: KAR
Checked by: BK
Reviewed by: JDL

Table 3: Summary of Rock Core Quality
Preliminary Geotechnical Design Report
Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine
MaineDOT WIN 027176.00

Test Boring Designation	Core Size	Run						TCR ¹		RQD ²		Physical Rock Parameters			Lithologic, Rock Mass and Discontinuity Description ^{5,6}	
		No.	Midpoint Depth Below Bedrock Surface (ft)	Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering ³	Estimated Field Strength ³		Rock Mass Rating [RMR] ⁴
				Start	End	Midpoint										
BB-BSA-101	NX (1.88)	R1	0.4	31.5	32.4	32.0	0.9	0.8	89%	0.00	0%	Very Poor	Slightly Weathered (W2)	Very Strong (R5)	31	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, very strong, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, smooth to very rough, tight to open, highly fractured, clay infilling at bottom of run [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	1.2	32.4	32.9	32.7	0.5	0.5	100%	0.00	0%	Very Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	30	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], clay and sand infilling at the top of run, strong to very strong, slightly weathered; discontinuities low angle to steep dipping, very close spacing, rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	3.2	32.9	36.5	34.7	3.6	3.6	100%	0.50	14%	Very Poor	Slightly Weathered (W2) to Fresh (W1)	Strong (R4) to Very Strong (R5)	39	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered to fresh; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R4	7.5	36.5	41.5	39.0	5.0	5.0	100%	3.00	60%	Fair	Fresh (W1)	Strong (R4)	56	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong, fresh; discontinuities low angle to steep dipping, very close spacing, rough to very rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-102	NX (1.88)	R1	2.5	12.2	17.2	14.7	5.0	4.5	90%	2.58	52%	Fair	Slightly Weathered (W2)	Strong (R4) to Extremely Strong (R6)	40	Grey, very fine to fine grained, thinly to thickly laminated, METAWACKE [metasandstone], frequent thin to thick calcite veins, strong to extremely strong, slightly weathered; discontinuities moderately to steeply dipping, close to moderately close spacing, irregular to planar, smooth to very rough, open; average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.5	17.2	22.2	19.7	5.0	4.9	98%	4.38	88%	Good	Fresh (W1)	Extremely Strong (R6)	72	Grey, very fine to fine grained, thinly laminated, METAWACKE [metasandstone], frequent calcite veins, extremely strong, fresh; discontinuities horizontal dipping, close to wide spacing, irregular to planar, smooth to very rough, open; average 0.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

Table 3: Summary of Rock Core Quality
Preliminary Geotechnical Design Report
Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine
MaineDOT WIN 027176.00

Test Boring Designation	Core Size	Run						TCR ¹		RQD ²		Physical Rock Parameters				Lithologic, Rock Mass and Discontinuity Description ^{5,6}
		No.	Midpoint Depth Below Bedrock Surface (ft)	Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering ³	Estimated Field Strength ³	Rock Mass Rating [RMR] ⁴	
				Start	End	Midpoint										
BB-BSA-103	NX (1.88)	R1	2.5	7.2	12.2	9.7	5.0	5.0	100%	1.54	31%	Poor	Slightly Weathered (W2)	Extremely Strong (R6)	44	Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite veins and thick quartz veins, extremely strong, thinly laminated, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, stepped to irregular, very rough to smooth, open; average 4.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.5	12.2	17.2	14.7	5.0	5.0	100%	3.50	70%	Fair	Fresh (W1)	Extremely Strong (R6)	62	Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite and quartz veins, extremely strong, thinly laminated, fresh; discontinuities moderately dipping, close to moderately close spacing, stepped to irregular, rough, open; average 0.8 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-104A	NX (1.88)	R1	3.1	21.0	26.0	23.5	5.0	4.8	95%	2.80	56%	Fair	Slightly Weathered (W2) to Fresh (W1)	Strong (R4) to Very Strong (R5)	41	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered to fresh, clay and sand infilling 22.5 ft to 23 ft; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.0	26.0	28.8	27.4	2.8	2.1	75%	1.70	61%	Fair	Fresh (W1)	Strong (R4) to Very Strong (R5)	58	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, fresh; discontinuities low angle to moderate dipping, very close spacing, rough to very rough, tight, average 0.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	9.5	28.8	31.0	29.9	2.2	2.0	91%	0.50	23%	Very Poor	Fresh (W1)	Strong (R4) to Very Strong (R5)	41	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong to very strong, fresh; discontinuities low angle to steep dipping, very close spacing, rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-105	NX (1.88)	R1	2.5	26.4	31.4	28.9	5.0	5.0	100%	1.50	30%	Poor	Slightly Weathered (W2) to Fresh (W1)	Strong (R4)	41	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong, slightly weathered to fresh; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.4	31.4	36.2	33.8	4.8	4.8	100%	3.60	75%	Fair	Fresh (W1)	Very Strong (R5)	58	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, very strong, fresh; discontinuities low angle to steep dipping, very close spacing, smooth to rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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MaineDOT WIN 027176.00

Test Boring Designation	Core Size	Run						TCR ¹		RQD ²		Physical Rock Parameters				Lithologic, Rock Mass and Discontinuity Description ^{5,6}
		No.	Midpoint Depth Below Bedrock Surface (ft)	Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering ³	Estimated Field Strength ³	Rock Mass Rating [RMR] ⁴	
				Start	End	Midpoint										
BB-BSA-106	NX (1.88)	R1	0.5	63.8	64.8	64.3	1.0	0.3	30%	0.00	0%	Very Poor	Slightly Weathered (W2) to Fresh (W1)	Strong (R4) to Very Strong (R5)	36	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered to fresh; discontinuities low angle dipping, very close to close spacing, rough to very rough, tight to open [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	3.1	64.8	69.1	67.0	4.3	4.3	100%	2.00	47%	Poor	Fresh (W1)	Strong (R4) to Very Strong (R5)	35	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, fresh with chemical weathering 67.4 ft to 68.3 ft, sand infilling 67.9 ft to 68.3 ft; discontinuities low angle to vertical dipping, very close to close spacing, smooth to rough, tight to open, average 3.3 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	7.8	69.1	74.1	71.6	5.0	5.0	100%	3.10	62%	Fair	Fresh (W1)	Weak (R2)	45	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, weak, fresh; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 1.4 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-107	NX (1.88)	R1	2.3	63.4	67.2	65.3	3.8	0.6	16%	0.00	0%	Very Poor	Highly Weathered (W4)	Strong (R4)	26	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling from 64.2 ft to 67.2; discontinuities low angle to steep dipping, close spacing, rough to very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	4.7	67.2	68.2	67.7	1.0	0.2	17%	0.00	0%	Very Poor	Highly Weathered (W4)	Strong (R4)	27	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling; discontinuities low angle dipping, close spacing, very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	7.2	68.2	72.2	70.2	4.0	3.8	95%	1.41	35%	Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	36	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered, occasional moderate to severe chemical weathering with sand infilling; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R4	11.7	72.2	77.2	74.7	5.0	5.0	100%	1.96	39%	Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	36	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered, occasional moderate to severe chemical weathering with sand and clay infilling; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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MaineDOT WIN 027176.00

Test Boring Designation	Core Size (in)	Run						TCR ¹		RQD ²		Physical Rock Parameters				Lithologic, Rock Mass and Discontinuity Description ^{5,6}
		No.	Midpoint Depth Below Bedrock Surface (ft)	Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering ³	Estimated Field Strength ³	Rock Mass Rating [RMR] ⁴	
				Start	End	Midpoint										
BB-BSA-108	NX (1.88)	R1	2.5	6.7	11.7	9.2	5.0	4.9	98%	2.92	58%	Fair	Slightly Weathered (W2)	Very Strong (R5) to Extremely Strong (R6)	51	Grey, very fine to fine grained, METAWACKE [metasandstone] with frequent calcite veins, very to extremely strong, thinly laminated, slightly weathered; discontinuities moderate to steep dipping, close to moderately close spacing, rough to polished, open; average 2.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	5.5	11.7	12.7	12.2	1.0	0.9	92%	0.42	42%	Poor	Slightly Weathered (W2) to Fresh (W1)	Extremely Strong (R6)	51	Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open; average 1.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R3	7.0	12.7	14.7	13.7	2.0	1.8	88%	0.33	17%	Very Poor	Slightly Weathered (W2) to Fresh (W1)	Extremely Strong (R6)	45	Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open; average 2.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R4	9.0	14.7	16.7	15.7	2.0	1.9	96%	0.71	35%	Poor	Slightly Weathered (W2) to Fresh (W1)	Extremely Strong (R6)	48	Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open; average 2.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-109A	NX (1.88)	R1	2.9	4.0	8.8	6.4	4.8	4.6	95%	1.42	30%	Poor	Slightly Weathered (W2) to Fresh (W1)	Very Strong (R5) to Extremely Strong (R6)	43	Grey, very fine grained, METAWACKE [metasandstone] with frequent calcite veins, very to extremely strong, thinly laminated, fresh to slightly weathered; discontinuities steep dipping, close spacing, planar to stepped, rough to smooth, open; average 2.1 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.9	8.8	14.0	11.4	5.2	5.1	99%	2.54	49%	Poor	Fresh (W1)	Very Strong (R5) to Extremely Strong (R6)	49	Grey, very fine grained, METAWACKE [metasandstone] with frequent calcite veins (0.1 to 0.7 in thick), very to extremely strong, thinly laminated, fresh; discontinuities low angle to steep dipping, very close to moderately close spacing, planar to stepped, rough to smooth, open; average 1.8 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
BB-BSA-110	NX (1.88)	R1	2.5	5.3	10.3	7.8	5.0	4.8	95%	2.46	49%	Poor	Fresh (W1)	Medium Strong (R3)	43	Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, medium strong, thinly laminated, fresh; discontinuities horizontal to steep dipping, close to moderately close spacing, stepped, smooth to polished, open; average 1.0 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	7.5	10.3	15.3	12.8	5.0	5.0	100%	3.54	71%	Fair	Fresh (W1)	Very Strong (R5) to Extremely Strong (R6)	54	Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, very to extremely strong, thinly laminated, fresh; discontinuities steep dipping, close to wide spacing, stepped, smooth, open; average 0.8 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

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MaineDOT WIN 027176.00

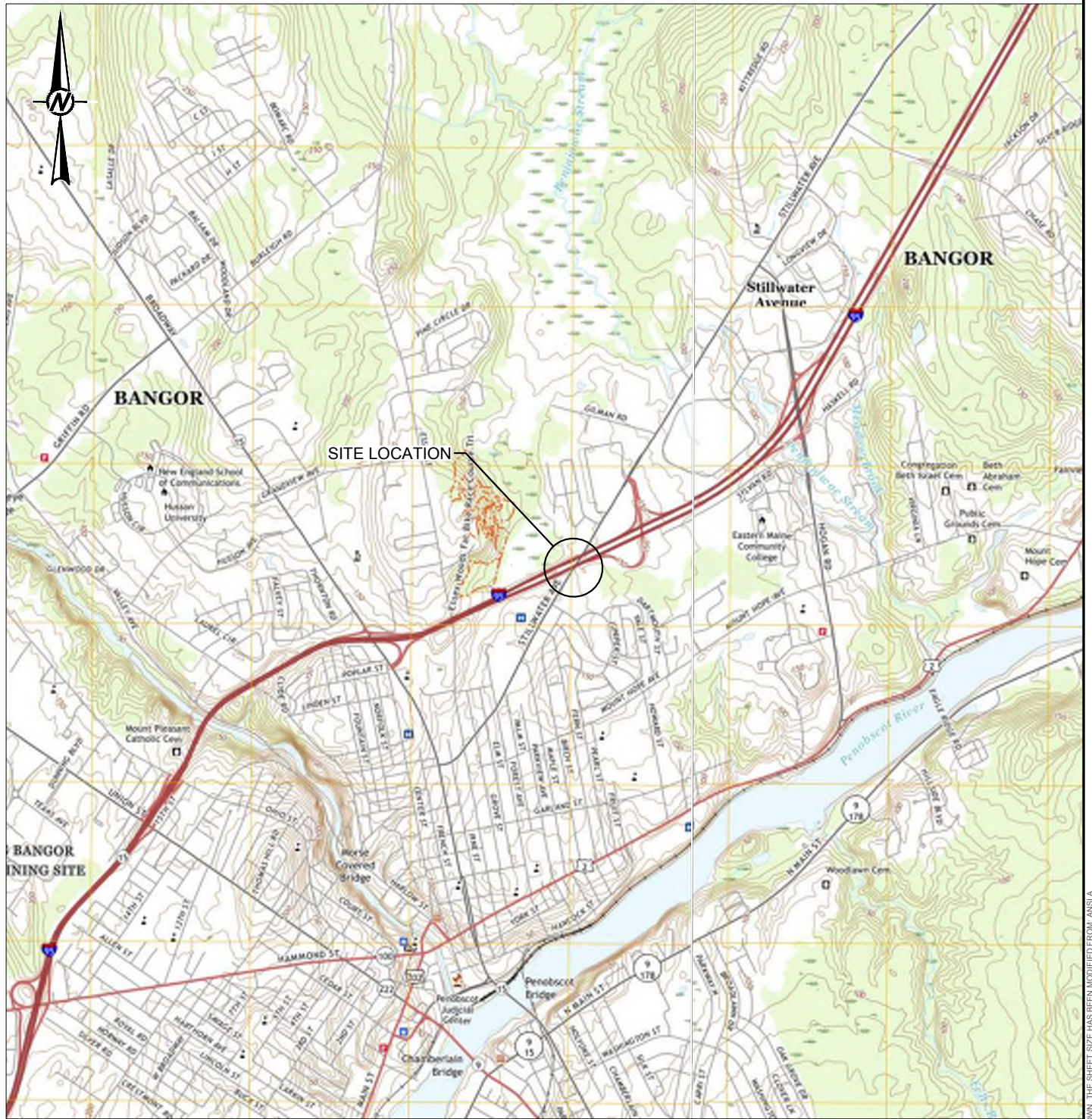
Test Boring Designation	Core Size	Run						TCR ¹		RQD ²		Physical Rock Parameters			Lithologic, Rock Mass and Discontinuity Description ^{5,6}	
		No.	Midpoint Depth Below Bedrock Surface (ft)	Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering ³	Estimated Field Strength ³		Rock Mass Rating [RMR] ⁴
				Start	End	Midpoint										
BB-BSA-111	NX (1.88)	R1	3.7	19.0	24.0	21.5	5.0	3.4	68%	0.75	15%	Very Poor	Slightly Weathered (W2)	Strong (R4) to Very Strong (R5)	37	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered with signs of chemical weathering; discontinuities low angle to steep dipping, close to very close spacing, rough to very rough, open to tight, highly fractured average from 19 ft to 21.3 ft [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].
		R2	8.7	24.0	29.0	26.5	5.0	5.0	100%	3.00	60%	Fair	Fresh (W1)	Strong (R4) to Very Strong (R5)	54	Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, fresh; discontinuities low angle dipping, very close spacing, rough, tight, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].

Notes:
1. TCR = total core recovery. Total core recovery is the length of core recovered divided by the length of the run.
2. RQD = rock quality designation. RQD is the total length of intact, full diameter core pieces recovered with a length greater than or equal to 4 inches measured along the core axis. The percent RQD is the total length of RQD measured divided by the run length. Note that vertical discontinuities are not included in determination of RQD.
3. Weathering and Estimated Field Strength based on Tables II.4 and II.3 (respectively) in Wyllie and Mah, 2004, Rock Slope Engineering: Civil and Mining, 4th Edition (based on ISRM, 1981).
4. Rock Mass Rating (RMR) System (Bieniawski, 1989) assigns numerical ratings to six parameters, including the strength of the intact rock, the RQD, the discontinuity spacing, groundwater conditions, and orientation of discontinuities. These ratings are summed to provide the RMR value. The rating adjustment for joint orientation was assigned a value of -4, which is the average of the orientation adjustments obtained from geologic field mapping of the exposed rock outcrops and which is based on the existing rock cut orientation. The proposed foundation orientation may allow for a different rating adjustment for joint orientation, and thus a modification to the RMR value shown on this table.
5. Bedrock formation name from: Pollock, Stephen G. 2011. Bedrock geology of the Bangor Quadrangle, Maine. Maine Geological Survey Open-File No. 11-57. Map scale 1:24,000.
6. ft = feet, in = inches

Prepared by: KAR
Checked by: BK
Reviewed by: JDL

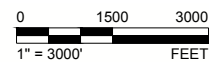
FIGURES

Last Edited By: usam701004 Date: 2024-08-14 Time: 9:48:43 AM Printed By: USAM701004 Date: 2024-08-14 Time: 9:54:44 AM
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REFERENCE(S)

1. BASE MAP TAKEN FROM U.S.G.S. 7.5 MINUTE QUADRANGLES OF BANGOR AND VEAZIE, MAINE DATED 2021



CLIENT
MAINE DEPARTMENT OF TRANSPORTATION

CONSULTANT



YYYY-MM-DD 2024-08-14

DESIGNED DEB

PREPARED AM

REVIEWED

APPROVED

PROJECT
DESIGN BUILD PHASE I
I-95 BRIDGE NO. 1427 & 5800 OVER STILLWATER AVENUE
BANGOR, ME (WIN 027176.00)

TITLE
SITE LOCATION MAP

PROJECT NO. CONTROL
US0025840.3905 0001-001

REV.
0

FIGURE
1

IF THIS MEASUREMENT DOES NOT MATCH WHAT IS SHOWN, THE SHEET SIZE HAS BEEN MODIFIED FROM: ANSI A



APPENDIX A

Boring Logs

UNIFIED SOIL CLASSIFICATION SYSTEM					MODIFIED BURMISTER SYSTEM																																											
MAJOR DIVISIONS			GROUP SYMBOLS	TYPICAL NAMES																																												
COARSE-GRAINED SOILS (more than half of material is larger than No. 200 sieve size)	GRAVELS (more than half of coarse fraction is larger than No. 4 sieve size)	CLEAN GRAVELS	GW	Well-graded gravels, gravel-sand mixtures, little or no fines.	<u>Descriptive Term</u>		<u>Portion of Total (%)</u>																																									
		(little or no fines)	GP	Poorly-graded gravels, gravel sand mixtures, little or no fines.	trace		0 - 10																																									
		GRAVEL WITH FINES (Appreciable amount of fines)	GM	Silty gravels, gravel-sand-silt mixtures.	little		11 - 20																																									
			GC	Clayey gravels, gravel-sand-clay mixtures.	some		21 - 35																																									
	SANDS (more than half of coarse fraction is smaller than No. 4 sieve size)	CLEAN SANDS	SW	Well-graded sands, Gravelly sands, little or no fines	adjective (e.g. Sandy, Clayey)		36 - 50																																									
		(little or no fines)	SP	Poorly-graded sands, Gravelly sand, little or no fines.																																												
FINE-GRAINED SOILS (more than half of material is smaller than No. 200 sieve size)	SILTS AND CLAYS (liquid limit less than 50)		SM	Silty sands, sand-silt mixtures	TERMS DESCRIBING DENSITY/CONSISTENCY <u>Coarse-grained soils</u> (more than half of material is larger than No. 200 sieve): Includes (1) clean gravels; (2) Silty or Clayey gravels; and (3) Silty, Clayey or Gravelly sands. Density is rated according to standard penetration resistance (N-value). <table><tr><th><u>Density of Cohesionless Soils</u></th><th><u>Standard Penetration Resistance</u> N₆₀-Value (blows per foot)</th></tr><tr><td>Very loose</td><td>0 - 4</td></tr><tr><td>Loose</td><td>5 - 10</td></tr><tr><td>Medium Dense</td><td>11 - 30</td></tr><tr><td>Dense</td><td>31 - 50</td></tr><tr><td>Very Dense</td><td>> 50</td></tr></table> <u>Fine-grained soils</u> (more than half of material is smaller than No. 200 sieve): Includes (1) inorganic and organic silts and clays; (2) Gravelly, Sandy or Silty clays; and (3) Clayey silts. Consistency is rated according to undrained shear strength as indicated. <table><tr><th><u>Consistency of Cohesive soils</u></th><th><u>SPT N₆₀-Value (blows per foot)</u></th><th><u>Approximate Undrained Shear Strength (psf)</u></th><th><u>Field Guidelines</u></th></tr><tr><td>Very Soft</td><td>WOH, WOR, WOP, <2</td><td>0 - 250</td><td>Fist easily penetrates</td></tr><tr><td>Soft</td><td>2 - 4</td><td>250 - 500</td><td>Thumb easily penetrates</td></tr><tr><td>Medium Stiff</td><td>5 - 8</td><td>500 - 1000</td><td>Thumb penetrates with moderate effort</td></tr><tr><td>Stiff</td><td>9 - 15</td><td>1000 - 2000</td><td>Indented by thumb with great effort</td></tr><tr><td>Very Stiff</td><td>16 - 30</td><td>2000 - 4000</td><td>Indented by thumbnail</td></tr><tr><td>Hard</td><td>>30</td><td>over 4000</td><td>Indented by thumbnail with difficulty</td></tr></table>				<u>Density of Cohesionless Soils</u>	<u>Standard Penetration Resistance</u> N ₆₀ -Value (blows per foot)	Very loose	0 - 4	Loose	5 - 10	Medium Dense	11 - 30	Dense	31 - 50	Very Dense	> 50	<u>Consistency of Cohesive soils</u>	<u>SPT N₆₀-Value (blows per foot)</u>	<u>Approximate Undrained Shear Strength (psf)</u>	<u>Field Guidelines</u>	Very Soft	WOH, WOR, WOP, <2	0 - 250	Fist easily penetrates	Soft	2 - 4	250 - 500	Thumb easily penetrates	Medium Stiff	5 - 8	500 - 1000	Thumb penetrates with moderate effort	Stiff	9 - 15	1000 - 2000	Indented by thumb with great effort	Very Stiff	16 - 30	2000 - 4000	Indented by thumbnail	Hard	>30	over 4000	Indented by thumbnail with difficulty
			<u>Density of Cohesionless Soils</u>	<u>Standard Penetration Resistance</u> N ₆₀ -Value (blows per foot)																																												
			Very loose	0 - 4																																												
	Loose	5 - 10																																														
	Medium Dense	11 - 30																																														
	Dense	31 - 50																																														
Very Dense	> 50																																															
<u>Consistency of Cohesive soils</u>	<u>SPT N₆₀-Value (blows per foot)</u>	<u>Approximate Undrained Shear Strength (psf)</u>	<u>Field Guidelines</u>																																													
Very Soft	WOH, WOR, WOP, <2	0 - 250	Fist easily penetrates																																													
Soft	2 - 4	250 - 500	Thumb easily penetrates																																													
Medium Stiff	5 - 8	500 - 1000	Thumb penetrates with moderate effort																																													
Stiff	9 - 15	1000 - 2000	Indented by thumb with great effort																																													
Very Stiff	16 - 30	2000 - 4000	Indented by thumbnail																																													
Hard	>30	over 4000	Indented by thumbnail with difficulty																																													
CL	Inorganic clays of low to medium plasticity, Gravelly clays, Sandy clays, Silty clays, lean clays.																																															
OL	Organic silts and organic Silty clays of low plasticity.																																															
SILTS AND CLAYS (liquid limit greater than 50)	MH	Inorganic silts, micaceous or diatomaceous fine Sandy or Silty soils, elastic silts.																																														
	CH	Inorganic clays of high plasticity, fat clays.																																														
	OH	Organic clays of medium to high plasticity, organic silts.																																														
	HIGHLY ORGANIC SOILS	Pt	Peat and other highly organic soils.																																													
Desired Soil Observations (in this order, if applicable): Color (Munsell color chart) Moisture (dry, damp, moist, wet) Density/Consistency (from above right hand side) Texture (fine, medium, coarse, etc.) Name (Sand, Silty Sand, Clay, etc., including portions - trace, little, etc.) Gradation (well-graded, poorly-graded, uniform, etc.) Plasticity (non-plastic, slightly plastic, moderately plastic, highly plastic) Structure (layering, fractures, cracks, etc.) Bonding (well, moderately, loosely, etc.,) Cementation (weak, moderate, or strong) Geologic Origin (till, marine clay, alluvium, etc.) Groundwater level					Rock Quality Designation (RQD): RQD (%) = <u>sum of the lengths of intact pieces of core* > 4 inches</u> length of core advance *Minimum NQ rock core (1.88 in. OD of core) Rock Quality Based on RQD <table><tr><th><u>Rock Quality</u></th><th><u>RQD (%)</u></th></tr><tr><td>Very Poor</td><td>≤25</td></tr><tr><td>Poor</td><td>26 - 50</td></tr><tr><td>Fair</td><td>51 - 75</td></tr><tr><td>Good</td><td>76 - 90</td></tr><tr><td>Excellent</td><td>91 - 100</td></tr></table> Desired Rock Observations (in this order, if applicable): Color (Munsell color chart) Texture (aphanitic, fine-grained, etc.) Rock Type (granite, schist, sandstone, etc.) Hardness (very hard, hard, mod. hard, etc.) Weathering (fresh, very slight, slight, moderate, mod. severe, severe, etc.) Geologic discontinuities/jointing: -dip (horiz - 0-5 deg., low angle - 5-35 deg., mod. dipping - 35-55 deg., steep - 55-85 deg., vertical - 85-90 deg.) -spacing (very close - <2 inch, close - 2-12 inch, mod. close - 1-3 feet, wide - 3-10 feet, very wide >10 feet) -tightness (tight, open, or healed) -infilling (grain size, color, etc.) Formation (Waterville, Ellsworth, Cape Elizabeth, etc.) RQD and correlation to rock quality (very poor, poor, etc.) ref: ASTM D6032 and FHWA NHI-16-072 GEC 5 - Geotechnical Site Characterization, Table 4-12 Recovery (inch/inch and percentage) Rock Core Rate (X.X ft - Y.Y ft (min:sec))				<u>Rock Quality</u>	<u>RQD (%)</u>	Very Poor	≤25	Poor	26 - 50	Fair	51 - 75	Good	76 - 90	Excellent	91 - 100																												
<u>Rock Quality</u>	<u>RQD (%)</u>																																															
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Maine Department of Transportation Geotechnical Section Key to Soil and Rock Descriptions and Terms Field Identification Information					Sample Container Labeling Requirements: WIN Blow Counts Bridge Name / Town Sample Recovery Boring Number Date Sample Number Personnel Initials Sample Depth																																											

Table A-2**Classification of Rock Material Strengths¹**

Grade	Description	Field Identification	Approx. Range of Uniaxial Compressive Strength	
			MPa	psi
S1	Very soft clay	Easily penetrated several inches by fist	<0.025	<4
S2	Soft clay	Easily penetrated several inches by thumb	0.025-0.05	4-7
S3	Firm clay	Can be penetrated several inches by thumb with moderate effort	0.05-0.10	7-15
S4	Stiff clay	Readily indented by thumb but penetrated only with great effort	0.10-0.25	15-35
S5	Very stiff clay	Readily indented by thumbnail	0.25-0.50	35-70
S6	Hard clay	Indented with difficulty by thumbnail	>0.50	>70
R0	Extremely weak rock	Indented by thumbnail	0.25-1.0	35-150
R1	Very weak rock	Crumbles under firm blows with point of geological hammer; can be peeled by a pocket knife	1-5	150-725
R2	Weak rock	Can be peeled by a pocket knife with difficulty; shallow indentations made by firm blow with point of geological hammer	5-25	725-3,500
R3	Medium strong rock	Cannot be scraped or peeled with a pocket knife; specimen can be fractured with single firm blow of geological hammer	25-50	3,500-7,000
R4	Strong rock	Specimen requires more than one blow of geological hammer to fracture it	50-100	7,000-15,000
R5	Very strong rock	Specimen requires many blows of geological hammer to fracture it	100-250	15,000-36,000
R6	Extremely strong rock	Specimen can only be chipped with geological hammer	>250	>36,000

Note: Grades S1 to S6 apply to cohesive soils, for example clays, silty clays, and combinations of silts and clays with sand, generally slow draining. Discontinuity wall strength will generally be characterized by grades R0-R6 (rock) while S1-S6 (clay) will generally apply to filled discontinuities.

¹ International Society for Rock Mechanics (ISRM), Commission on standardization of laboratory and field tests (1978): Suggested methods for the quantitative description of discontinuities in rock masses. Int. J. Rock Mech. Min. Sci. & Geomech. Abstr., Vol. 15, No. 6, pp. 319-368.

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-101 WIN: 027176.00					
Driller: Seaboard		Elevation (ft.): 150.52		Auger ID/OD:							
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/29/24 (21:00); 7/30/24 (3:15)		Drilling Method: SSA, Drive & Wash		Core Barrel: NQ/NX							
Boring Location: N: 482856.27, E: 1735264.27		Casing ID/OD: 4" (ID)		Water Level*: 24.8' at 1:47 7/30/24							
Hammer Efficiency Factor: 1.087		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
<div style="display: flex; justify-content: space-between; font-size: 0.8em;"> <div> Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt </div> <div> R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person </div> <div> S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_{u(lab)} = Lab Vane Undrained Shear Strength (psf) q_p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected </div> <div> T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test </div> </div>											
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
0	1D	24/15	0.70 - 2.70	12-12-12-11	24	43	SSA	149.9		7" Asphalt Pavement	Fines = 16.8% A-1-b (0), SM
										Light Olive Brown, dry, dense, fine to coarse SAND, some gravel, little silt (FILL).	
	2D	24/22	2.70 - 4.70	10-21-21-21	42	76				Olive with brown, dry, hard, SILT, some fine to coarse gravel, little fine to coarse sand, non-plastic (FILL).	
5	3D	24/22	5.00 - 7.00	15-28-43-42	71	129				Olive with brown, dry, hard, SILT, some fine to coarse gravel, little fine to coarse sand, non-plastic (FILL).	
	4D	24/22	7.00 - 9.00	24-16-26-39	42	76				Olive with brown, dry to moist (becomes moist at 8.9' bgs), hard, SILT, some fine to coarse sand, little fine to coarse gravel, non-plastic (FILL).	
10	5D	24/22	10.00 - 12.00	11-13-16-17	29	53				Olive with brown, moist, hard, SILT, some fine to coarse sand, little fine to coarse gravel, non-plastic (FILL).	
15	6D	22/6	15.00 - 16.83	16-16-10-22	26	47	OPEN	137.0		Olive brown, moist, dense, fine to coarse SAND, some fine to coarse gravel, some silt (SILTY SAND and GRAVEL)	WC = 10.7% Fines = 28.8% A-2-4 (0), SM-GM
20	7D	24/9	20.00 - 22.00	13-22-30-30	52	94			Olive brown, moist, dense, fine to coarse SAND, some fine to coarse gravel, some silt (SILTY SAND and GRAVEL)		
									Brown, wet, very dense, fine to medium SAND, some fine gravel, some silt (SILTY SAND WITH GRAVEL)		
									Increased roller bit resistance		
25	8D	24/6	25.00 - 27.00	29-33-34-23	67	121			Dark grayish brown, wet, very dense, fine to coarse SANDY GRAVEL, little silt (SANDY GRAVEL)		
30											
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level reading taken on 7/30/24 at 1:47 am was made after the rock coring.											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 1 of 3 Boring No.: BB-BSA-101	

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-101							
WIN: 027176.00													
Driller: Seaboard		Elevation (ft.): 150.52		Auger ID/OD:									
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon									
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in									
Date Start/Finish: 7/29/24 (21:00); 7/30/24 (3:15)		Drilling Method: SSA, Drive & Wash		Core Barrel: NQ/NX									
Boring Location: N: 482856.27, E: 1735264.27		Casing ID/OD: 4" (ID)		Water Level*: 24.8' at 1:47 7/30/24									
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person				S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected					
				T _v = Pocket Torvane Shear Strength (psf)				WC = Water Content, percent					
				LL = Liquid Limit				PL = Plasticity Limit					
				G = Grain Size Analysis				C = Consolidation Test					
Sample Information													
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.		
30	9D	8/3	30.00 - 30.67	50/3"	R					Grey, wet, hard, SILT, some fine to coarse sand, some fine to coarse gravel, trace clay, fractured rock fragments (GLACIAL TILL)			
	R-1	10.8/9.6	31.50 - 32.40	RQD = 0%			NQ/NX	119.0					
	R-2	6/6	32.40 - 32.90	RQD = 0%									
	R-3	43.2/43.2	32.90 - 36.50	RQD = 14%									
35													
	R-4	60/60	36.50 - 41.50	RQD = 60%									
40													
45													
50													
55													
60													
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level reading taken on 7/30/24 at 1:47 am was made after the rock coring.													
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 2 of 3			
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-BSA-101			

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine				Boring No.: BB-BSA-101 WIN: 027176.00																																																																																																																		
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Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-102	
WIN: 027176.00							
Driller: Seaboard		Elevation (ft.): 133.5		Auger ID/OD:			
Operator: Kevin Hanscom		Datum: Maine East Zone		Sampler: Standard Split Spoon			
Logged By: Lina-Maria Pua		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140 lbs/30 in			
Date Start/Finish: 05/07/24 (23:53); 05/08/24 (02:12)		Drilling Method: SSA, Cased Wash		Core Barrel: NX			
Boring Location: N: 482969.08, E: 1735451.57		Casing ID/OD: 3 in/3.25 in		Water Level*: 9.3 ft on 05/08/24 at 01:59			
Hammer Efficiency Factor: 1.066		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>					
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _{u(lab)} = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test							
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0							SSA
	1D	24/11.5	1.00 - 3.00	14-13-20-38	33	59	
	2D	24/12	3.00 - 5.00	15-24-12-43	36	64	
5	3D	24/11	5.00 - 7.00	47-22-10-12	32	57	40
							48
	4D	24/12	7.00 - 9.00	15-14-9-39	23	41	45
							92
10	5D	24/5	9.00 - 11.00	69-34-27-13	61	108	36
							63
							100
	R1	60/54	12.20 - 17.20	RQD = 73%			135
							NX
15							
	R2	60/59	17.20 - 22.20	RQD = 98%			
20							
25							
30							
Visual Description and Remarks 7.5" Asphalt Pavement Brown, moist, very dense, fine to medium SAND, some fine gravel, little silt (FILL). Brown, dry to moist, very dense, medium to fine SILTY SAND, some fine gravel, non-plastic (FILL). q _p > 0.9ksf Brown to yellow, moist to wet, hard, SILT, some sand, trace gravel, nonplastic to low plasticity (SANDY SILT). Brown to yellow, wet, hard, SANDY SILT, trace fine gravel, non-plastic to low plasticity (SANDY SILT). q _p = 0.8ksf, 0.9ksf Brown to yellow, wet, very dense, fine to coarse GRAVEL, some fine to coarse sand, some silt, low to medium plasticity (GRAVEL) Bedrock encountered at 12.2 feet bgs Top of Bedrock at Elev. 121.3 ft. R1 (12.2'-17.2'): Grey, very fine to fine grained, thinly to thickly laminated, METAWACKE [metasandstone], frequent thin to thick calcite veins, strong to extremely strong, slightly weathered; discontinuities moderately to steeply dipping, close to moderately close spacing, irregular to planar, smooth to very rough, open; average 3.2 fractures per foot, chemical weathering in joints [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = Fair 90% Recovery Rock Core Rate (min:sec) 12.2-13.2 ft (2:24) 13.2-14.2 ft (3:05) 14.2-15.2 ft (3:17) 15.2-16.2 ft (3:03) 16.2-17.2 ft (3:19) R2 (17.2'-22.2'): Grey, very fine to fine grained, thinly laminated, METAWACKE [metasandstone], frequent calcite veins, extremely strong, fresh; discontinuities horizontal dipping, close to wide spacing, irregular to planar, smooth to very rough, open; average 0.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = Fair 98% Recovery Rock Core Rate (min:sec) 17.2-18.2 ft (2:54) 18.2-19.2 ft (3:07) 19.2-20.2 ft (2:48) 20.2-21.2 ft (3:15)							
Laboratory Testing Results/ AASHTO and Unified Class.							
WC = 3.7% Fines = 14.0% A-1-b(0), SM WC = 8.6% Fines = 38.0% A-4 (0), SM Fines = 50.2% A-4 (0), ML WC = 15.5% Fines = 25.6% A-2-4 (0), GM							
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level reading taken on 5/8/24 at 01:59 was made 15 minutes after completion of drilling with bottom of casing at 12.2 ft bgs.							
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.							

[illegible]

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-103 WIN: 027176.00					
Driller: Seaboard			Elevation (ft.): 132.13		Auger ID/OD:						
Operator: Kevin Hanscom			Datum: Maine East Zone		Sampler: Standard Split Spoon						
Logged By: Lina-Maria Pua			Rig Type: Diedrich D-50		Hammer Wt./Fall: 140 lbs/30 in						
Date Start/Finish: 05/08/24 (21:32); 05/08/24 (23:30)			Drilling Method: SSA, Cased Wash		Core Barrel: NX						
Boring Location: N: 482888.01, E: 1735425.94			Casing ID/OD: 3 in/3.25 in		Water Level*: 5.2 ft on 05/08/24 at 23:14						
Hammer Efficiency Factor: 1.066			Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>								
<div style="display: flex; justify-content: space-between; font-size: 0.8em;"> <div> Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt </div> <div> R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person </div> <div> S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_u(lab) = Lab Vane Undrained Shear Strength (psf) q_p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected </div> <div> T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test </div> </div>											
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
0							SSA	131.5		Asphalt Pavement Brown, dry, dense, SILTY GRAVEL, some sand, poorly-graded (FILL). 2DA, Top 1 in: Brown, dry, medium dense, SILTY GRAVEL, some sand, poorly-graded (FILL). 2DB, Bottom 11 in: Grey, dry, medium dense, angular GRAVEL, some weathered rock fragments (WEATHERED BEDROCK). Grey, moist to wet, very dense, WEATHERED BEDROCK, some silt, little sand (WEATHERED BEDROCK). Bedrock encountered at 7.2 feet bgs Top of Bedrock at Elev. 124.9 ft R1 (7.2'-12.2'): Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite veins and thick quartz veins, extremely strong, thinly laminated, slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, stepped to irregular, very rough to smooth, open. average 4.0 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 100% Recovery Rock Core Rate (min:sec) 7.2-8.2 ft (4:32) 8.2-9.2 ft (4:43) 9.2-10.2 ft (5:32) 10.2-11.2 ft (5:50) 11.2-12.2 ft (6:37) R2 (12.2'-17.2'): Grey, very fine to fine grained, METAWACKE [metasandstone] with thin calcite and quartz veins, extremely strong, thinly laminated, fresh; discontinuities moderately dipping, close to moderately close spacing, stepped to irregular, rough, open, average 0.8 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = Excellent 100% Recovery	Bottom of Exploration at 17.2 feet below ground surface. Boring backfilled with bentonite chips in the rock core socket, gravel to bottom of pavement and patched with cold patch asphalt.
	1D	24/16	1.00 - 3.00	21-24-21-21	45	80		129.0			
	2D	24/12	3.00 - 5.00	7-10-6-48	16	28					
5	3D	26.4/15.5	5.00 - 7.20	45-34-45-50/4"	79	140					
	R1	60/60	7.20 - 12.20	RQD = 31%			NX	124.9			
10											
	R2	60/60	12.20 - 17.20	RQD = 71%							
15											
20											
25											
30											

Remarks:

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by MaineDOT.
- Water level reading taken on 5/8/24 at 23:14 was made after completion of drilling with bottom of casing at 7.2 ft bgs.

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

 * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

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Boring No.: BB-BSA-103

[illegible]

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine				Boring No.: BB-BSA-104A WIN: 027176.00				
Driller: Seaboard			Elevation (ft.): 151.97			Auger ID/OD:						
Operator: Ryan H.			Datum: Maine East Zone			Sampler: Standard Split Spoon						
Logged By: D. Burgess			Rig Type: DieDrich D-50			Hammer Wt./Fall: 140lb/30in						
Date Start/Finish: 7/30/24 (23:40); 7/31/24 (2:33)			Drilling Method: SSA, Drive & Wash			Core Barrel: NX						
Boring Location: N: 483017.59, E: 1735600.99			Casing ID/OD: 4" (ID)			Water Level*: Not measured						
Hammer Efficiency Factor: NA			Hammer Type: Automatic <input type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _{u(lab)} = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test												
Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0							SSA	151.3		8" Asphalt pavement		
5												
10												
15										Wood coming up in wash water		
20							NX	131.6		Possible bedrock.		
25	R-1	60/57	21.00 - 26.00	RQD = 56%						Bedrock encountered at 20.4 feet bgs Top of Bedrock at Elev. 131.6 ft R1 (21.0' - 26.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered to fresh, clay and sand infilling 22.5 ft to 23 ft; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 1.6 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 95% recovery 56% RQD Rock Core Rate (min:sec) 21.0 - 22.0 ft (3:06) 22.0 - 23.0 ft (2:42)		
30	R-2	33.6/25.2	26.00 - 28.80	RQD = 61%								
	R-3	26.4/24	28.80 - 31.00	RQD = 23%								
Remarks: 1. As-drilled boring locations and ground surface elevations were provided by HNTB.												
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.											Page 1 of 2 Boring No.: BB-BSA-104A	

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-104A WIN: 027176.00					
Driller: Seaboard		Elevation (ft.): 151.97		Auger ID/OD:							
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess		Rig Type: DieDrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/30/24 (23:40); 7/31/24 (2:33)		Drilling Method: SSA, Drive & Wash		Core Barrel: NX							
Boring Location: N: 483017.59, E: 1735600.99		Casing ID/OD: 4" (ID)		Water Level*: Not measured							
Hammer Efficiency Factor: NA				Hammer Type: Automatic <input type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>							
<div style="display: flex; justify-content: space-between; font-size: 0.8em;"> <div> Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt </div> <div> R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person </div> <div> S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_u(lab) = Lab Vane Undrained Shear Strength (psf) q_p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected </div> <div> T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test </div> </div>											
Depth (ft.)	Sample Information								Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing	Blows			
30									121.0	23.0 - 24.0 ft (2:08) 24.0 - 25.0 ft (2:14) 25.0 - 26.0 ft (2:50) R2 (26.0' - 28.8'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, fresh; discontinuities low angle to moderate dipping, very close spacing, rough to very rough, tight, average 0.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 75% recovery 61% RQD Rock Core Rate (min:sec) 26.0 - 27.0 ft (2:19) 27.0 - 28.0 ft (2:28) 28.0 - 28.8 ft (0:15) R3 (28.8' - 31.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] strong to very strong, fresh; discontinuities low angle to steep dipping, very close spacing, rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 91% recovery 23% RQD Rock Core Rate (min:sec) 28.8 - 29.0 ft (0:08) 29.0 - 30.0 ft (2:56) 30.0 - 31.0 ft (3:18)	
35											
40											
45											
50											
55											
60											
Remarks: 1. As-drilled boring locations and ground surface elevations were provided by HNTB.											
Stratification lines represent approximate boundaries between soil types; transitions may be gradual. * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Page 2 of 2 Boring No.: BB-BSA-104A	

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine				Boring No.: BB-BSA-105 WIN: 027176.00							
Driller: Seaboard				Elevation (ft.): 152.05				Auger ID/OD:							
Operator: Ryan H.				Datum: Maine East Zone				Sampler: Standard Split Spoon							
Logged By: D. Burgess				Rig Type: Diedrich D-50				Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/31/24 (20:07); 8/1/24 (0:30)				Drilling Method: SSA, Cased Wash				Core Barrel: NX							
Boring Location: N: 482984.9, E: 1735593.56				Casing ID/OD:				Water Level*: 17.0' BGS 11:56 7/31/24							
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>											
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person				S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _{u(lab)} = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected				T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test			
Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.			
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows								
0	1D	24/18	0.90 - 2.90	14-14-15-14	29	53	SSA		151.2		10" Asphalt pavement.				
											Olive brown, dry, very dense, fine to coarse SAND, some fine to coarse gravel, little silt (FILL).	0.8' Fines = 16.2% A-1-b (0), SM			
	2D	24/19	2.90 - 4.90	9-11-13-12	24	43									
											Olive with brown, dry, hard, SILT, some fine to coarse sand, some fine to coarse gravel, non- plastic (FILL).				
5	3D	8/8	5.00 - 5.67	11-50/2"	R						Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).	Fines = 46.4% A-4 (0), ML/ SM			
	4D	24/10	7.00 - 9.00	13-23-20-16	43	78					Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).				
10	5D	13.5/7	10.00 - 11.13	11-31-50/1.5"	R						Dark grayish brown, dry, hard, SANDY SILT, trace gravel (FILL).				
15	6D	24/13	15.00 - 17.00	3-4-8-11	12	22					Grayish brown, wet, medium dense, SILT, some fine to coarse sand, little fine to coarse subrounded gravel (SANDY SILT to SILTY SAND).	WC = 20.5% Fines = 55.7% A-4 (0), ML			
20	7D	24/11	20.00 - 22.00	14-11-20-18	31	56					Increased drilling resistance. Olive brown, wet, very dense SILTY SAND, little fine to coarse gravel (SANDY SILT to SILTY SAND).	WC = 11.7% Fines = 40.3% A-4 (0), ML/ SM			
25	8D	14/6	25.00 - 26.17	20-28-30/2"			OPEN				Grey, wet, very dense, fractured rock with fine to coarse sand (WEATHERED ROCK)				
	R-1	60/60	26.40 - 31.40	RQD = 30%			NX								
30															
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level reading taken on 7/31/24 at 23:58 was made after the rock coring.															
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.											Page 1 of 2				
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.											Boring No.: BB-BSA-105				

[illegible]

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-106							
Driller: Seaboard				Elevation (ft.): 143.6		Auger ID/OD:							
Operator: Ryan H.				Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess				Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/25/24 (20:19); 7/29/24 (1:56)				Drilling Method: SSA, Cased Wash		Core Barrel: NX							
Boring Location: N: 482611.2, E: 1735095.82				Casing ID/OD: 4" (ID)		Water Level*: Refer to remarks note 3							
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person				S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _{u(lab)} = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected					
T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test													
Sample Information										Visual Description and Remarks		Laboratory Testing Results/ AASHTO and Unified Class.	
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)	Graphic Log				
0							SSA	142.8		10" Asphalt Pavement			
	1D	24/13	1.00 - 3.00	14-9-7-5	16	29				Brown, dry, medium dense, fine to coarse SAND, some fine gravel, trace silt (FILL).			
	2D	24/19	3.00 - 5.00	11-13-18-20	31	56				Olive with brown, moist, hard, SILT, some fine to medium sand, some fine to coarse gravel, non-plastic (FILL)			
5	3D	24/15	5.00 - 7.00	13-16-37-30	53	96				Olive with brown, moist, hard, SILT, some fine to medium sand, some fine to coarse gravel, non-plastic (FILL)			
	4D	24/0	7.00 - 9.00	25-27-22-23	49	89				No recovery.			
10	5D	24/13	10.00 - 12.00	8-9-11-27	20	36	64			Olive with brown, moist, hard, SILT, some fine to medium sand, some fine to coarse gravel, non-plastic (FILL)			
							148						
							133						
							166						
15	6D	24/9	15.00 - 17.00	12-31-20-15	51	92	87			Grey, wet, very dense, fine to coarse SAND, flakey fractured rock fragments (FILL).			
							124			Possible boulder or cobbles 12 to 15" thick.			
							OPEN						
20	7D	24/22	20.00 - 22.00	5-6-3-4	9	16	24			Olive with grey and orange mottling, wet, very stiff, CLAY, trace sand, medium plasticity (CLAY). Pp = 4.0 to 6.0 ksf.	WC = 26% Fines = 98.9% LL = 37 PL = 19 PI = 18 LI = 0.4 A-6 (19), CL		
							26						
							22						
							34						
							31						
25	8D	24/24	25.00 - 27.00	4-7-8-9	15	27	42			Olive with grey and orange mottling, wet, very stiff, CLAY, trace sand, medium plasticity (CLAY). Pp = 6.0 to 8.0 ksf.	WC = 28% Fines = 99.7% LL = 36 PL = 19 PI = 17 LI = 0.5 A-6 (18), CL		
							55						
							61						
							54						
30							35						

Remarks:

- Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
- As-drilled boring locations and ground surface elevations were provided by HNTB.
- Water level measured during drilling at 20.55' bgs on 7/26/24 at 3:23, 20.55' bgs on 7/28/24 at 20:19. Water level measured at 24.9' bgs on 7/29/24 at 1:08 was made after the rock coring.

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

Page 1 of 4

* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

Boring No.: BB-BSA-106

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-106							
WIN: 027176.00													
Driller: Seaboard		Elevation (ft.): 143.6		Auger ID/OD:									
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon									
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in									
Date Start/Finish: 7/25/24 (20:19); 7/29/24 (1:56)		Drilling Method: SSA, Cased Wash		Core Barrel: NX									
Boring Location: N: 482611.2, E: 1735095.82		Casing ID/OD: 4" (ID)		Water Level*: Refer to remarks note 3									
Hammer Efficiency Factor: 1.087		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>											
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt		R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person		S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected		T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test							
Depth (ft.)	Sample Information							Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.			
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				Elevation (ft.)		
30	9D	24/24	30.00 - 32.00	WOH/18"-8			49	112.1		Grey, wet, very soft, CLAY, trace sand medium plasticity (CLAY). P _p < 1.0 tsf.	WC = 29% Fines = 98.7% LL = 26 PL = 15 PI = 11 LI = 1.3 A-6 (9), CL		
							42						
							56						
							100						
							57						
35	10D	24/12	35.00 - 37.00	4-2-6-7	8	14	43						
							40						
							42						
							51						
							42						
40	11D	24/10	40.00 - 42.00	5-3-7-7	10	18	59						
							48						
							50						
							52						
							40						
45	12D	24/18	45.00 - 47.00	3-4-4-6	8	14	53						
							49						
							53						
							61						
							43						
50	13D	24/12	50.00 - 52.00	10-8-6-11	14	25	54						
							42						
							96						
							173						
							248						
55	14D	24/15	55.00 - 57.00	14-13-16-19	29	53	61						
							45						
							62						
							108						
60							112						
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level measured during drilling at 20.55'bs on 7/26/24 at 3:23, 20.55'bs on 7/28/24 at 20:19. Water level measured at 24.9'bs on 7/29/24 at 1:08 was made after the rock coring.													
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.									Page 2 of 4				
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.									Boring No.: BB-BSA-106				

[illegible]

[illegible]

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-107							
Driller: Seaboard				Elevation (ft.): 143.11		Auger ID/OD:							
Operator: Ryan H.				Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess				Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/22/24 (21:09); 7/24/24 (0:25)				Drilling Method: SSA, Drive & Wash		Core Barrel: NX							
Boring Location: N: 482578.95, E: 1735092.78				Casing ID/OD: 4" (ID)		Water Level*: Refer to remarks note 3							
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person				S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected					
T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test													
Sample Information													
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.		
0	1D	24/14	0.70 - 2.70	8-10-8-6	18	33	SSA	142.6		6" Asphalt Pavement	Fines = 55.2% A-4 (0), ML		
										Brown, dry, medium dense, fine to coarse SAND, some fine to coarse gravel, trace silt (FILL).			
	2D	24/16	2.70 - 4.70	6-8-8-17	16	29				Grayish brown, dry, medium dense, SANDY SILT, trace fine gravel, non-plastic (FILL).			
5	3D	24/19	4.70 - 6.70	12-19-18-18	37	67				Grayish brown, dry, hard, SANDY SILT, trace fine gravel, non-plastic (FILL).			
	4D	24/10	6.70 - 8.70	14-7-18-10	25	45				Grayish brown, dry, hard, SANDY SILT, trace fine gravel, non-plastic (FILL).			
	5D	24/6	8.70 - 10.70	4-3-4-4	7	13				Grayish brown, dry, stiff, SANDY SILT, trace fine gravel, slightly plastic (FILL).			
10	6D	24/9	10.70 - 12.70	6-8-41-50/2"	49	89				Olive brown, wet, hard, SILT, some fine to coarse sand, trace fine gravel, slightly plastic, fractured rock fragments (FILL). Pp = 7.0 ksf	WC = 14.7% Fines = 62.3% A-4 (0), ML		
15	7D	24/5	15.00 - 17.00	12-19-20-8	39	71				Olive brown, wet, very dense, fine to coarse SAND, fractured scaly rock fragments (FILL).	WC = 24% Fines = 98.3% LL = 33 PL = 17 PI = 16 LI = -0.4 A-6 (15), CL		
20	8D	24/14	20.00 - 22.00	17-4-7-6	11	20				Grey with orange, mottled, wet, very stiff, CLAY, trace sand, medium plasticity (CLAY). Pp = 6.0 ksf	Fines = 99.3% A-6 (37), CL		
25	9D	24/24	25.00 - 27.00	4-3-6-6	9	16				Grey to brown, mottled, wet, very stiff, CLAY, trace sand (CLAY) Pp = 4.5 to 5.0 ksf	Fines = 99.3% A-6 (37), CL		
30													

Remarks:

1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.

2. As-drilled boring locations and ground surface elevations were provided by HNTB.

3. Water level measured during drilling at 6.45' bgs on 7/23/24 at 3:28, 18.7' bgs on 7/24/24 at 3:22, 19.3' bgs on 7/24/24 at 20:09. Water level measured at 23.9' bgs on 7/24/24 at 23:51 was made after the rock coring.

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

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 Boring No.: BB-BSA-107

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-107 WIN: 027176.00					
Driller: Seaboard		Elevation (ft.): 143.11		Auger ID/OD:							
Operator: Ryan H.		Datum: Maine East Zone		Sampler: Standard Split Spoon							
Logged By: D. Burgess		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/22/24 (21:09); 7/24/24 (0:25)		Drilling Method: SSA, Drive & Wash		Core Barrel: NX							
Boring Location: N: 482578.95, E: 1735092.78		Casing ID/OD: 4"(ID)		Water Level*: Refer to remarks note 3							
Hammer Efficiency Factor: 1.087		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>									
<div style="display: flex; justify-content: space-between; font-size: 0.8em;"> <div> Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt </div> <div> R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person </div> <div> S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_{u(lab)} = Lab Vane Undrained Shear Strength (psf) q_p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected </div> <div> T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test </div> </div>											
Depth (ft.)	Sample Information								Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)			
30	10D	24/17	30.00 - 32.00	3-3-3-3	6	11	70	108.1		Greyish brown, moist, medium stiff, CLAY, trace sand, medium plasticity, interbedded silt seams (CLAY). Pp < 2.0 ksf FV-1: 442psf / 118psf (55mmx110mm Vane) FV-2: 813psf / 415psf (55mmx110mm Vane)	WC = 28% Fines = 99.1% LL = 28 PL = 16 PI = 12 LI = 1 A-6 (11), CL
							63				
							56				
							390				
							63				
35	11D	24/0	35.00 - 37.00	12-11-15-10	26	47	104				
							96				
							87				
							78				
							63				
40	12D	24/6	40.00 - 42.00	5-7-12-12	19	34	73				
							76				
							103				
							111				
							81				
45	13D	24/4	45.00 - 47.00	9-9-6-9	15	27	105				
							103				
							111				
							118				
							90				
50	14D	24/8	50.00 - 52.00	6-8-15-8	23	42	81				
							89				
							105				
							113				
							89				
55	15D	24/14	55.00 - 57.00	26-41-51-50/4"	92	167	60				
							198				
							171				
							212				
60							196				
								89.6		No recovery - washed water had fine to coarse gravel and clay fragments.	WC = 10% Fines = 42.1% LL = 17 PL = 13 PI = 4 LI = -0.8 A-4 (0), SC/ SM
								53.5		Brownish grey, wet, dense, SILTY SAND, little coarse gravel, slightly plastic (SILTY SAND)	WC = 10% Fines = 39.6% LL = 20 PL = 12 PI = 8 LI = -0.3 A-4 (0), SC
								53.5		Brownish grey, wet, medium dense, SILTY SAND, little coarse gravel, slightly plastic (SILTY SAND).	WC = 10% Fines = 38.3% A-4 (0), SM
								53.5		Greyish brown, wet, dense, CLAYEY SAND, some gravel, low plasticity (CLAYEY SAND).	WC = 10% Fines = 39.6% LL = 20 PL = 12 PI = 8 LI = -0.3 A-4 (0), SC
								53.5		Olive with brown mottled, wet, very dense, SILTY SAND, little gravel, non-plastic (GLACIAL TILL).	WC = 10.6% Fines = 38.3% A-4 (0), SM

Remarks:
 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
 2. As-drilled boring locations and ground surface elevations were provided by HNTB.
 3. Water level measured during drilling at 6.45' bgs on 7/23/24 at 3:28, 18.7' bgs on 7/24/24 at 3:22, 19.3' bgs on 7/24/24 at 20:09. Water level measured at 23.9' bgs on 7/24/24 at 23:51 was made after the rock coring.

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

 * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

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Boring No.: BB-BSA-107

Maine Department of Transportation						Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-107																																																																																																																																																																																																																																																																																		
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<table border="1"><thead><tr><th rowspan="2">Depth (ft.)</th><th colspan="7">Sample Information</th><th rowspan="2">Graphic Log</th><th rowspan="2">Visual Description and Remarks</th><th rowspan="2">Laboratory Testing Results/AASHTO and Unified Class.</th></tr><tr><th>Sample No.</th><th>Pen./Rec. (in.)</th><th>Sample Depth (ft.)</th><th>Blows (/6 in.) Shear Strength (psf) or RQD (%)</th><th>N-uncorrected</th><th>N₆₀</th><th>Casing Blows</th><th>Elevation (ft.)</th></tr></thead><tbody><tr><td>60</td><td>16D</td><td>8/8</td><td>60.00 - 60.67</td><td>53-50/2"</td><td>R</td><td></td><td>OPEN</td><td rowspan="4">79.7</td><td rowspan="4"></td><td>Olive with brown mottled, wet, very dense, SILT, some fine round to subround gravel, trace fine to medium sand, weathered coarse gravel (GLACIAL TILL).</td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td>R-1</td><td>45.6/7.2</td><td>63.40 - 67.20</td><td>RQD = 0%</td><td></td><td></td><td>R</td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>NX</td></tr><tr><td>65</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td rowspan="4">65.9</td><td rowspan="4"></td><td>Bedrock encountered at 63.4 feet bgs Top of Bedrock Elev. 80.1 ft R1 (63.4' - 67.2'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling from 64.2 ft to 67.2; discontinuities low angle to steep dipping, close spacing, rough to very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 16% recovery 0% RQD Rock Core Rate (min:sec) 63.4 - 64.2 ft (1:09) 64.2 - 65.0 ft (1:29) 65.0 - 65.3 ft (0:41) 65.3 - 66.3 ft (1:51) 66.3 - 67.2 ft (1:13) R2 (67.2' - 68.2'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] strong, highly weathered with clay and sand infilling; discontinuities low angle dipping, close spacing, very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 17% recovery 0% RQD Rock Core Rate (min:sec) 67.2 - 68.2 ft (0:29) R3 (68.2' - 72.2): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered, occasional moderate to severe chemical weathering with sand infilling; discontinuities low angle to steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.5 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = poor 95% recovery 35% RQD Rock Core Rate (min:sec) 68.2 - 69.2 ft (1:42) 69.2 - 70.2 ft (1:59) 70.2 - 71.2 ft (2:32) 71.2 - 72.2 ft (1:28) R4 (72.2' - 77.2): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with calcite veins, strong to very strong, slightly weathered, occasional moderate to severe chemical weathering with sand and clay infilling; discontinuities low angle to</td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td>R-2</td><td>12/2.04</td><td>67.20 - 68.20</td><td>RQD = 0%</td><td></td><td></td><td></td></tr><tr><td></td><td>R-3</td><td>48/45.6</td><td>68.20 - 72.20</td><td>RQD = 35%</td><td></td><td></td><td></td></tr><tr><td>70</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td rowspan="4">65.9</td><td rowspan="4"></td><td></td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td>R-4</td><td>60/60</td><td>72.20 - 77.20</td><td>RQD = 39%</td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>75</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td rowspan="4">65.9</td><td rowspan="4"></td><td></td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>80</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td rowspan="4">65.9</td><td rowspan="4"></td><td></td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>85</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td rowspan="4">65.9</td><td rowspan="4"></td><td></td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td>90</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td rowspan="4">65.9</td><td rowspan="4"></td><td></td><td rowspan="4"></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr><tr><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr></tbody></table>												Depth (ft.)	Sample Information							Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)	60	16D	8/8	60.00 - 60.67	53-50/2"	R		OPEN	79.7		Olive with brown mottled, wet, very dense, SILT, some fine round to subround gravel, trace fine to medium sand, weathered coarse gravel (GLACIAL TILL).											R-1	45.6/7.2	63.40 - 67.20	RQD = 0%			R								NX	65								65.9		Bedrock encountered at 63.4 feet bgs Top of Bedrock Elev. 80.1 ft R1 (63.4' - 67.2'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone], strong, highly weathered with clay and sand infilling from 64.2 ft to 67.2; discontinuities low angle to steep dipping, close spacing, rough to very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 16% recovery 0% RQD Rock Core Rate (min:sec) 63.4 - 64.2 ft (1:09) 64.2 - 65.0 ft (1:29) 65.0 - 65.3 ft (0:41) 65.3 - 66.3 ft (1:51) 66.3 - 67.2 ft (1:13) R2 (67.2' - 68.2'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] strong, highly weathered with clay and sand infilling; discontinuities low angle dipping, close spacing, very rough, open, highly fractured [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. 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Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine				Boring No.: BB-BSA-107 WIN: 027176.00							
Driller: Seaboard				Elevation (ft.) 143.11				Auger ID/OD:							
Operator: Ryan H.				Datum: Maine East Zone				Sampler: Standard Split Spoon							
Logged By: D. Burgess				Rig Type: Diedrich D-50				Hammer Wt./Fall: 140lb/30in							
Date Start/Finish: 7/22/24 (21:09); 7/24/24 (0:25)				Drilling Method: SSA, Drive & Wash				Core Barrel: NX							
Boring Location: N: 482578.95, E: 1735092.78				Casing ID/OD: 4"(ID)				Water Level*: Refer to remarks note 3							
Hammer Efficiency Factor: 1.087				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>											
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt				R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140 lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person				S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected				T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test			
Depth (ft.)	Sample Information								Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.				
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)							
90									steep dipping, very close to close spacing, rough to very rough, tight to open, average 3.2 fractures per foot [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = poor 100% recovery 39% RQD Rock Core Rate (min:sec) 72.2 - 73.2 ft (2:07) 73.2 - 74.2 ft (1:35) 74.2 - 75.2 ft (1:53) 75.2 - 76.2 ft (1:32) 76.2 - 77.2 ft (1:30) Bottom of Exploration at 77.2 feet below ground surface. Boring backfilled with bentonite chips in the rock core socket, drill cuttings and gravel to bottom of pavement and patched with cold patch asphalt.						
120															
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by HNTB. 3. Water level measured during drilling at 6.45' bgs on 7/23/24 at 3:28, 18.7' bgs on 7/24/24 at 3:22, 19.3' bgs on 7/24/24 at 20:09. Water level measured at 23.9' bgs on 7/24/24 at 23:51 was made after the rock coring.															
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.										Page 4 of 4					
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.										Boring No.: BB-BSA-107					

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-108				
WIN: 027176.00										
Driller: Seaboard		Elevation (ft.): 129.45		Auger ID/OD:						
Operator: Kevin Hanscom		Datum: Maine East Zone		Sampler: Standard Split Spoon						
Logged By: Lina-Maria Pua		Rig Type: Diedrich D-50		Hammer Wt./Fall: 140 lbs/30 in						
Date Start/Finish: 05/07/24 (21:55); 05/07/24 (23:30)		Drilling Method: SSA, Cased Wash		Core Barrel: NX						
Boring Location: N: 482749.52, E: 1735322.13		Casing ID/OD: 3 in/3.25 in		Water Level*: 4.8 ft on 05/07/24 at 22:20						
Hammer Efficiency Factor: 1.066		Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>								
Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person S _u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S _u (lab) = Lab Vane Undrained Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N ₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected T _v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test										
Depth (ft.)	Sample Information							Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.	
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows			
0							SSA	128.9	7.5" Asphalt Pavement	MC = 8.0% Fines = 28.5% A-2-4 (0), SM
	1D	24/16	1.00 - 3.00	22-18-16-20	34	60			Brown to yellow, dry, very dense, fine to coarse SAND, some silt, little fine gravel (FILL).	
	2D	24/9	3.00 - 5.00	15-14-24-16	38	68			2DA To 2 in: Brown to yellow, dry, very dense, fine to coarse SAND, some silt, little fine gravel (FILL).	
5	3D	24/12	5.00 - 7.00	12-12-12-50/2"	24	43			2DB Bottom 7 in: Grey, dry, very dense, GRAVEL, some sand, little silt (GRAVEL)	
	R1	60/59	6.70 - 11.70	RQD = 59%					Brown, wet, dense, GRAVEL, some sand, little silt (GRAVEL). Grey angular GRAVEL with some sand and little silt in the tip of the split spoon.	
							NX			
10									Bedrock encountered at 6.7 feet bgs Top of Bedrock at Elev. 122.8 ft	
	R2	12/11	11.70 - 12.70	RQD = 40%					R1 (6.7'-11.1'): Grey, very fine to fine grained, METAWACKE [metasandstone] with frequent calcite veins, very to extremely strong, thinly laminated, slightly weathered; discontinuities moderate to steep dipping, close to moderately close spacing, rough to polished, open. average 2.6 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].	
	R3	24/21	12.70 - 14.70	RQD = 19%					Rock Mass Quality = fair 98% Recovery Rock Core Rate (min:sec) 6.7-7.7 ft (2:33) 7.7-8.7 ft (2:46) 8.7-9.7 ft (3:19) 9.7-10.7 ft (2:51) 10.7-11.7 ft (3:17)	
15	R4	24/23	14.70 - 16.70	RQD = 37%					R2 (11.1'-12.7'): Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open. average 1.0 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].	
20									Rock Mass Quality = poor 92% Recovery Rock Core Rate (min:sec) 11.7-12.7 ft (3:07)	
									R3 (12.7'-14.7'): Grey, very fine to fine grained, METAWACKE [metasandstone] with some calcite veins, extremely strong, thinly laminated, fresh to slightly weathered; discontinuities low angle to steep dipping, very close to close spacing, planar to stepped, rough to smooth, open. average 2.5 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION].	
25									Rock Mass Quality = very poor 88% Recovery Rock Core Rate (min:sec) 12.7-13.7 ft (2:04) 13.7-14.7 ft (3:25)	
30									R4 (14.7'-16.7'): Grey, very fine to fine grained, METAWACKE	
Remarks: 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023. 2. As-drilled boring locations and ground surface elevations were provided by MaineDOT. 3. Water level reading taken on 5/7/24 at 22:20 was made before the start of rock coring with bottom of casing at 6.7 ft bgs.										
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.								Page 1 of 2		
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.								Boring No.: BB-BSA-108		

[illegible]

<div>Maine Department of Transportation</div> <div>Soil/Rock Exploration Log</div> <div>US CUSTOMARY UNITS</div>				<div>Project: MaineDOT I-95 Bridges Over Stillwater Avenue</div> <div>Location: Bangor, Maine</div>				<div>Boring No.: BB-BSA-109</div> <div>WIN: 027176.00</div>																																																																																																																																																																																																																																												
Driller: Seaboard			Elevation (ft.): 126.99			Auger ID/OD: 4.0 in/4.5 in																																																																																																																																																																																																																																														
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Date Start/Finish: 05/07/24 (1:20); 05/07/24 (2:30)			Drilling Method: Hollow Stem Augers			Core Barrel: NX																																																																																																																																																																																																																																														
Boring Location: N: 482636.37, E: 1735255.48			Casing ID/OD:			Water Level*: Not Measured																																																																																																																																																																																																																																														
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<div>Definitions:</div> <div>D = Split Spoon Sample</div> <div>MD = Unsuccessful Split Spoon Sample Attempt</div> <div>U = Thin Wall Tube Sample</div> <div>MU = Unsuccessful Thin Wall Tube Sample Attempt</div> <div>V = Field Vane Shear Test, PP = Pocket Penetrometer</div> <div>MV = Unsuccessful Field Vane Shear Test Attempt</div>			<div>R = Rock Core Sample</div> <div>SSA = Solid Stem Auger</div> <div>HSA = Hollow Stem Auger</div> <div>RC = Roller Cone</div> <div>WOH = Weight of 140lb. Hammer</div> <div>WOR/C = Weight of Rods or Casing</div> <div>WO1P = Weight of One Person</div>			<div>S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf)</div> <div>S_{u(lab)} = Lab Vane Undrained Shear Strength (psf)</div> <div>q_p = Unconfined Compressive Strength (ksf)</div> <div>N-uncorrected = Raw Field SPT N-value</div> <div>Hammer Efficiency Factor = Rig Specific Annual Calibration Value</div> <div>N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency</div> <div>N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected</div>			<div>T_v = Pocket Torvane Shear Strength (psf)</div> <div>WC = Water Content, percent</div> <div>LL = Liquid Limit</div> <div>PL = Plastic Limit</div> <div>PI = Plasticity Index</div> <div>G = Grain Size Analysis</div> <div>C = Consolidation Test</div>																																																																																																																																																																																																																																											
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Driller: Seaboard				Elevation (ft.) 127.53				Auger ID/OD:							
Operator: Kevin Hanscom				Datum: Maine East Zone				Sampler: Standard Split Spoon							
Logged By: Lina-Maria Pua				Rig Type: Diedrich D-50				Hammer Wt./Fall: 140 lbs/30 in							
Date Start/Finish: 05/08/24 (20:09); 05/08/24 (21:22)				Drilling Method: SSA, Cased Wash				Core Barrel: NX							
Boring Location: N: 482660.73, E: 1735292.34				Casing ID/OD: 3.0 in/3.25 in				Water Level*: 3.1 ft on 05/08/24 at 20:34							
Hammer Efficiency Factor: 1.066				Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>											
<div>Definitions:</div> <div>D = Split Spoon Sample</div> <div>MD = Unsuccessful Split Spoon Sample Attempt</div> <div>U = Thin Wall Tube Sample</div> <div>MU = Unsuccessful Thin Wall Tube Sample Attempt</div> <div>V = Field Vane Shear Test, PP = Pocket Penetrometer</div> <div>MV = Unsuccessful Field Vane Shear Test Attempt</div>				<div>R = Rock Core Sample</div> <div>SSA = Solid Stem Auger</div> <div>HSA = Hollow Stem Auger</div> <div>RC = Roller Cone</div> <div>WOH = Weight of 140lb. Hammer</div> <div>WOR/C = Weight of Rods or Casing</div> <div>WO1P = Weight of One Person</div>				<div>S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf)</div> <div>S_u(lab) = Lab Vane Undrained Shear Strength (psf)</div> <div>q₀ = Unconfined Compressive Strength (ksf)</div> <div>N_u-uncorrected = Raw Field SPT N-value</div> <div>Hammer Efficiency Factor = Rig Specific Annual Calibration Value</div> <div>N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency</div> <div>N₆₀ = (Hammer Efficiency Factor/60%)*N_u-uncorrected</div>				<div>T_v = Pocket Torvane Shear Strength (psf)</div> <div>WC = Water Content, percent</div> <div>LL = Liquid Limit</div> <div>PL = Plastic Limit</div> <div>PI = Plasticity Index</div> <div>G = Grain Size Analysis</div> <div>C = Consolidation Test</div>			
Sample Information												Graphic Log		Laboratory Testing Results/ AASHTO and Unified Class.	
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing	Blows	Elevation (ft.)						
0								SSA	126.9	Asphalt Pavement		0-6			
	1D	24/11	1.00 - 3.00	16-21-16-20	37	66				Brown, dry, dense, Silty GRAVEL, little sand (FILL).					
	2D	24/6	3.00 - 5.00	10-8-9-21	17	30				Grey, wet, medium dense, Silty angular GRAVEL, trace sand (FILL).					
5	3D	3/3	5.00 - 5.25	50/3"	R			NX	122.2	Grey, wet, very dense, angular GRAVEL, some silt, trace sand, poorly-graded (FILL).		5-13			
	R1	60/57	5.30 - 10.30	RQD = 52%						Bedrock encountered at 5.3 feet bgs Top of Bedrock at Elev. 122.2 ft R1 (5.3'-10.3'): Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, medium strong, thinly laminated, fresh; discontinuities horizontal to steep dipping, close to moderately close spacing, stepped, smooth to polished, open. average 1.0 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 95% Recovery Rock Core Rate (min:sec) 5.3-6.3 ft (2:20) 6.3-7.3 ft (2:31) 7.3-8.3 ft (2:21) 8.3-9.3 ft (2:54) 9.3-10.3 ft (3:10)					
10	R2	60/60	10.30 - 15.30	RQD = 72%						R2 (10.3'-15.3'): Grey, very fine grained, METAWACKE [metasandstone] with frequent thick and thin calcite veins, very to extremely strong, thinly laminated, fresh; discontinuities steep dipping, close to wide spacing, stepped, smooth, open. average 0.8 fractures per foot [MEDIUM BEDDEED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = fair 100% Recovery Rock Core Rate (min:sec) 10.3-11.3 ft (3:15) 11.3-12.3 ft (2:42) 12.3-13.3 ft (3:30) 13.3-14.3 ft (2:58) 14.3-15.3 ft (3:40)		15-30			
15									112.2						
20															
25															
30															
Remarks:															
1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.															
2. As-drilled boring locations and ground surface elevations were provided by MaineDOT.															
3. Water level reading taken on 5/8/24 at 20:34 was made before the start of rock coring with bottom of casing at 5.3 ft bgs.															
Stratification lines represent approximate boundaries between soil types; transitions may be gradual.												Page 1 of 1			
* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.												Boring No.: BB-BSA-110			

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS				Project: MaineDOT I-95 Bridges Over Stillwater Avenue Location: Bangor, Maine		Boring No.: BB-BSA-111 WIN: 027176.00					
Driller: Seaboard			Elevation (ft.): 148.27		Auger ID/OD:						
Operator: Ryan H.			Datum: Maine East Zone		Sampler: Standard Split Spoon						
Logged By: D. Burgess			Rig Type: Diedrich D-50		Hammer Wt./Fall: 140lb/30in						
Date Start/Finish: 7/25/24 (0:44); 7/25/24 (4:25)			Drilling Method: SSA, Cased Wash		Core Barrel: NX						
Boring Location: N: 482728.68, E: 1735418.07			Casing ID/OD: 4" (ID)		Water Level*: 14.75' 4:07 7/25/24						
Hammer Efficiency Factor: 1.087			Hammer Type: Automatic <input checked="" type="checkbox"/> Hydraulic <input type="checkbox"/> Rope & Cathead <input type="checkbox"/>								
<div style="display: flex; justify-content: space-between; font-size: 0.8em;"> <div> Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample Attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample Attempt V = Field Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Field Vane Shear Test Attempt </div> <div> R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = Weight of 140lb. Hammer WOR/C = Weight of Rods or Casing WO1P = Weight of One Person </div> <div> S_u = Peak/Remolded Field Vane Undrained Shear Strength (psf) S_{u(lab)} = Lab Vane Undrained Shear Strength (psf) q_p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw Field SPT N-value Hammer Efficiency Factor = Rig Specific Annual Calibration Value N₆₀ = SPT N-uncorrected Corrected for Hammer Efficiency N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected </div> <div> T_v = Pocket Torvane Shear Strength (psf) WC = Water Content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test </div> </div>											
Depth (ft.)	Sample Information							Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows				
0	1D	24/9	0.60 - 2.60	9-11-9-11	20	36	SSA	147.7		7" Asphalt pavement	Fines = 13.5% A-1-a (0), GM-SM
										Olive brown, moist, dense, fine to coarse SAND AND fine to coarse GRAVEL, little silt (FILL).	
	2D	24/19	3.00 - 5.00	11-20-22-16	42	76				Olive with brown, moist, hard, SILT, some round to subround gravel, little fine to medium sand, weathered coarse gravel, non-plastic (FILL).	Fines = 61.6% A-4 (0), ML
5	3D	13.5/12	5.00 - 6.13	13-21-50/1.5"	R		165			Light olive brown, moist, hard, SANDY SILT, trace gravel, non-plastic (FILL).	
	4D	24/12	7.00 - 9.00	12-26-20-13	46	83	47			Fractured rock fragments, trace organics (roots) (FILL).	
							88				
							47				
10	5D	24/22	10.00 - 12.00	7-9-11-15	20	36	59	138.8		Olive with dark grey, moist, hard, SANDY SILT, trace gravel, non-plastic (FILL).	
							73			Olive with orange mottled, moist, hard, CLAY, trace sand, medium plasticity (CLAY). Pp 3.0 to 3.5 tsf	WC = 21% Fines = 99.4% LL = 32 PL = 17 PI = 15 LI = 0.3
							146				
							210				
							119				
15	6D	24/13	15.00 - 17.00	19-24-16-45	40	72	71	134.8		Grayish brown, wet, very dense, SAND and GRAVEL, little silt, and fractured rock fragments (GLACIAL TILL).	WC = 13.4% Fines = 20.0% A-1-b (0), SM/GM
							95				
							208				
							NX				
20	R-1	60/40.8	19.00 - 24.00	RQD = 15%				130.5		Bedrock encountered at 17.8 feet bgs Top of Bedrock at Elev. 130.5 ft R1 (19.0' - 24.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, strong to very strong, slightly weathered with signs of chemical weathering; discontinuities low angle to steep dipping, close to very close spacing, rough to very rough, open to tight, highly fractured average from 19 ft to 21.3 ft [MEDIUM BEDDED FACIES, PENOBSCOT RIVER MEMBER, BANGOR FORMATION]. Rock Mass Quality = very poor 68% recovery 15% RQD	
25	R-2	60/60	24.00 - 29.00	RQD = 60%					Rock Core Rate (min:sec) 19.0 - 20.0 ft (2:11) 20.0 - 21.0 ft (1:11) 21.0 - 22.0 ft (1:55) 22.0 - 23.0 ft (1:49) 23.0 - 24.0 ft (1:56) R2 (24.0' - 29.0'): Grey, very fine grained, thinly to very thinly bedded, METAWACKE [metasandstone] with frequent calcite veins, very strong to strong, fresh; discontinuities low angle dipping, very		
30								119.3			

Remarks:
 1. Hammer Efficiency factor provided by S.W. Cole and taken from "2023PA00074 - SW Cole - SPT Report" by GRL Engineers Inc., dated 11/10/2023.
 2. As-drilled boring locations and ground surface elevations were provided by HNTB.
 3. Water level reading taken on 7/25/24 at 4:07 am was made after the rock coring.

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

 * Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

Page 1 of 2

Boring No.: BB-BSA-111

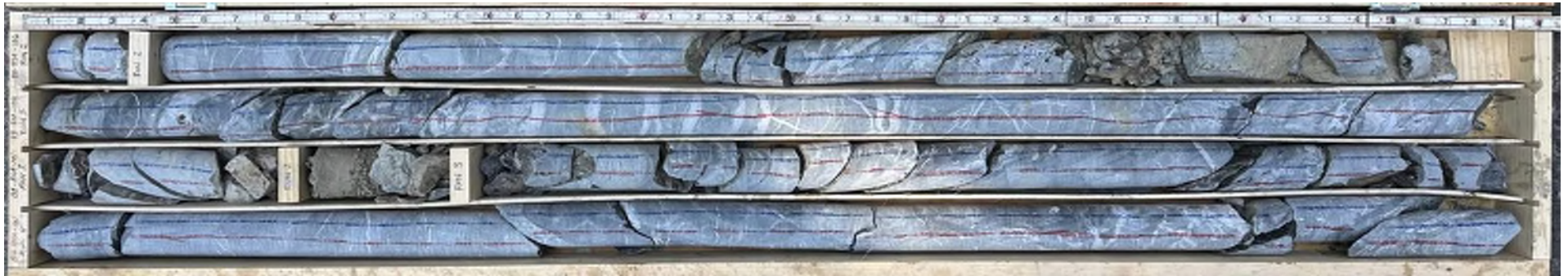
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APPENDIX B

Rock Core Photographs

APPENDIX B
ROCK CORE PHOTOGRAPHS
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE
BANGOR, MAINE
MAINEDOT WIN #027176.00

Boring	Run	Depth Below Surface		Recovery			RQD		Rock Type	Box Row	Date Cored
		Feet		Feet		%	Feet	%			
BB-BSA-101	R1	31.5	- 32.4	0.8	/ 0.9	89	0.0 / 0.9	0	Metawacke	3	7/29/2024
	R2	32.4	- 32.9	0.5	/ 0.5	100	0.0 / 0.5	0	Metawacke	3	7/29/2024
	R3	32.9	- 36.5	3.6	/ 3.6	100	0.5 / 3.6	14	Metawacke	3	7/29/2024
	R4	36.5	- 41.5	5.0	/ 5.0	100	3.0 / 5.0	60	Metawacke	4	7/29/2024
BB-BSA-106	R1	63.8	- 64.8	0.3	/ 1.0	30	0 / 0.3	0	Metawacke	1	7/28/2024
	R2	64.8	- 69.1	4.3	/ 4.3	100	2 / 4.3	47	Metawacke	1	7/28/2024
	R3	69.1	- 74.1	5.0	/ 5.0	100	3.6 / 5.0	62	Metawacke	2	7/28/2024



Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN
 Checked By: LMP
 Reviewed By: JDL

APPENDIX B
ROCK CORE PHOTOGRAPHS
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE
BANGOR, MAINE
MAINEDOT WIN #027176.00

Boring	Run	Depth Below Surface	Recovery		RQD		Rock Type	Box Row	Date Cored
		Feet	Feet	%	Feet	%			
BB-BSA-102	R1	12.2 - 17.2	4.50 / 5.0	90	3.7 / 5.0	73	Metawacke	3	5/8/2024
	R2	17.2 - 22.2	4.9 / 5.0	98	4.9 / 5.0	98	Metawacke	4	5/8/2024
BB-BSA-108	R1	6.7 - 11.7	4.9 / 5.0	98	3.0 / 5.0	59	Metawacke	1	5/7/2024
	R2	11.7 - 12.7	0.9 / 1.0	92	0.4 / 1.0	40	Metawacke	2	5/7/2024
	R3	12.7 - 14.7	1.76 / 2.0	88	0.38 / 2.0	19	Metawacke	2	5/7/2024
	R4	14.7 - 16.7	1.92 / 2.0	96	0.74 / 2.0	37	Metawacke	2	5/7/2024



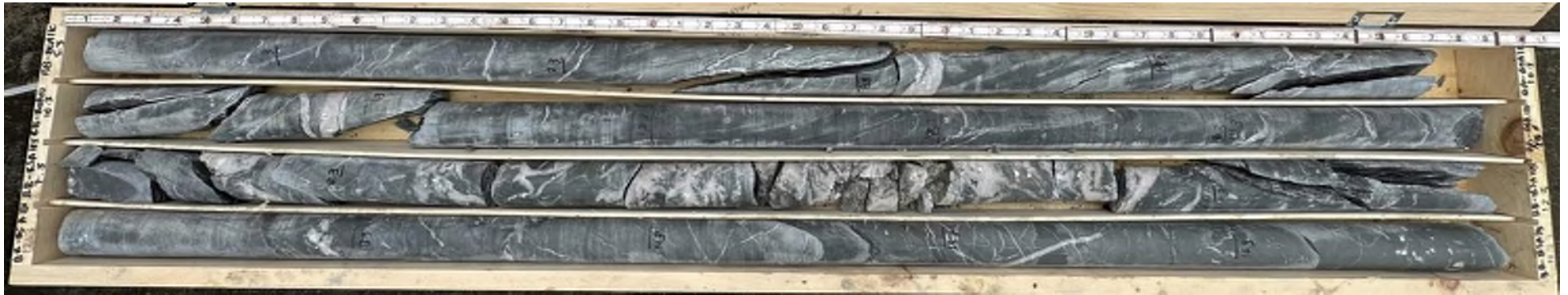
Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

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 Checked By: LMP
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APPENDIX B
ROCK CORE PHOTOGRAPHS
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE
BANGOR, MAINE
MAINEDOT WIN #027176.00

Boring	Run	Depth Below Surface		Recovery		RQD		Rock Type	Box Row	Date Cored	
		Feet		Feet	%	Feet	%				
BB-BSA-103	R1	7.2	- 12.2	5.0	/ 5.0	100	1.6 / 5.0	31	Metawacke	3	5/8/2024
	R2	12.2	- 17.2	5.0	/ 5.0	100	3.6 / 5.0	71	Metawacke	4	5/8/2024
BB-BSA-110	R1	5.3	- 10.3	4.8	/ 5.0	95	2.6 / 5.0	52	Metawacke	1	5/8/2024
	R2	10.3	- 15.3	5.0	/ 5.0	100	3.6 / 5.0	72	Metawacke	2	5/8/2024



Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

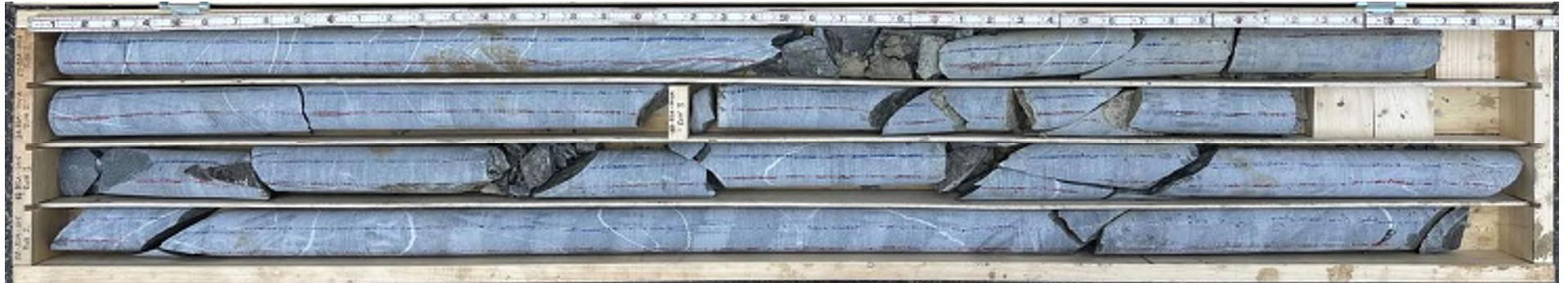
Prepared By: RJN

Checked By: LMP

Reviewed By: JDL

APPENDIX B
ROCK CORE PHOTOGRAPHS
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE
BANGOR, MAINE
MAINEDOT WIN #027176.00

Boring	Run	Depth Below Surface	Recovery			RQD		Rock Type	Box Row	Date Cored
		Feet	Feet		%	Feet	%			
BB-BSA-104A	R1	21.0 - 26.0	4.8 / 5.0		95	2.8 / 5.0	56	Metawacke	1	7/30/2024
	R2	26.0 - 28.8	2.1 / 2.8		75	1.7 / 2.8	61	Metawacke	2	7/30/2024
	R3	28.8 - 31.0	2.0 / 2.2		91	0.5 / 2.2	23	Metawacke	2	7/30/2024
BB-BSA-105	R1	26.4 - 31.4	5.0 / 5.0		100	1.5 / 5.0	30	Metawacke	3	7/31/2024
	R2	31.4 - 36.2	4.8 / 4.8		100	3.6 / 4.8	75	Metawacke	4	7/31/2024



Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN

Checked By: LMP

Reviewed By: JDL

APPENDIX B
ROCK CORE PHOTOGRAPHS
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE
BANGOR, MAINE
MAINEDOT WIN #027176.00

Boring	Run	Depth Below Surface	Recovery			RQD		Rock Type	Box Row	Date Cored
		Feet	Feet		%	Feet	%			
BB-BSA-107	R1	63.4 - 67.2	0.6 / 3.8		23	0.0 / 3.8	0	Metawacke	1	7/23/2024
	R2	67.2 - 68.2	0.2 / 1.0		17	0.0 / 1.0	0	Metawacke	1	7/24/2024
	R3	68.2 - 72.2	3.8 / 4.0		95	1.4 / 4.0	35	Metawacke	1	7/24/2024
	R4	72.2 - 77.2	5.0 / 5.0		100	2.0 / 5.0	39	Metawacke	2	7/24/2024
BB-BSA-111	R1	19.0 - 24.0	3.4 / 5.0		68	0.8 / 5.0	15	Metawacke	3	7/24/2024
	R2	24.0 - 29.0	5.0 / 5.0		100	3.0 / 5.0	60	Metawacke	4	7/24/2024



Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN

Checked By: LMP

Reviewed By: JDL

APPENDIX B
ROCK CORE PHOTOGRAPHS
MAINEDOT I-95 BRIDGE OVER STILLWATER AVENUE
BANGOR, MAINE
MAINEDOT WIN #027176.00

Boring	Run	Depth Below Surface	Recovery		RQD		Rock Type	Box Row	Date Cored
		Feet	Feet	%	Feet	%			
BB-BSA109A	R1	4.0 - 8.8	4.3 / 4.8	90	1.6 / 4.8	33	Metawacke	2	5/7/2024
	R2	8.8 - 13.9	4.8 / 5.1	93	2.5 / 5.1	49	Metawacke	2,3	5/7/2024



- Notes:
- 1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
 - 2. Top of each core run is on the left and increases with depth to the right.

Prepared By: RJN
Checked By: LMP
Reviewed By: JDL

APPENDIX C

Laboratory Test Results

Client:	WSP USA, Inc.	Project No:	GTX-319180
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH		
Boring ID: ---	Sample Type: ---	Tested By:	ajl
Sample ID: ---	Test Date: 08/12/24	Checked By:	ank
Depth : ---	Test Id: 780399		

Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
BB-BSA-101	4D	7-9 ft	Moist, olive brown sandy silt with gravel	11.1
BB-BSA-101	6D	15-17 ft	Moist, olive brown silty sand with gravel	10.7
BB-BSA-101	8D	25-27 ft	Moist, dark grayish brown silty gravel with sand	9.6
BB-BSA-104	4D	7-9 ft	Moist, dark grayish brown silty sand with gravel	6.5
BB-BSA-104	5D	10-12 ft	Moist, grayish brown sandy silt	11.1
BB-BSA-104	7D	20-22 ft	Moist, greenish gray silt with sand	16.4
BB-BSA-105	6D	15-17 ft	Moist, grayish brown sandy silt	20.5
BB-BSA-105	7D	20-22ft	Moist, olive brown silty sand with gravel	11.7
BB-BSA-106	14D	55-57 ft	Moist, gray silty sand	46.5
BB-BSA-107	6D	10.7-12.7 ft	Moist, olive brown silt with sand	14.7

Notes: Temperature of Drying : 110° Celsius



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	08/14/24
Depth :	---	Test Id:	780423
		Tested By:	ajl
		Checked By:	ank

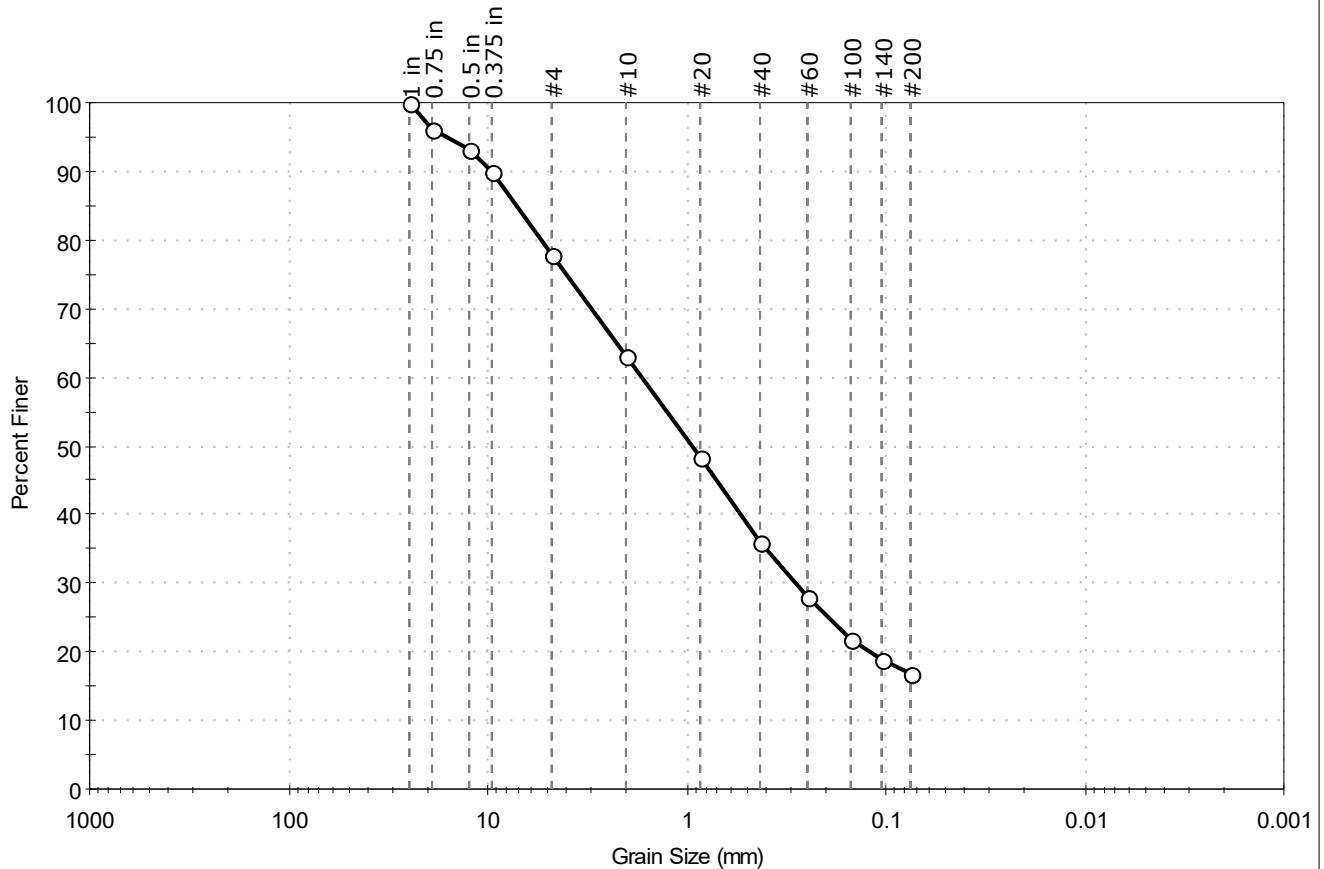
Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content,%
BB-BSA-107	15D	55-57 ft	Moist, grayish brown silty sand with gravel	10.6
BB-BSA-111	6D	15-17 ft	Moist, grayish brown silty sand with gravel	13.4

Notes: Temperature of Drying : 110° Celsius

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-101	Sample Type: Jar
Sample ID: 1D	Test Date: 08/19/24
Depth: 0.7-2.7 ft	Test Id: 780401
Test Comment: ---	Tested By: ajl
Visual Description: Moist, light olive brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	22.0	61.2	16.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	93		
0.375 in	9.50	90		
#4	4.75	78		
#10	2.00	63		
#20	0.85	48		
#40	0.42	36		
#60	0.25	28		
#100	0.15	22		
#140	0.11	19		
#200	0.075	17		

Coefficients

$D_{85} = 7.1397 \text{ mm}$ $D_{30} = 0.2832 \text{ mm}$
 $D_{60} = 1.6778 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.9366 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

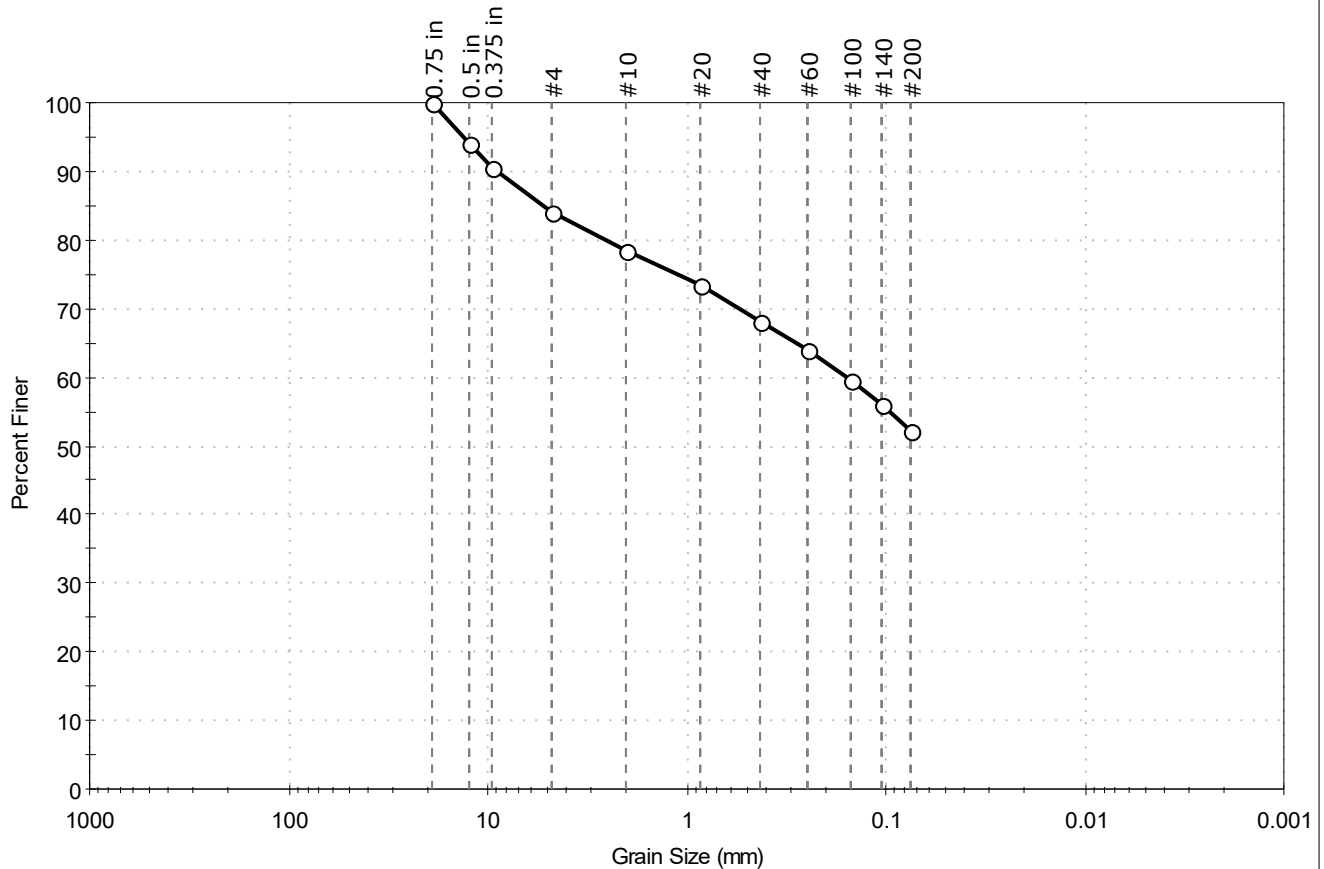
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-101	Sample Type:	Jar
Sample ID:	4D	Test Date:	08/19/24
Depth :	7-9 ft	Test Id:	780402
Test Comment:	---		
Visual Description:	Moist, olive brown sandy silt with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	15.8	32.0	52.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	94		
0.375 in	9.50	91		
#4	4.75	84		
#10	2.00	79		
#20	0.85	73		
#40	0.42	68		
#60	0.25	64		
#100	0.15	59		
#140	0.11	56		
#200	0.075	52		

Coefficients

$D_{85} = 5.2031 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.1591 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

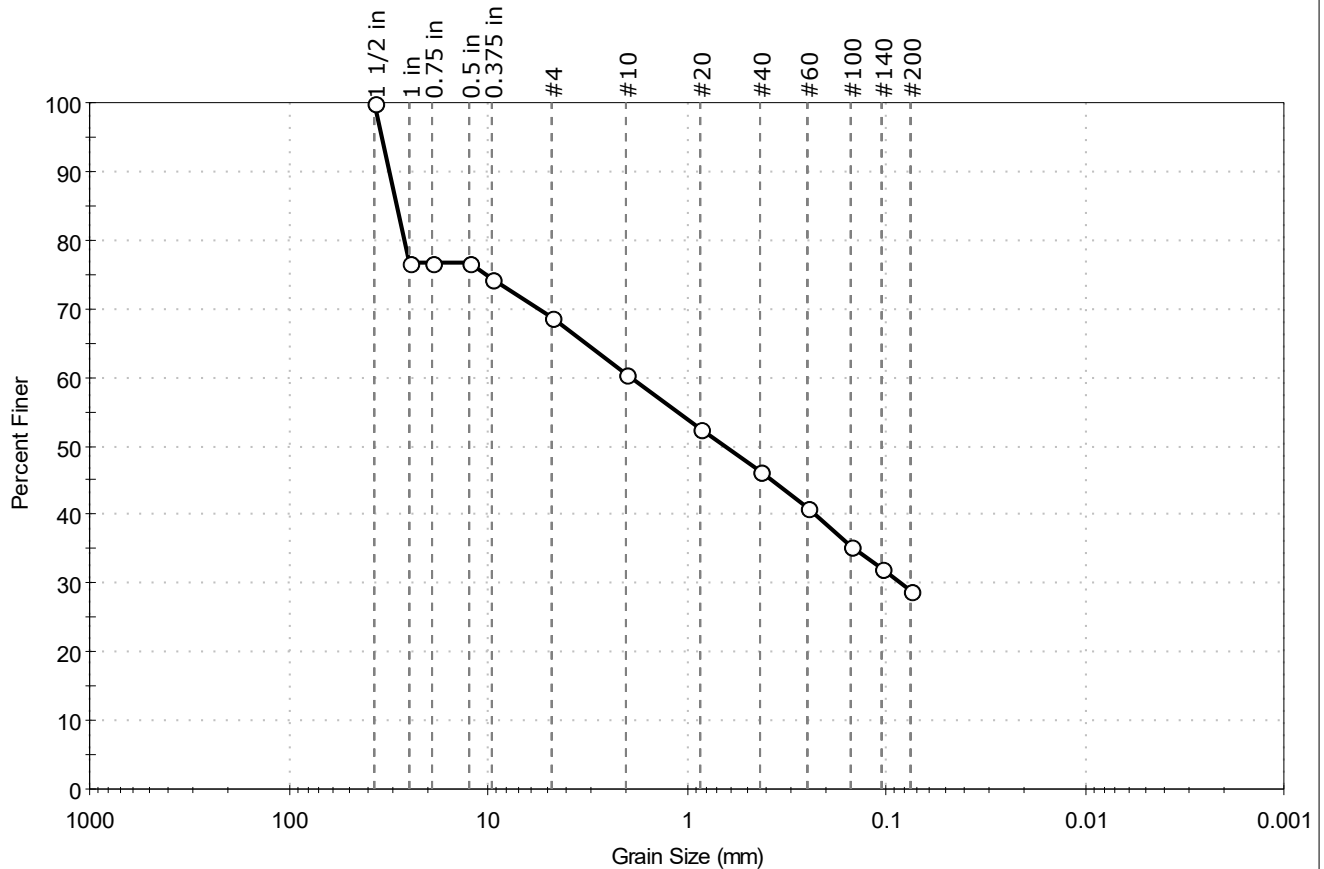
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.
 Project: MaineDOT I-95 Bridge over Stillwater
 Location: Merrimack, NH
 Project No: GTX-319180
 Boring ID: BB-BSA-101
 Sample Type: Jar
 Tested By: ajl
 Sample ID: 6D
 Test Date: 08/16/24
 Checked By: ank
 Depth: 15-17 ft
 Test Id: 780403
 Test Comment: ---
 Visual Description: Moist, olive brown silty sand with gravel
 Sample Comment: ---

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	31.2	40.0	28.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2 in	37.50	100		
1 in	25.00	77		
0.75 in	19.00	77		
0.5 in	12.50	77		
0.375 in	9.50	74		
#4	4.75	69		
#10	2.00	61		
#20	0.85	53		
#40	0.42	46		
#60	0.25	41		
#100	0.15	35		
#140	0.11	32		
#200	0.075	29		

Coefficients

D₈₅ = 28.9113 mm D₃₀ = 0.0851 mm
 D₆₀ = 1.8753 mm D₁₅ = N/A
 D₅₀ = 0.6407 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM N/A

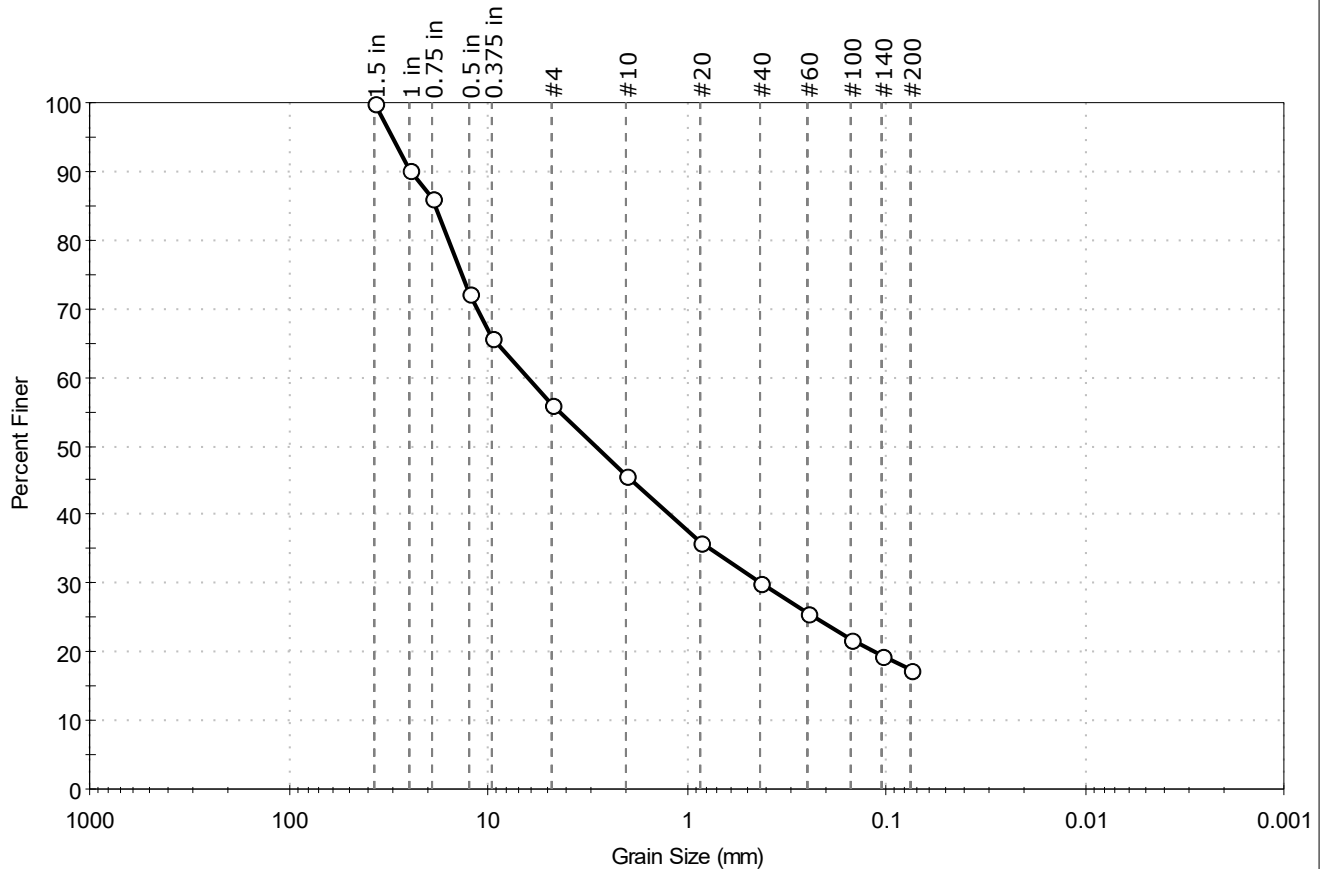
AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-101	Sample Type:	Jar
Sample ID:	8D	Test Date:	08/19/24
Depth :	25-27 ft	Test Id:	780404
Test Comment:	---		
Visual Description:	Moist, dark grayish brown silty gravel with sand		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	43.8	38.7	17.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	90		
0.75 in	19.00	86		
0.5 in	12.50	72		
0.375 in	9.50	66		
#4	4.75	56		
#10	2.00	46		
#20	0.85	36		
#40	0.42	30		
#60	0.25	26		
#100	0.15	22		
#140	0.11	19		
#200	0.075	18		

Coefficients

$D_{85} = 18.3264 \text{ mm}$ $D_{30} = 0.4200 \text{ mm}$
 $D_{60} = 6.2648 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 2.8644 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

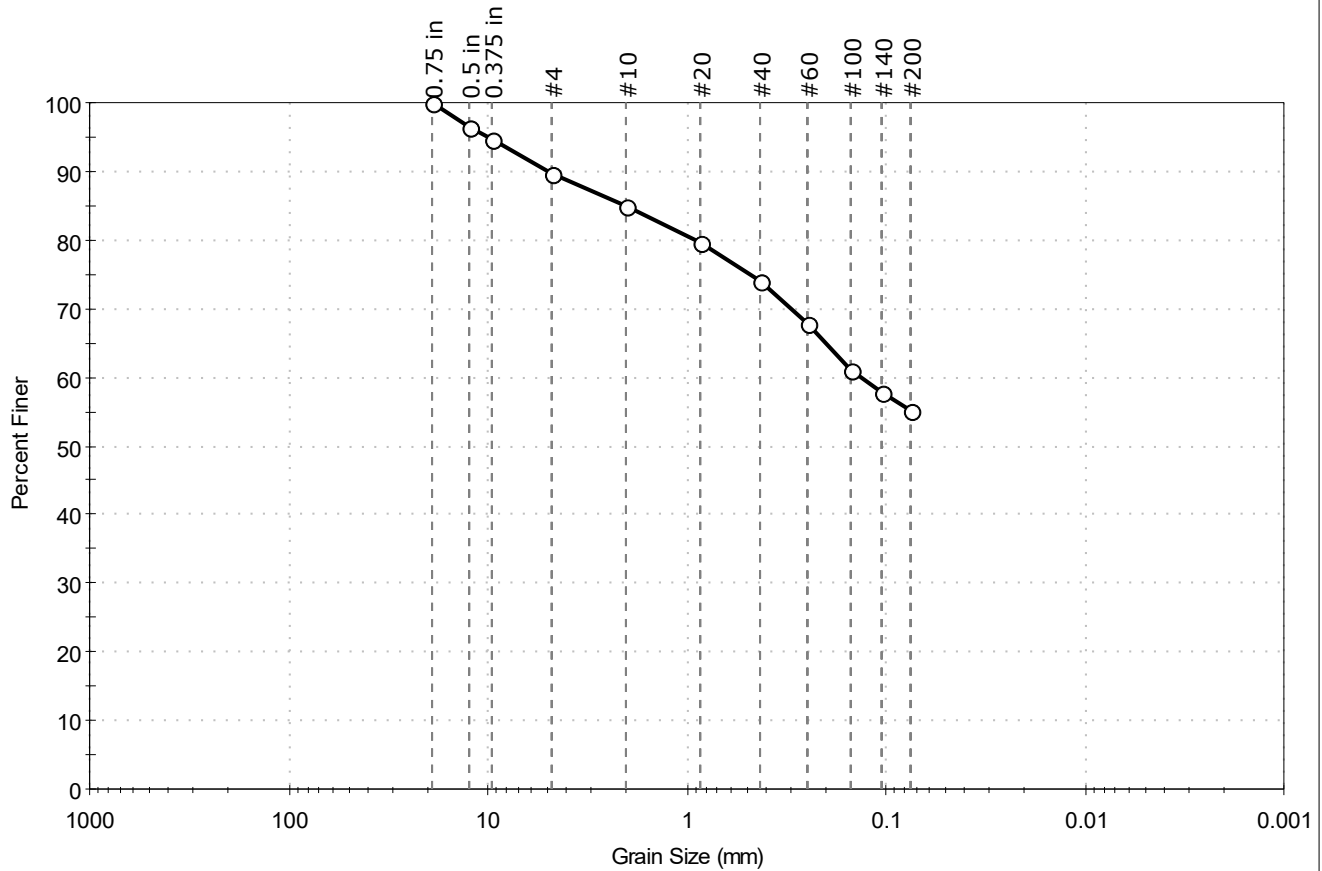
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-104	Sample Type:	Jar
Sample ID:	2D	Test Date:	08/19/24
Depth :	2.8-4.8 ft	Test Id:	780405
Test Comment:	---		
Visual Description:	Moist, dark grayish brown sandy silt		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.4	34.3	55.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	96		
0.375 in	9.50	95		
#4	4.75	90		
#10	2.00	85		
#20	0.85	80		
#40	0.42	74		
#60	0.25	68		
#100	0.15	61		
#140	0.11	58		
#200	0.075	55		

Coefficients

D ₈₅ = 1.9913 mm	D ₃₀ = N/A
D ₆₀ = 0.1326 mm	D ₁₅ = N/A
D ₅₀ = N/A	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

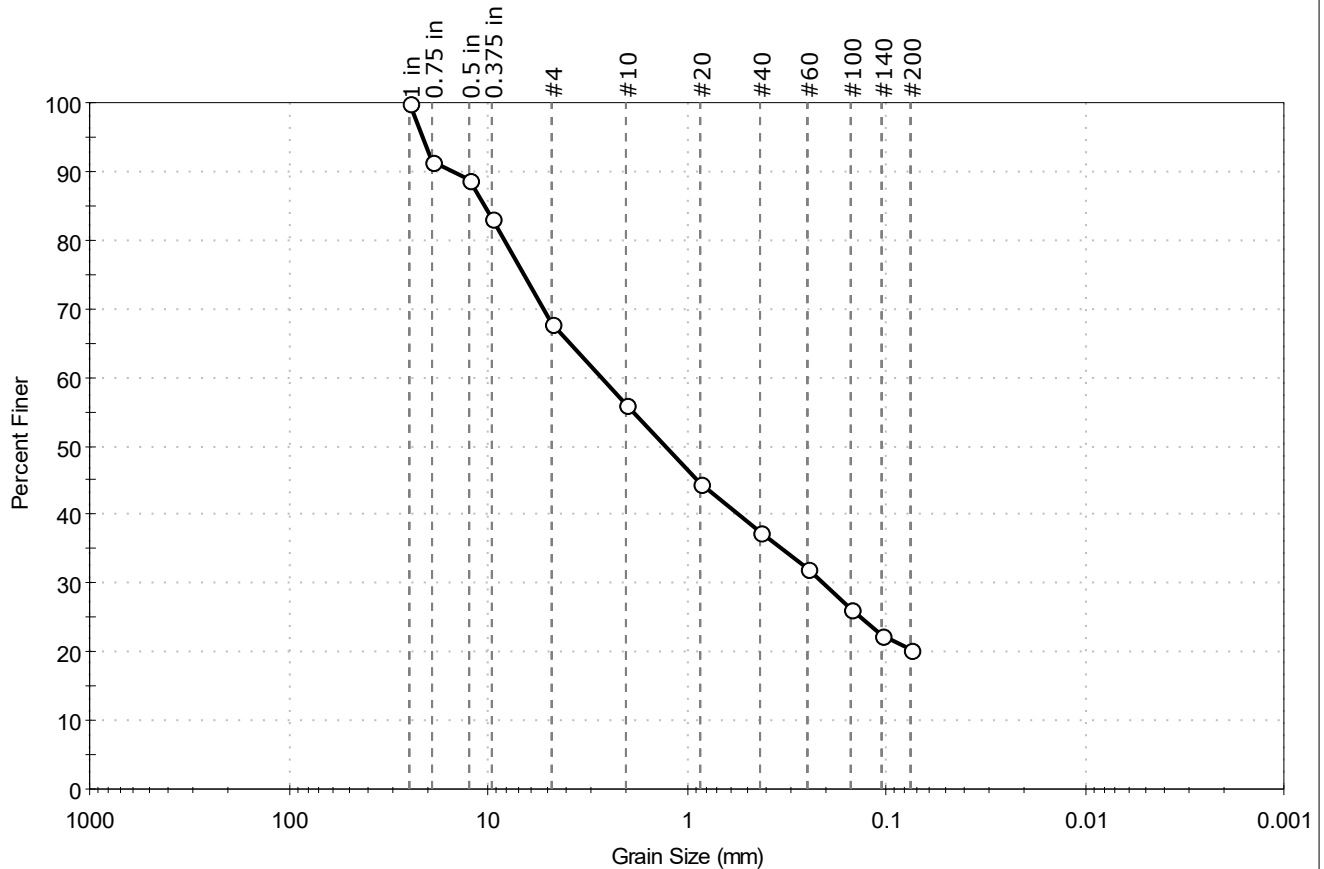
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-104	Sample Type: Jar
Sample ID: 4D	Test Date: 08/19/24
Depth: 7-9 ft	Test Id: 780406
Test Comment: ---	Tested By: ajl
Visual Description: Moist, dark grayish brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	32.0	47.6	20.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	92		
0.5 in	12.50	89		
0.375 in	9.50	83		
#4	4.75	68		
#10	2.00	56		
#20	0.85	45		
#40	0.42	37		
#60	0.25	32		
#100	0.15	26		
#140	0.11	23		
#200	0.075	20		

Coefficients

$D_{85} = 10.3977$ mm $D_{30} = 0.2076$ mm
 $D_{60} = 2.6769$ mm $D_{15} = \text{N/A}$
 $D_{50} = 1.2727$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

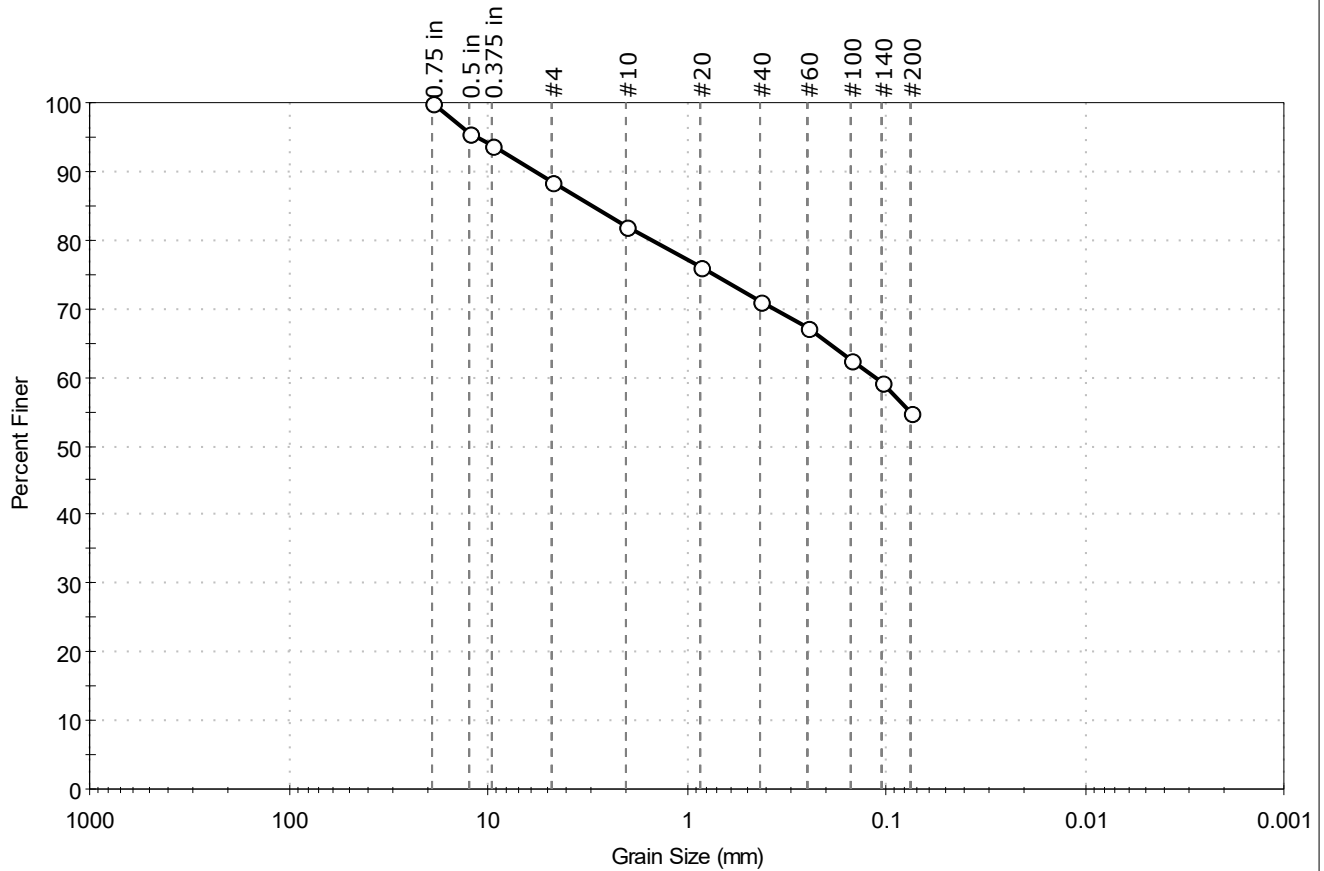
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-104	Sample Type: Jar
Sample ID: 5D	Test Date: 08/19/24
Depth: 10-12 ft	Test Id: 780407
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown sandy silt	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	11.6	33.5	54.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	96		
0.375 in	9.50	94		
#4	4.75	88		
#10	2.00	82		
#20	0.85	76		
#40	0.42	71		
#60	0.25	67		
#100	0.15	63		
#140	0.11	59		
#200	0.075	55		

Coefficients

$D_{85} = 3.0173 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.1137 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

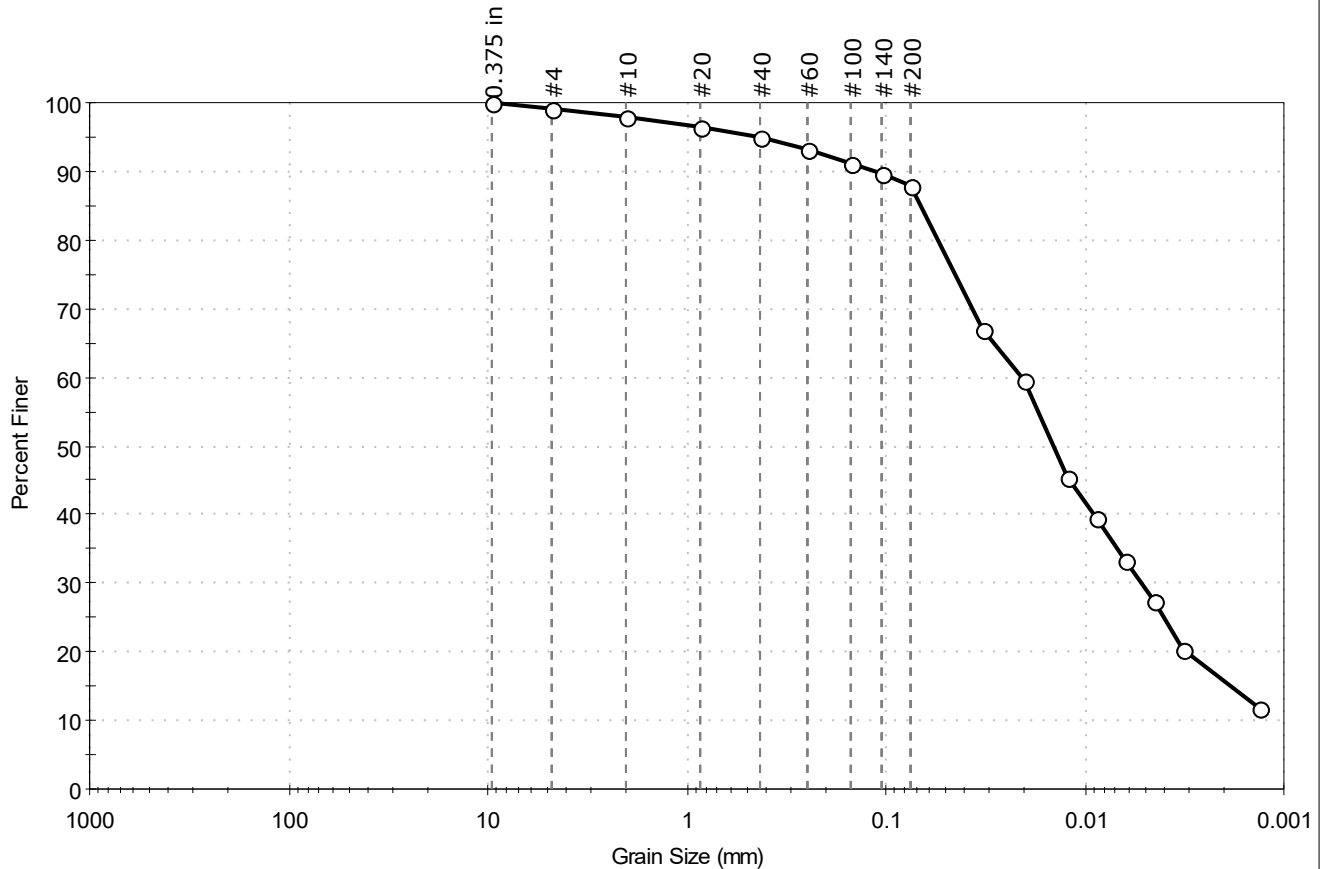
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-104	Sample Type: Jar
Sample ID: 6D	Tested By: ajl
Depth: 15-17 ft	Test Date: 08/15/24
	Checked By: ank
	Test Id: 780410
Test Comment: ---	
Visual Description: Moist, grayish brown clay	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	1.0	11.2	87.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	99		
#10	2.00	98		
#20	0.85	96		
#40	0.42	95		
#60	0.25	93		
#100	0.15	91		
#140	0.11	90		
#200	0.075	88		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0324	67		
---	0.0201	60		
---	0.0122	45		
---	0.0088	39		
---	0.0063	33		
---	0.0045	27		
---	0.0032	20		
---	0.0013	12		

Coefficients

$D_{85} = 0.0670$ mm $D_{30} = 0.0052$ mm
 $D_{60} = 0.0205$ mm $D_{15} = 0.0019$ mm
 $D_{50} = 0.0143$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Lean CLAY (CL)

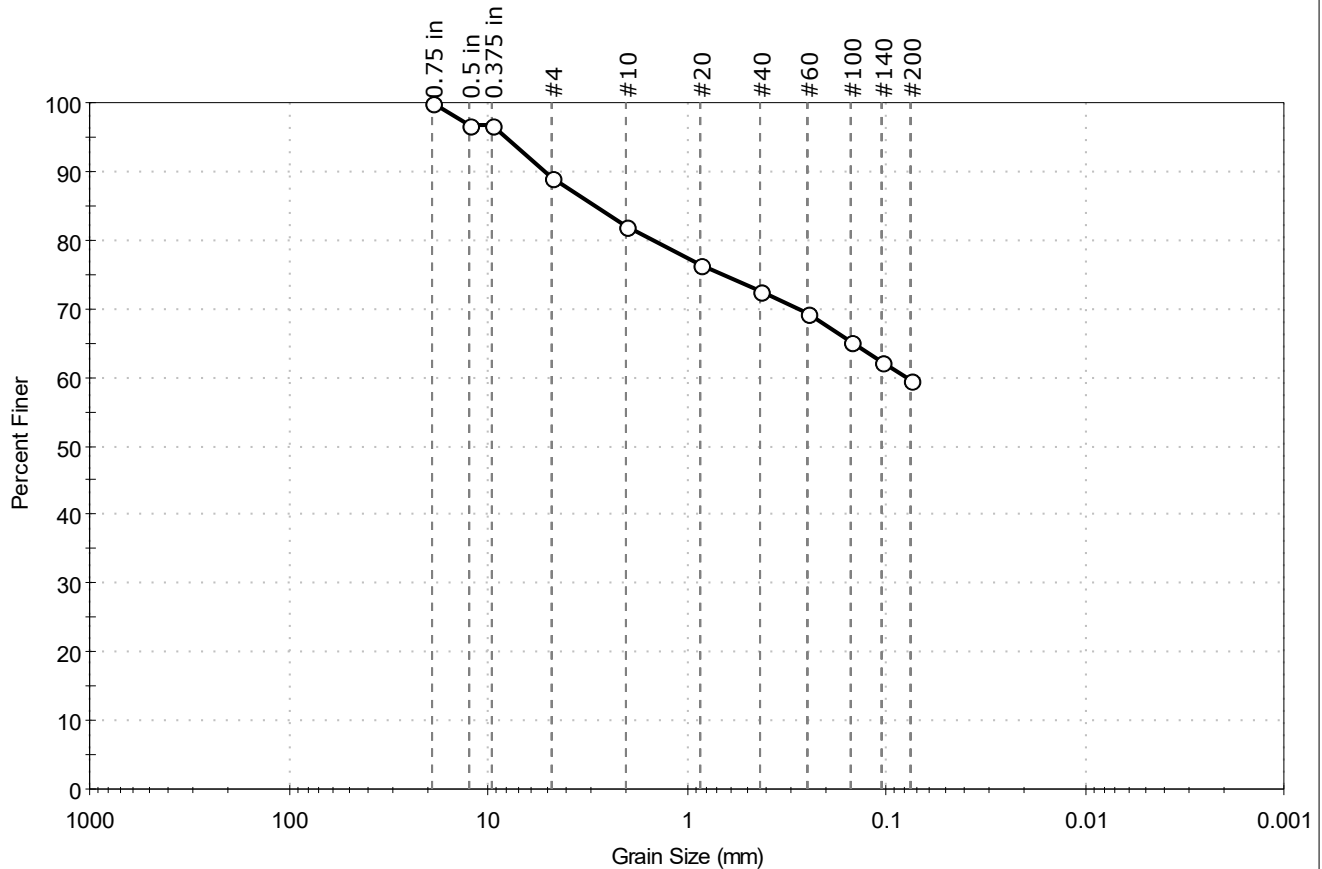
AASHTO Clayey Soils (A-6 (10))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-104	Sample Type: Jar	Tested By: ajl
Sample ID: 7D	Test Date: 08/19/24	Checked By: ank
Depth : 20-22 ft	Test Id: 780408	
Test Comment: ---		
Visual Description: Moist, greenish gray silt with sand		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.8	29.7	59.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	97		
0.375 in	9.50	97		
#4	4.75	89		
#10	2.00	82		
#20	0.85	76		
#40	0.42	72		
#60	0.25	69		
#100	0.15	65		
#140	0.11	62		
#200	0.075	59		

Coefficients

$D_{85} = 2.8830 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.0799 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

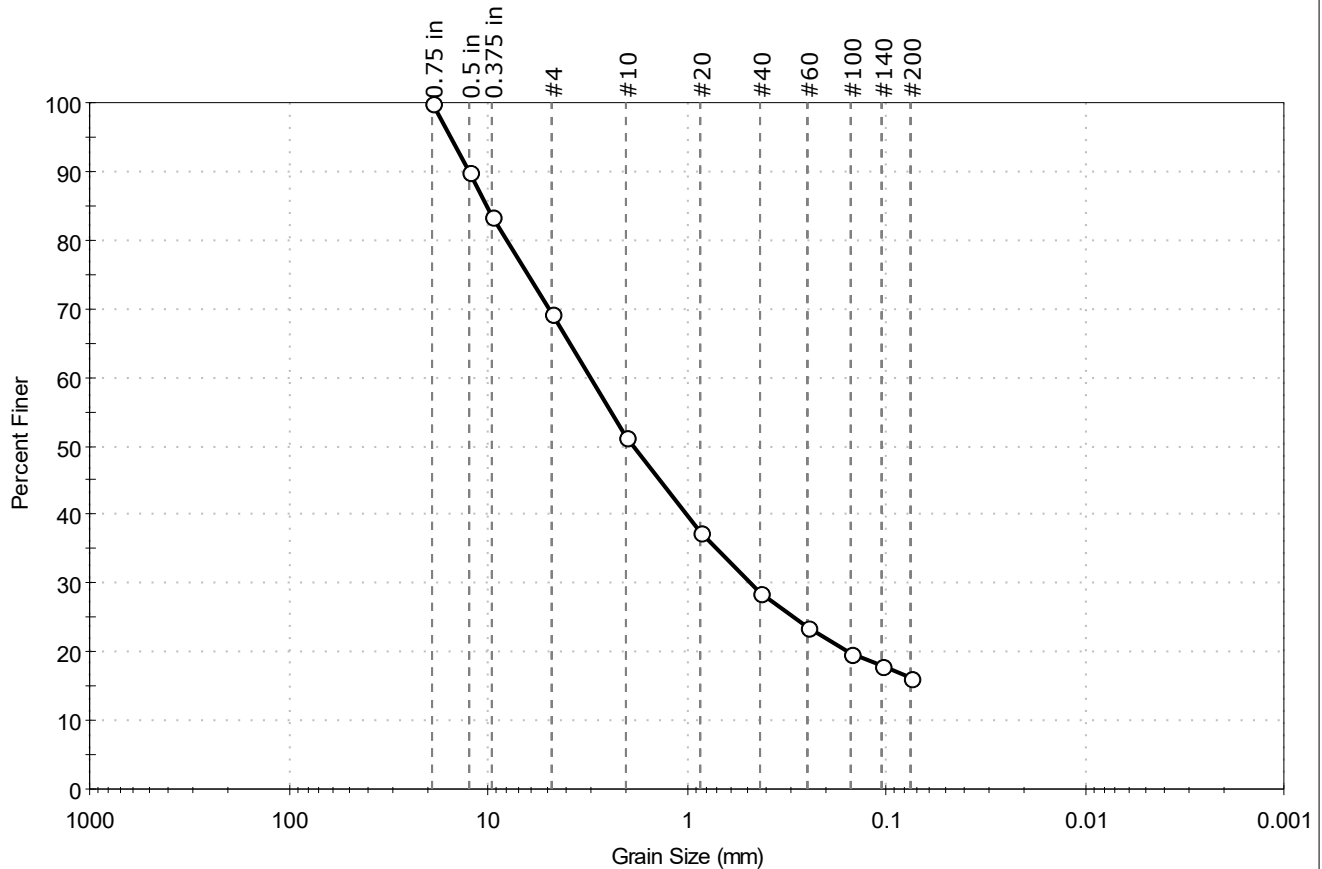
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-105	Sample Type:	Jar
Sample ID:	1D	Test Date:	08/19/24
Depth :	0.9-2.9 ft	Test Id:	780366
Test Comment:	---		
Visual Description:	Moist, olive brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	30.7	53.1	16.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	90		
0.375 in	9.50	83		
#4	4.75	69		
#10	2.00	51		
#20	0.85	37		
#40	0.42	29		
#60	0.25	24		
#100	0.15	20		
#140	0.11	18		
#200	0.075	16		

Coefficients

$D_{85} = 10.1411$ mm $D_{30} = 0.4740$ mm
 $D_{60} = 3.0347$ mm $D_{15} = \text{N/A}$
 $D_{50} = 1.8370$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

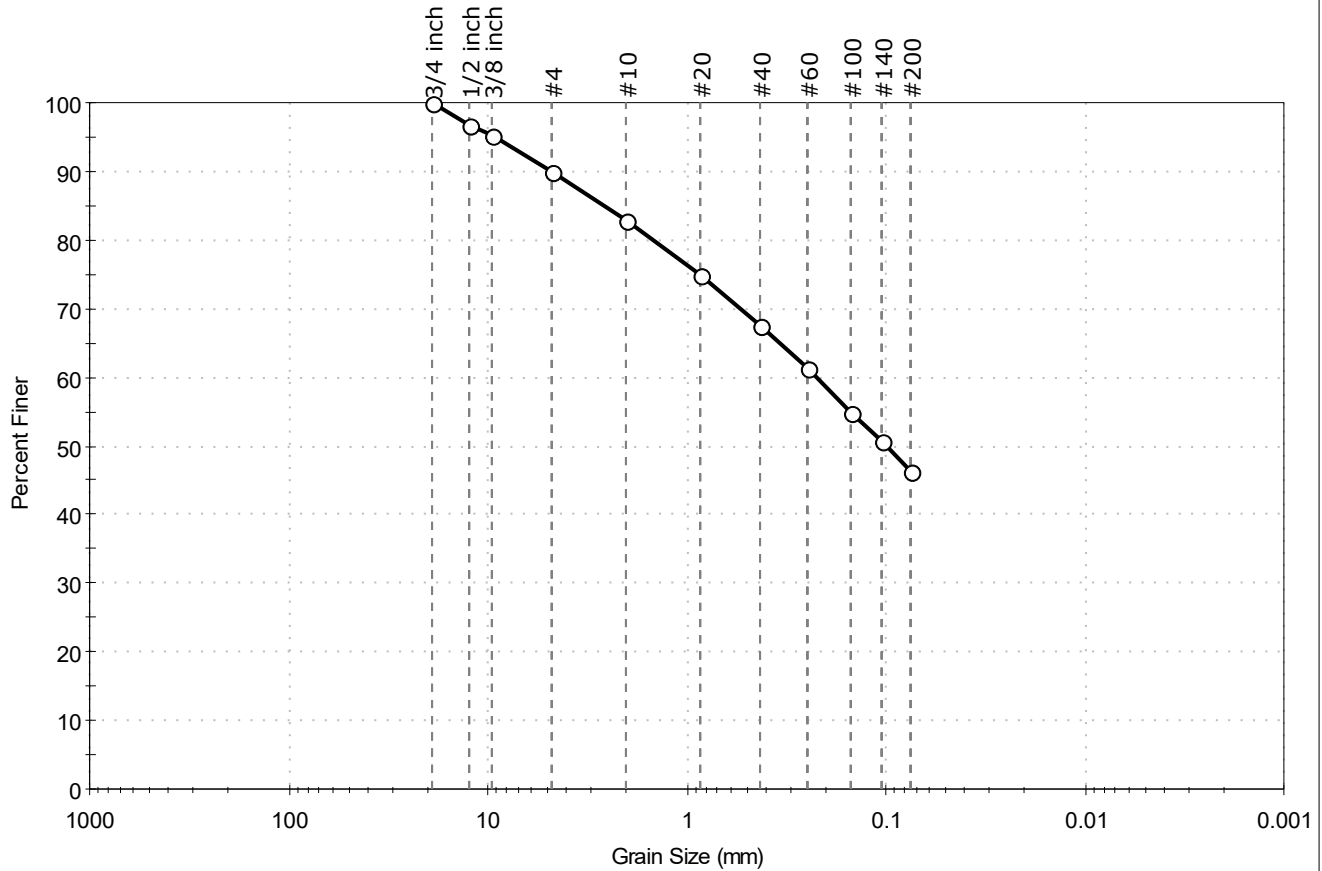
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-105	Sample Type:	Jar
Sample ID:	3D	Test Date:	08/19/24
Depth :	5-5.6 ft	Test Id:	780367
Test Comment:	---		
Visual Description:	Moist, dark grayish brown silty sand		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.0	43.6	46.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
3/4 inch	19.00	100		
1/2 inch	12.50	97		
3/8 inch	9.50	95		
#4	4.75	90		
#10	2.00	83		
#20	0.85	75		
#40	0.42	67		
#60	0.25	61		
#100	0.15	55		
#140	0.11	51		
#200	0.075	46		

Coefficients

$D_{85} = 2.5683 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.2264 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.1002 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

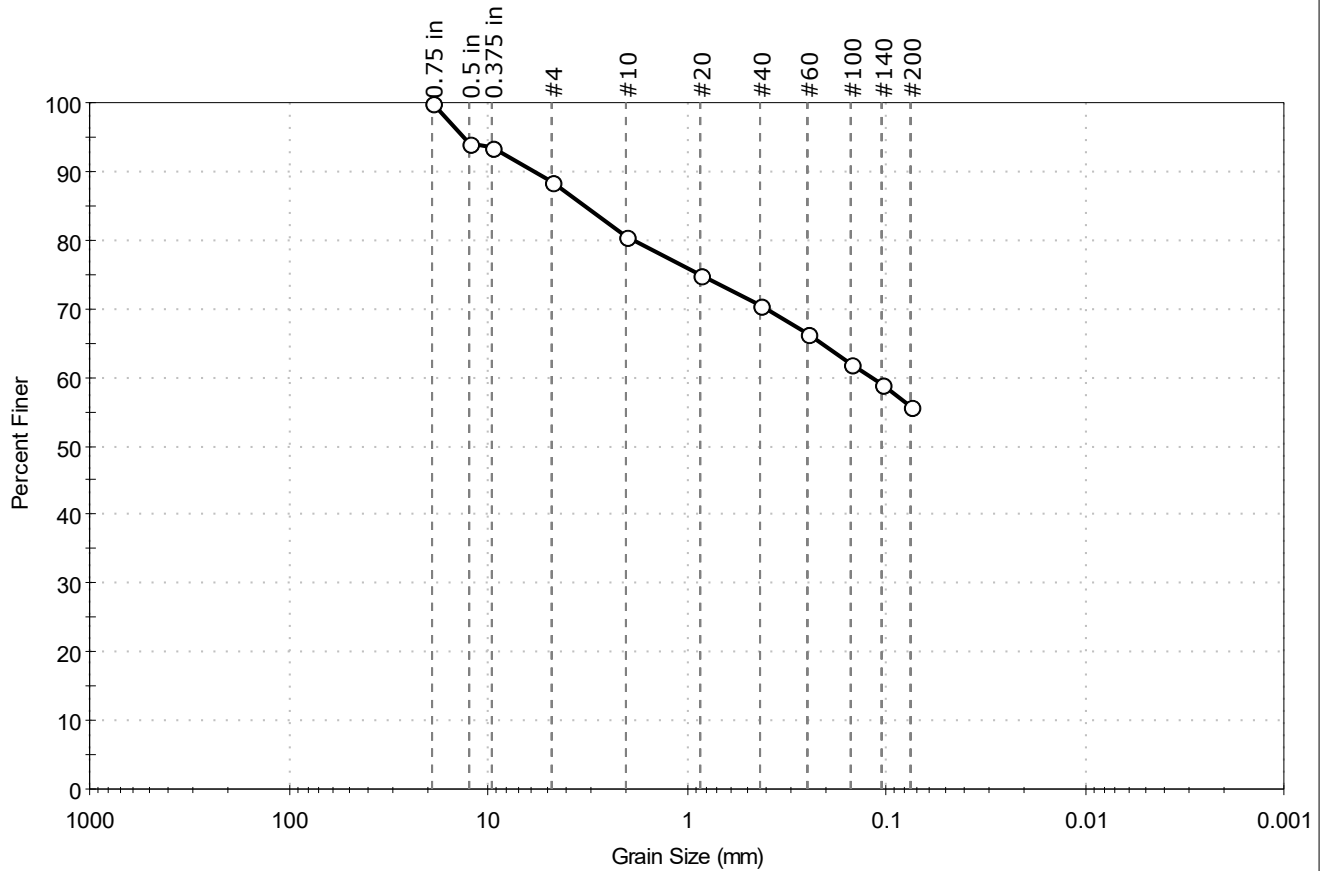
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-105	Sample Type: Jar	Tested By: ajl
Sample ID: 6D	Test Date: 08/19/24	Checked By: ank
Depth: 15-17 ft	Test Id: 780368	
Test Comment: ---		
Visual Description: Moist, grayish brown sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	11.4	32.9	55.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	94		
0.375 in	9.50	93		
#4	4.75	89		
#10	2.00	81		
#20	0.85	75		
#40	0.42	70		
#60	0.25	67		
#100	0.15	62		
#140	0.11	59		
#200	0.075	56		

Coefficients

$D_{85} = 3.2112 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.1201 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

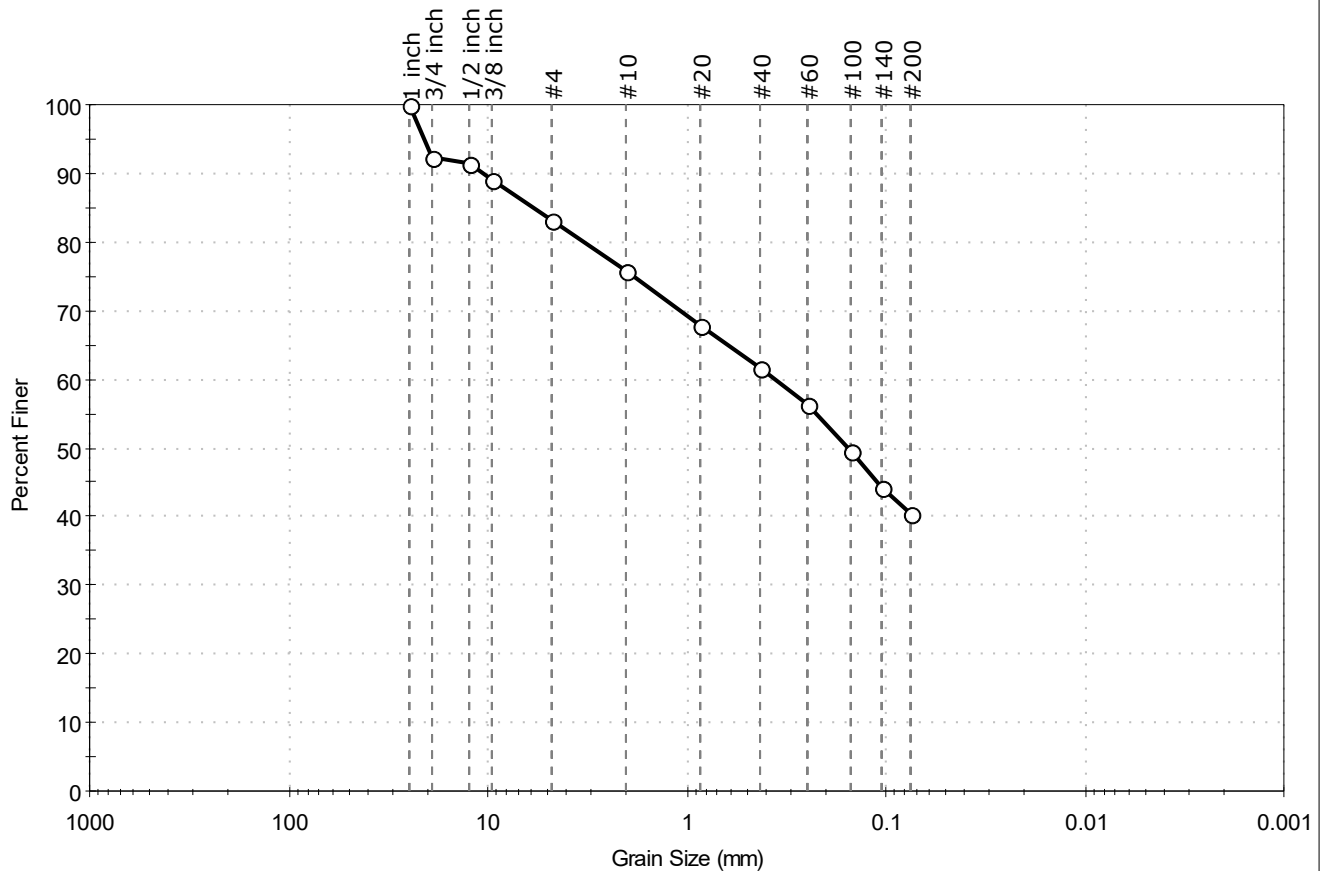
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-105	Sample Type:	Jar
Sample ID:	7D	Test Date:	08/19/24
Depth :	20-22ft	Test Id:	780369
Test Comment:	---		
Visual Description:	Moist, olive brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	16.9	42.8	40.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	92		
1/2 inch	12.50	91		
3/8 inch	9.50	89		
#4	4.75	83		
#10	2.00	76		
#20	0.85	68		
#40	0.42	62		
#60	0.25	56		
#100	0.15	49		
#140	0.11	44		
#200	0.075	40		

Coefficients

$D_{85} = 5.8920 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.3574 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.1564 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

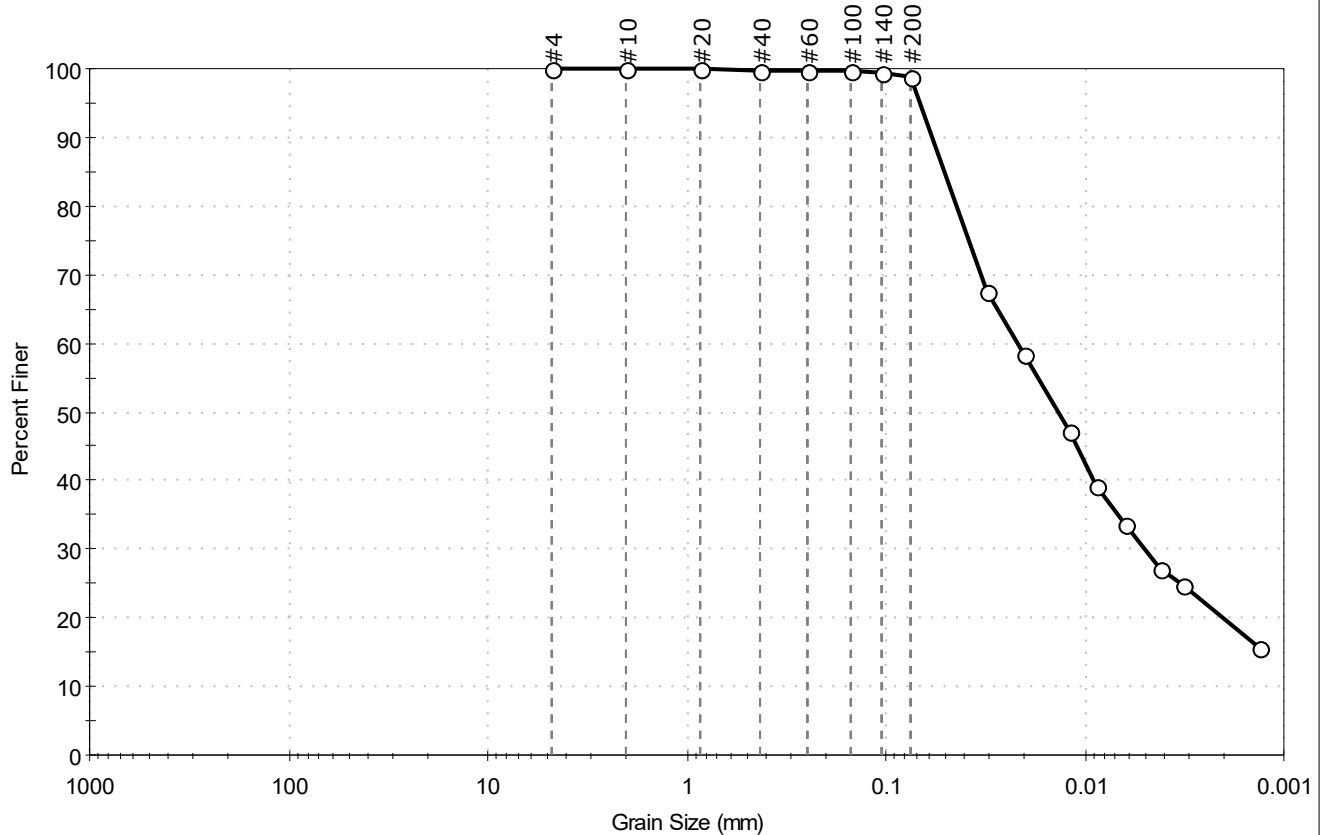
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-106	Sample Type: Jar	Tested By: ajl
Sample ID: 7D	Test Date: 08/15/24	Checked By: ank
Depth : 20-22 ft	Test Id: 780382	
Test Comment: ---		
Visual Description: Moist, light olive brown clay		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	1.1	98.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	99		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0314	67		
---	0.0203	58		
---	0.0121	47		
---	0.0087	39		
---	0.0062	34		
---	0.0042	27		
---	0.0032	25		
---	0.0013	16		

Coefficients

$D_{85} = 0.0510$ mm $D_{30} = 0.0050$ mm
 $D_{60} = 0.0219$ mm $D_{15} = \text{N/A}$
 $D_{50} = 0.0137$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Lean CLAY (CL)

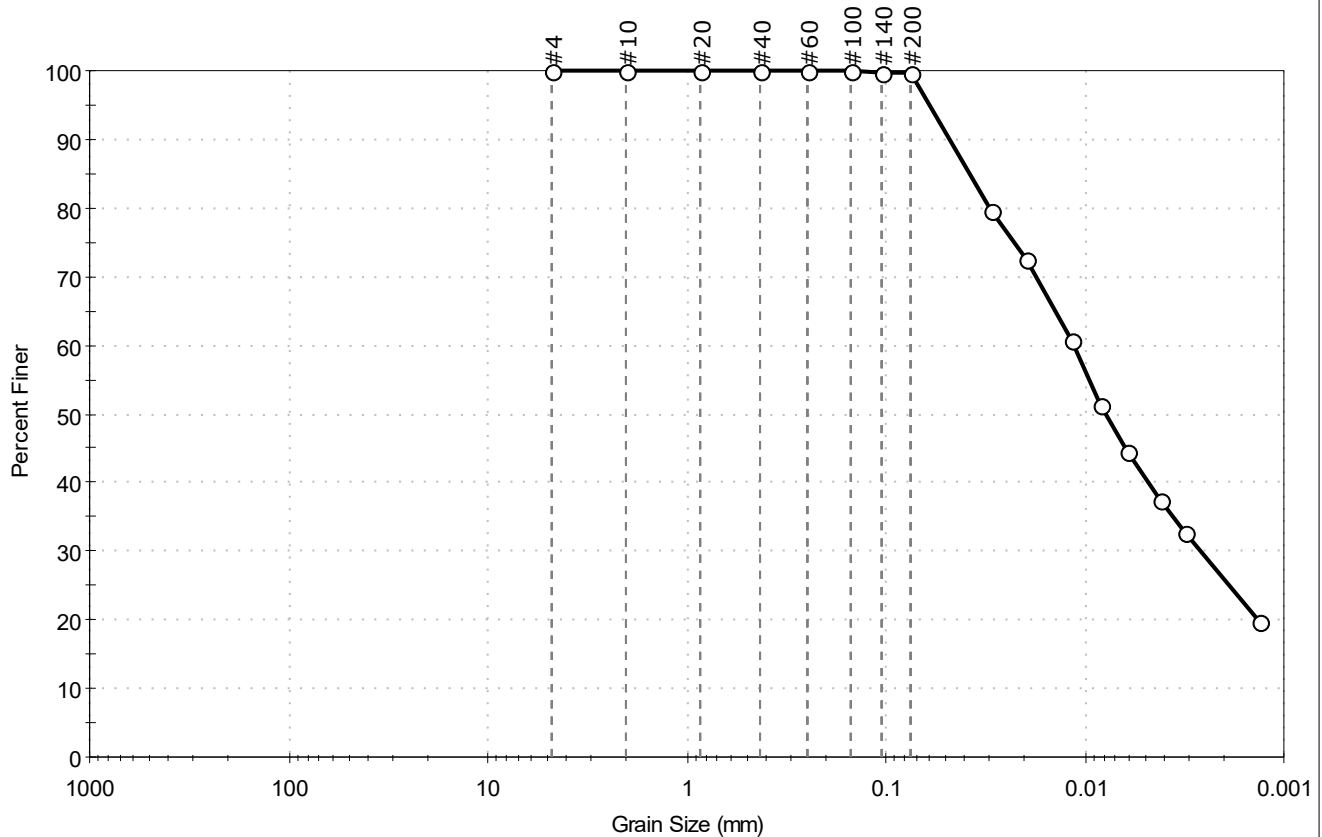
AASHTO Clayey Soils (A-6 (19))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.
 Project: MaineDOT I-95 Bridge over Stillwater
 Location: Merrimack, NH
 Project No: GTX-319180
 Boring ID: BB-BSA-106
 Sample Type: Jar
 Tested By: ajl
 Sample ID: 8D
 Test Date: 08/15/24
 Checked By: ank
 Depth: 25-27 ft
 Test Id: 780383
 Test Comment: ---
 Visual Description: Moist, grayish brown clay
 Sample Comment: ---

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.3	99.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	100		
#200	0.075	100		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0298	80		
---	0.0196	73		
---	0.0117	61		
---	0.0084	51		
---	0.0061	44		
---	0.0042	37		
---	0.0031	33		
---	0.0013	20		

Coefficients

D₈₅ = 0.0383 mm D₃₀ = 0.0026 mm
 D₆₀ = 0.0113 mm D₁₅ = N/A
 D₅₀ = 0.0079 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM Lean CLAY (CL)

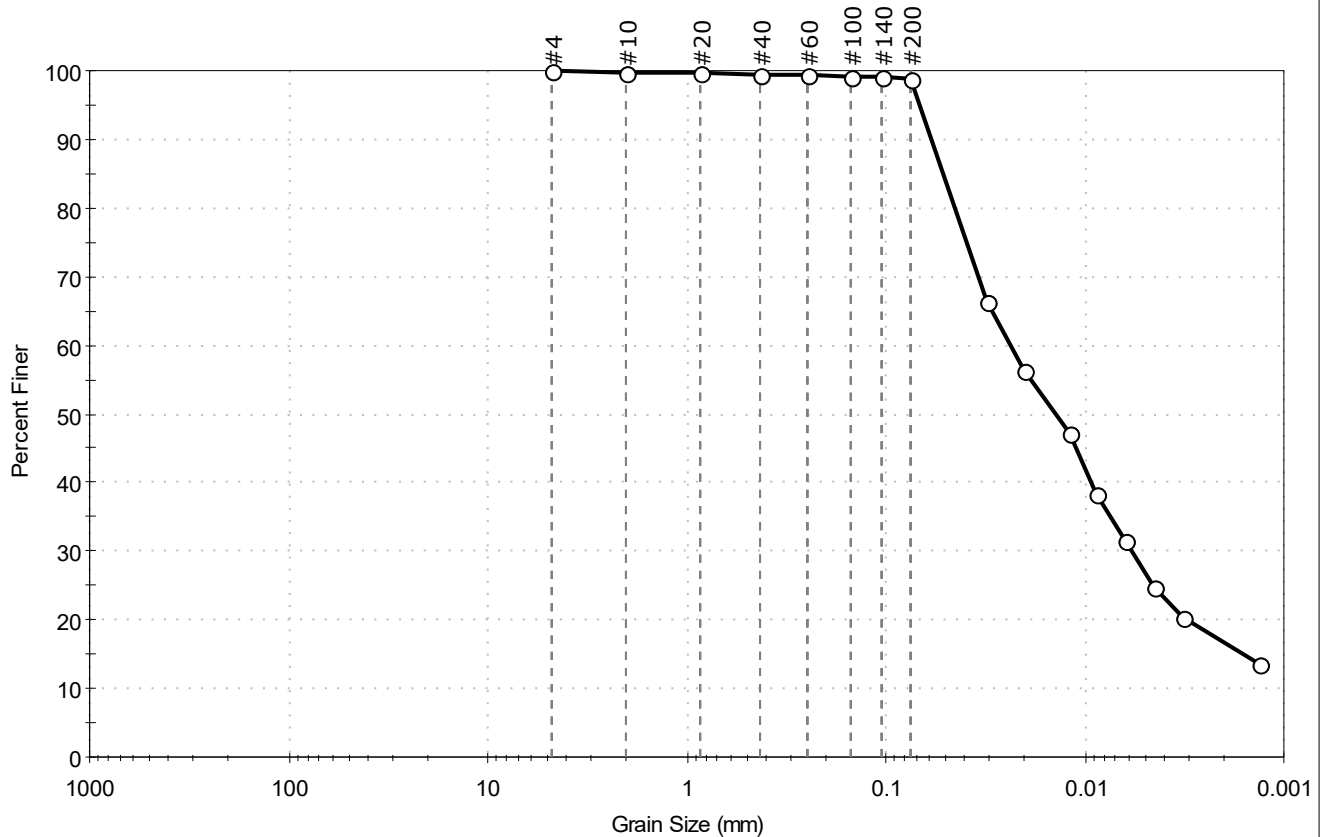
AASHTO Clayey Soils (A-6 (18))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-106	Sample Type: Jar	Tested By: ajl
Sample ID: 9D	Test Date: 08/15/24	Checked By: ank
Depth : 30-32 ft	Test Id: 780384	
Test Comment: ---		
Visual Description: Moist, gray clay		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	1.3	98.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	99		
#60	0.25	99		
#100	0.15	99		
#140	0.11	99		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0308	66		
---	0.0202	56		
---	0.0121	47		
---	0.0087	38		
---	0.0063	32		
---	0.0045	25		
---	0.0032	20		
---	0.0013	14		

Coefficients

$D_{85} = 0.0515$ mm $D_{30} = 0.0058$ mm
 $D_{60} = 0.0236$ mm $D_{15} = 0.0016$ mm
 $D_{50} = 0.0141$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Lean CLAY (CL)

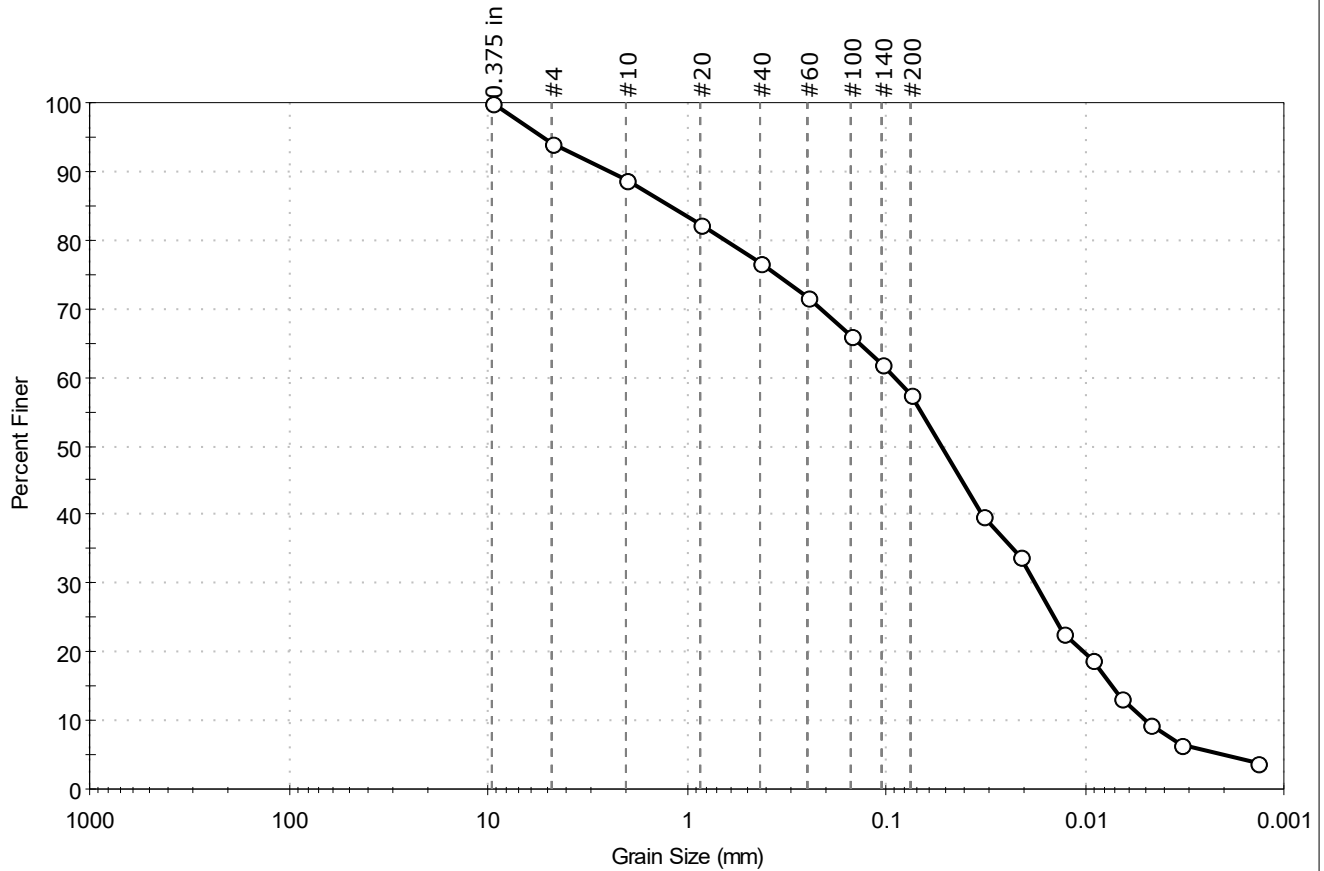
AASHTO Clayey Soils (A-6 (9))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-106	Sample Type: Jar	Tested By: ajl
Sample ID: 11D	Test Date: 08/15/24	Checked By: ank
Depth: 40-42 ft	Test Id: 780385	
Test Comment: ---		
Visual Description: Moist, gray sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	6.0	36.4	57.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	94		
#10	2.00	89		
#20	0.85	82		
#40	0.42	77		
#60	0.25	72		
#100	0.15	66		
#140	0.11	62		
#200	0.075	58		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0327	40		
---	0.0212	34		
---	0.0128	23		
---	0.0091	19		
---	0.0065	13		
---	0.0047	9		
---	0.0033	7		
---	0.0014	4		

Coefficients

$D_{85} = 1.2010 \text{ mm}$ $D_{30} = 0.0177 \text{ mm}$
 $D_{60} = 0.0912 \text{ mm}$ $D_{15} = 0.0073 \text{ mm}$
 $D_{50} = 0.0526 \text{ mm}$ $D_{10} = 0.0049 \text{ mm}$
 $C_u = 18.612$ $C_c = 0.701$

Classification

ASTM Sandy SILT (ML)

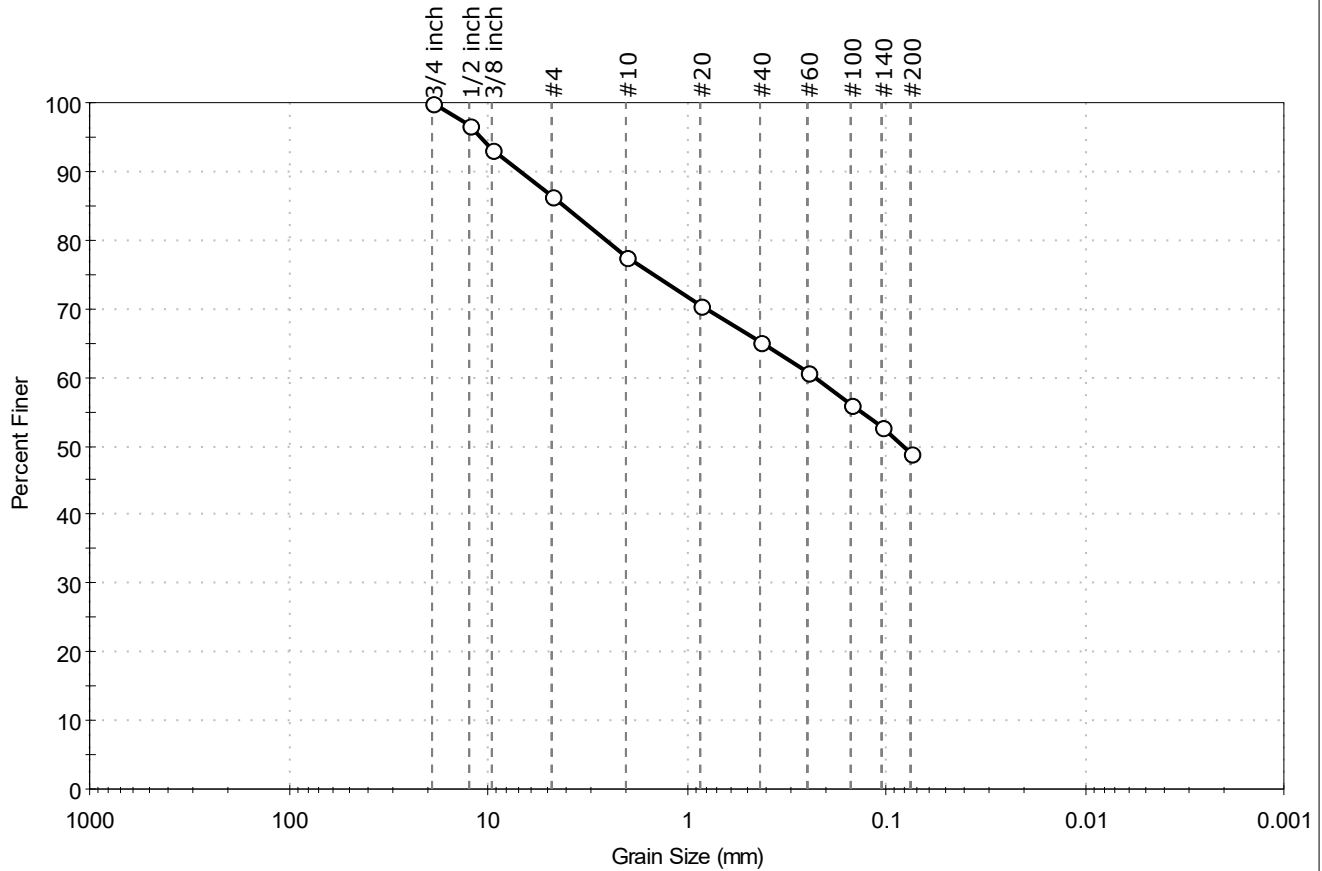
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	14D	Test Date:	08/16/24
Depth :	55-57 ft	Test Id:	780380
Test Comment:	---		
Visual Description:	Moist, gray silty sand		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	13.6	37.5	48.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
3/4 inch	19.00	100		
1/2 inch	12.50	97		
3/8 inch	9.50	93		
#4	4.75	86		
#10	2.00	77		
#20	0.85	70		
#40	0.42	65		
#60	0.25	61		
#100	0.15	56		
#140	0.11	53		
#200	0.075	49		

Coefficients

$D_{85} = 4.1627 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.2272 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.0828 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

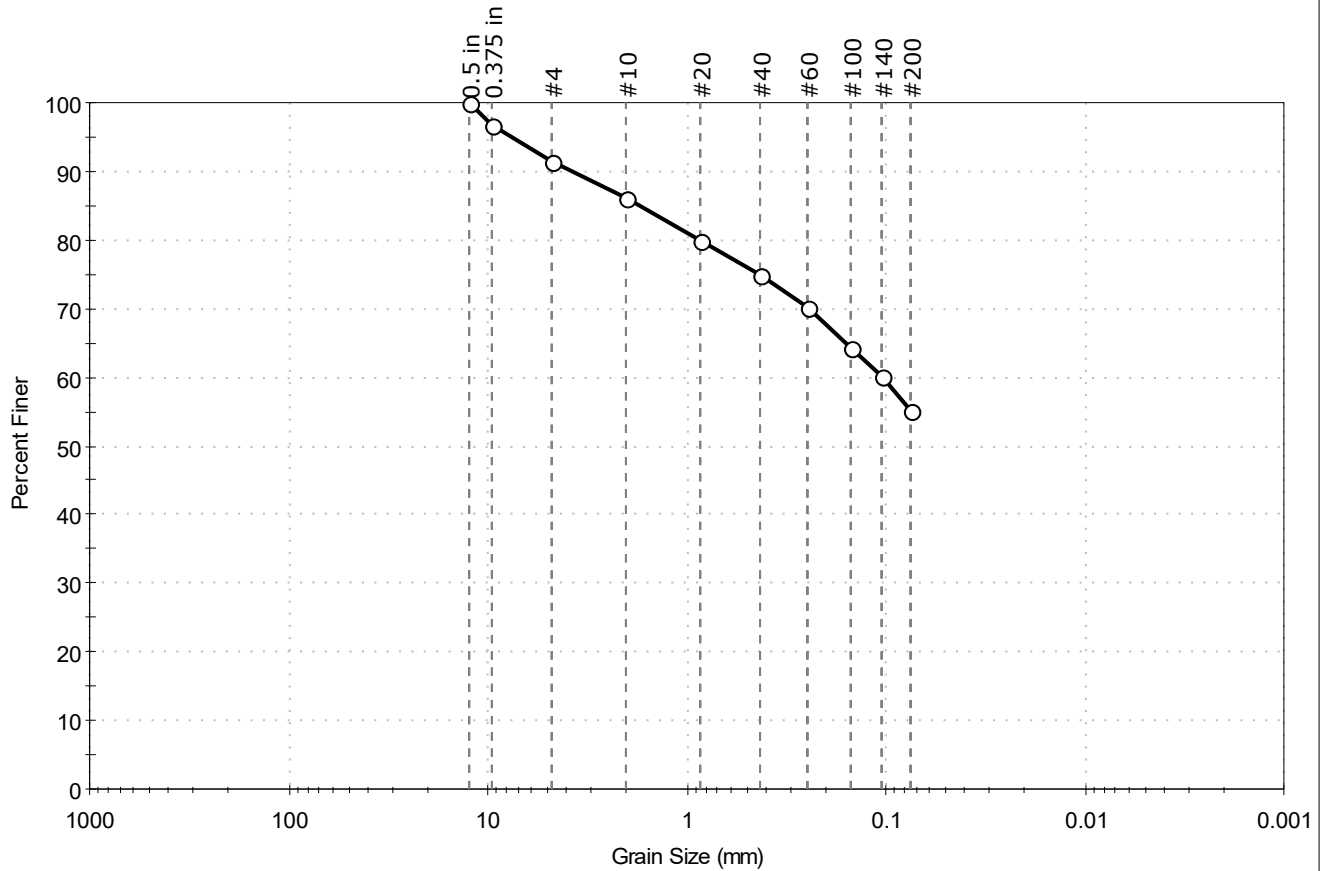
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-107	Sample Type: Jar	Tested By: ajl
Sample ID: 3D	Test Date: 08/19/24	Checked By: ank
Depth : 4.7-6.7 ft	Test Id: 780391	
Test Comment: ---		
Visual Description: Moist, grayish brown sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	8.5	36.3	55.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.5 in	12.50	100		
0.375 in	9.50	97		
#4	4.75	92		
#10	2.00	86		
#20	0.85	80		
#40	0.42	75		
#60	0.25	70		
#100	0.15	64		
#140	0.11	60		
#200	0.075	55		

Coefficients

$D_{85} = 1.6952 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.1052 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

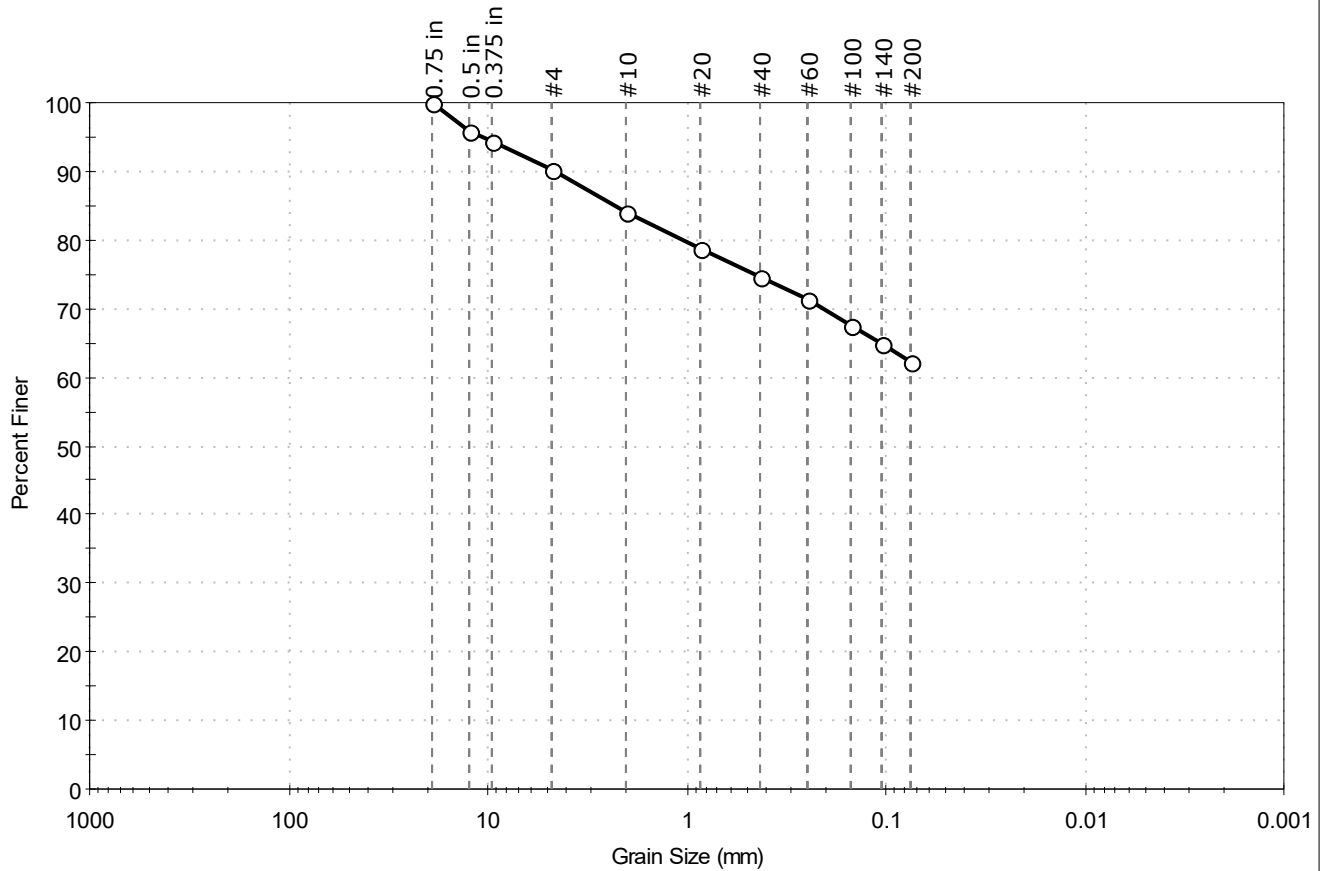
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	6D	Test Date:	08/19/24
Depth :	10.7-12.7 ft	Test Id:	780392
Test Comment:	---		
Visual Description:	Moist, olive brown silt with sand		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	9.7	28.0	62.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	96		
0.375 in	9.50	94		
#4	4.75	90		
#10	2.00	84		
#20	0.85	79		
#40	0.42	75		
#60	0.25	71		
#100	0.15	68		
#140	0.11	65		
#200	0.075	62		

Coefficients

$D_{85} = 2.2895 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = \text{N/A}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

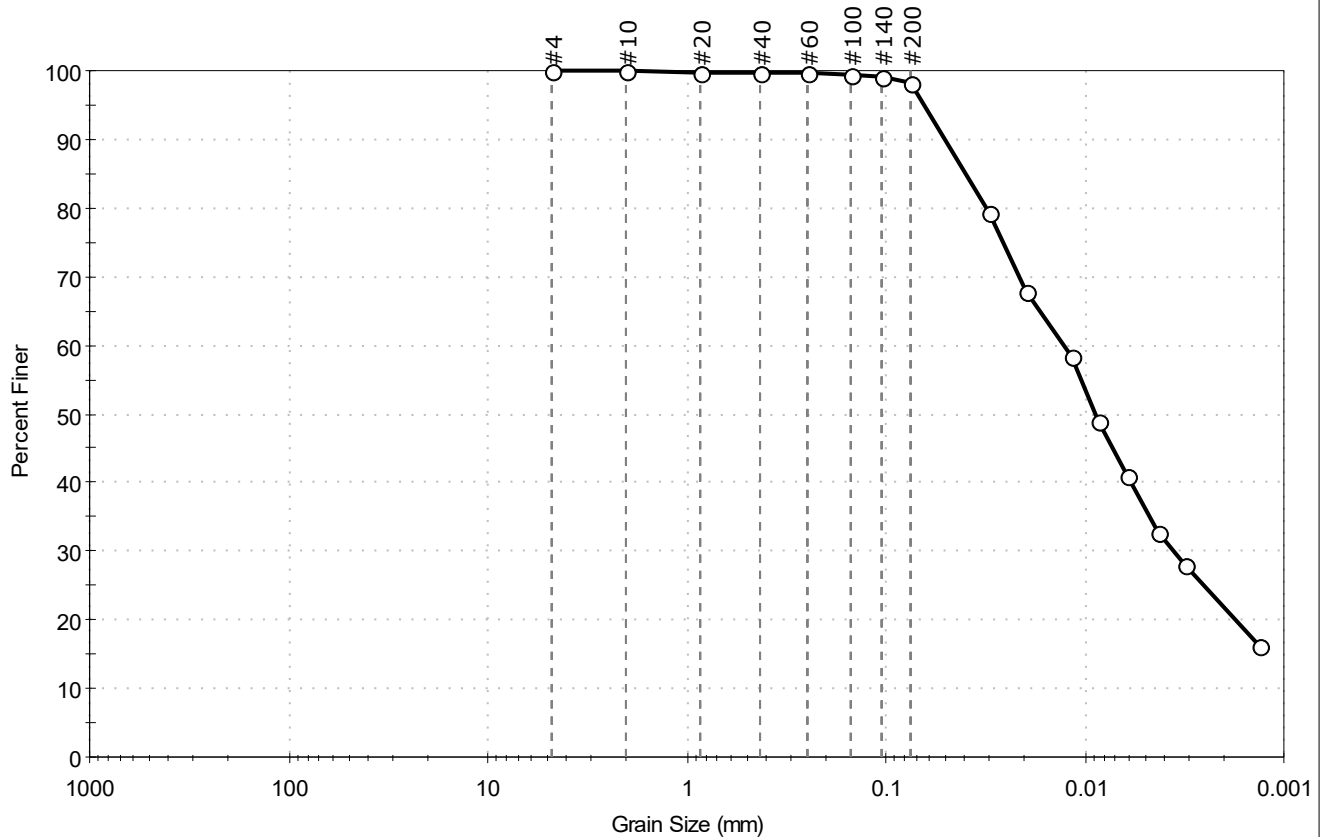
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-107	Sample Type: Jar
Sample ID: 8D	Test Date: 08/15/24
Depth: 20-22 ft	Test Id: 780395
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown clay	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	1.7	98.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	99		
#140	0.11	99		
#200	0.075	98		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0303	79		
---	0.0196	68		
---	0.0117	58		
---	0.0085	49		
---	0.0061	41		
---	0.0043	33		
---	0.0032	28		
---	0.0013	16		

Coefficients

$D_{85} = 0.0395$ mm $D_{30} = 0.0036$ mm
 $D_{60} = 0.0127$ mm $D_{15} = \text{N/A}$
 $D_{50} = 0.0088$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Lean CLAY (CL)

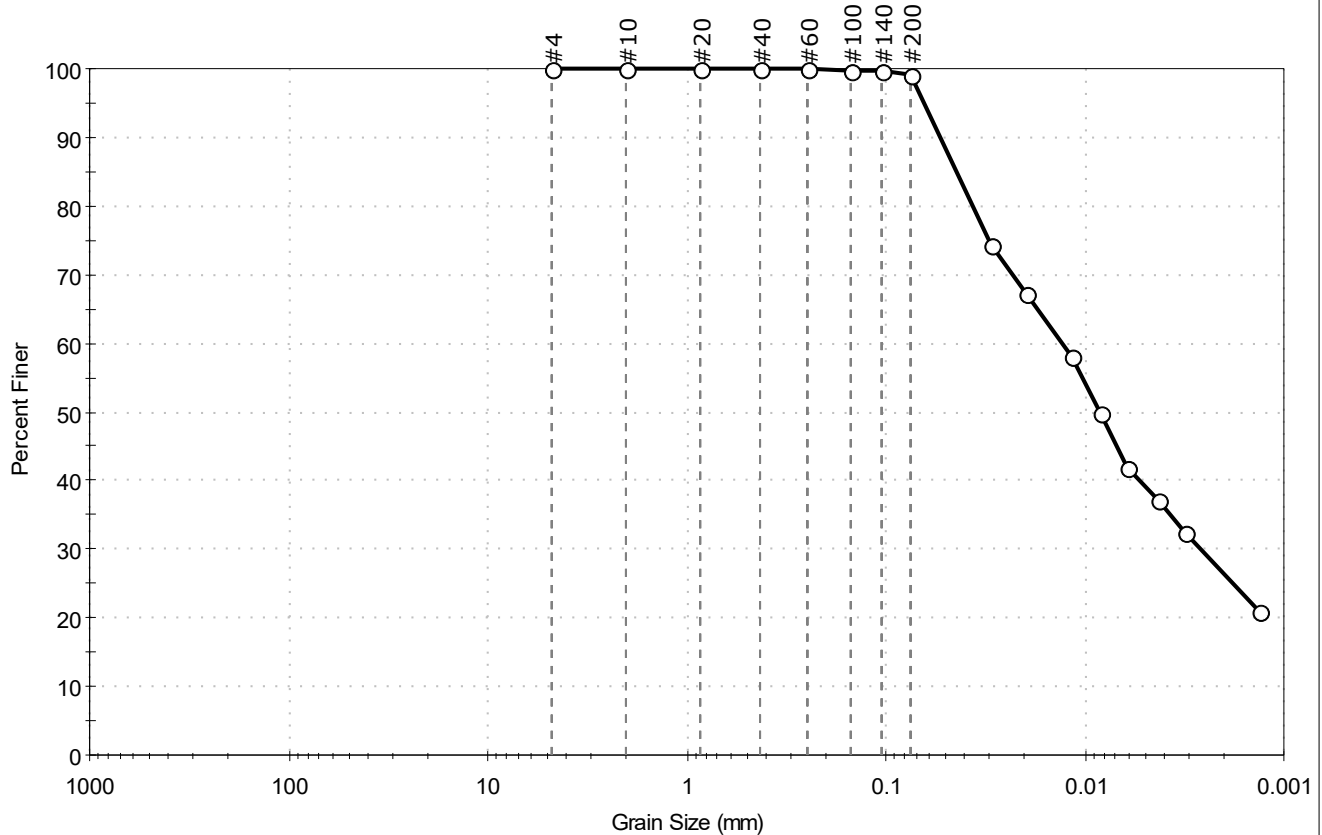
AASHTO Clayey Soils (A-6 (15))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.
 Project: MaineDOT I-95 Bridge over Stillwater
 Location: Merrimack, NH
 Project No: GTX-319180
 Boring ID: BB-BSA-107
 Sample Type: Jar
 Tested By: ajl
 Sample ID: 9D
 Test Date: 08/15/24
 Checked By: ank
 Depth: 25-27 ft
 Test Id: 780396
 Test Comment: ---
 Visual Description: Moist, olive brown clay
 Sample Comment: ---

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.7	99.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	100		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0295	74		
---	0.0198	67		
---	0.0117	58		
---	0.0083	50		
---	0.0061	42		
---	0.0043	37		
---	0.0031	33		
---	0.0013	21		

Coefficients

D₈₅ = 0.0440 mm D₃₀ = 0.0026 mm
 D₆₀ = 0.0131 mm D₁₅ = N/A
 D₅₀ = 0.0084 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM Lean CLAY (CL)

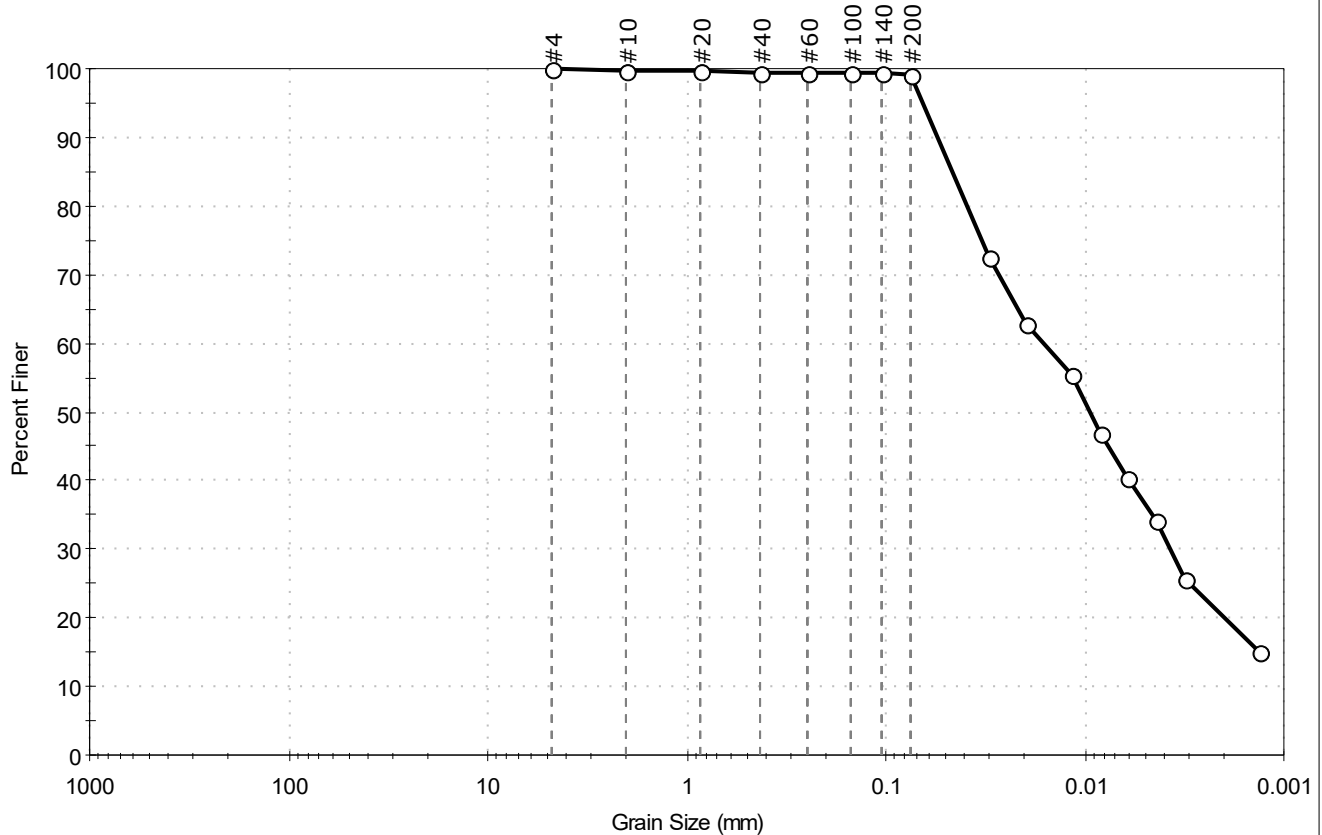
AASHTO Clayey Soils (A-6 (37))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-107	Sample Type: Jar	Tested By: ajl
Sample ID: 10D	Test Date: 08/15/24	Checked By: ank
Depth: 30-32 ft	Test Id: 780397	
Test Comment: ---		
Visual Description: Moist, grayish brown clay		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.9	99.1

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	99		
#100	0.15	99		
#140	0.11	99		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0305	73		
---	0.0196	63		
---	0.0117	55		
---	0.0085	47		
---	0.0061	41		
---	0.0044	34		
---	0.0032	26		
---	0.0013	15		

Coefficients

$D_{85} = 0.0465$ mm $D_{30} = 0.0037$ mm
 $D_{60} = 0.0160$ mm $D_{15} = 0.0013$ mm
 $D_{50} = 0.0095$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Lean CLAY (CL)

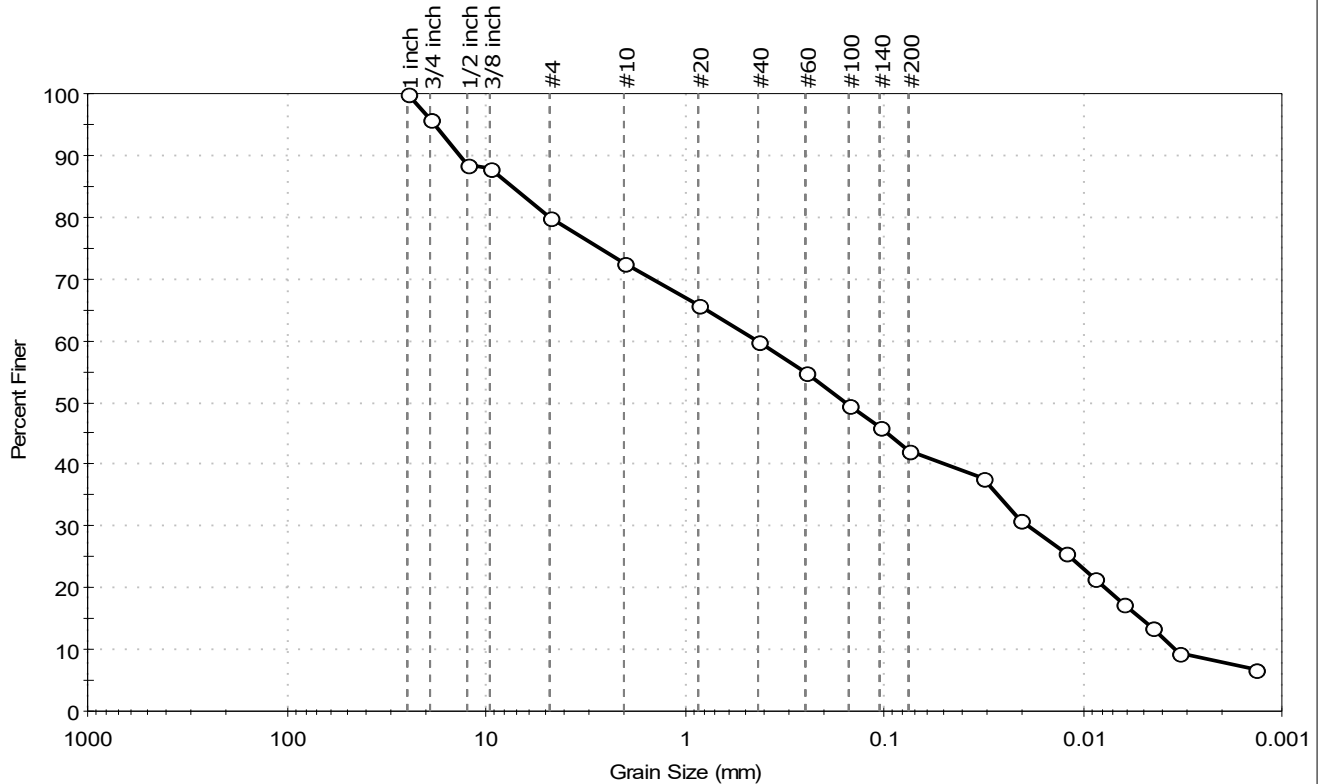
AASHTO Clayey Soils (A-6 (11))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-107	Sample Type: Jar	Tested By: ajl
Sample ID: 12D	Test Date: 08/15/24	Checked By: ank
Depth: 40-42 ft	Test Id: 781642	
Test Comment: ---		
Visual Description: Moist, brownish gray silty clayey sand with gravel		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	19.9	38.0	42.1

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	96		
1/2 inch	12.50	88		
3/8 inch	9.50	88		
#4	4.75	80		
#10	2.00	73		
#20	0.85	66		
#40	0.42	60		
#60	0.25	55		
#100	0.15	49		
#140	0.11	46		
#200	0.075	42		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0320	38		
---	0.0207	31		
---	0.0122	26		
---	0.0088	22		
---	0.0063	17		
---	0.0045	13		
---	0.0033	9		
---	0.0014	7		

Coefficients

D₈₅ = 7.3626 mm D₃₀ = 0.0188 mm
 D₆₀ = 0.4262 mm D₁₅ = 0.0052 mm
 D₅₀ = 0.1580 mm D₁₀ = 0.0034 mm
 C_u = 125.353 C_c = 0.244

Classification

ASTM Silty, Clayey SAND with Gravel (SC-SM)

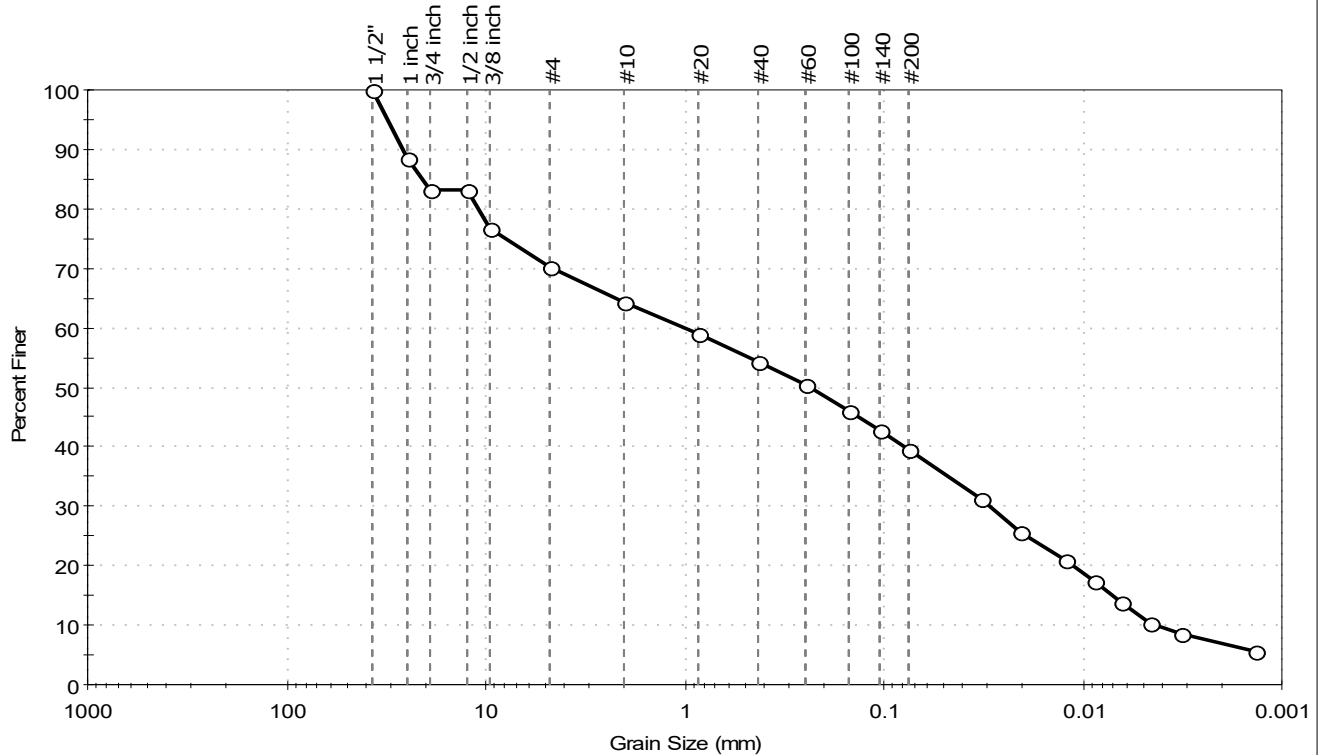
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-107	Sample Type: Jar
Sample ID: 14D	Tested By: ajl
Depth: 50-52 ft	Test Date: 08/15/24
	Checked By: ank
	Test Id: 780394
Test Comment: ---	
Visual Description: Moist, grayish brown clayey sand with gravel	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	29.9	30.5	39.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	89		
3/4 inch	19.00	83		
1/2 inch	12.50	83		
3/8 inch	9.50	77		
#4	4.75	70		
#10	2.00	64		
#20	0.85	59		
#40	0.42	54		
#60	0.25	51		
#100	0.15	46		
#140	0.11	43		
#200	0.075	40		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0325	31		
---	0.0209	26		
---	0.0123	21		
---	0.0088	17		
---	0.0064	14		
---	0.0046	10		
---	0.0033	9		
---	0.0014	6		

Coefficients

$D_{85} = 20.8858 \text{ mm}$ $D_{30} = 0.0294 \text{ mm}$
 $D_{60} = 0.9990 \text{ mm}$ $D_{15} = 0.0071 \text{ mm}$
 $D_{50} = 0.2343 \text{ mm}$ $D_{10} = 0.0042 \text{ mm}$
 $C_u = 237.857$ $C_c = 0.206$

Classification

ASTM Clayey SAND with Gravel (SC)

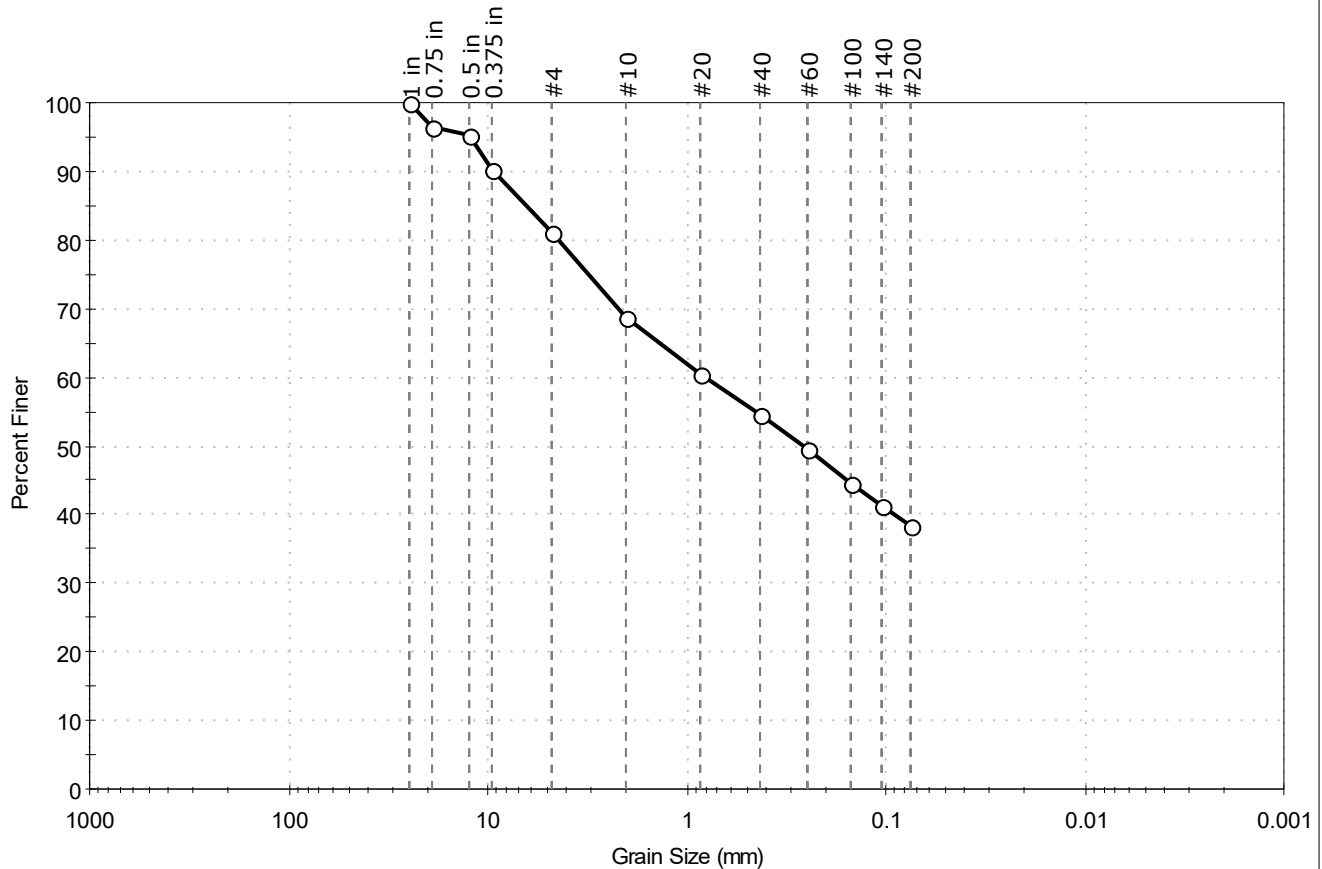
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-107	Sample Type: Jar	Tested By: ajl
Sample ID: 15D	Test Date: 08/16/24	Checked By: ank
Depth : 55-57 ft	Test Id: 780393	
Test Comment: ---		
Visual Description: Moist, grayish brown silty sand with gravel		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	19.0	42.7	38.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	95		
0.375 in	9.50	90		
#4	4.75	81		
#10	2.00	69		
#20	0.85	61		
#40	0.42	55		
#60	0.25	50		
#100	0.15	45		
#140	0.11	41		
#200	0.075	38		

Coefficients

$D_{85} = 6.3985 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.7963 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.2606 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

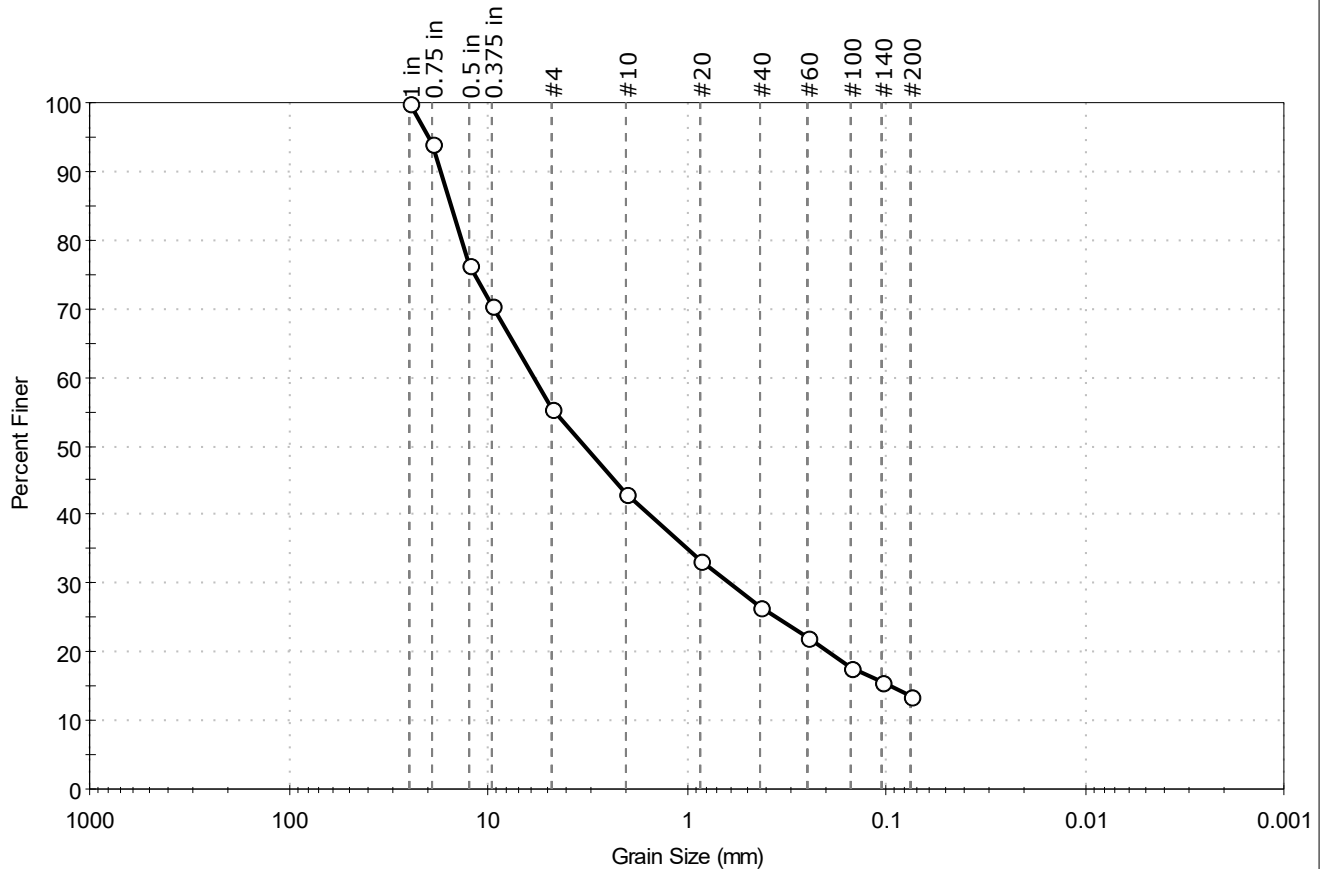
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-111	Sample Type:	Jar
Sample ID:	1D	Test Date:	08/16/24
Depth :	1-3 ft	Test Id:	780418
Test Comment:	---		
Visual Description:	Moist, olive brown silty gravel with sand		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	44.5	42.0	13.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	94		
0.5 in	12.50	76		
0.375 in	9.50	70		
#4	4.75	55		
#10	2.00	43		
#20	0.85	33		
#40	0.42	27		
#60	0.25	22		
#100	0.15	18		
#140	0.11	16		
#200	0.075	13		

Coefficients

$D_{85} = 15.3239$ mm $D_{30} = 0.5991$ mm
 $D_{60} = 5.8553$ mm $D_{15} = 0.0959$ mm
 $D_{50} = 3.2528$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

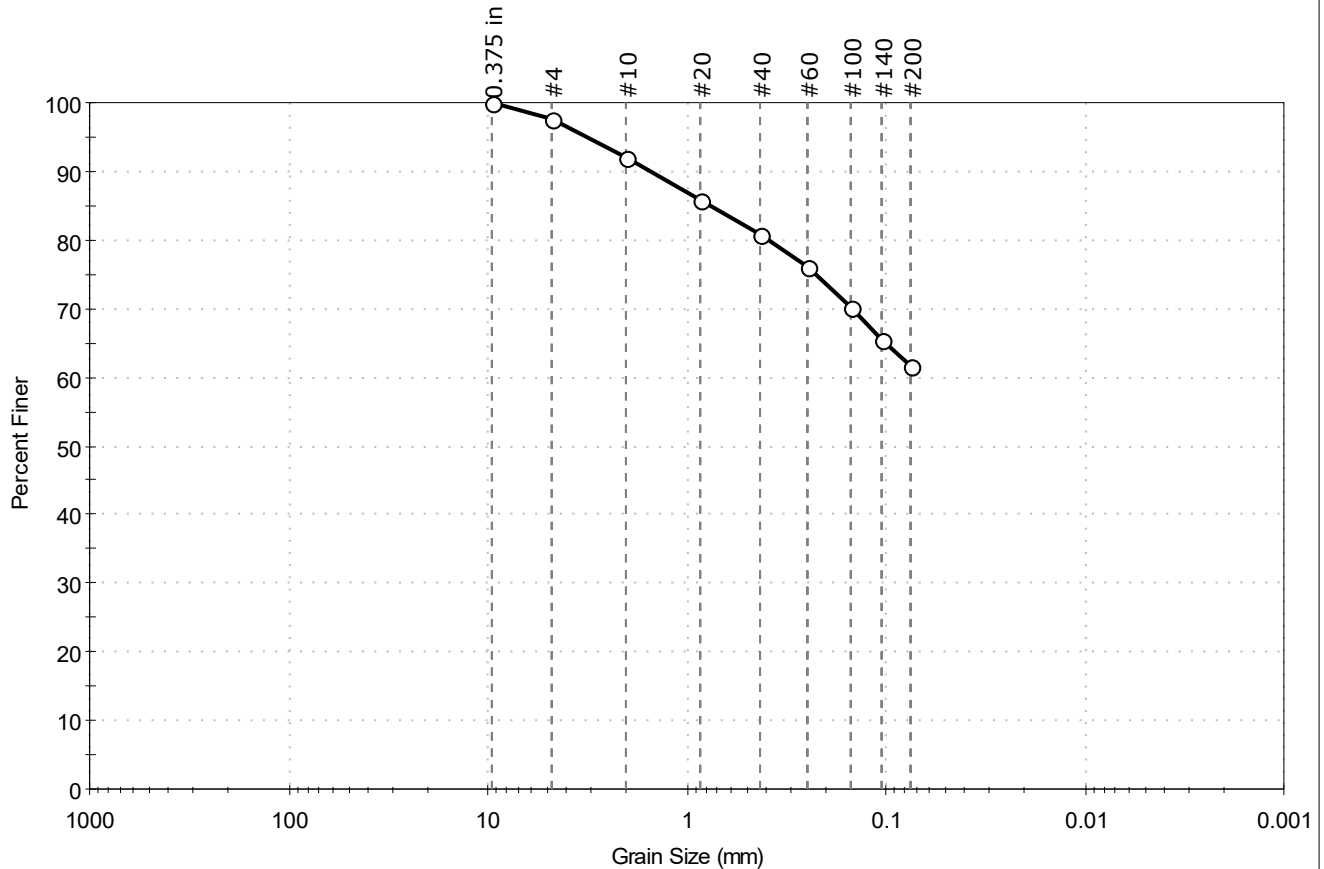
AASHTO Stone Fragments, Gravel and Sand (A-1-a (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-111	Sample Type: Jar	Tested By: ajl
Sample ID: 3D	Test Date: 08/19/24	Checked By: ank
Depth: 5-7 ft	Test Id: 780420	
Test Comment: ---		
Visual Description: Moist, light olive brown sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	2.4	36.0	61.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	98		
#10	2.00	92		
#20	0.85	86		
#40	0.42	81		
#60	0.25	76		
#100	0.15	70		
#140	0.11	66		
#200	0.075	62		

Coefficients

$D_{85} = 0.7542 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = \text{N/A}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

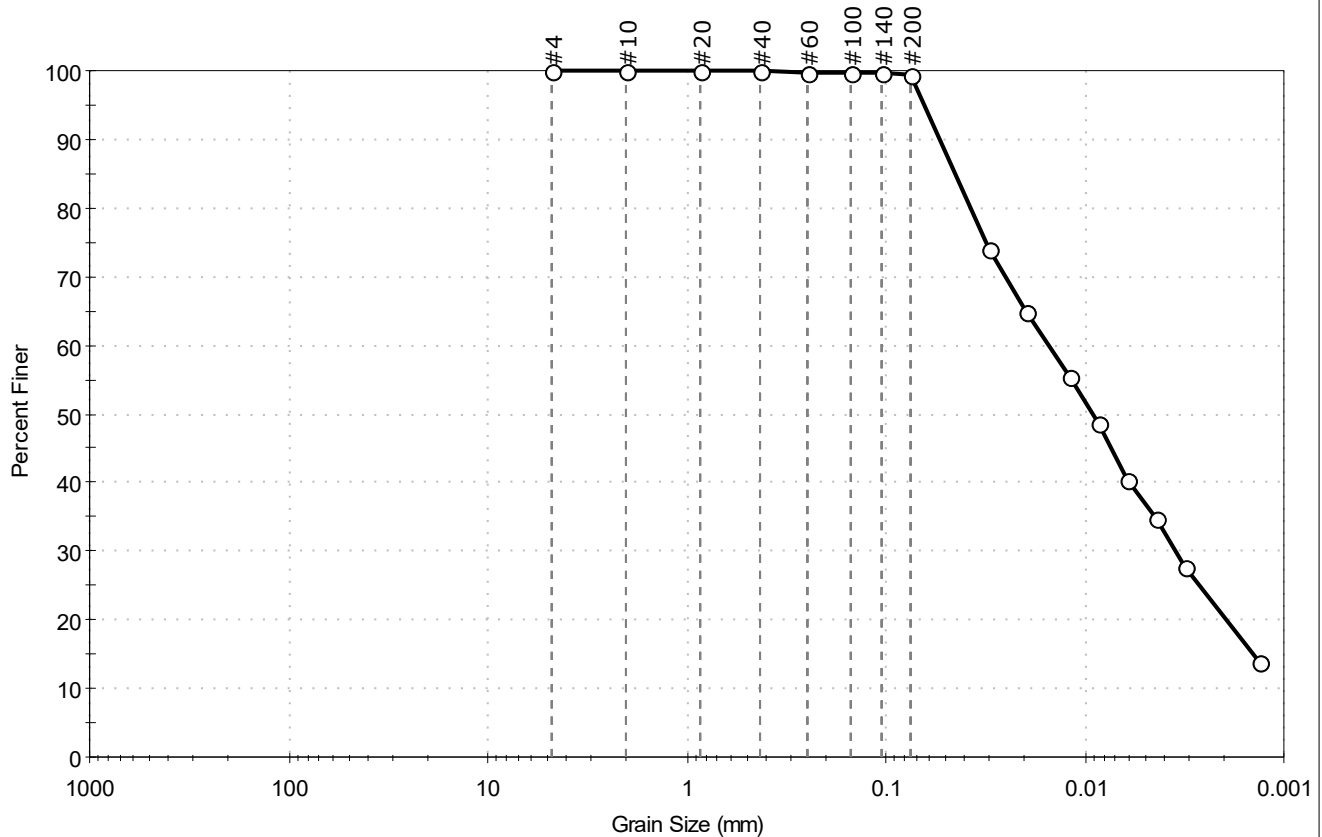
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-111	Sample Type: Jar
Sample ID: 5D	Test Date: 08/15/24
Depth: 10-12 ft	Test Id: 780422
Test Comment: ---	Tested By: ajl
Visual Description: Moist, olive brown clay	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	0.6	99.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	100		
#140	0.11	100		
#200	0.075	99		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.0305	74		
---	0.0196	65		
---	0.0118	56		
---	0.0085	49		
---	0.0061	40		
---	0.0044	35		
---	0.0032	28		
---	0.0013	14		

Coefficients

$D_{85} = 0.0450$ mm $D_{30} = 0.0035$ mm
 $D_{60} = 0.0151$ mm $D_{15} = 0.0014$ mm
 $D_{50} = 0.0091$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Lean CLAY (CL)

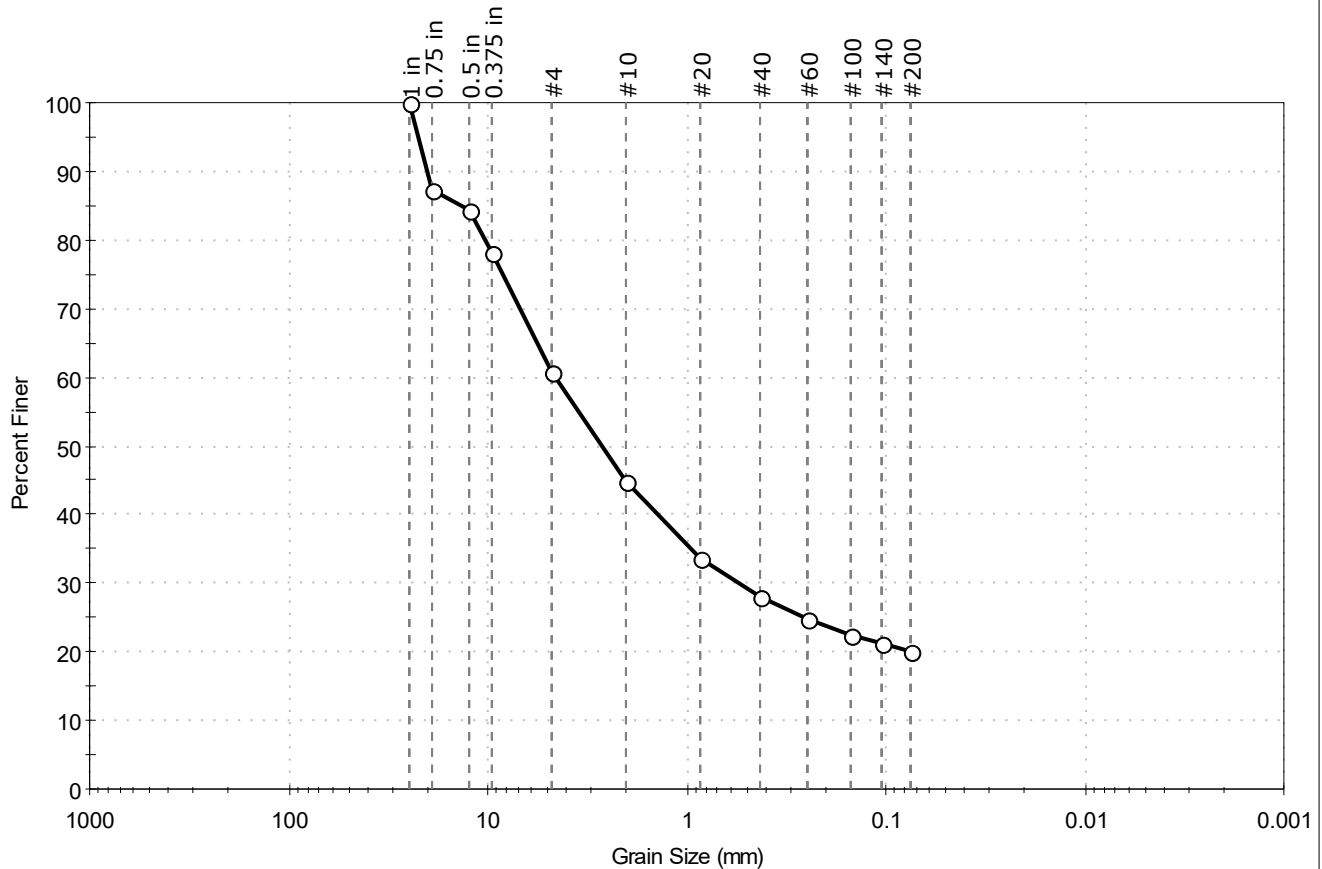
AASHTO Clayey Soils (A-6 (15))

Sample/Test Description

Sand/Gravel Particle Shape : ---
 Sand/Gravel Hardness : ---
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-111	Sample Type: Jar	Tested By: ajl
Sample ID: 6D	Test Date: 08/16/24	Checked By: ank
Depth: 15-17 ft	Test Id: 780421	
Test Comment: ---		
Visual Description: Moist, grayish brown silty sand with gravel		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	39.3	40.7	20.0

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	87		
0.5 in	12.50	84		
0.375 in	9.50	78		
#4	4.75	61		
#10	2.00	45		
#20	0.85	34		
#40	0.42	28		
#60	0.25	25		
#100	0.15	22		
#140	0.11	21		
#200	0.075	20		

Coefficients

D₈₅ = 13.6712 mm D₃₀ = 0.5440 mm
 D₆₀ = 4.5692 mm D₁₅ = N/A
 D₅₀ = 2.6581 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM N/A

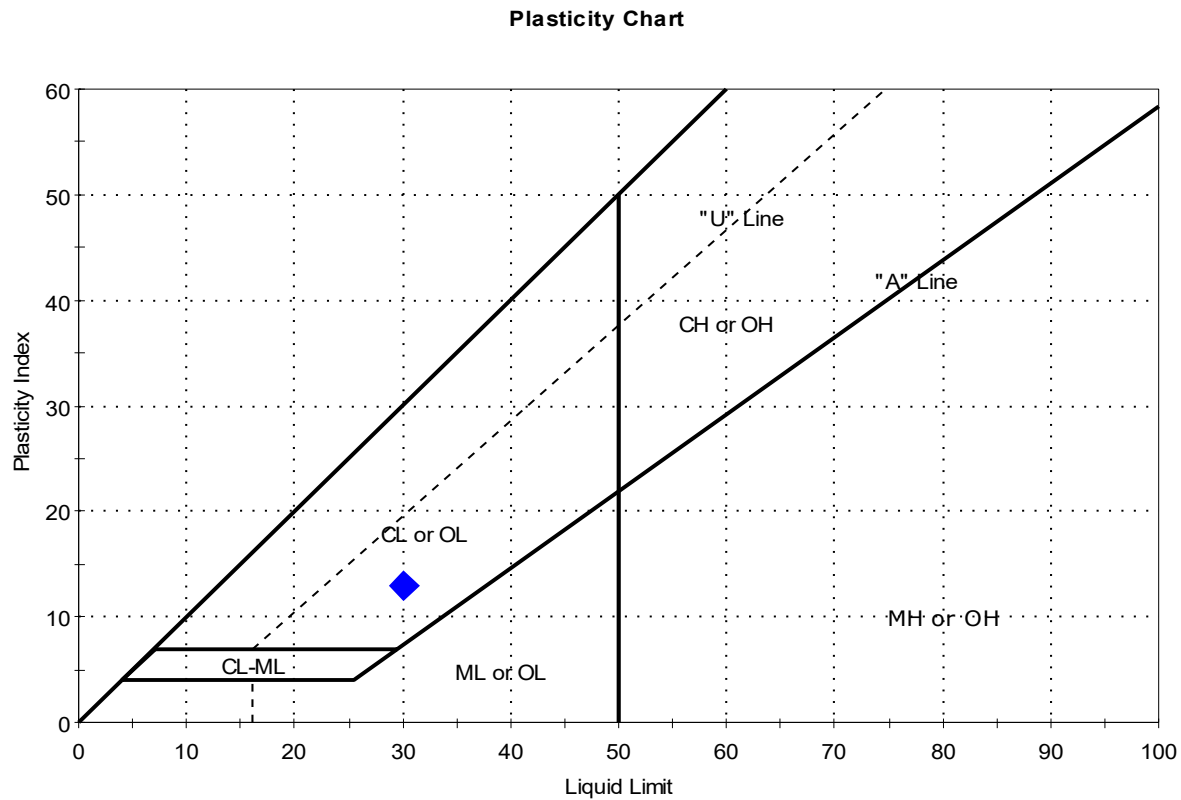
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH	Boring ID: BB-BSA-104	Sample Type: Jar
	Sample ID: 6D	Test Date: 08/16/24
	Depth: 15-17 ft	Test Id: 780409
Test Comment: ---		
Visual Description: Moist, grayish brown clay		
Sample Comment: ---		

Atterberg Limits - ASTM D4318

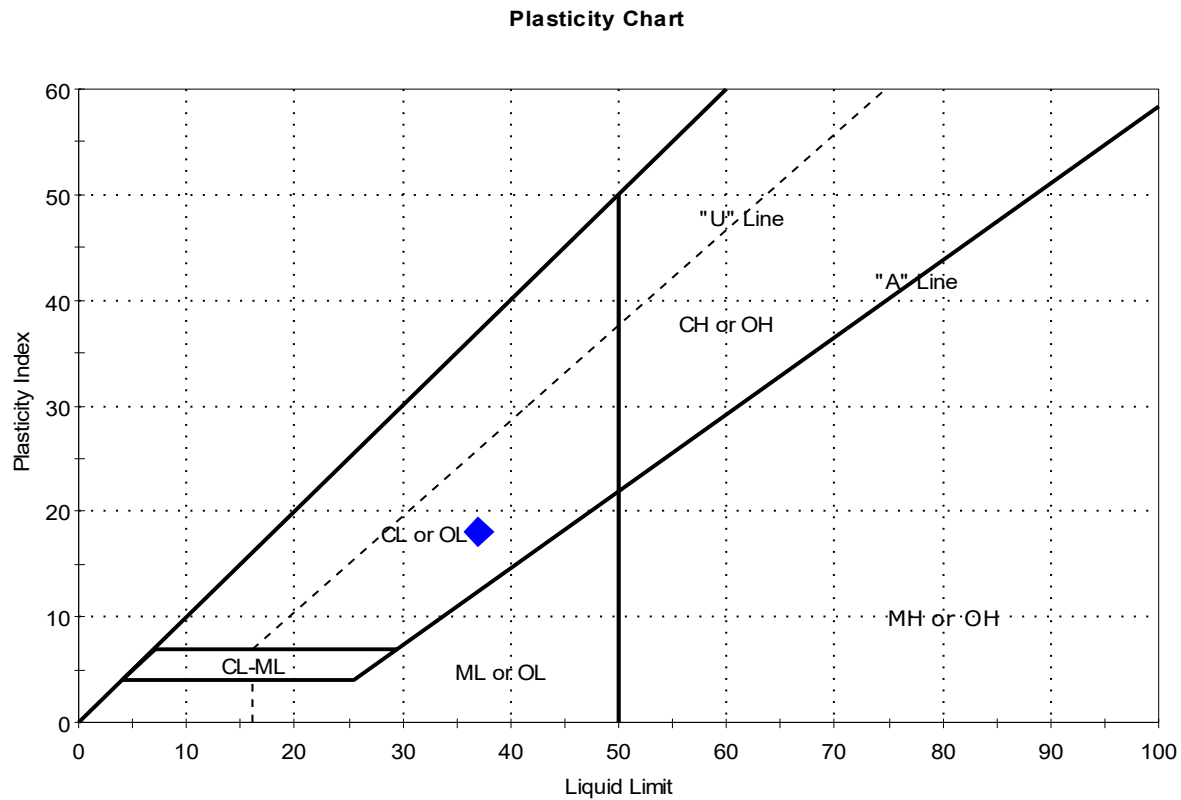


Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	6D	B-BSA-10	15-17 ft	25	30	17	13	0.6	Lean CLAY (CL)

Sample Prepared using the WET method
 5% Retained on #40 Sieve
 Dry Strength: VERY HIGH
 Dilatancy: SLOW
 Toughness: LOW

Client:	WSP USA, Inc.			Project No:	GTX-319180
Project:	MaineDOT I-95 Bridge over Stillwater				
Location:	Merrimack, NH				
Boring ID:	BB-BSA-106	Sample Type:	Jar	Tested By:	cam
Sample ID:	7D	Test Date:	08/19/24	Checked By:	ank
Depth :	20-22 ft	Test Id:	780372		
Test Comment:	---				
Visual Description:	Moist, light olive brown clay				
Sample Comment:	---				

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	7D	B-BSA-10	20-22 ft	26	37	19	18	0.4	Lean CLAY (CL)

Sample Prepared using the WET method

0% Retained on #40 Sieve

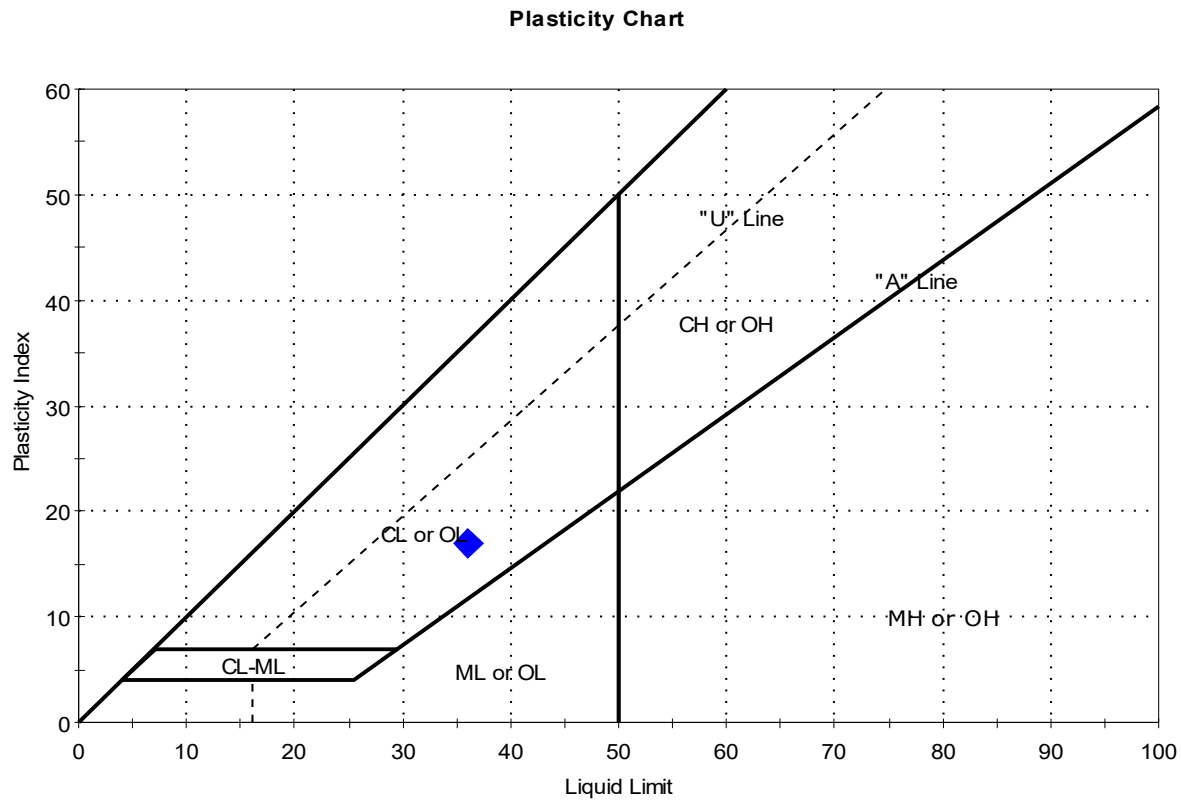
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	8D	Test Date:	08/19/24
Depth :	25-27 ft	Test Id:	780373
Test Comment:	---		
Visual Description:	Moist, grayish brown clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	8D	B-BSA-10	25-27 ft	28	36	19	17	0.5	Lean CLAY (CL)

Sample Prepared using the WET method

0% Retained on #40 Sieve

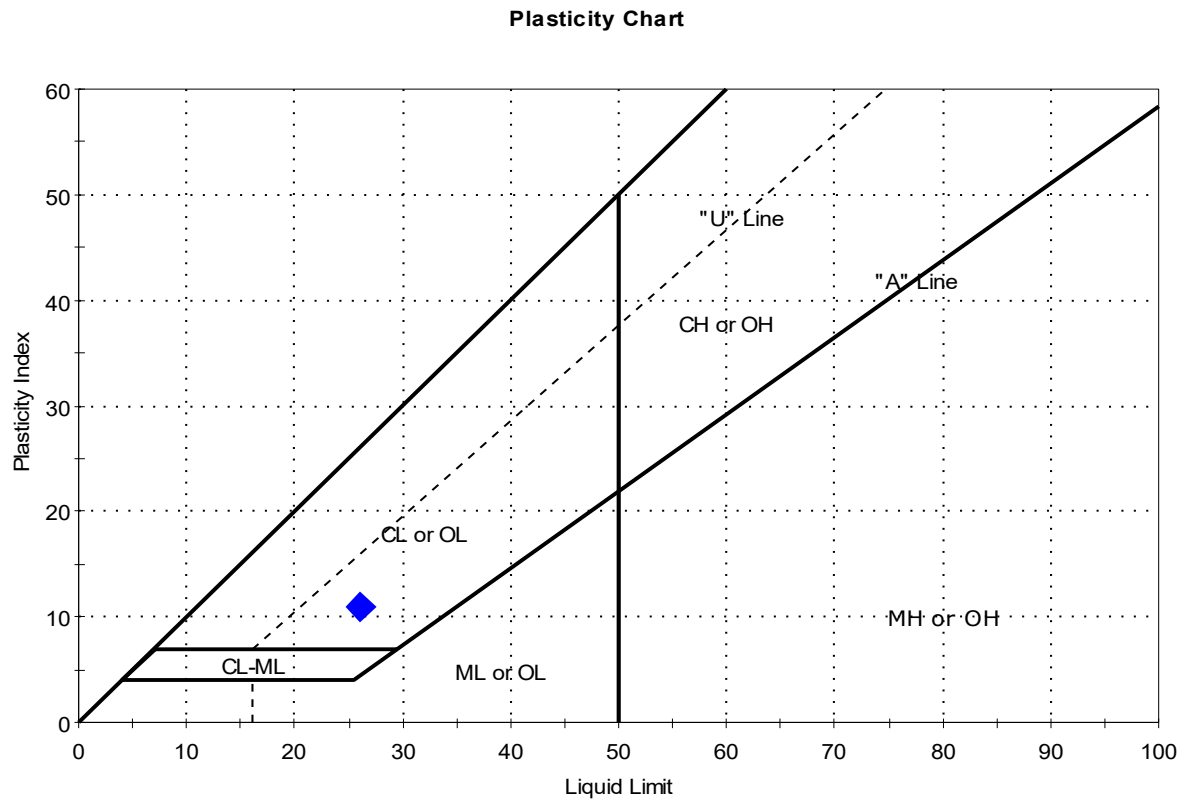
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	9D	Test Date:	08/16/24
Depth :	30-32 ft	Test Id:	780374
Test Comment:	---		
Visual Description:	Moist, gray clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	9D	B-BSA-10	30-32 ft	29	26	15	11	1.3	Lean CLAY (CL)

Sample Prepared using the WET method

1% Retained on #40 Sieve

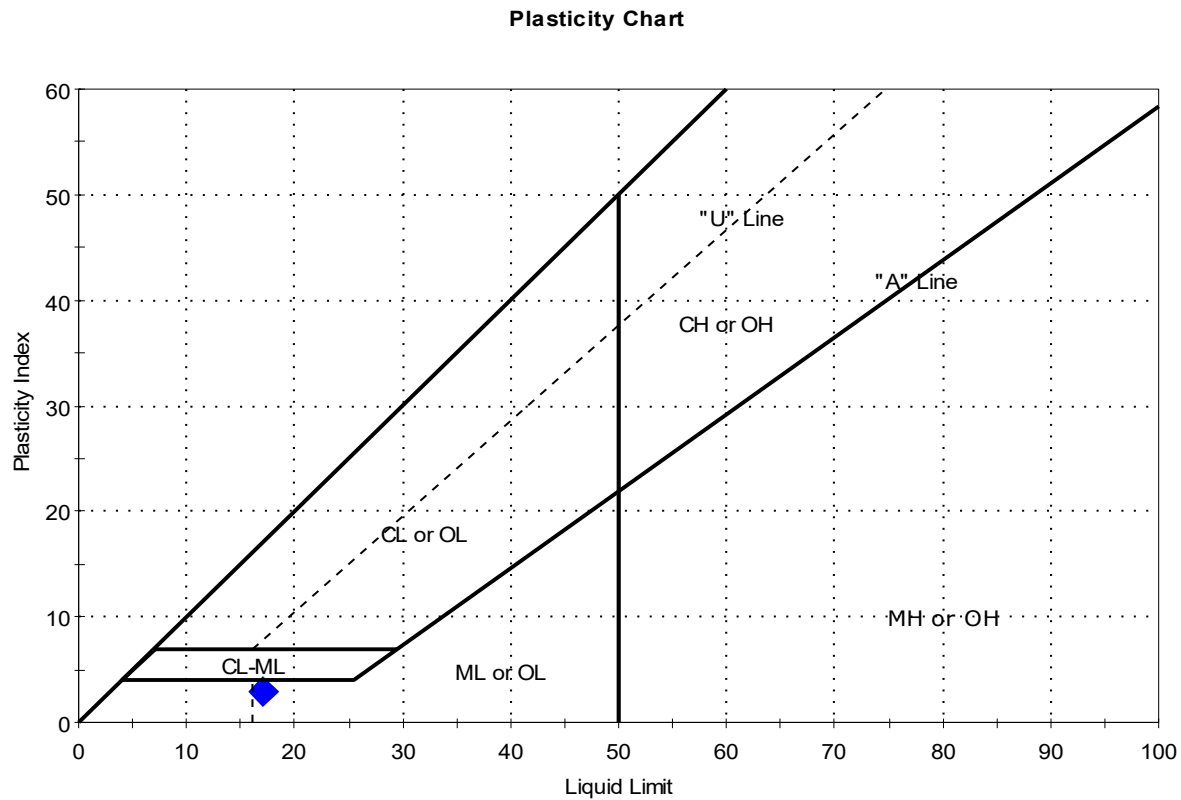
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-106	Sample Type:	Jar
Sample ID:	11D	Test Date:	08/16/24
Depth :	40-42 ft	Test Id:	780375
Test Comment:	---		
Visual Description:	Moist, gray sandy silt		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	11D	B-BSA-10	40-42 ft	11	17	14	3	-0.8	Sandy SILT (ML)

Sample Prepared using the WET method

23% Retained on #40 Sieve

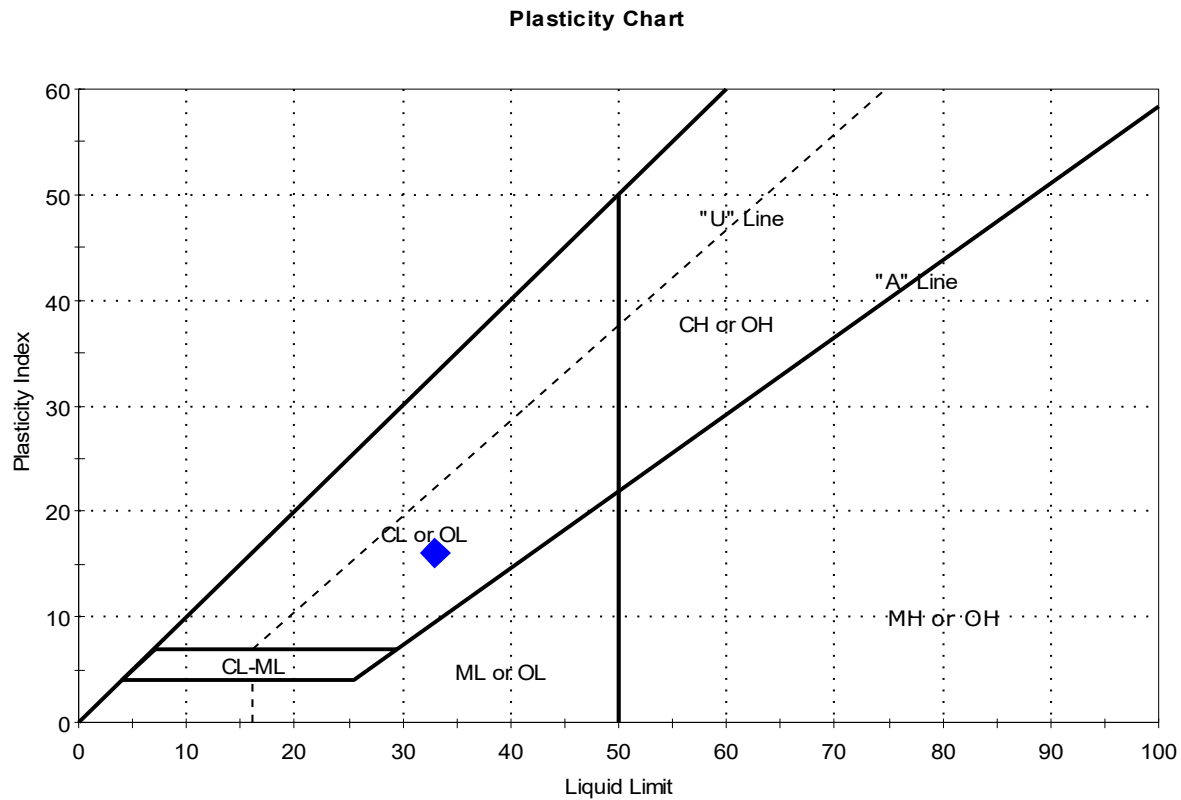
Dry Strength: n/a

Dilatancy: n/a

Toughness: n/a

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-107	Sample Type: Jar	Tested By: cam
Sample ID: 8D	Test Date: 08/19/24	Checked By: ank
Depth : 20-22 ft	Test Id: 780386	
Test Comment: ---		
Visual Description: Moist, grayish brown clay		
Sample Comment: ---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	8D	B-BSA-10	20-22 ft	24	33	17	16	0.4	Lean CLAY (CL)

Sample Prepared using the WET method

0% Retained on #40 Sieve

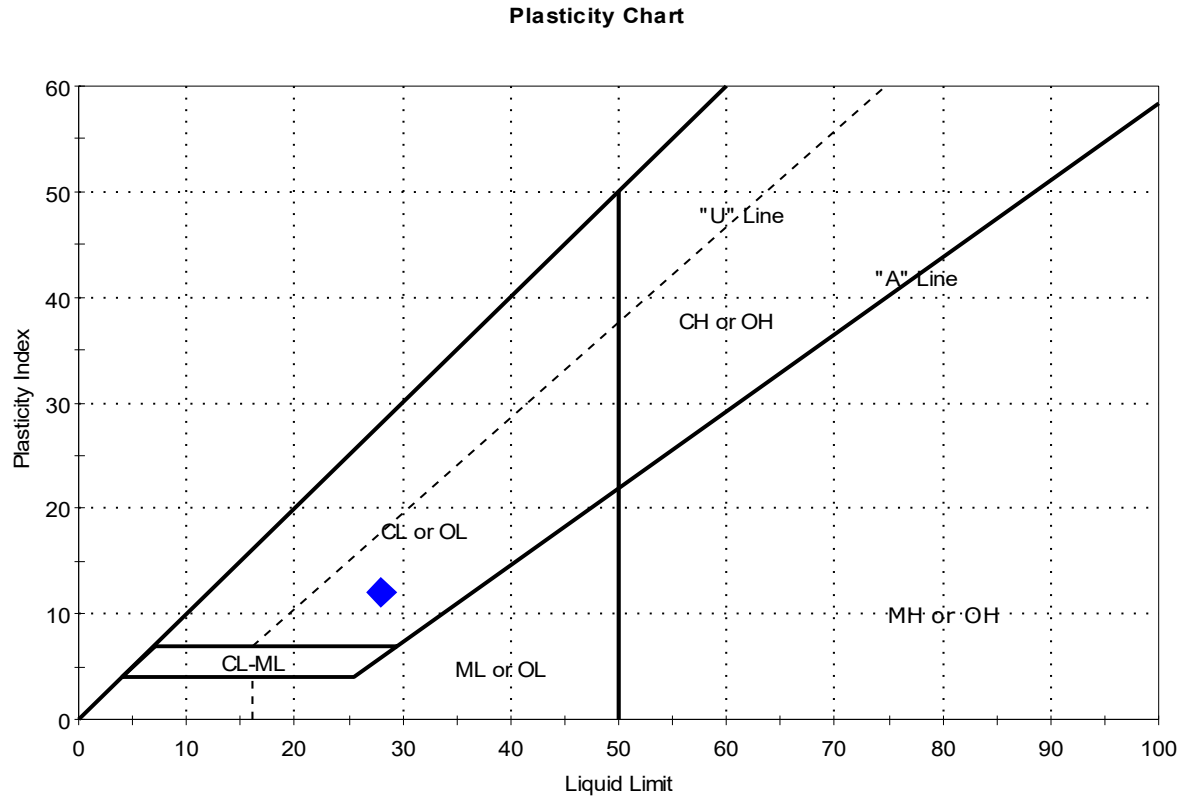
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	10D	Test Date:	08/19/24
Depth :	30-32 ft	Test Id:	780388
Test Comment:	---		
Visual Description:	Moist, grayish brown clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	10D	B-BSA-10	30-32 ft	28	28	16	12	1	Lean CLAY (CL)

Sample Prepared using the WET method

0% Retained on #40 Sieve

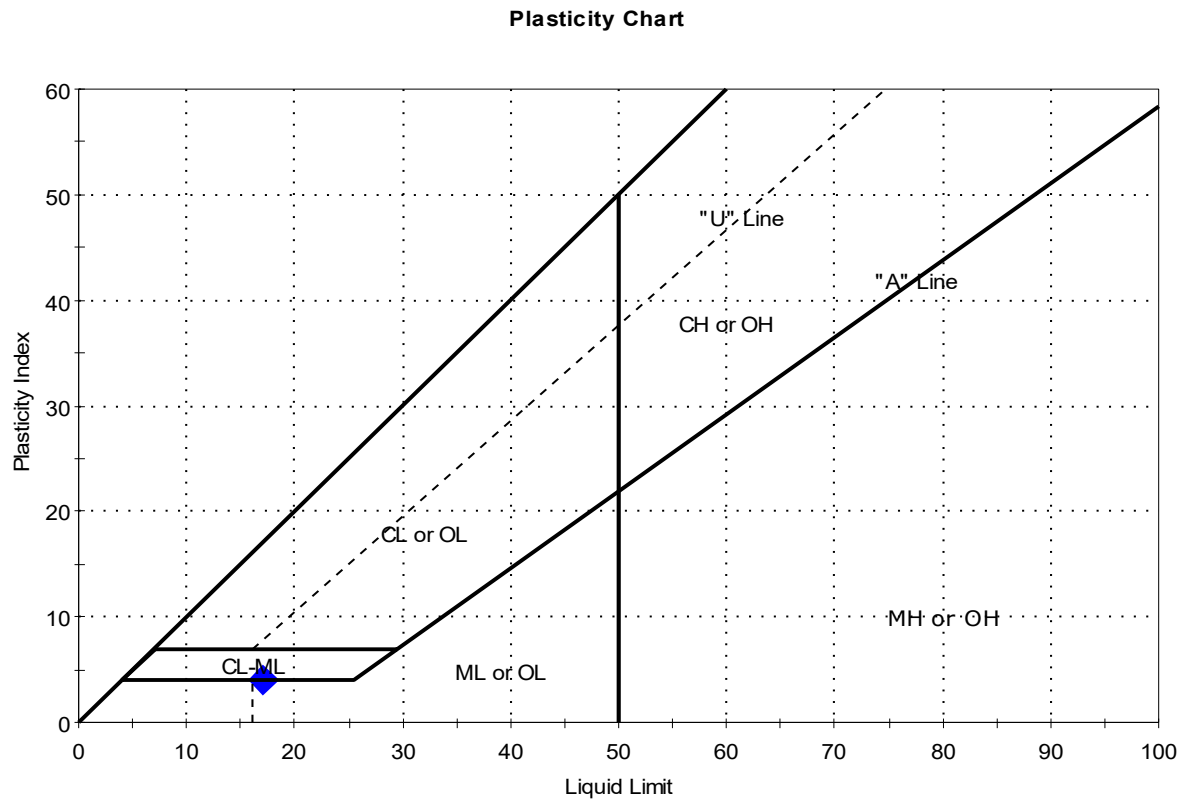
Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	12D	Test Date:	08/16/24
Depth :	40-42 ft	Test Id:	780389
Test Comment:	---		
Visual Description:	Moist, brownish gray silty clayey sand with gravel		
Sample Comment:	---		

Atterberg Limits - ASTM D4318

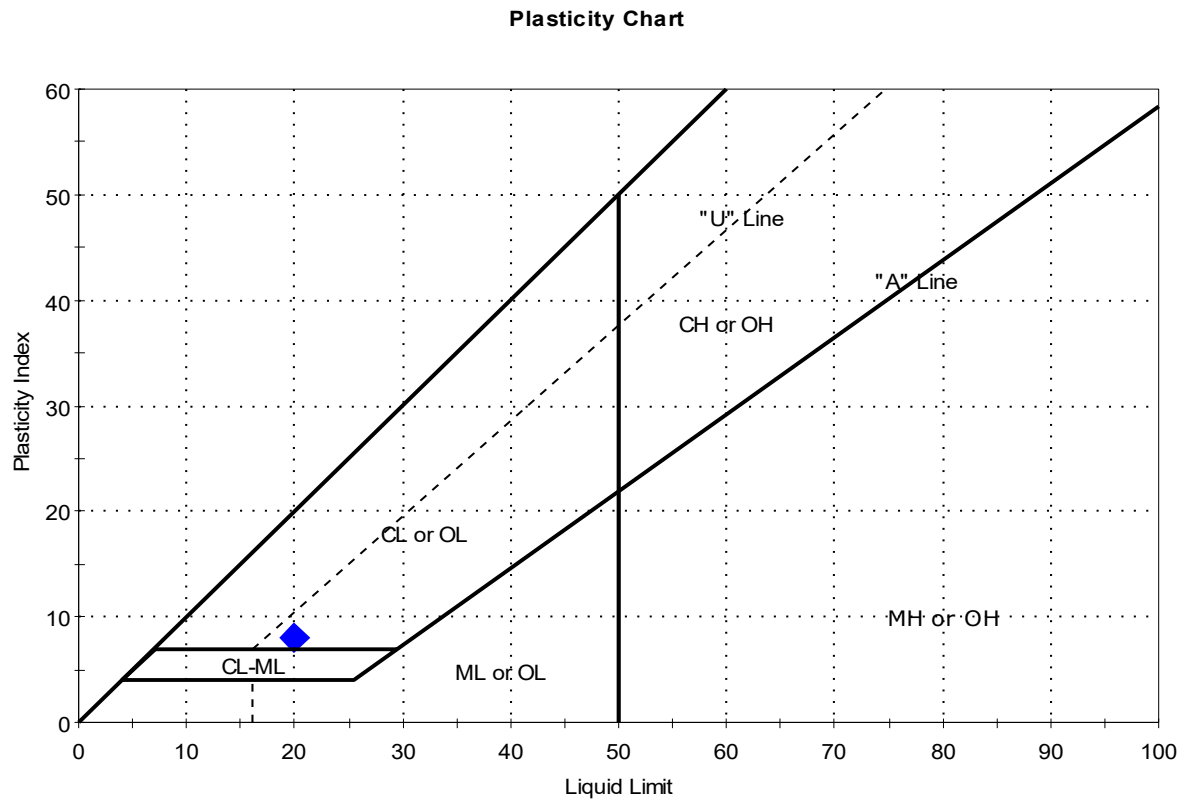


Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	12D	B-BSA-10	40-42 ft	10	17	13	4	-0.8	Silty, Clayey SAND with Gravel (SC-SM)

Sample Prepared using the WET method
 40% Retained on #40 Sieve
 Dry Strength: VERY HIGH
 Dilatancy: SLOW
 Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-107	Sample Type:	Jar
Sample ID:	14D	Test Date:	08/15/24
Depth :	50-52 ft	Test Id:	780390
Test Comment:	---		
Visual Description:	Moist, grayish brown clayey sand with gravel		
Sample Comment:	---		

Atterberg Limits - ASTM D4318

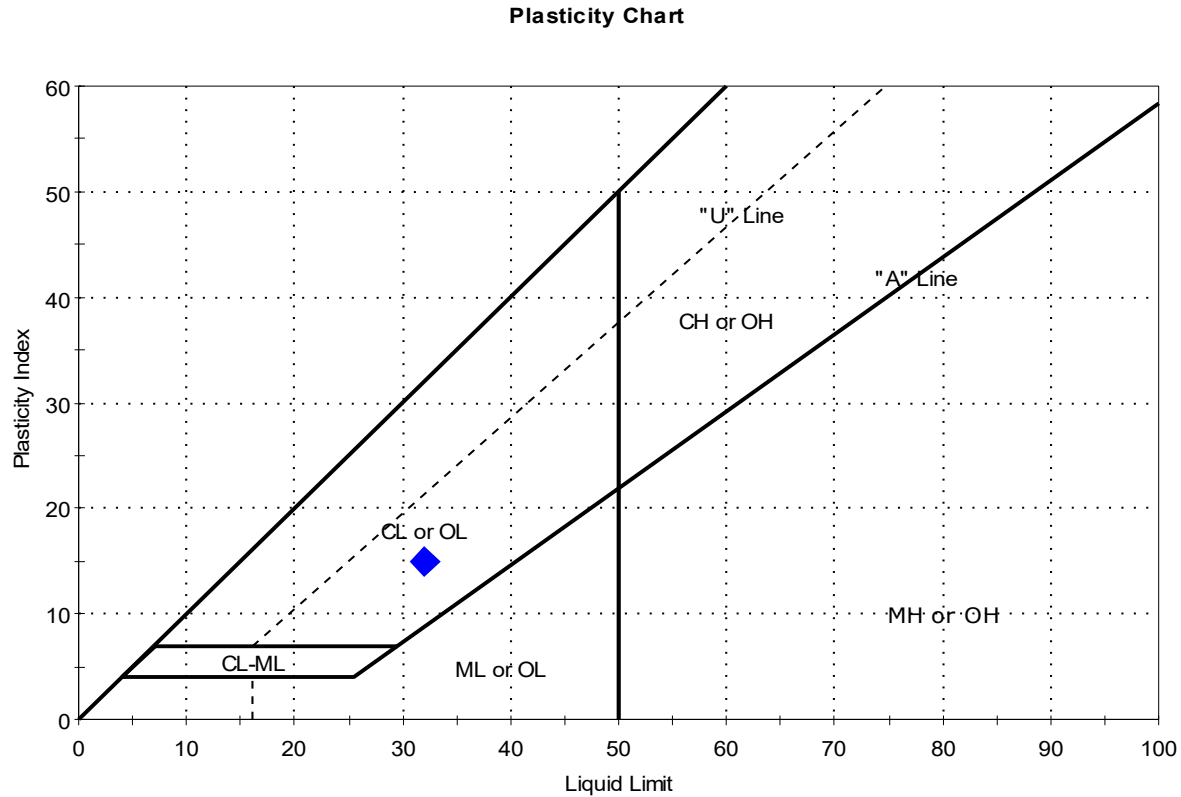


Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	14D	B-BSA-10	50-52 ft	10	20	12	8	-0.3	Clayey SAND with Gravel (SC)

Sample Prepared using the WET method
 46% Retained on #40 Sieve
 Dry Strength: VERY HIGH
 Dilatancy: SLOW
 Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-111	Sample Type:	Jar
Sample ID:	5D	Test Date:	08/16/24
Depth :	10-12 ft	Test Id:	780417
Test Comment:	---		
Visual Description:	Moist, olive brown clay		
Sample Comment:	---		

Atterberg Limits - ASTM D4318



Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	5D	B-BSA-11	10-12 ft	21	32	17	15	0.3	Lean CLAY (CL)

Sample Prepared using the WET method

0% Retained on #40 Sieve

Dry Strength: VERY HIGH

Dilatancy: SLOW

Toughness: LOW

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	06/05/24
Depth :	---	Test Id:	771711
		Tested By:	ajl
		Checked By:	ank

Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
BB-BSA-102	1D	1-3ft	Moist, brown silty sand with gravel	3.7
BB-BSA-102	2D	3-5ft	Moist, brown silty sand with gravel	8.6
BB-BSA-102	5D	9-11ft	Moist, light brown silty gravel with sand	15.5
BB-BSA-108	1D	0-2ft	Moist, yellowish brown silty sand with gravel	8.0
BB-BSA-109	2D	3-5ft	Moist, grayish brown silty gravel with sand	5.7
BB-BSA-109	4D	7-9ft	Moist, brown silty sand with gravel	11.7

Notes: Temperature of Drying : 110° Celsius



Client:	WSP USA, Inc.		Project No:	GTX-319180
Project:	MaineDOT I-95 Bridge over Stillwater			
Location:	Merrimack, NH			
Boring ID:	---	Sample Type:	---	Tested By: ajl
Sample ID:	---	Test Date:	06/07/24	Checked By: ank
Depth :	---	Test Id:	771713	

pH of Soil by ASTM D4972

Boring ID	Sample ID	Depth	Visual Description	pH of Soil in Distilled Water	pH of Soil in Calcium Chloride
BB-BSA-102	1D	1-3ft	Moist, brown silty sand with gravel	7.9	7.2
BB-BSA-109	2D	3-5ft	Moist, grayish brown silty gravel with sand	8.2	7.3

Notes: Sample Preparation: screened through #10 sieve
Method A, pH meter used



Client:	WSP USA, Inc.
Project:	MaineDOT I-95 Bridge Over Stillwater
Location:	Merrimack, NH
GTX#:	319180
Test Date:	06/10/24
Due Date:	06/13/24
Tested By:	NMK
Checked By:	ank

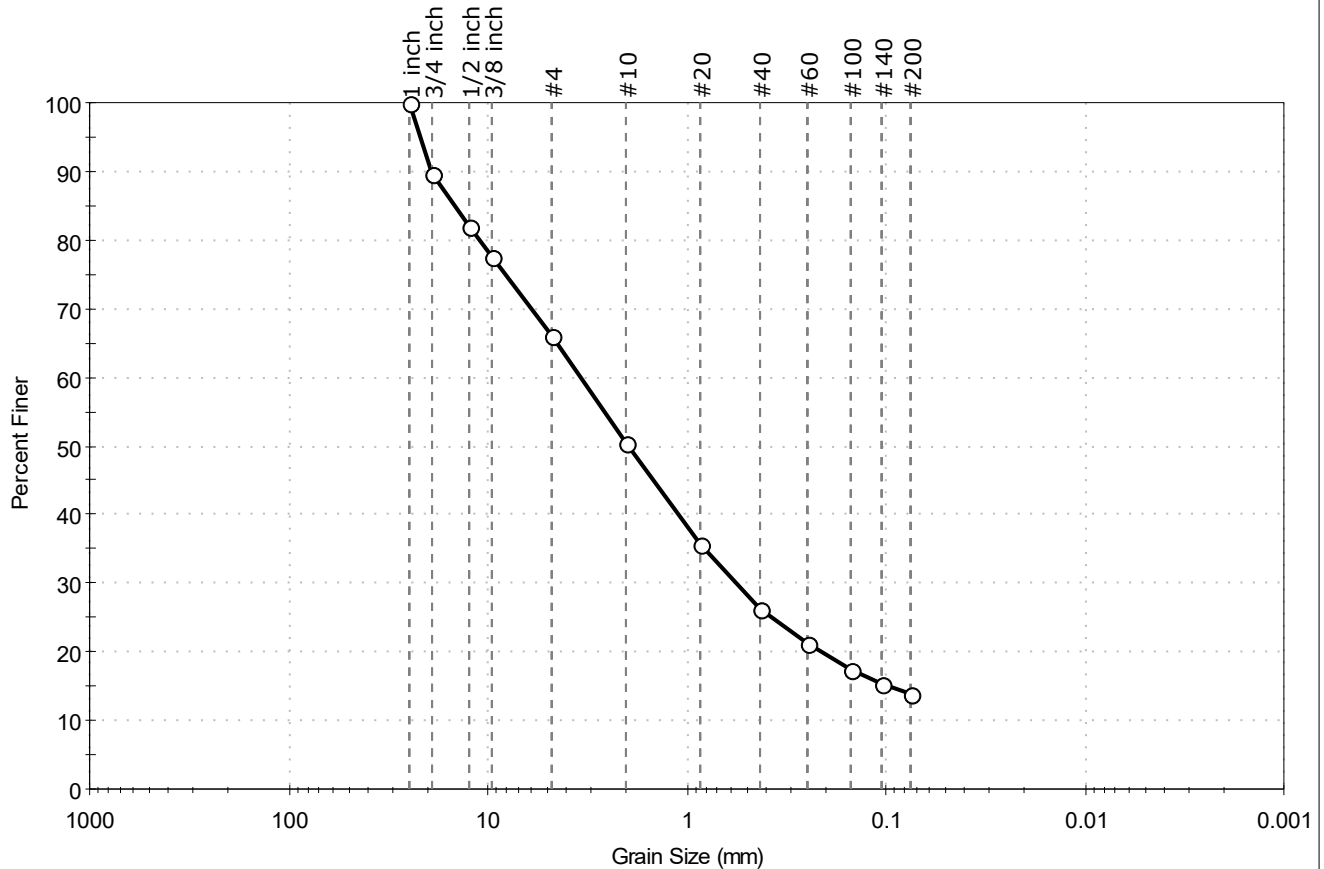
Laboratory Measurement of Soil Resistivity Using the Wenner Four-Electrode Method by ASTM G57 (Laboratory Measurement)

Boring ID	Sample ID	Depth, ft.	Sample Description	Electrical Resistivity, ohm-cm	Electrical Conductivity, (ohm-cm) ⁻¹
BB-BSA-102	1D	1-3 ft	Moist, brown silty gravel	1,202	8.32E-04

Notes: Test Equipment: Nilsson Model 400 Soil Resistance Meter, MC Miller Soil Box
Water added to sample to create a thick slurry prior to testing (saturated condition).
Electrical Conductivity is calculated as inverse of Electrical Resistivity (per ASTM G57)
Test conducted in standard laboratory atmosphere: 68-73 F

Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-102	Sample Type:	Jar
Sample ID:	1D	Test Date:	06/10/24
Depth :	1-3ft	Test Id:	771699
Test Comment:	---		
Visual Description:	Moist, brown silty sand with gravel		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	34.0	52.0	14.0

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	90		
1/2 inch	12.50	82		
3/8 inch	9.50	78		
#4	4.75	66		
#10	2.00	51		
#20	0.85	36		
#40	0.42	26		
#60	0.25	21		
#100	0.15	17		
#140	0.11	15		
#200	0.075	14		

Coefficients

$D_{85} = 14.7631 \text{ mm}$ $D_{30} = 0.5584 \text{ mm}$
 $D_{60} = 3.3977 \text{ mm}$ $D_{15} = 0.0975 \text{ mm}$
 $D_{50} = 1.9370 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

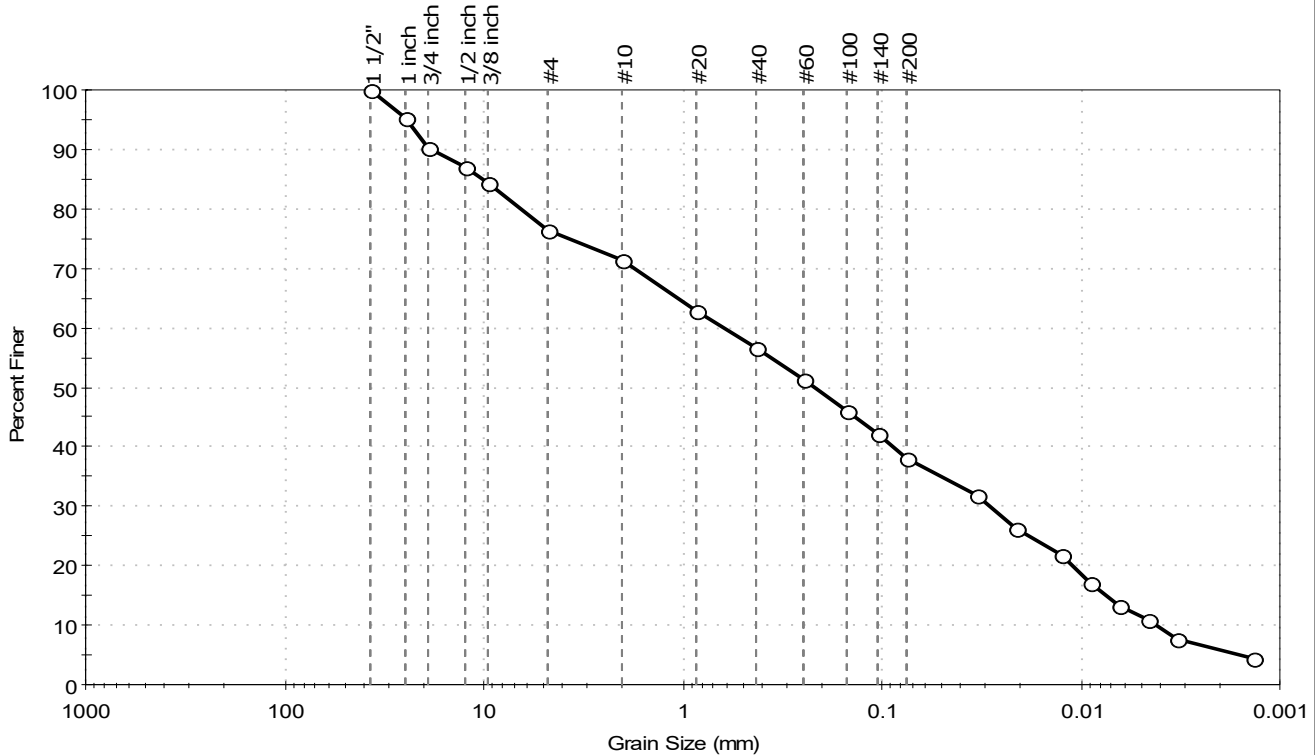
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-102	Sample Type: Jar
Sample ID: 2D	Tested By: ajl
Depth: 3-5ft	Test Date: 06/11/24
	Checked By: ank
	Test Id: 771725
Test Comment: ---	
Visual Description: Moist, brown silty sand with gravel	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913/D7928



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	23.6	38.4	38.0

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	95		
3/4 inch	19.00	90		
1/2 inch	12.50	87		
3/8 inch	9.50	84		
#4	4.75	76		
#10	2.00	71		
#20	0.85	63		
#40	0.42	57		
#60	0.25	51		
#100	0.15	46		
#140	0.11	42		
#200	0.075	38		
Hydrometer	Particle Size (mm)	Percent Finer	Spec. Percent	Complies
---	0.030	32		
---	0.0213	26		
---	0.0125	22		
---	0.0090	17		
---	0.0065	13		
---	0.0046	11		
---	0.0033	8		
---	0.0014	4		

Coefficients

$D_{85} = 10.2078 \text{ mm}$ $D_{30} = 0.0286 \text{ mm}$
 $D_{60} = 0.6168 \text{ mm}$ $D_{15} = 0.0074 \text{ mm}$
 $D_{50} = 0.2201 \text{ mm}$ $D_{10} = 0.0042 \text{ mm}$
 $C_u = 146.857$ $C_c = 0.316$

Classification

ASTM N/A

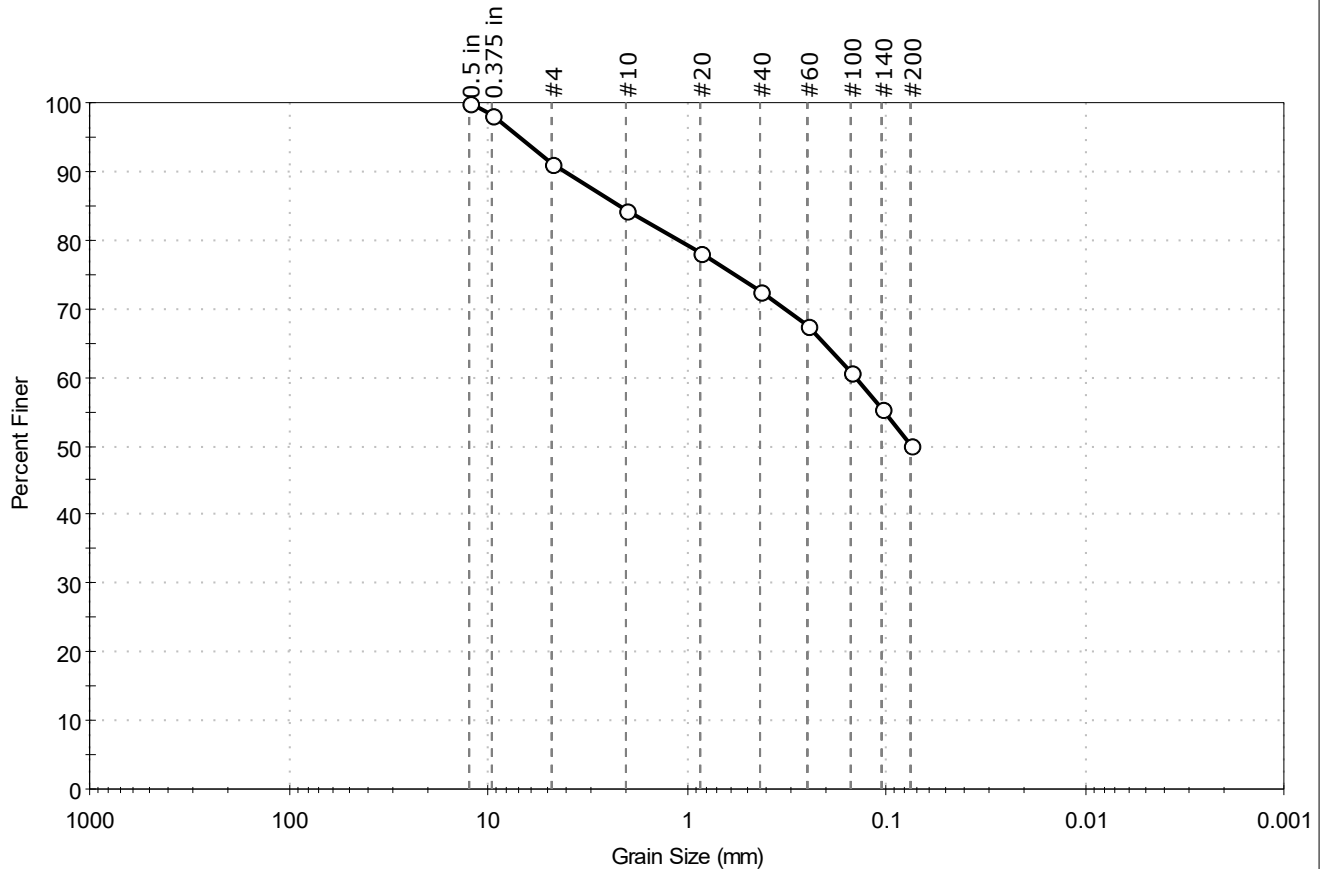
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD
 Dispersion Device : Apparatus A - Mech Mixer
 Dispersion Period : 1 minute
 Est. Specific Gravity : 2.65
 Separation of Sample: #200 Sieve

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-102	Sample Type: Jar	Tested By: ajl
Sample ID: 4D	Test Date: 06/11/24	Checked By: ank
Depth: 7-9ft	Test Id: 771701	
Test Comment: ---		
Visual Description: Moist, brown sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	8.7	41.1	50.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.5 in	12.50	100		
0.375 in	9.50	98		
#4	4.75	91		
#10	2.00	84		
#20	0.85	78		
#40	0.42	73		
#60	0.25	67		
#100	0.15	61		
#140	0.11	55		
#200	0.075	50		

Coefficients

$D_{85} = 2.1488 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.1431 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM Sandy SILT (ML)

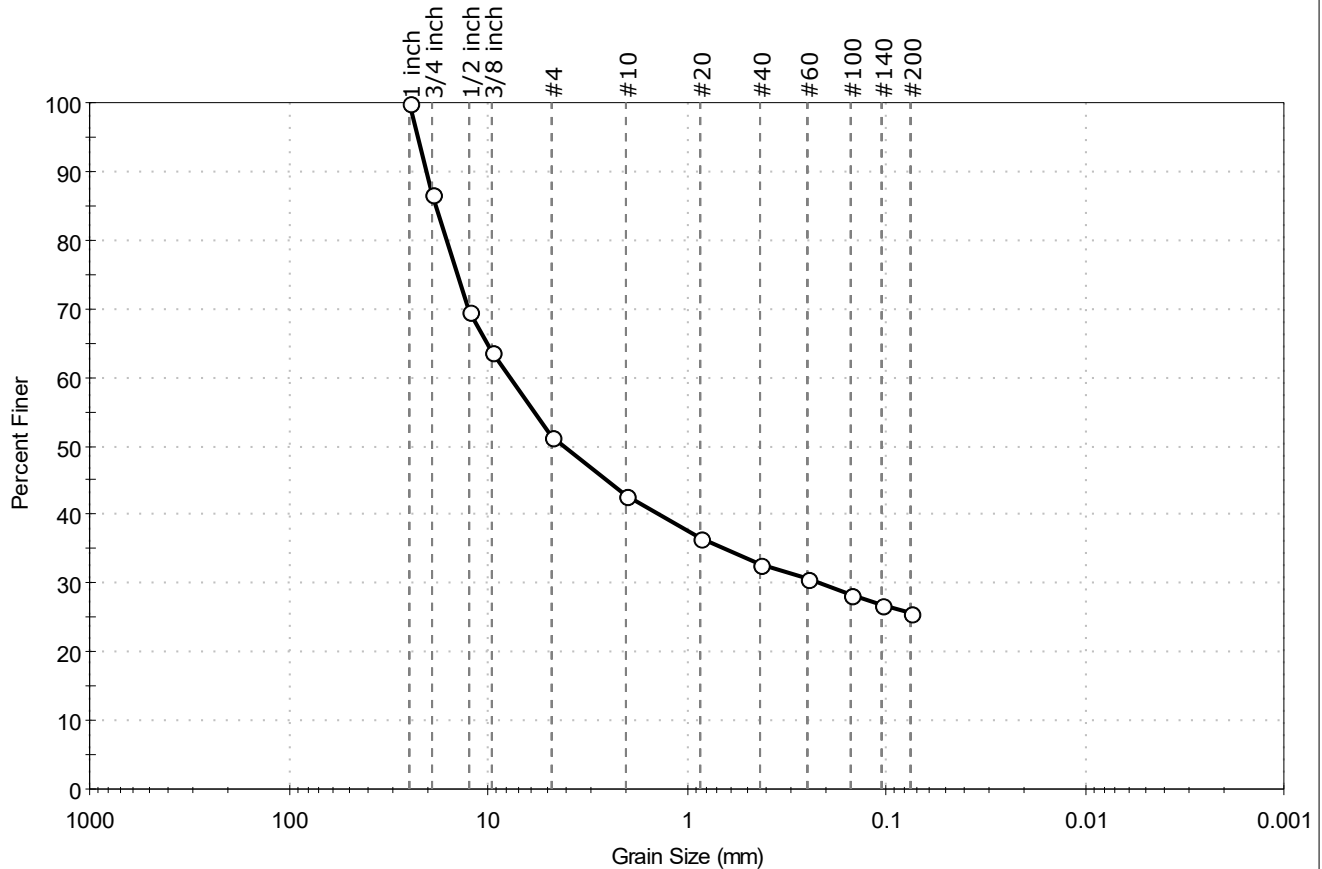
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-102	Sample Type: Jar	Tested By: ajl
Sample ID: 5D	Test Date: 06/10/24	Checked By: ank
Depth : 9-11ft	Test Id: 771702	
Test Comment: ---		
Visual Description: Moist, light brown silty gravel with sand		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	48.7	25.7	25.6

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 inch	25.00	100		
3/4 inch	19.00	87		
1/2 inch	12.50	70		
3/8 inch	9.50	64		
#4	4.75	51		
#10	2.00	43		
#20	0.85	36		
#40	0.42	33		
#60	0.25	31		
#100	0.15	28		
#140	0.11	27		
#200	0.075	26		

Coefficients

$D_{85} = 18.2066 \text{ mm}$ $D_{30} = 0.2200 \text{ mm}$
 $D_{60} = 7.7553 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 4.1504 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

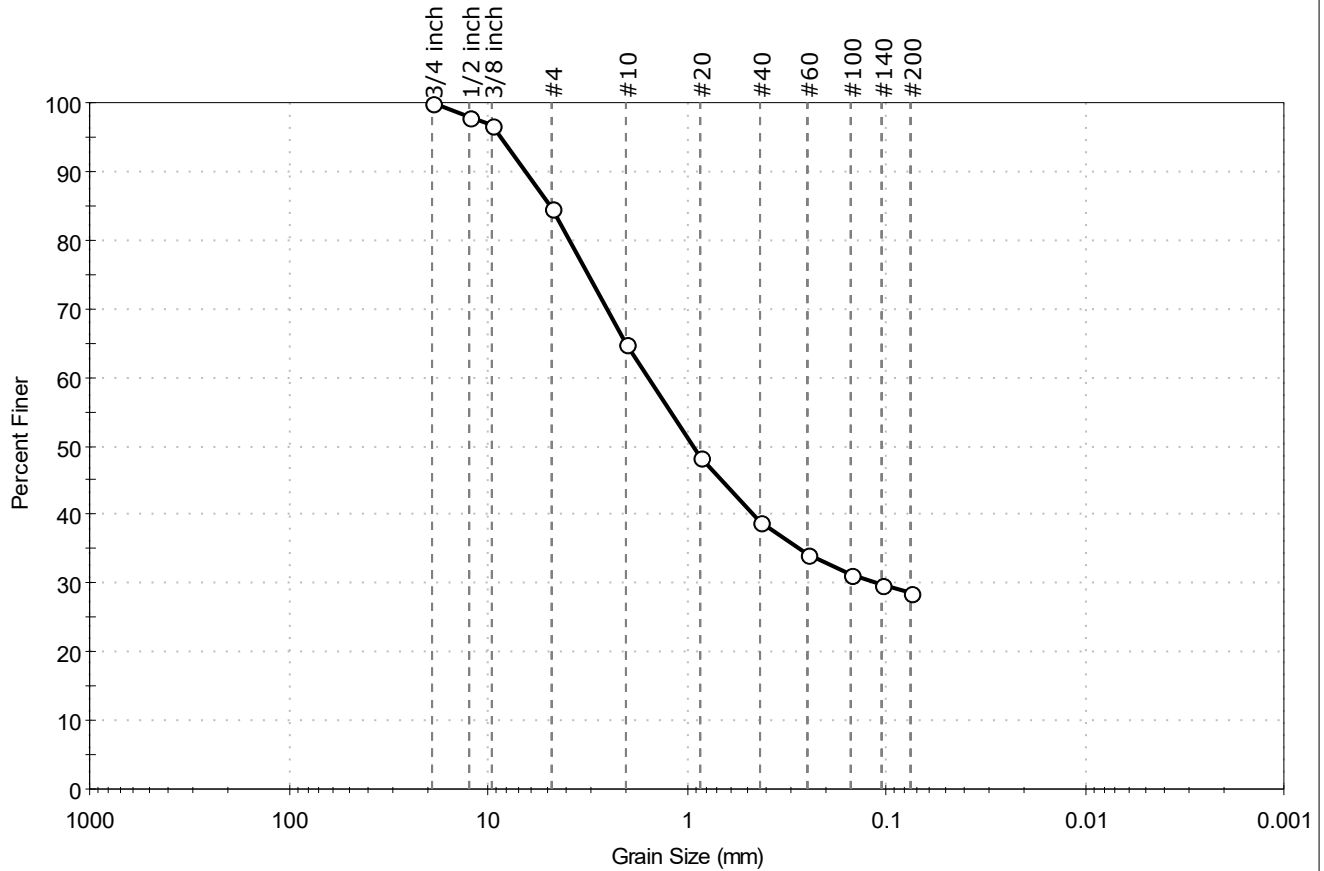
AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-108	Sample Type: Jar
Sample ID: 1D	Test Date: 06/10/24
Depth: 0-2ft	Test Id: 771703
Test Comment: ---	Tested By: ajl
Visual Description: Moist, yellowish brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	15.4	56.1	28.5

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
3/4 inch	19.00	100		
1/2 inch	12.50	98		
3/8 inch	9.50	97		
#4	4.75	85		
#10	2.00	65		
#20	0.85	48		
#40	0.42	39		
#60	0.25	34		
#100	0.15	31		
#140	0.11	30		
#200	0.075	28		

Coefficients

D₈₅ = 4.8781 mm D₃₀ = 0.1095 mm
 D₆₀ = 1.5572 mm D₁₅ = N/A
 D₅₀ = 0.9286 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM N/A

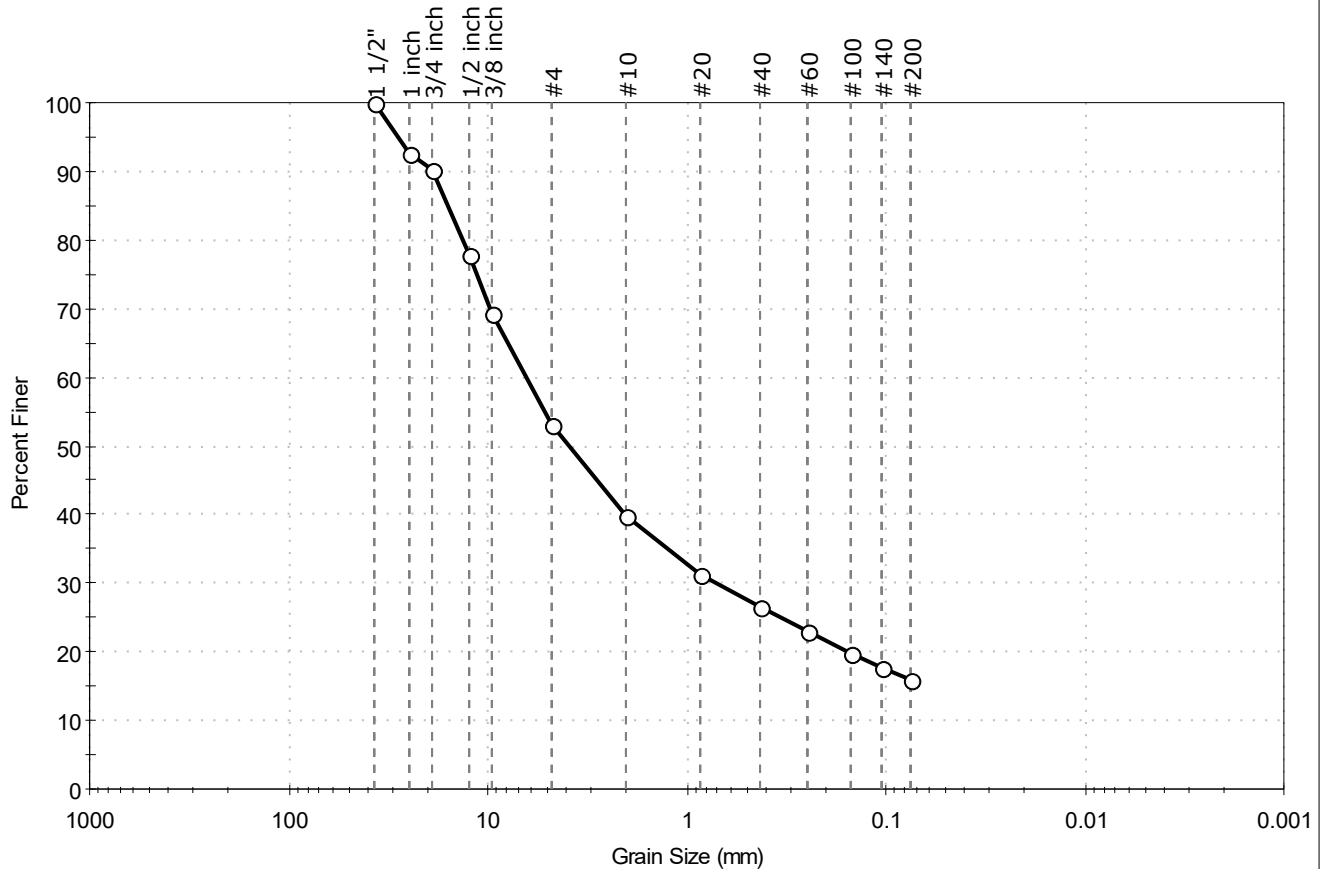
AASHTO Silty Gravel and Sand (A-2-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180
Project: MaineDOT I-95 Bridge over Stillwater	
Location: Merrimack, NH	
Boring ID: BB-BSA-109	Sample Type: Jar
Sample ID: 2D	Test Date: 06/11/24
Depth: 3-5ft	Test Id: 771704
Test Comment: ---	Tested By: ajl
Visual Description: Moist, grayish brown silty gravel with sand	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	46.8	37.3	15.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	93		
3/4 inch	19.00	90		
1/2 inch	12.50	78		
3/8 inch	9.50	69		
#4	4.75	53		
#10	2.00	40		
#20	0.85	31		
#40	0.42	26		
#60	0.25	23		
#100	0.15	20		
#140	0.11	18		
#200	0.075	16		

Coefficients

$D_{85} = 15.9069 \text{ mm}$ $D_{30} = 0.7017 \text{ mm}$
 $D_{60} = 6.3678 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 3.8773 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

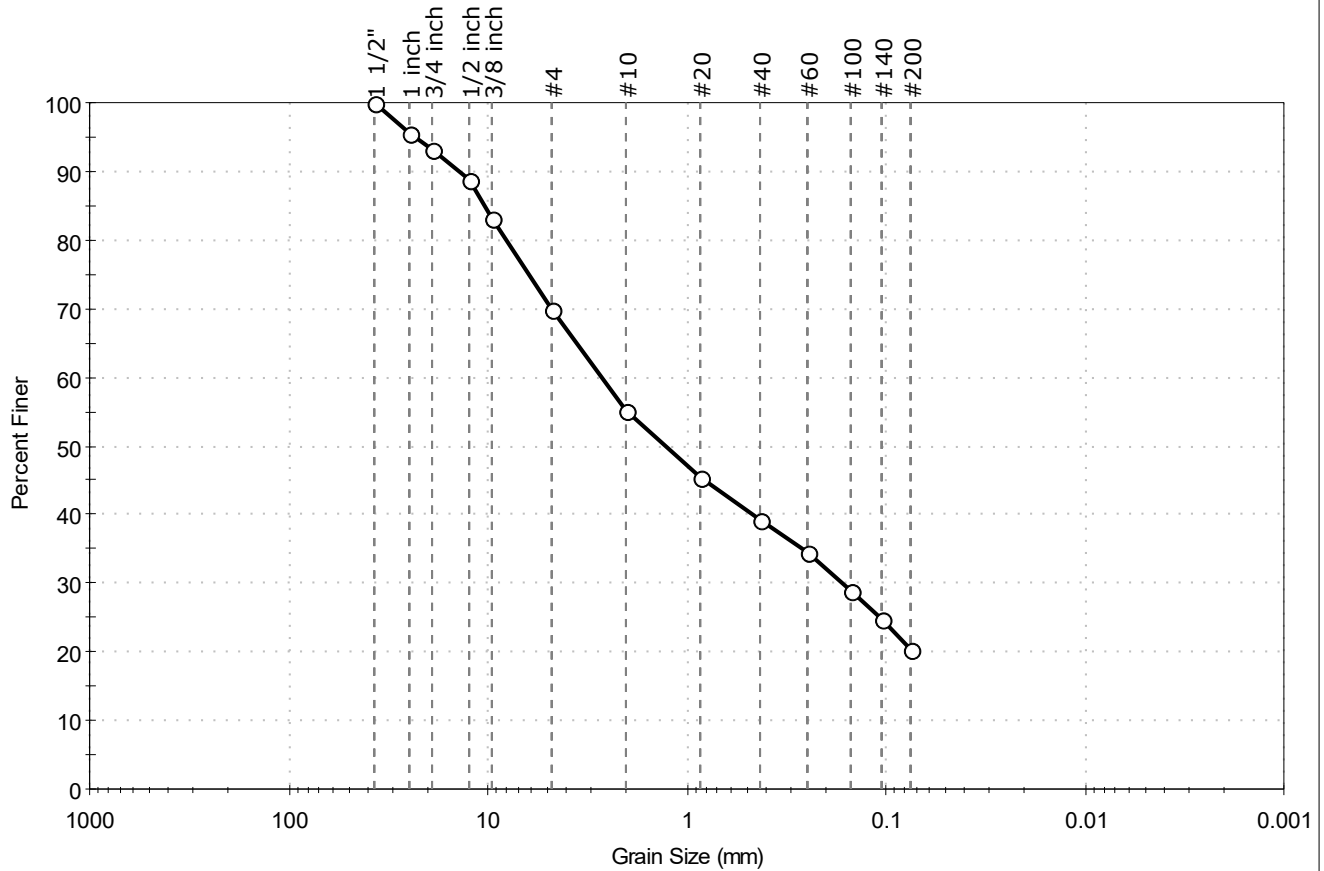
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-319180	
Project: MaineDOT I-95 Bridge over Stillwater		
Location: Merrimack, NH		
Boring ID: BB-BSA-109	Sample Type: Jar	Tested By: ajl
Sample ID: 4D	Test Date: 06/10/24	Checked By: ank
Depth: 7-9ft	Test Id: 771705	
Test Comment: ---		
Visual Description: Moist, brown silty sand with gravel		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	30.1	49.6	20.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 1/2"	37.50	100		
1 inch	25.00	96		
3/4 inch	19.00	93		
1/2 inch	12.50	89		
3/8 inch	9.50	83		
#4	4.75	70		
#10	2.00	55		
#20	0.85	45		
#40	0.42	39		
#60	0.25	35		
#100	0.15	29		
#140	0.11	25		
#200	0.075	20		

Coefficients

$D_{85} = 10.4311 \text{ mm}$ $D_{30} = 0.1670 \text{ mm}$
 $D_{60} = 2.6443 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 1.2721 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD



Client:	WSP USA, Inc.		
Project:	MaineDOT I-95 Bridge over Stillwater		
Location:	Merrimack, NH	Project No:	GTX-319180
Boring ID:	BB-BSA-102	Sample Type:	Jar
Sample ID:	4D	Test Date:	06/10/24
Depth :	7-9ft	Test Id:	771698
Test Comment:	---		
Visual Description:	Moist, brown sandy silt		
Sample Comment:	---		

Atterberg Limits - ASTM D4318

Sample Determined to be non-plastic

Symbol	Sample ID	Boring	Depth	Natural Moisture Content, %	Liquid Limit	Plastic Limit	Plasticity Index	Liquidity Index	Soil Classification
◆	4D	B-BSA-10	7-9ft	13	n/a	n/a	n/a	n/a	Sandy SILT (ML)

27% Retained on #40 Sieve

Dry Strength: n/a

Dilatancy: n/a

Toughness: n/a

The sample was determined to be Non-Plastic



GEOTESTING EXPRESS INCORPORATED
125 NAGOG PARK
ACTON MA 01720-3451
USA

Analysis No.	TS-A2411955
Report Date	14 June 2024
Date Sampled	12 June 2024
Date Received	13 June 2024
Where Sampled	Acton, MA USA
Sampled By	Client

When examined to the applicable requirements of:

AASHTO T 291-18	“Standard Method of Test for Determining Water-Soluble Chloride Ion Content in Soil” Method B
AASHTO T 290-20	“Standard Method of Test for Determining Water-Soluble Sulfate Ion Content in Soil”

AASHTO T 291 – Chloride (Method B)

Sample		Results		Minimum Detection Limit
		ppm (mg/kg)	% ¹	
BB-BSA-102		215.	0.0215	10.
1D	1 – 3'			
BB-BSA-109		59.	0.0059	
2D	3 – 5'			

NOTE: ¹Percent by weight after drying and prepared as per the Standard.

AASHTO T 290 – Sulfates (Soluble)

Sample		Results		Minimum Detection Limit
		ppm (mg/kg)	% ¹	
BB-BSA-102		< 10.	< 0.0010	10.
1D	1 – 3'			
BB-BSA-109		< 10.	< 0.0010	
2D	3 – 5'			

NOTE: ¹Percent by weight after drying and prepared as per the Standard.

END OF ANALYSIS

Merrill Lee

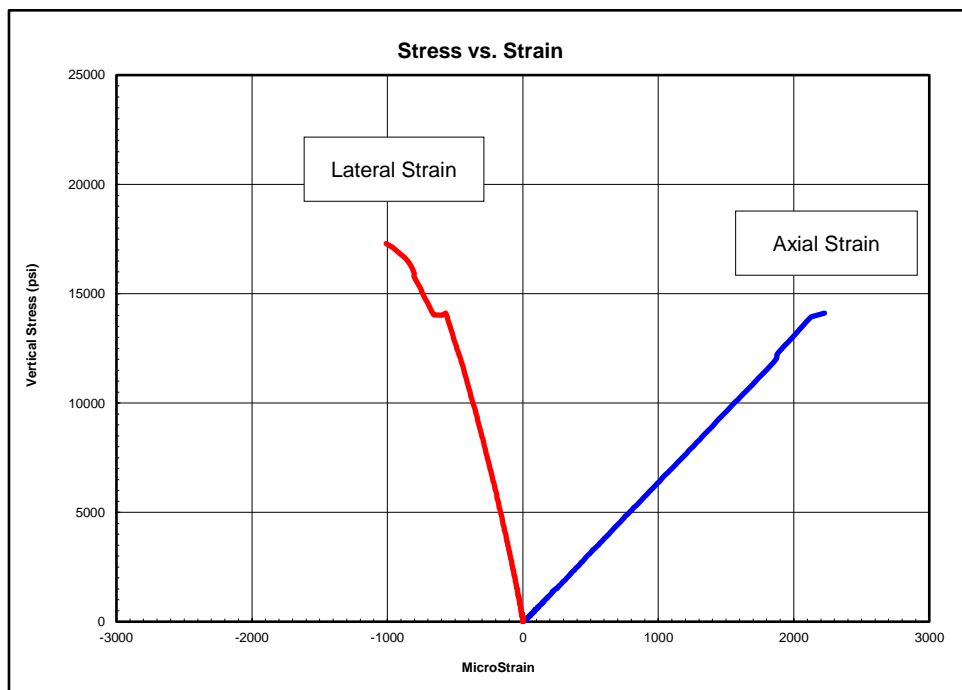
Merrill Gee P.E. – Engineer in Charge

Page 1 of 1



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-102
Sample ID:	R1
Depth, ft:	14.87-15.25
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 17,296 psi

The axial strain gauges failed before the peak value was attained. Young's Modulus and Poisson's Ratio could not be determined within the third stress range for this test.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
1700-6300	6,470,000	0.23
6300-11000	6,460,000	0.27
11000-15600	---	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

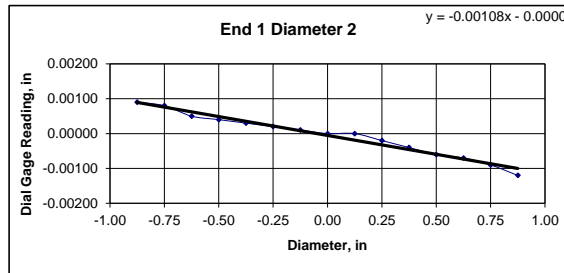
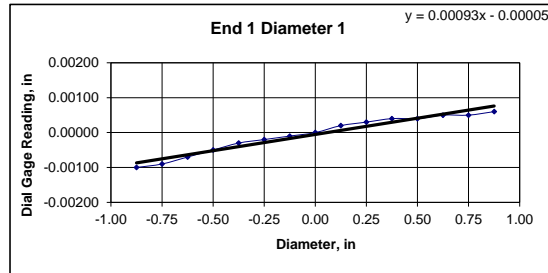


Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-102		
Sample ID:	R1		
Depth (ft):	14.87-15.25		
Visual Description:	See photographs		

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
Specimen Length, in:	1 4.38	2 4.38	Average 4.38	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.?	
Specimen Diameter, in:	1.97	1.97	1.97	YES	
Specimen Mass, g:	593.5			Maximum difference must be < 0.020 in.	
Bulk Density, lb/ft ³ :	169			Straightness Tolerance Met?	
Length to Diameter Ratio:	2.2			YES	
Minimum Diameter Tolerance Met?				YES	
Length to Diameter Ratio Tolerance Met?				YES	

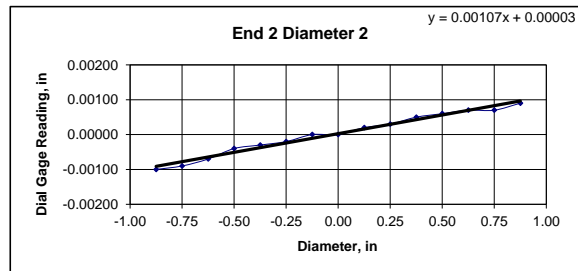
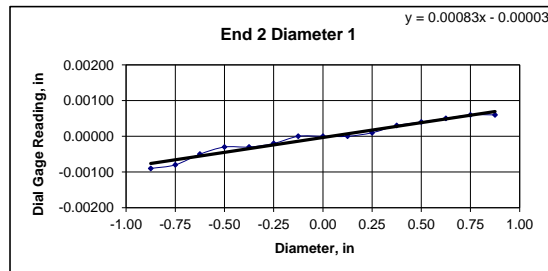
END FLATNESS AND PARALLELISM (Procedure FP1)														
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	-0.00100	-0.00090	-0.00070	-0.00050	-0.00030	-0.00020	-0.00010	0.00000	0.00020	0.00030	0.00040	0.00040	0.00050	0.00060
Diameter 2, in (rotated 90°)	0.00090	0.00080	0.00050	0.00040	0.00030	0.00020	0.00010	0.00000	0.00000	-0.00020	-0.00040	-0.00060	-0.00070	-0.00090
Difference between max and min readings, in:														
0° = 0.00160 90° = 0.00210														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	-0.00090	-0.00080	-0.00050	-0.00030	-0.00030	-0.00020	0.00000	0.00000	0.00000	0.00010	0.00030	0.00040	0.00050	0.00060
Diameter 2, in (rotated 90°)	-0.00100	-0.00090	-0.00070	-0.00040	-0.00030	-0.00020	0.00000	0.00000	0.00020	0.00030	0.00050	0.00060	0.00070	0.00090
Difference between max and min readings, in:														
0° = 0.0015 90° = 0.0019														
Maximum difference must be < 0.0020 in. Difference = ± 0.00105														
Flatness Tolerance Met?														
NO														



DIAMETER 1

End 1:	Slope of Best Fit Line	0.00093
	Angle of Best Fit Line:	0.05337
End 2:	Slope of Best Fit Line	0.00083
	Angle of Best Fit Line:	0.04764
Maximum Angular Difference:		0.00573

Parallelism Tolerance Met? NO
Spherically Seated



DIAMETER 2

End 1:	Slope of Best Fit Line	0.00108
	Angle of Best Fit Line:	0.06204
End 2:	Slope of Best Fit Line	0.00107
	Angle of Best Fit Line:	0.06139
Maximum Angular Difference:		0.00065

Parallelism Tolerance Met? YES
Spherically Seated

PERPENDICULARITY (Procedure P1)						(Calculated from End Flatness and Parallelism measurements above)	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$	
Diameter 1, in	0.00160	1.970	0.00081	0.047	YES	Perpendicularity Tolerance Met?	
Diameter 2, in (rotated 90°)	0.00210	1.970	0.00107	0.061	YES	YES	
END 2							
Diameter 1, in	0.00150	1.970	0.00076	0.044	YES		
Diameter 2, in (rotated 90°)	0.00190	1.970	0.00096	0.055	YES		



Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-102	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R1		
Depth (ft):	14.87-15.25		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543**

END FLATNESS

END 1

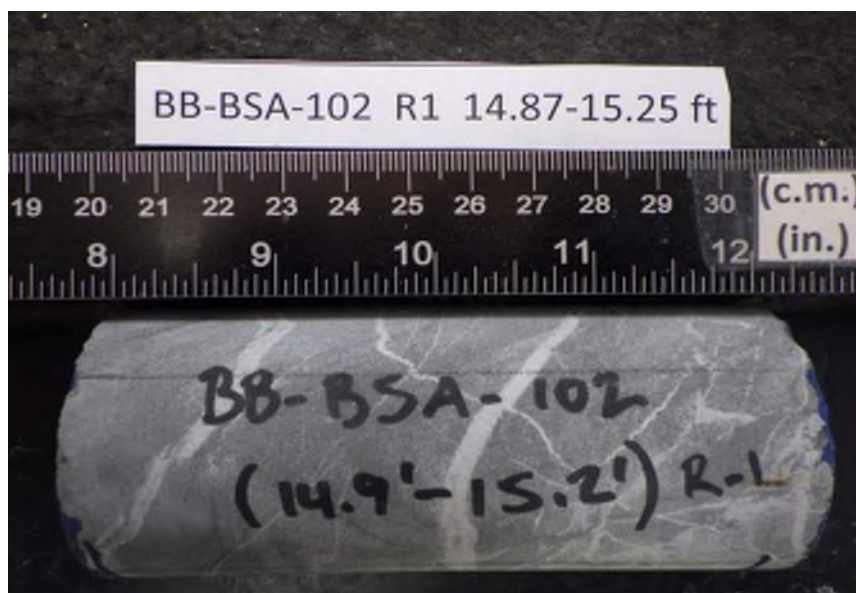
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	smd
Checked By:	jsc
Boring ID:	BB-BSA-102
Sample ID:	R1
Depth, ft:	14.87-15.25



After cutting and grinding

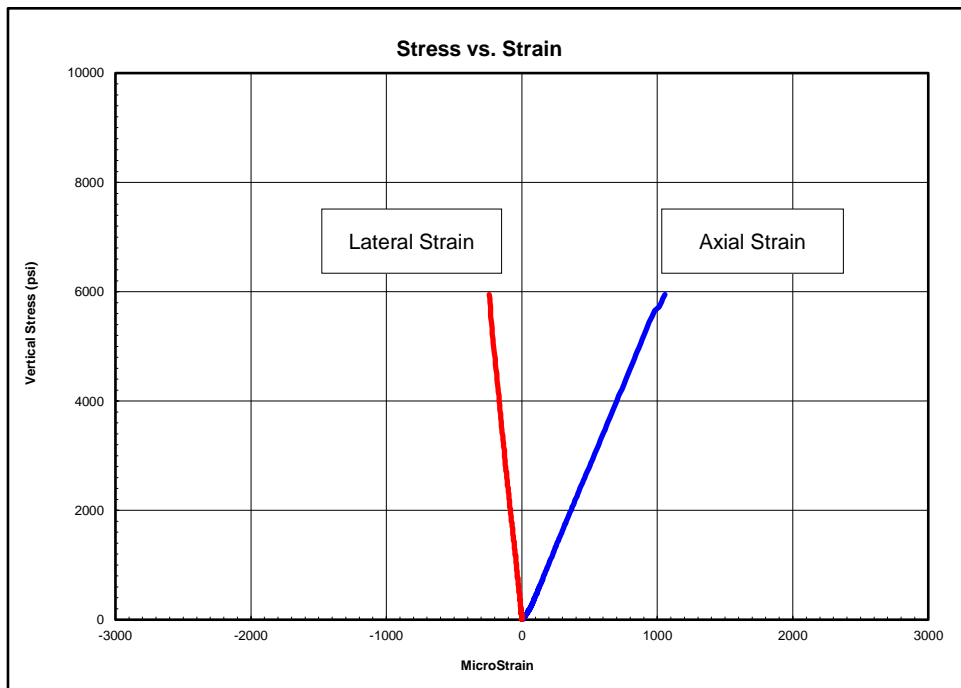


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-110
Sample ID:	R1
Depth, ft:	5.93-6.31
Sample Type:	rock core
Sample Description:	See photographs Intact material and discontinuity failure Best Effort end preparation performed

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 5,948 psi

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
600-2200	6,020,000	0.26
2200-3800	5,880,000	0.25
3800-5400	6,000,000	0.25

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

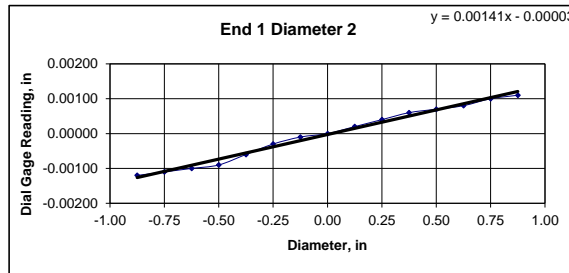
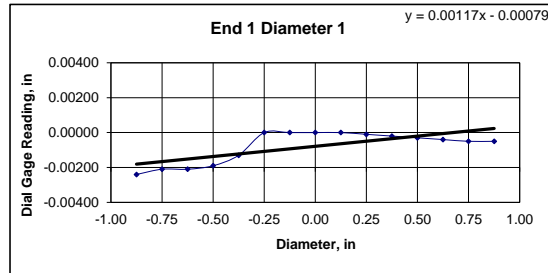


Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-110		
Sample ID:	R1		
Depth (ft):	5.93-6.31		
Visual Description:	See photographs		

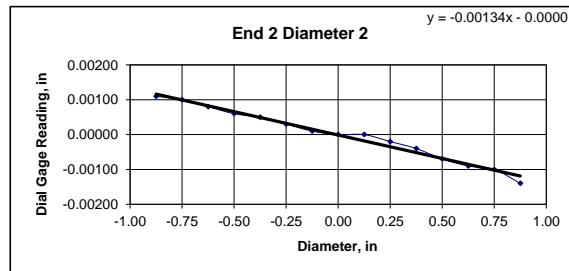
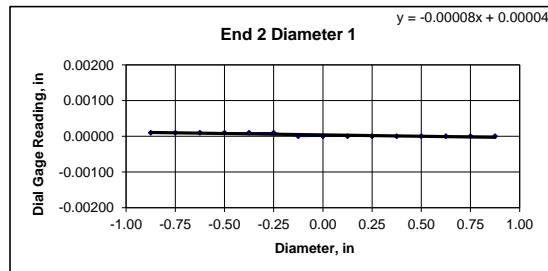
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.? YES	
Specimen Length, in:	4.41	4.41	4.41	Maximum difference must be < 0.020 in. Straightness Tolerance Met? YES	
Specimen Diameter, in:	1.97	1.97	1.97		
Specimen Mass, g:	604.37				
Bulk Density, lb/ft ³	171				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES	Length to Diameter Ratio Tolerance Met? YES		

END FLATNESS AND PARALLELISM (Procedure FP1)														
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	-0.00240	-0.00210	-0.00210	-0.00190	-0.00130	0.00000	0.00000	0.00000	0.00000	-0.00010	-0.00020	-0.00030	-0.00040	-0.00050
Diameter 2, in (rotated 90°)	-0.00120	-0.00110	-0.00100	-0.00090	-0.00060	-0.00030	-0.00010	0.00000	0.00020	0.00040	0.00060	0.00070	0.00080	0.00100
Difference between max and min readings, in: 0° = 0.00240 90° = 0.00230														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Diameter 2, in (rotated 90°)	0.00110	0.00100	0.00080	0.00060	0.00050	0.00030	0.00010	0.00000	0.00000	-0.00020	-0.00040	-0.00070	-0.00090	-0.00100
Difference between max and min readings, in: 0° = 0.0001 90° = 0.0025 Maximum difference must be < 0.0020 in. Difference = ± 0.00125 Flatness Tolerance Met? NO														



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00117
Angle of Best Fit Line:	0.06695
End 2:	
Slope of Best Fit Line	0.00008
Angle of Best Fit Line:	0.00442
Maximum Angular Difference:	0.06253
Parallelism Tolerance Met? Spherically Seated	NO



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00141
Angle of Best Fit Line:	0.08087
End 2:	
Slope of Best Fit Line	0.00134
Angle of Best Fit Line:	0.07694
Maximum Angular Difference:	0.00393
Parallelism Tolerance Met? Spherically Seated	YES

PERPENDICULARITY (Procedure P1)					(Calculated from End Flatness and Parallelism measurements above)	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$
Diameter 1, in	0.00240	1.970	0.00122	0.070	YES	Perpendicularity Tolerance Met? YES
Diameter 2, in (rotated 90°)	0.00230	1.970	0.00117	0.067	YES	
END 2						
Diameter 1, in	0.00010	1.970	0.00005	0.003	YES	
Diameter 2, in (rotated 90°)	0.00250	1.970	0.00127	0.073	YES	



Client:	WSP USA, Inc.	Test Date:	6/12/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-110	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R1		
Depth (ft):	5.93-6.31		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO ASTM D4543

END FLATNESS

END 1

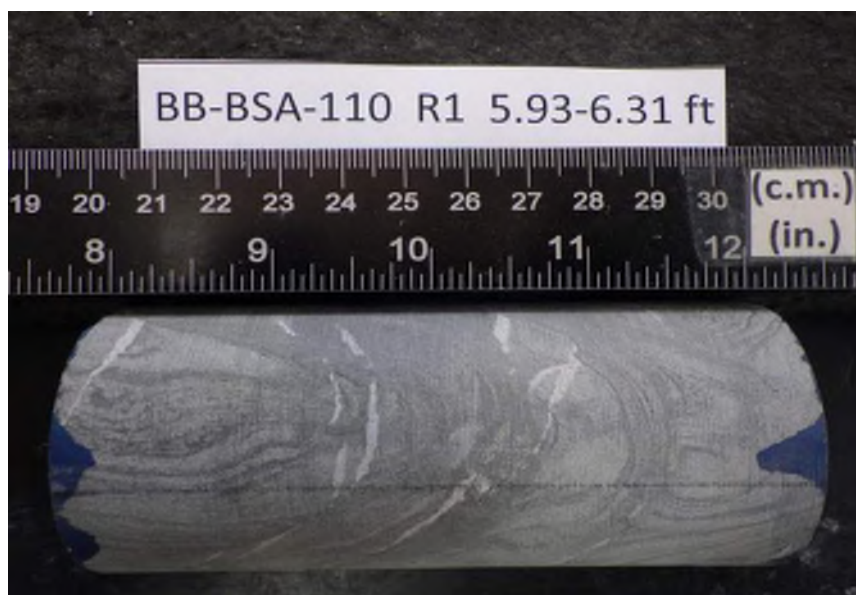
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	6/13/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-110
Sample ID:	R1
Depth, ft:	5.93-6.31



After cutting and grinding

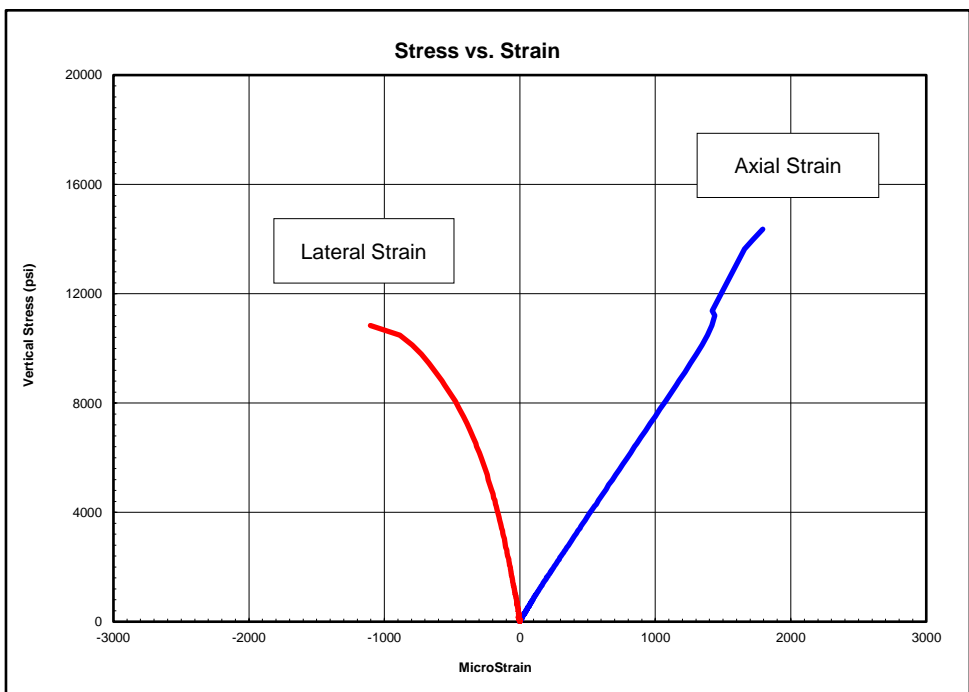


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-101
Sample ID:	R-4
Depth, ft:	37-37.3
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 14,361 psi

The lateral strain gauges failed before the peak value was attained. Poisson's Ratio could not be determined within the second and third stress ranges.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
1400-5300	7,410,000	0.34
5300-9100	7,340,000	---
9100-12900	11,000,000	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

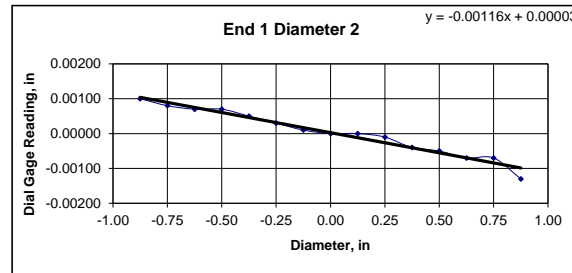
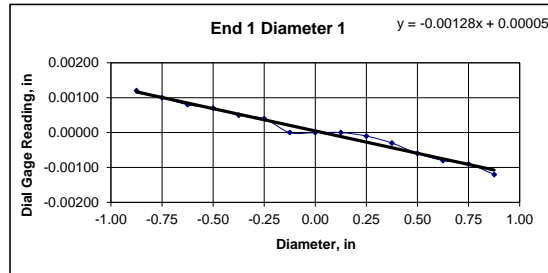


Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-101		
Sample ID:	R-4		
Depth (ft):	37-37.3		
Visual Description:	See photographs		

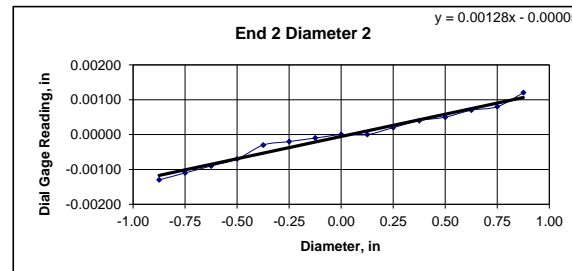
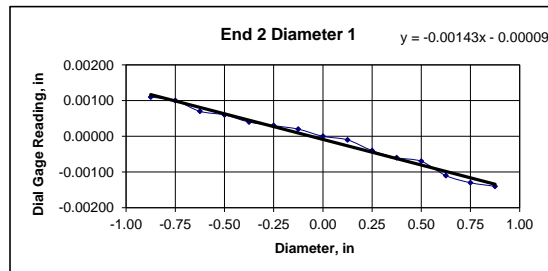
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap \leq 0.02 in.? YES	
Specimen Length, in:	4.33	4.33	4.33	Maximum difference must be $<$ 0.020 in.	
Specimen Diameter, in:	1.97	1.97	1.97	Straightness Tolerance Met? YES	
Specimen Mass, g:	589.14				
Bulk Density, lb/ft ³ :	170				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES			
		Length to Diameter Ratio Tolerance Met? YES			

END FLATNESS AND PARALLELISM (Procedure FP1)															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	0.00120	0.00100	0.00080	0.00070	0.00050	0.00040	0.00000	0.00000	0.00000	-0.00010	-0.00030	-0.00060	-0.00080	-0.00090	-0.00120
Diameter 2, in (rotated 90°)	0.00100	0.00080	0.00070	0.00070	0.00050	0.00030	0.00010	0.00000	0.00000	-0.00010	-0.00040	-0.00050	-0.00070	-0.00070	-0.00130
Difference between max and min readings, in: 0° = 0.00240 90° = 0.00230															
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	0.00110	0.00100	0.00070	0.00060	0.00040	0.00030	0.00020	0.00000	-0.00010	-0.00040	-0.00060	-0.00070	-0.00110	-0.00130	-0.00140
Diameter 2, in (rotated 90°)	-0.00130	-0.00110	-0.00090	-0.00070	-0.00030	-0.00020	-0.00010	0.00000	0.00000	0.00020	0.00040	0.00050	0.00070	0.00080	0.00120
Difference between max and min readings, in: 0° = 0.0025 90° = 0.0025 Maximum difference must be < 0.0020 in. Difference = ± 0.00125															
Flatness Tolerance Met? NO															



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00128
Angle of Best Fit Line:	0.07334
End 2:	
Slope of Best Fit Line	0.00143
Angle of Best Fit Line:	0.08218
Maximum Angular Difference:	0.00884
Parallelism Tolerance Met? Spherically Seated	NO



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00116
Angle of Best Fit Line:	0.06630
End 2:	
Slope of Best Fit Line	0.00128
Angle of Best Fit Line:	0.07317
Maximum Angular Difference:	0.00688
Parallelism Tolerance Met? Spherically Seated	NO

PERPENDICULARITY (Procedure P1)						(Calculated from End Flatness and Parallelism measurements above)	
END 1		Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be \leq 0.25°
Diameter 1, in		0.00240	1.970	0.00122	0.070	YES	
Diameter 2, in (rotated 90°)		0.00230	1.970	0.00117	0.067	YES	Perpendicularity Tolerance Met? YES
END 2							
Diameter 1, in		0.00250	1.970	0.00127	0.073	YES	
Diameter 2, in (rotated 90°)		0.00250	1.970	0.00127	0.073	YES	



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-101	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-4		
Depth (ft):	37-37.3		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

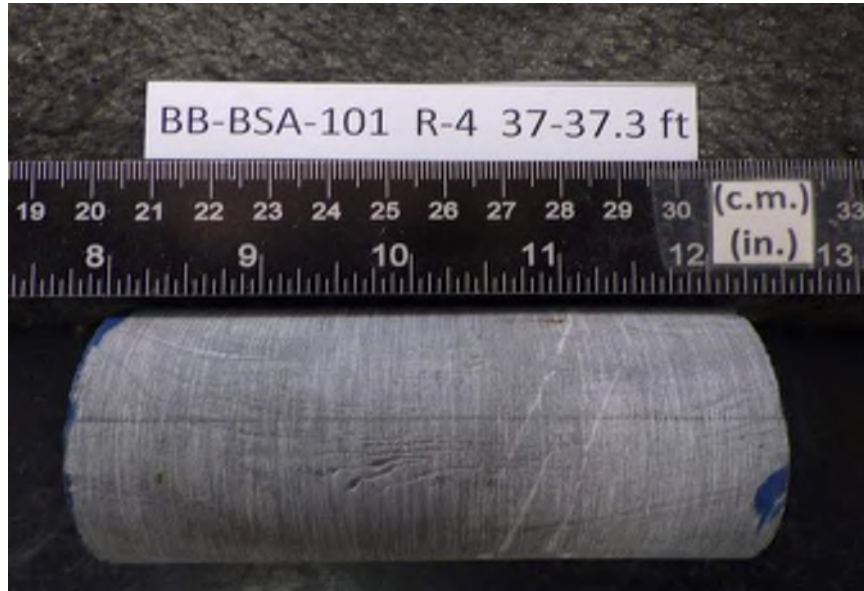
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-101
Sample ID:	R-4
Depth, ft:	37-37.3



After cutting and grinding

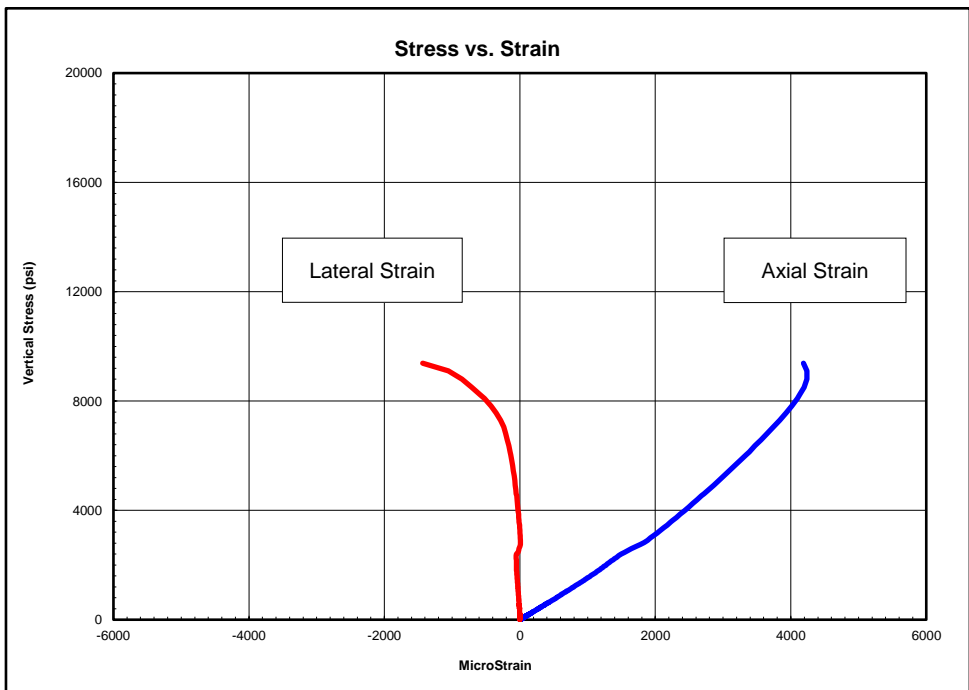


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-105
Sample ID:	R-1
Depth, ft:	28.8-29.1
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 9,458 psi

Poisson's Ratio within the first and third stress ranges could not be determined.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
900-3500	1,610,000	---
3500-6000	2,190,000	0.10
6000-8500	2,730,000	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

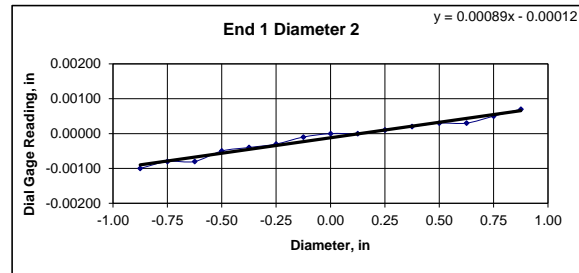
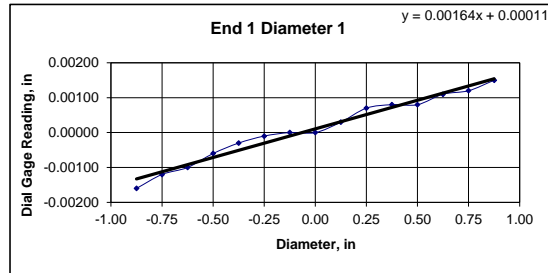


Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-105		
Sample ID:	R-1		
Depth (ft):	28.8-29.1		
Visual Description:	See photographs		

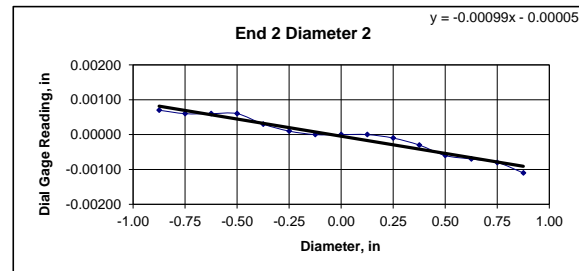
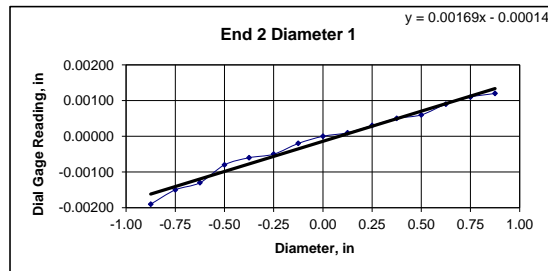
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap \leq 0.02 in.? YES	
Specimen Length, in:	4.30	4.30	4.30	Maximum difference must be $<$ 0.020 in. Straightness Tolerance Met? YES	
Specimen Diameter, in:	1.96	1.96	1.96		
Specimen Mass, g:	582.84				
Bulk Density, lb/ft ³	171				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES	Length to Diameter Ratio Tolerance Met? YES		

END FLATNESS AND PARALLELISM (Procedure FP1)													
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	-0.00160	-0.00120	-0.00100	-0.00060	-0.00030	-0.00010	0.00000	0.00000	0.00030	0.00070	0.00080	0.00080	0.00110
Diameter 2, in (rotated 90°)	-0.00100	-0.00080	-0.00080	-0.00050	-0.00040	-0.00030	-0.00010	0.00000	0.00000	0.00010	0.00020	0.00030	0.00030
Difference between max and min readings, in: 0° = 0.00310 90° = 0.00170													
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	-0.00190	-0.00150	-0.00130	-0.00080	-0.00060	-0.00050	-0.00020	0.00000	0.00010	0.00030	0.00050	0.00060	0.00090
Diameter 2, in (rotated 90°)	0.00070	0.00060	0.00060	0.00060	0.00030	0.00010	0.00000	0.00000	0.00000	-0.00010	-0.00030	-0.00060	-0.00070
Difference between max and min readings, in: 0° = 0.0031 90° = 0.0018 Maximum difference must be $<$ 0.0020 in. Difference = \pm 0.00155													
Flatness Tolerance Met? NO													



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00164
Angle of Best Fit Line:	0.09396
End 2:	
Slope of Best Fit Line	0.00169
Angle of Best Fit Line:	0.09675
Maximum Angular Difference:	0.00278
Parallelism Tolerance Met? Spherically Seated	YES



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00089
Angle of Best Fit Line:	0.05091
End 2:	
Slope of Best Fit Line	0.00099
Angle of Best Fit Line:	0.05648
Maximum Angular Difference:	0.00557
Parallelism Tolerance Met? Spherically Seated	NO

PERPENDICULARITY (Procedure P1)						Perpendicularity Tolerance Met?	Maximum angle of departure must be \leq 0.25°
END 1	Difference, Maximum and Minimum (in.)		Diameter (in.)		Slope		
Diameter 1, in	0.00310		1.960		0.00158	0.091	YES
Diameter 2, in (rotated 90°)	0.00170		1.960		0.00087	0.050	YES
END 2							Perpendicularity Tolerance Met? YES
Diameter 1, in	0.00310		1.960		0.00158	0.091	YES
Diameter 2, in (rotated 90°)	0.00180		1.960		0.00092	0.053	YES



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-105	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-1		
Depth (ft):	28.8-29.1		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

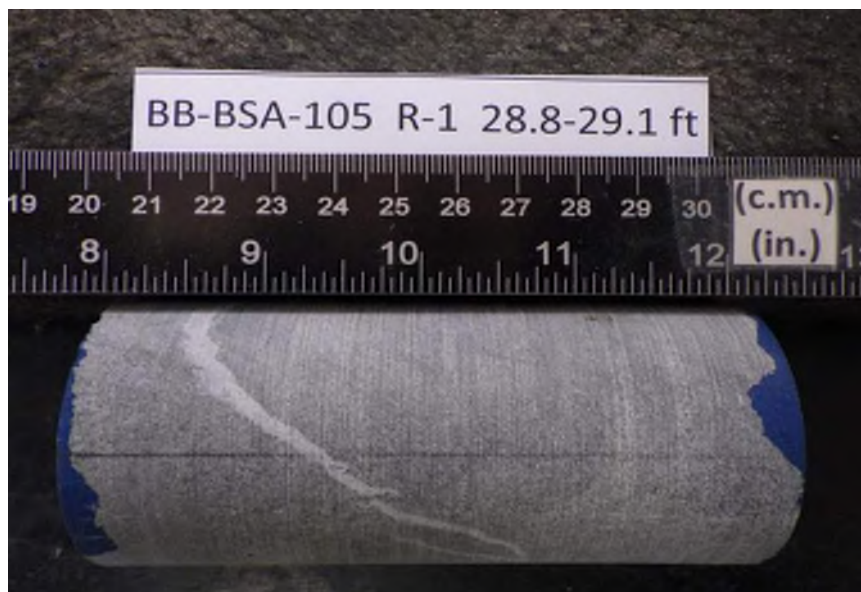
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-105
Sample ID:	R-1
Depth, ft:	28.8-29.1



After cutting and grinding

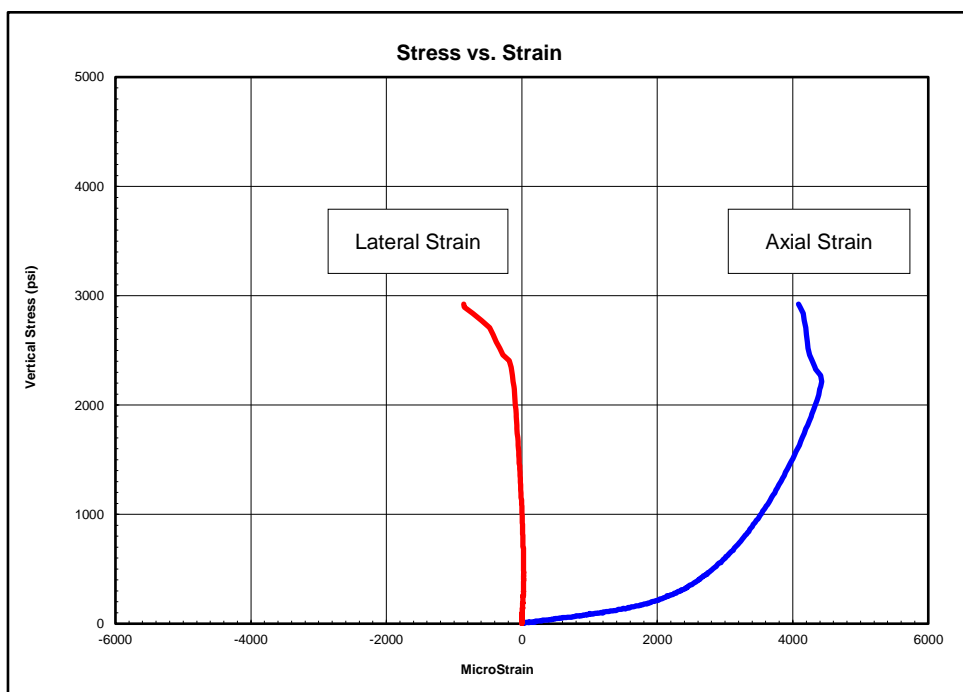


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-106
Sample ID:	R-3
Depth, ft:	69.3-69.6
Sample Type:	rock core
Sample Description:	See photographs Intact material failure Best Effort end preparation performed

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 3,226 psi

The strain gauges failed before the peak value was attained. Young's Modulus and Poisson's Ratio could not be determined within the third stress range.

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
300-1200	626,000	0.03
1200-2000	1,310,000	0.14
2000-2900	---	---

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

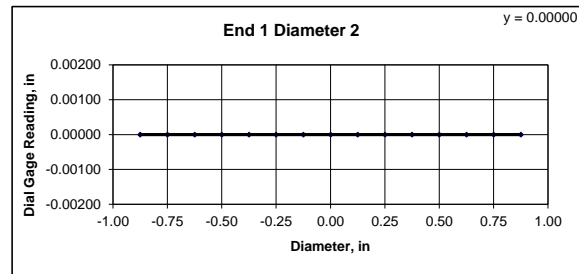
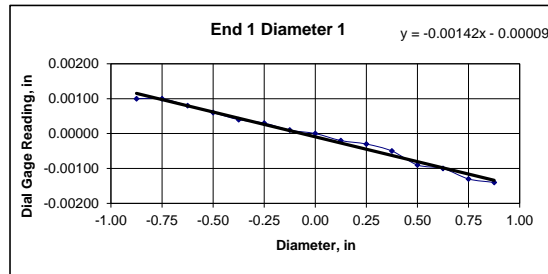


Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-106		
Sample ID:	R-3		
Depth (ft):	69.3-69.6		
Visual Description:	See photographs		

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.? NO	
Specimen Length, in:	4.40	4.40	4.40	Maximum difference must be < 0.020 in. Straightness Tolerance Met? NO	
Specimen Diameter, in:	1.96	1.96	1.96		
Specimen Mass, g:	603.87				
Bulk Density, lb/ft ³	173				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES	Length to Diameter Ratio Tolerance Met? YES		

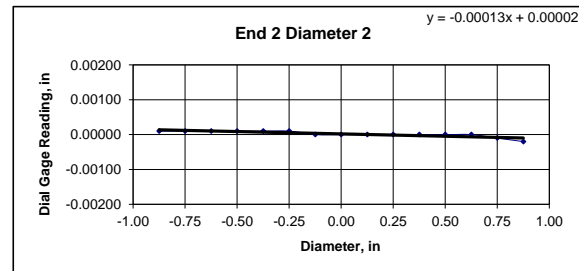
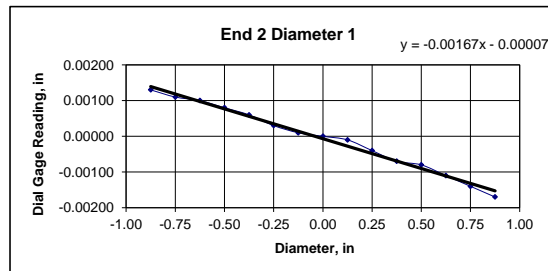
END FLATNESS AND PARALLELISM (Procedure FP1)														
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	0.00100	0.00100	0.00080	0.00060	0.00040	0.00030	0.00010	0.00000	-0.00020	-0.00030	-0.00050	-0.00090	-0.00100	-0.00130
Diameter 2, in (rotated 90°)	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Difference between max and min readings, in: 0° = 0.00240 90° = 0.00000														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	0.00130	0.00110	0.00100	0.00080	0.00060	0.00030	0.00010	0.00000	-0.00010	-0.00040	-0.00070	-0.00080	-0.00110	-0.00140
Diameter 2, in (rotated 90°)	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00020
Difference between max and min readings, in: 0° = 0.003 90° = 0.0003 Maximum difference must be < 0.0020 in. Difference = ± 0.00150 Flatness Tolerance Met? NO														



DIAMETER 1

End 1:	Slope of Best Fit Line	0.00142
	Angle of Best Fit Line:	0.08152
End 2:	Slope of Best Fit Line	0.00167
	Angle of Best Fit Line:	0.09560
Maximum Angular Difference:		0.01408

Parallelism Tolerance Met? NO
Spherically Seated



DIAMETER 2

End 1:	Slope of Best Fit Line	0.00000
	Angle of Best Fit Line:	0.00000
End 2:	Slope of Best Fit Line	0.00013
	Angle of Best Fit Line:	0.00769
Maximum Angular Difference:		0.00769

Parallelism Tolerance Met? NO
Spherically Seated

PERPENDICULARITY (Procedure P1)						(Calculated from End Flatness and Parallelism measurements above)	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$	
Diameter 1, in	0.00240	1.960	0.00122	0.070	YES	Perpendicularity Tolerance Met? YES	
Diameter 2, in (rotated 90°)	0.00000	1.960	0.00000	0.000	YES		
END 2							
Diameter 1, in	0.00300	1.960	0.00153	0.088	YES		
Diameter 2, in (rotated 90°)	0.00030	1.960	0.00015	0.009	YES		



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-106	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-3		
Depth (ft):	69.3-69.6		
Visual Description:	See photographs		

**BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543**

END FLATNESS

END 1

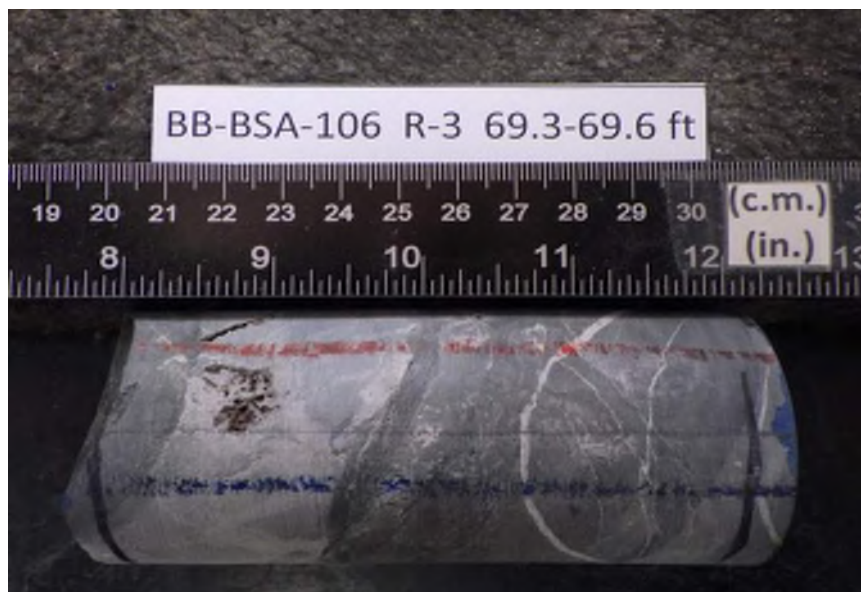
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

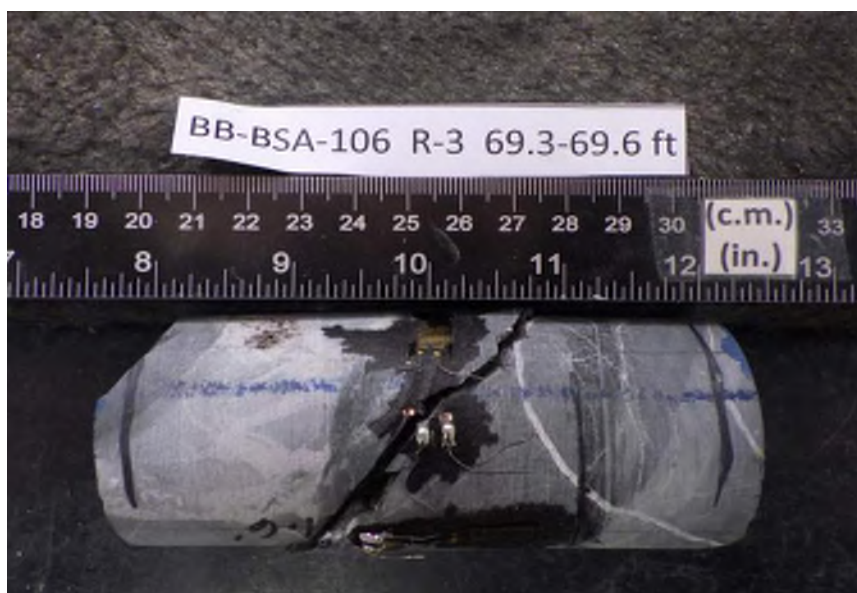
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-106
Sample ID:	R-3
Depth, ft:	69.3-69.6



After cutting and grinding

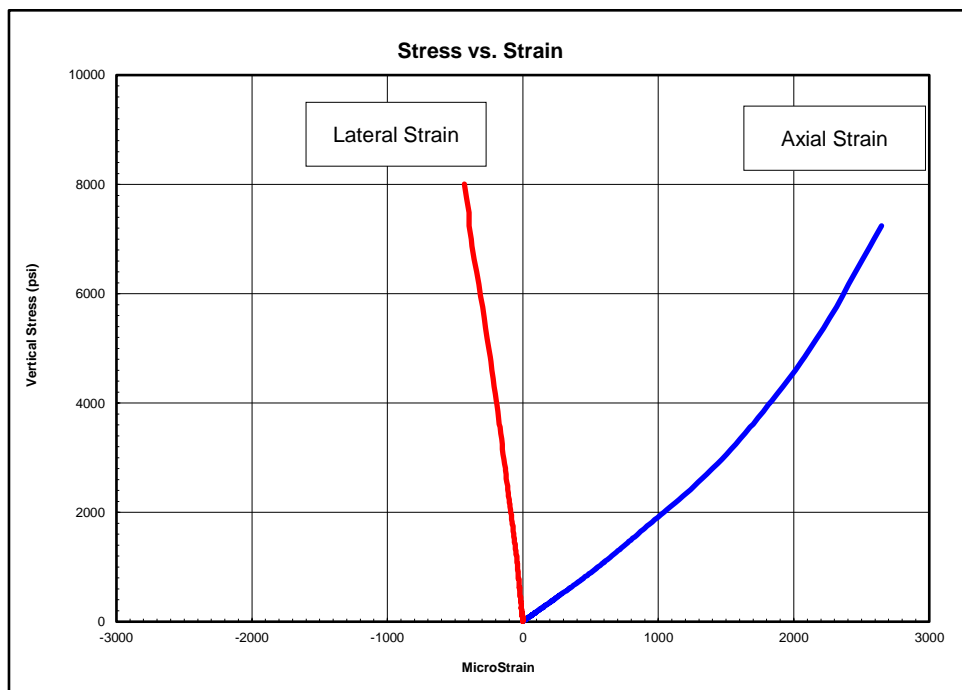


After break



Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	jsc
Boring ID:	BB-BSA-111
Sample ID:	R-1
Depth, ft:	21.4-21.7
Sample Type:	rock core
Sample Description:	See photographs Intact material and discontinuity failure Best Effort end preparation performed

Compressive Strength and Elastic Moduli of Rock by ASTM D7012 - Method D



Peak Compressive Stress: 8,006 psi

Stress Range, psi	Young's Modulus, psi	Poisson's Ratio
800-2900	2,080,000	0.10
2900-5100	3,070,000	0.17
5100-7200	4,360,000	0.29

Notes: Test specimen tested at the approximate as-received moisture content and at standard laboratory temperature.
The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
Young's Modulus and Poisson's Ratio calculated using the tangent to the line in the stress range listed.
Calculations assume samples are isotropic, which is not necessarily the case.

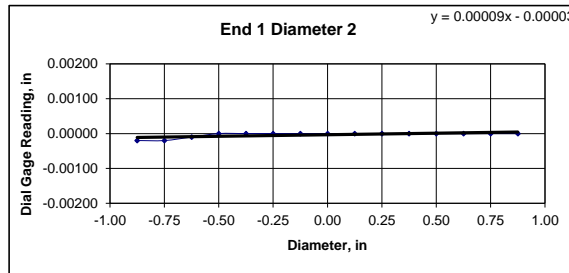
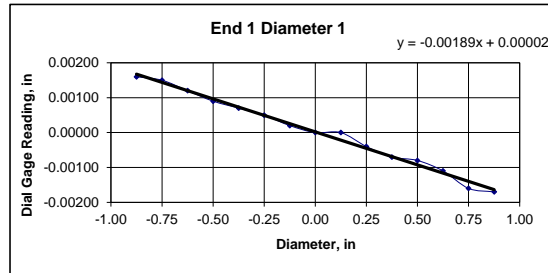


Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-111		
Sample ID:	R-1		
Depth (ft):	21.4-21.7		
Visual Description:	See photographs		

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap \leq 0.02 in.? NO	
Specimen Length, in:	4.52	4.52	4.52	Maximum difference must be $<$ 0.020 in. Straightness Tolerance Met? NO	
Specimen Diameter, in:	1.96	1.96	1.96		
Specimen Mass, g:	619.07				
Bulk Density, lb/ft ³	173				
Length to Diameter Ratio:	2.3				
				Minimum Diameter Tolerance Met? YES	
				Length to Diameter Ratio Tolerance Met? YES	

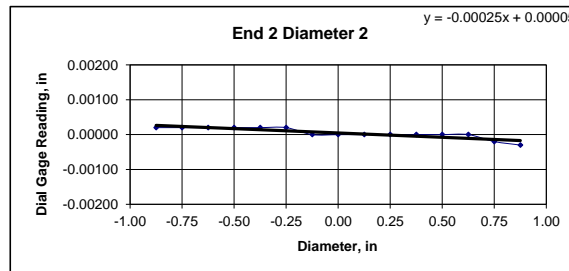
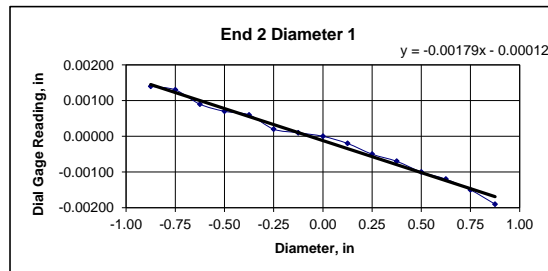
END FLATNESS AND PARALLELISM (Procedure FP1)													
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	0.00160	0.00150	0.00120	0.00090	0.00070	0.00050	0.00020	0.00000	0.00000	-0.00040	-0.00070	-0.00080	-0.00110
Diameter 2, in (rotated 90°)	-0.00020	-0.00020	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Difference between max and min readings, in: 0° = 0.00330 90° = 0.00020													
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	0.00140	0.00130	0.00090	0.00070	0.00060	0.00020	0.00010	0.00000	-0.00020	-0.00050	-0.00070	-0.00100	-0.00120
Diameter 2, in (rotated 90°)	0.00020	0.00020	0.00020	0.00020	0.00020	0.00020	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00020
Difference between max and min readings, in: 0° = 0.0033 90° = 0.0005 Maximum difference must be $<$ 0.0020 in. Difference = \pm 0.00165													
Flatness Tolerance Met? NO													



DIAMETER 1

End 1:		
Slope of Best Fit Line	0.00189	
Angle of Best Fit Line:	0.10837	
End 2:		
Slope of Best Fit Line	0.00179	
Angle of Best Fit Line:	0.10280	
Maximum Angular Difference:	0.00557	

Parallelism Tolerance Met? NO
Spherically Seated



DIAMETER 2

End 1:		
Slope of Best Fit Line	0.00009	
Angle of Best Fit Line:	0.00507	
End 2:		
Slope of Best Fit Line	0.00025	
Angle of Best Fit Line:	0.01424	
Maximum Angular Difference:	0.00917	

Parallelism Tolerance Met? NO
Spherically Seated

PERPENDICULARITY (Procedure P1)						(Calculated from End Flatness and Parallelism measurements above)	
END 1						Difference, Maximum and Minimum (in.)	Diameter (in.)
Diameter 1, in	0.00330	1.960	0.00168	0.096	YES		
Diameter 2, in (rotated 90°)	0.00020	1.960	0.00010	0.006	YES		
						Perpendicularity Tolerance Met?	
						Maximum angle of departure must be \leq 0.25°	
						Perpendicularity Tolerance Met? YES	
END 2							
Diameter 1, in	0.00330	1.960	0.00168	0.096	YES		
Diameter 2, in (rotated 90°)	0.00050	1.960	0.00026	0.015	YES		



Client:	WSP USA, Inc.	Test Date:	8/28/2024
Project Name:	MaineDOT I-95 Bridge over Stillwater	Tested By:	gp
Project Location:	Merrimack, NH	Checked By:	smd
GTX #:	319180		
Boring ID:	BB-BSA-111	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	R-1		
Depth (ft):	21.4-21.7		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

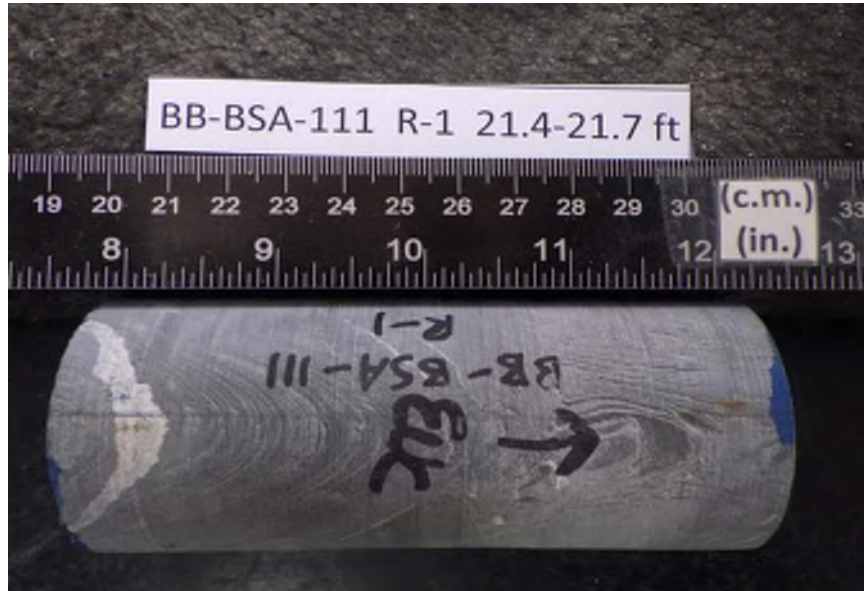
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	MaineDOT I-95 Bridge over Stillwater
Project Location:	Merrimack, NH
GTX #:	319180
Test Date:	8/29/2024
Tested By:	gp
Checked By:	smd
Boring ID:	BB-BSA-111
Sample ID:	R-1
Depth, ft:	21.4-21.7



After cutting and grinding



After break

APPENDIX D

Rock Discontinuity Calculations

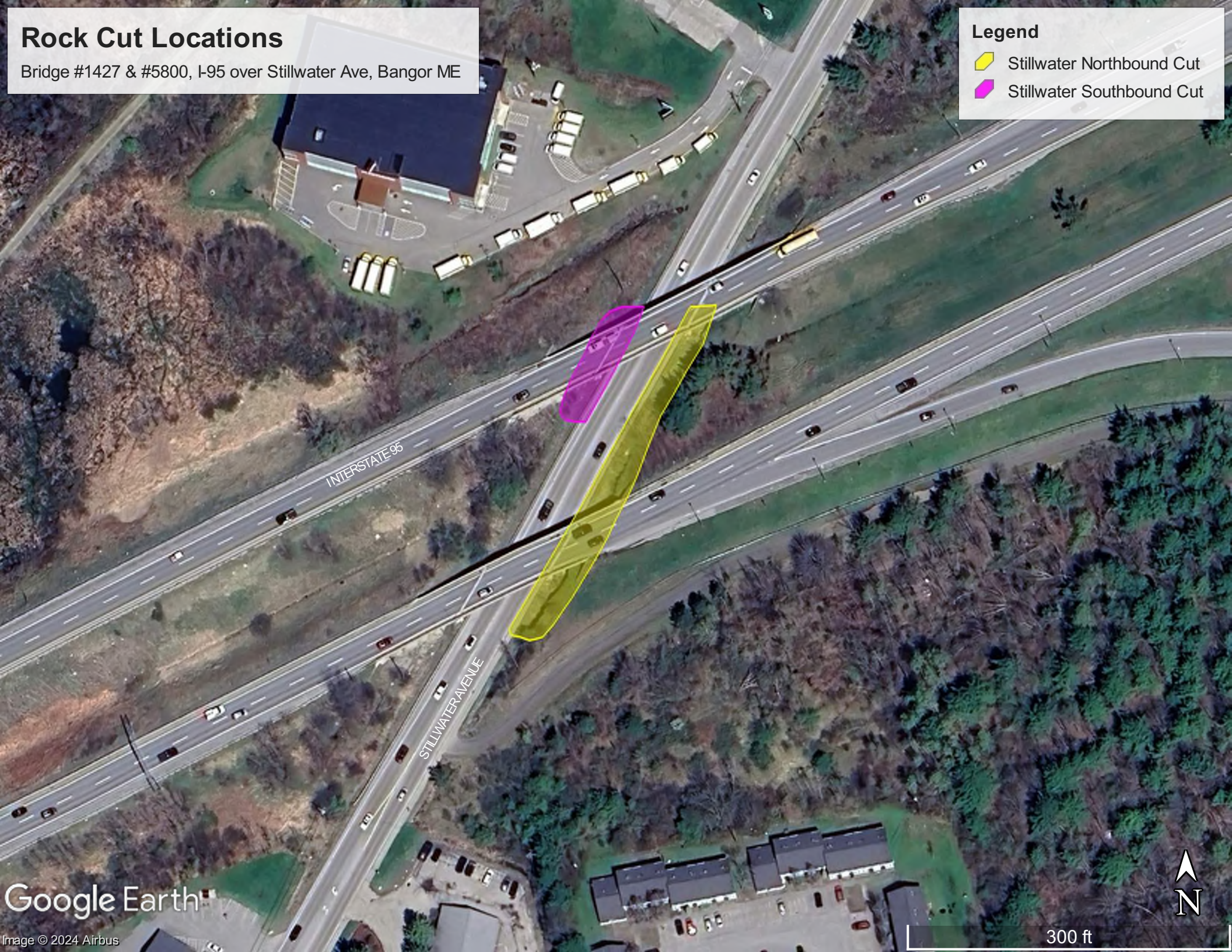
Rock Cut Locations

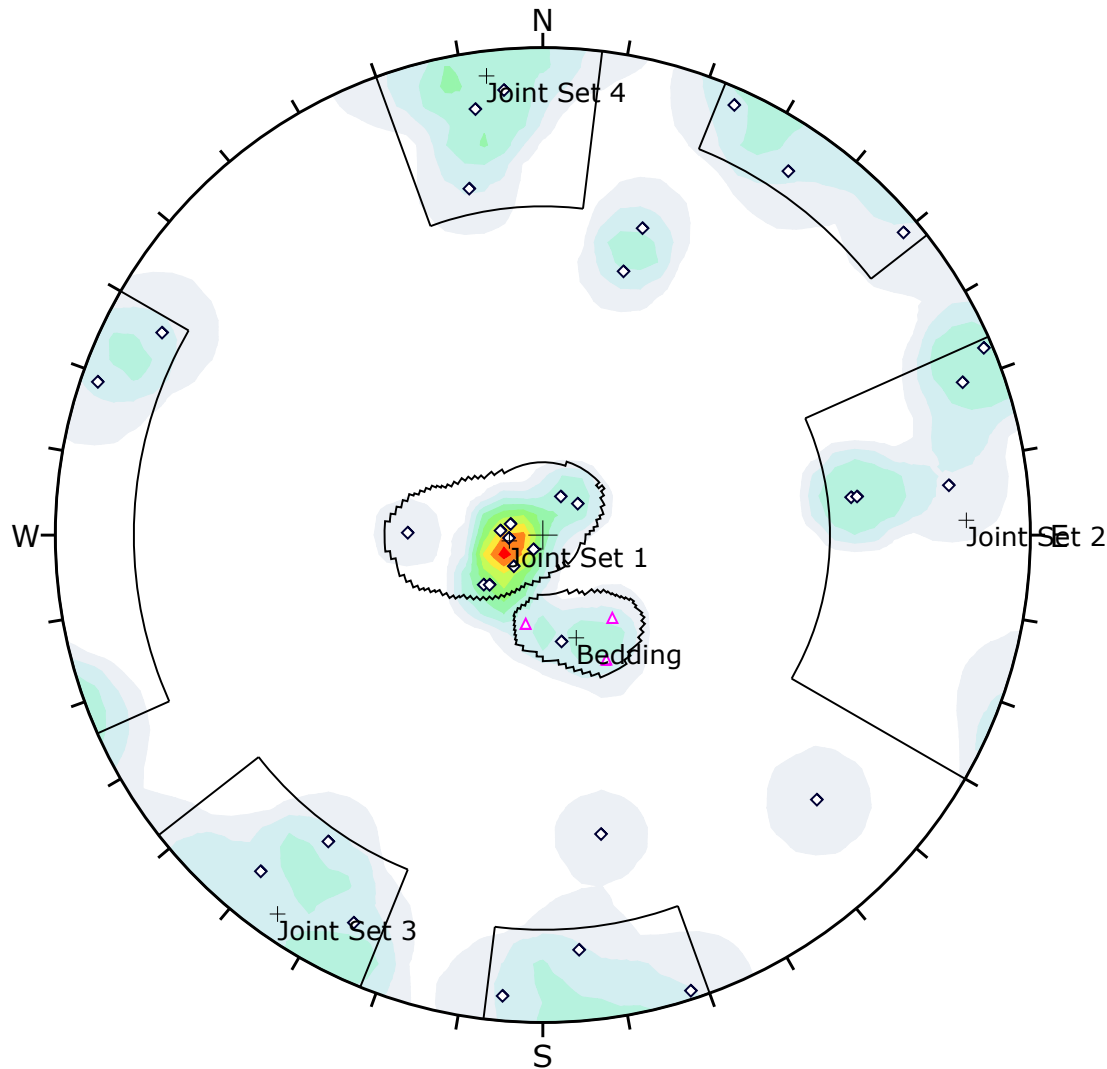
Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor ME

Legend

Stillwater Northbound Cut

Stillwater Southbound Cut





Symbol	TYPE	Quantity
▲	bedding	3
◆	joint	34

Color	Density Concentrations
	0.00 - 1.40
	1.40 - 2.80
	2.80 - 4.20
	4.20 - 5.60
	5.60 - 7.00
	7.00 - 8.40
	8.40 - 9.80
	9.80 - 11.20
	11.20 - 12.60
	12.60 - 14.00
Contour Data	Pole Vectors
Maximum Density	13.44%
Contour Distribution	Fisher
Counting Circle Size	1.0%

	Color	Dip	Dip Direction	Label
Mean Set Planes				
1m	■	8	80	Joint Set 1
2m	■	82	268	Joint Set 2
3m	■	87	35	Joint Set 3
4m	■	87	173	Joint Set 4
5m	■	25	342	Bedding

Plot Mode	Pole Vectors
Vector Count	37 (37 Entries)
Hemisphere	Lower
Projection	Equal Angle



Project

I-95 Bridge #1427 & #5800 over Stillwater Ave, Bangor ME, MaineDOT WIN 027176.00

Analysis Description

Outcrops along Stillwater Ave Northbound and Southbound

Drawn By

KAR

Checked By

BK

Reviewed By

JDL

Scale

N/A

Date

5/21/2024

File Name

Stillwater-outcrop-data.dips8

Appendix D.1

Appendix D.2: Calculation of Rock Mass Rating

Preliminary Geotechnical Design Report

Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine

MaineDOT WIN 027176.00

References:

1. Bieniawski, Z.T. 1989. Engineering Rock Mass Classifications: A Complete Manual for Engineers and Geologists in Mining, Civil, and Petroleum Engineering. John Wiley & Sons.

2. Wyllie, Duncan C. 1999. Foundations on Rock, 2nd Edition. E&FN Spon.

3. Hoek, Evert. 2006. Practical Rock Engineering. Rocscience Inc.

- Notes:
1. The RMR ratings for parameter 1 (intact rock strength), parameter 2 (drill core quality RQD), and parameter 3 (discontinuity spacing) are selected using Charts A, B, and C, respectively, from Bieniawski 1989 (Ref. 1). For core runs on which UCS lab testing was not performed, the intact strength rating is selected based on field strength estimates using Table 3.5 from Wyllie 1999 (Ref. 2).
2. The RMR ratings for parameter 4 (discontinuity condition) are selected using Section E of Table 4 from Hoek 2006 (Ref. 3).
3. The RMR ratings for parameter 5 (groundwater) are selected using Table 3.5 from Wyllie 1999 (Ref. 2).
4. For the outcrop discontinuities, the RQD is correlated from discontinuity spacing based on Chart D from Bieniawski 1989 (Ref. 1).
5. For the boring core runs, the persistence rating is based on an average of the persistence measurements at the outcrops.
6. The rating adjustment for joint orientation (parameter B) is selected from Bieniawski 1989 (Ref. 1), using an orientation adjustment of -15 ("unfavorable" for foundations) for the bedding set based on the kinematic possibility of planar sliding and for joint set 2 based on the kinematic possibility of toppling. Since the boring rock core was collected unoriented, an average of all outcrop orientation adjustments is used for the boring core runs.

Prepared by: KAR

Checked by: BK

Reviewed by: JDL

Overall average RMR = 54

Boring or Outcrop	Run Number or Discontinuity ID	Intact Strength			RQD (%)	Fracture Spacing			A. Classification Parameters										B. Rating adjustment for joint orientation	RMR
		UCS (psi)	UCS (MPa)	Field Strength Estimate		Average fractures per foot	Average spacing (ft)	Average spacing (mm)	1	2	3	4						5		
									Strength of rock	RQD	Spacing of joints	Condition of Joints						Ground water		
												Persistence	Aperture	Roughness	Infilling	Weathering	Total			
BB-BSA-101	R1	-	-	Very Strong (R5)	0	broken	-	-	12	3	5	2	0	1	0	5	8	7	-4	31
	R2	-	-	Strong (R4) to Very Strong (R5)	0	broken	-	-	7	3	5	2	0	5	0	5	12	7	-4	30
	R3	-	-	Strong (R4) to Very Strong (R5)	14	3.5	0.3	87	7	5	6	2	0	5	6	5	18	7	-4	39
	R4	-	-	Strong (R4)	60	1.6	0.6	191	9	12	8	2	5	5	6	6	24	7	-4	56
BB-BSA-102	R1	17,296	119	Strong (R4) to Extremely Strong (R6)	52	3.2	0.3	95	11	10	6	2	0	1	2	5	10	7	-4	40
	R2	-	-	Extremely Strong (R6)	88	0.2	5.0	1524	15	18	16	2	0	6	6	6	20	7	-4	72
BB-BSA-103	R1	-	-	Extremely Strong (R6)	31	4.0	0.3	76	15	7	6	2	1	1	4	5	13	7	-4	44
	R2	-	-	Extremely Strong (R6)	70	2.0	0.5	152	15	14	7	2	4	5	6	6	23	7	-4	62
BB-BSA-104A	R1	-	-	Strong (R4) to Very Strong (R5)	56	1.6	0.6	191	7	11	8	2	0	5	0	5	12	7	-4	41
	R2	-	-	Strong (R4) to Very Strong (R5)	61	0.5	2.0	610	7	12	12	2	5	5	6	6	24	7	-4	58
	R3	-	-	Strong (R4) to Very Strong (R5)	23	3.5	0.3	87	7	6	6	2	0	5	6	6	19	7	-4	41
BB-BSA-105	R1	-	-	Strong (R4)	30	3.2	0.3	95	7	7	6	2	0	5	6	5	18	7	-4	41
	R2	-	-	Very Strong (R5)	75	1.6	0.6	191	12	15	8	2	5	1	6	6	20	7	-4	58
BB-BSA-106	R1	-	-	Strong (R4) to Very Strong (R5)	0	broken	-	-	7	3	5	2	0	5	6	5	18	7	-4	36
	R2	-	-	Strong (R4) to Very Strong (R5)	47	3.3	0.3	92	7	10	6	2	0	1	0	6	9	7	-4	35
	R3	-	-	Weak (R2)	62	1.4	0.7	218	3	12	8	2	0	5	6	6	19	7	-4	45
BB-BSA-107	R1	-	-	Strong (R4)	0	broken	-	-	7	3	5	2	0	5	0	1	8	7	-4	26
	R2	-	-	Strong (R4)	0	broken	-	-	7	3	5	2	0	6	0	1	9	7	-4	27
	R3	-	-	Strong (R4) to Very Strong (R5)	35	3.5	0.3	87	7	8	6	2	0	5	0	5	12	7	-4	36
	R4	-	-	Strong (R4) to Very Strong (R5)	39	3.2	0.3	95	7	8	6	2	0	5	0	5	12	7	-4	36

Boring or Outcrop	Run Number or Discontinuity ID	Intact Strength			RQD (%)	Fracture Spacing			A. Classification Parameters										B. Rating adjustment for joint orientation	RMR
		UCS (psi)	UCS (MPa)	Field Strength Estimate		Average fractures per foot	Average spacing (ft)	Average spacing (mm)	1	2	3	4						5		
									Strength of rock	RQD	Spacing of joints	Condition of Joints						Ground water		
												Persistence	Aperture	Roughness	Infilling	Weathering	Total			
BB-BSA-108	R1	-	-	Very Strong (R5) to Extremely Strong (R6)	58	2.6	0.4	117	12	11	7	2	0	5	6	5	18	7	-4	51
	R2	-	-	Extremely Strong (R6)	42	1.0	1.0	305	15	9	9	2	1	1	6	5	15	7	-4	51
	R3	-	-	Extremely Strong (R6)	17	2.5	0.4	122	15	5	7	2	1	1	6	5	15	7	-4	45
	R4	-	-	Extremely Strong (R6)	35	2.0	0.5	152	15	8	7	2	1	1	6	5	15	7	-4	48
BB-BSA-109A	R1	-	-	Very Strong (R5) to Extremely Strong (R6)	30	1.8	0.6	169	12	7	7	2	0	1	6	5	14	7	-4	43
	R2	-	-	Very Strong (R5) to Extremely Strong (R6)	49	1.6	0.6	191	12	10	8	2	1	1	6	6	16	7	-4	49
BB-BSA-110	R1	5,948	41	Medium Strong (R3)	49	1.0	1.0	305	5	10	9	2	1	1	6	6	16	7	-4	43
	R2	-	-	Very Strong (R5) to Extremely Strong (R6)	71	0.8	1.3	381	12	14	10	2	0	1	6	6	15	7	-4	54
BB-BSA-111	R1	-	-	Strong (R4) to Very Strong (R5)	15	broken	-	-	6	5	5	2	0	5	6	5	18	7	-4	37
	R2	-	-	Strong (R4) to Very Strong (R5)	60	1.6	0.6	191	7	12	8	2	5	5	6	6	24	7	-4	54
Outcrop along Stillwater Ave Northbound	Disc. 1	-	-	-	20	-	0.2	61	15	5	6	2	1	5	6	5	19	10	-15	40
	Disc. 2	-	-	-	93	-	1.5	457	15	19	10	2	0	3	0	5	10	10	0	64
	Disc. 3	-	-	-	99	-	2.8	853	15	20	13	6	0	3	6	5	20	10	0	78
	Disc. 4	-	-	-	85	-	0.9	274	15	17	9	4	0	1	0	5	10	10	-15	46
	Disc. 5	-	-	-	100	-	5.9	1798	15	20	16	4	1	1	6	5	17	10	0	78
	Disc. 6	-	-	-	95	-	1.6	488	15	19	11	2	1	3	6	5	17	10	0	72
	Disc. 7	-	-	R6	41	-	0.3	91	15	9	6	2	6	5	6	5	24	10	-15	49
	Disc. 8	-	-	-	100	-	5.9	1798	15	20	16	6	0	1	0	5	12	10	0	73
	Disc. 9	-	-	-	88	-	1.1	335	4	18	9	2	1	3	6	5	17	10	0	58
	Disc. 10	-	-	-	86	-	1.0	305	4	17	9	2	0	3	2	5	12	10	0	52
	Disc. 11	-	-	R3	100	-	3.7	1128	4	20	14	4	0	5	2	5	16	10	0	64
	Disc. 12	-	-	-	100	-	4.5	1372	4	20	15	2	1	3	6	5	17	10	0	66
	Disc. 13	-	-	-	100	-	5.4	1646	4	20	16	4	1	3	6	5	19	10	-15	54
	Disc. 14	-	-	-	85	-	0.9	274	15	17	9	2	0	3	2	5	12	10	0	63
	Disc. 15	-	-	R6	100	-	5.1	1554	15	20	16	4	6	1	6	5	22	10	-15	68
	Disc. 16	-	-	-	91	-	1.3	396	15	18	10	2	0	5	2	5	14	10	0	67
	Disc. 17	-	-	-	99	-	2.5	762	15	20	13	2	1	3	2	5	13	10	0	71
	Disc. 18	-	-	-	99	-	2.5	762	15	20	13	2	6	1	6	5	20	10	0	78
	Disc. 19	-	-	-	96	-	1.8	549	12	19	11	2	1	5	6	5	19	10	0	71
	Disc. 20	-	-	-	96	-	1.7	518	12	19	11	2	0	3	0	5	10	10	-15	47
	Disc. 21	-	-	-	56	-	0.4	122	12	11	7	4	1	1	6	5	17	10	-15	42
	Disc. 22	-	-	-	96	-	1.8	549	12	19	11	2	1	3	6	5	17	10	-15	54
	Disc. 23	-	-	R5	98	-	2.0	610	12	20	12	2	0	1	2	5	10	10	0	64
	Disc. 24	-	-	-	92	-	1.4	427	12	18	10	2	6	3	6	5	22	10	0	72
	Disc. 25	-	-	R6	99	-	2.3	701	15	20	12	2	6	3	6	5	22	10	0	79
	Disc. 26	-	-	-	99	-	2.2	671	15	20	12	2	0	1	2	5	10	10	0	67
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	Disc. 28	-	-	-	96	-	1.8	549	15	19	11	2	0	5	2	5	14	10	0	69
	Disc. 29	-	-	R6	99	-	2.2	671	15	20	12	2	1	5	4	5	17	10	0	74
	Disc. 30	-	-	R6	95	-	1.6	488	15	19	11	2	0	3	2	5	12	10	0	67
	Disc. 31	-	-	R6	99	-	2.3	701	15	20	12	4	0	3	0	5	12	10	0	69

Boring or Outcrop	Run Number or Discontinuity ID	Intact Strength			RQD (%)	Fracture Spacing			A. Classification Parameters										B. Rating adjustment for joint orientation	RMR
		UCS (psi)	UCS (MPa)	Field Strength Estimate		Average fractures per foot	Average spacing (ft)	Average spacing (mm)	1	2	3	4						5		
									Strength of rock	RQD	Spacing of joints	Condition of Joints						Ground water		
												Persistence	Aperture	Roughness	Infilling	Weathering	Total			
Outcrop along Stillwater Ave Southbound	Disc. 32	-	-	-	85	-	0.9	274	15	17	9	4	0	6	0	5	15	10	0	66
	Disc. 33	-	-	-	20	-	0.2	61	15	5	6	4	1	5	2	5	17	10	0	53
	Disc. 34	-	-	-	41	-	0.3	91	12	9	6	4	1	6	2	5	18	10	-15	40
	Disc. 35	-	-	-	98	-	2.0	610	12	20	12	4	0	5	6	5	20	10	0	74
	Disc. 36	-	-	R5	76	-	0.6	183	12	15	8	6	1	1	2	5	15	10	0	60
	Disc. 37	-	-	-	56	-	0.4	122	12	11	7	4	0	1	6	5	16	10	-15	41

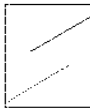
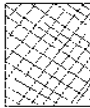
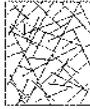



Appendix D.3: Calculation of Geological Strength Index
Preliminary Geotechnical Design Report
Bridge #1427 & #5800, I-95 over Stillwater Ave, Bangor, Maine
MaineDOT WIN 027176.00

Prepared by: KAR
Checked by: BK
Reviewed by: JDL

GSI =

55

Table 5: Most common GSI ranges for typical sandstones.*

GEOLOGICAL STRENGTH INDEX FOR JOINTED ROCKS (Hoek and Marinos, 2000) From the lithology, structure and surface conditions of the discontinuities, estimate the average value of GSI. Do not try to be too precise. Quoting a range from 33 to 37 is more realistic than stating that GSI = 35. <u>Note that the table does not apply to structurally controlled failures.</u> Where weak planar structural planes are present in an unfavourable orientation with respect to the excavation face, these will dominate the rock mass behaviour. The shear strength of surfaces in rocks that are prone to deterioration as a result of changes in moisture content will be reduced if water is present. When working with rocks in the fair to very poor categories, a shift to the right may be made for wet conditions. Water pressure is dealt with by effective stress analysis.			
		SURFACE CONDITIONS	
		VERY GOOD Very rough, fresh unweathered surfaces	
		GOOD Rough, slightly weathered, iron stained surfaces	
		FAIR Smooth, moderately weathered and altered surfaces	
		POOR Slickensided, highly weathered surfaces with compact coatings or fillings or angular fragments	
		VERY POOR Slickensided, highly weathered surfaces with soft clay coatings or fillings	
STRUCTURE		DECREASING SURFACE QUALITY →	
	INTACT OR MASSIVE - intact rock specimens or massive in situ rock with few widely spaced discontinuities	90 80	N/A
	BLOCKY - well interlocked undisturbed rock mass consisting of cubical blocks formed by three intersecting discontinuity sets	70 1 60	
	VERY BLOCKY - interlocked, partially disturbed mass with multi-faceted angular blocks formed by 4 or more joint sets	★	
	BLOCKY/DISTURBED/SEAMY - folded with angular blocks formed by many intersecting discontinuity sets. Persistence of bedding planes or schistosity	40	
	DISINTEGRATED - poorly interlocked, heavily broken rock mass with mixture of angular and rounded rock pieces	30	
	LAMINATED/SHEARED - Lack of blockiness due to close spacing of weak schistosity or shear planes	20	10
		← DECREASING INTERLOCKING OF ROCK PIECES	
		N/A	N/A

***WARNING:**
The shaded areas are indicative and may not be appropriate for site specific design purposes. Mean values are not suggested for indicative characterisation; the use of ranges is recommended

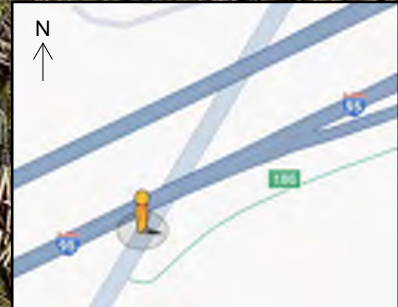
1. Massive or bedded (no clayey cement present)
2. Brecciated (no clayey cement present)

GSI chart from: Marinos, Paul, and Hoek, Evert. November 2000. GSI: a geologically friendly tool for rock mass strength estimation. ISRM International Symposium, Melbourne, Australia, paper number ISRM-IS-2000-035.

APPENDIX E

Rock Cut Discontinuity Photographs

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

NORTH

SOUTH

Date: 11/4/2024
Prepared: KAR
Checked: LMP
Reviewed: MEL

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

03

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

Date: 11/4/2024
Prepared: KAR
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Reviewed: MEL

BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

04

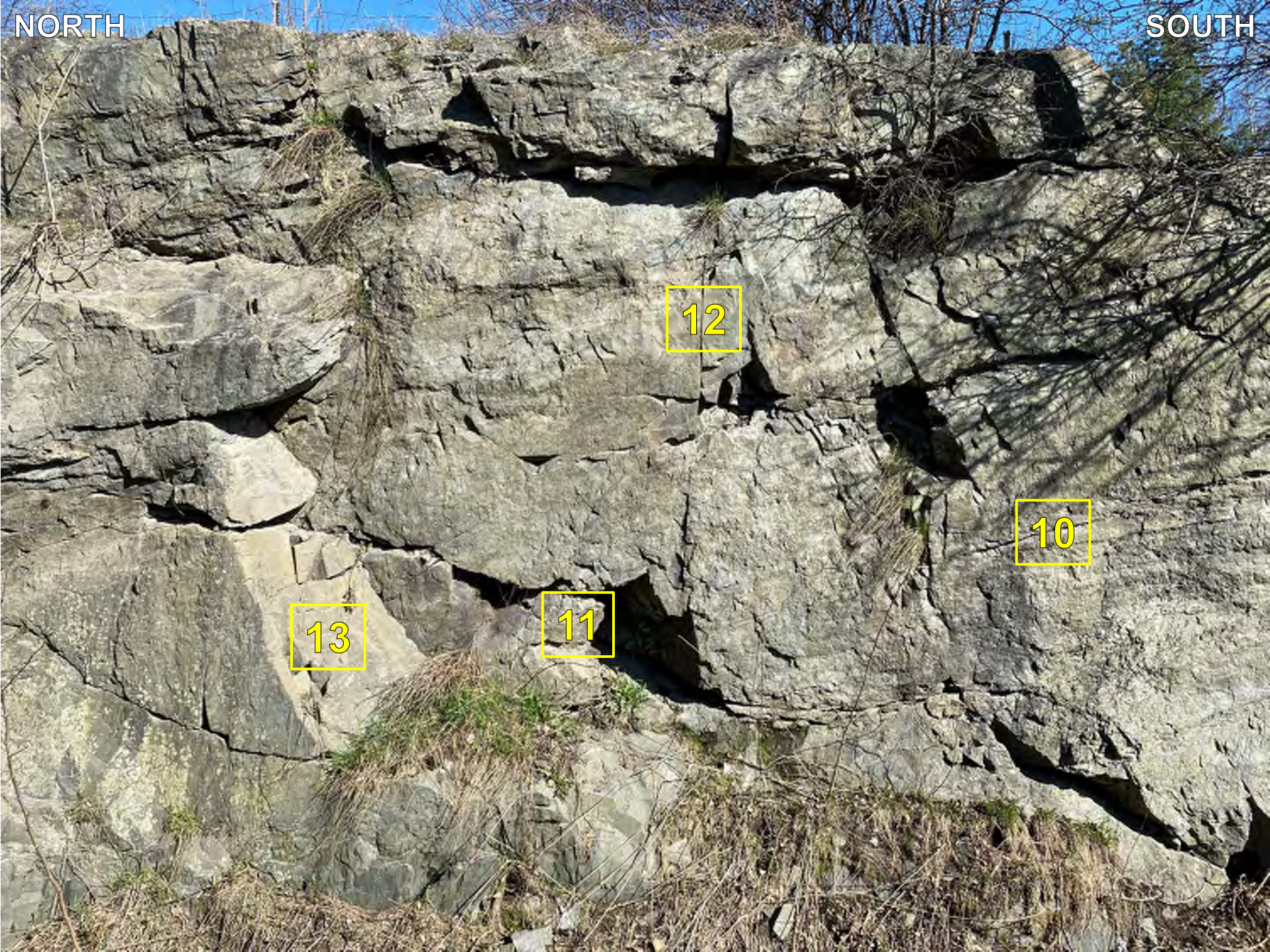
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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH



Date: 11/4/2024
Prepared: KAR
Checked: LMP
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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

05
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH



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Reviewed: MEL

BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

06

OF 54

NORTH

SOUTH

Date: 11/4/2024
Prepared: KAR
Checked: LMP
Reviewed: MEL

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

07

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH

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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

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08

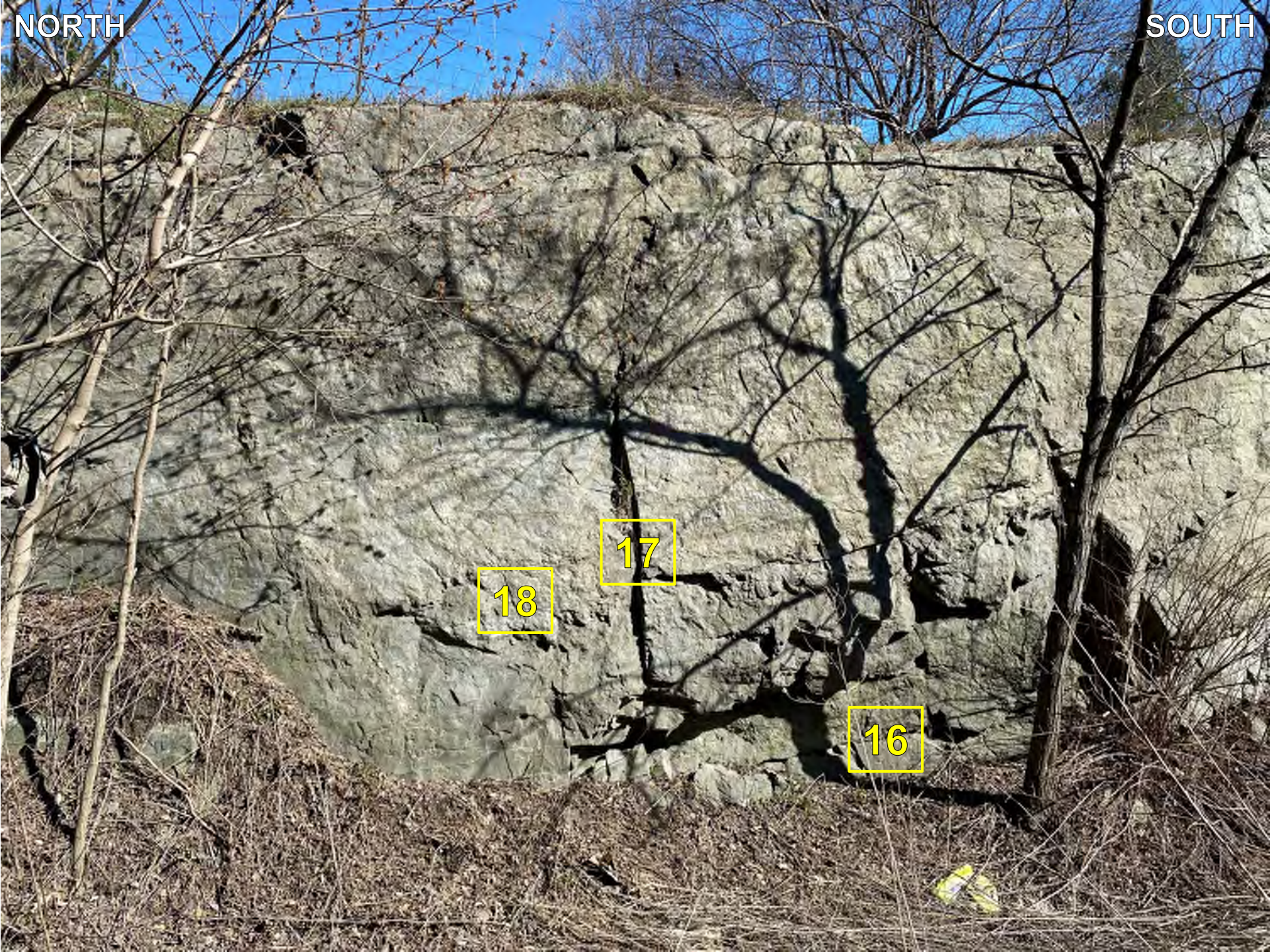
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH



Date: 11/4/2024
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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

09
OF 54

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND

19

18

17

BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

10
OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

11

OF 54

NORTH

SOUTH

Date: 11/4/2024
Prepared: KAR
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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

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OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

13

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



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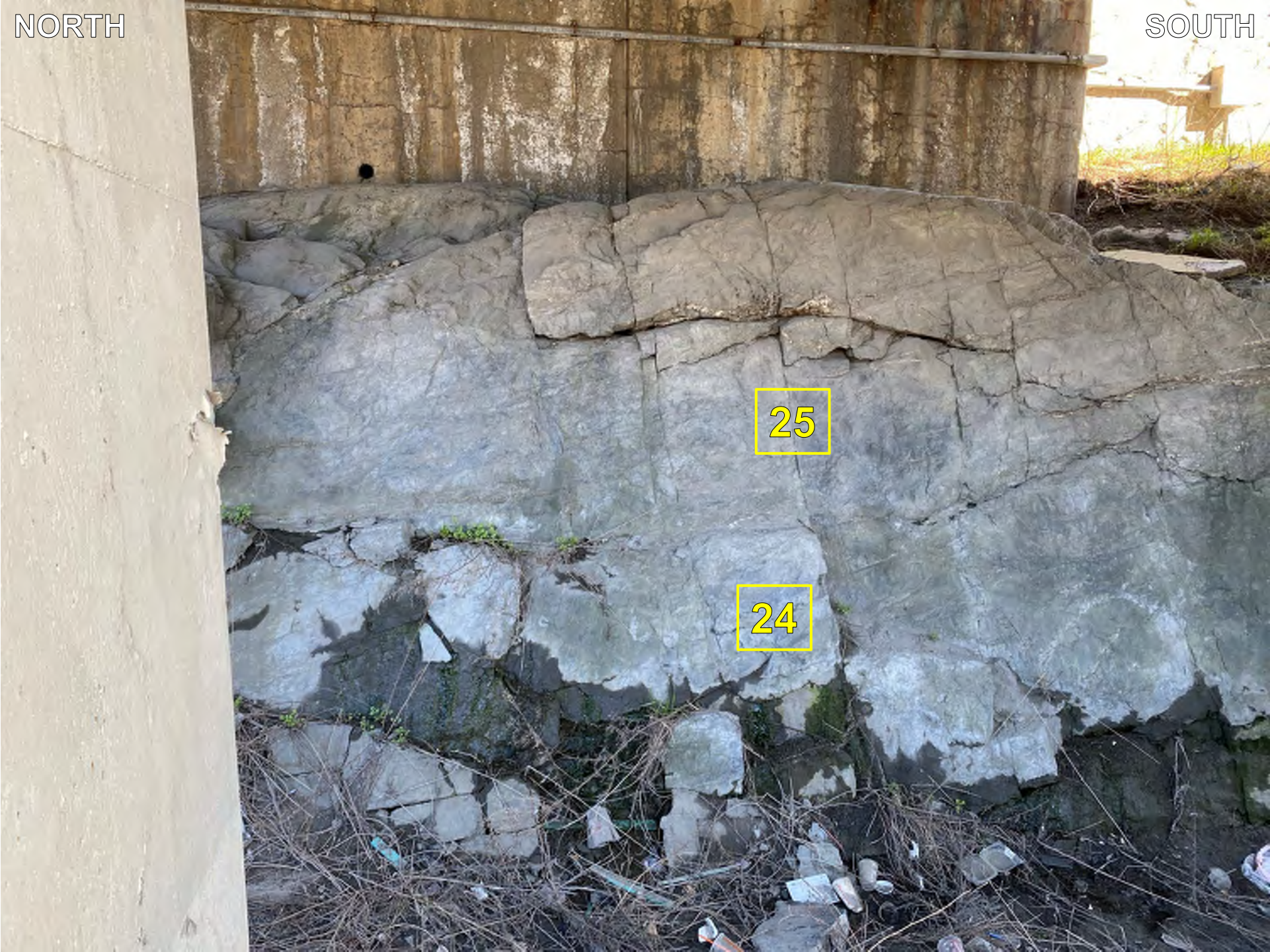
14
OF 54

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
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OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



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MAINEDOT WIN 027176.00

SHEET NUMBER

16

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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17

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH



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MAINEDOT WIN 027176.00

SHEET NUMBER

18

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH



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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

19
OF 54

NORTH

SOUTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

20
OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

21
OF 54

NORTH

SOUTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND

29

28

BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

22
OF 54



NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

23
OF 54



NORTH

SOUTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
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MAINEDOT WIN 027176.00

SHEET NUMBER

24

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
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BRIDGE #1427 & #5800
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OF 54



NORTH

SOUTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
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27

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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BRIDGE #1427 & #5800
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SHEET NUMBER

28
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



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30

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH

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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

31
OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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BRIDGE #1427 & #5800
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SHEET NUMBER

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OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

34

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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BRIDGE #1427 & #5800
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MAINEDOT WIN 027176.00

SHEET NUMBER

35
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH



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BRIDGE #1427 & #5800
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SHEET NUMBER

36
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH



SOUTH

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37

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH

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BRIDGE #1427 & #5800
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MAINEDOT WIN 027176.00

SHEET NUMBER

38
OF 54

NORTH

SOUTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



BRIDGE #1427 & #5800
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MAINEDOT WIN 027176.00

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE NORTHBOUND



NORTH

SOUTH



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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

40

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH

NORTH

Date: 11/4/2024
Prepared: KAR
Checked: LMP
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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

41

OF 54



SOUTH

NORTH

Date: 11/4/2024
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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

42

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH



NORTH

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Prepared: KAR
Checked: LMP
Reviewed: MEL

BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

43
OF 54

SOUTH

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800
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MAINEDOT WIN 027176.00

SHEET NUMBER

44
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH



NORTH

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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

45

OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH



NORTH

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MAINEDOT WIN 027176.00

SHEET NUMBER

46
OF 54

SOUTH

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

47

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH



NORTH

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BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
MAINEDOT WIN 027176.00

SHEET NUMBER

48

OF 54

SOUTH

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
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SHEET NUMBER

49

OF 54



SOUTH

NORTH

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STILLWATER AVENUE SOUTHBOUND



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SHEET NUMBER

50

OF 54



SOUTH

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



BRIDGE #1427 & #5800
I-95 OVER STILLWATER AVE, BANGOR, MAINE
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SHEET NUMBER

51

OF 54



SOUTH

NORTH

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ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



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SHEET NUMBER

52

OF 54



ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH



NORTH

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BRIDGE #1427 & #5800
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SHEET NUMBER

53
OF 54

ROCK CUT DISCONTINUITY ID LOCATIONS
STILLWATER AVENUE SOUTHBOUND



SOUTH

NORTH



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