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Memorandum

To: Ernie Martin
From: Karen Gross
Date: 2/11/2011
Subject: Final Geotechnical Information
Series 100 Report No. 2011-102
Biddeford, Elm Street (Rte. 1), PIN 14814.00

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All subsurface investigations and lab testing information have been completed for the Route 1 (Elm Street) project in Biddeford. The primary focus of these investigations is to determine the general types of pavement materials and subsurface soils in order to select the appropriate pavement treatment for this project.

Background Information

The project begins at the intersection with Beaudoin Avenue and extends southerly 0.54 miles to the intersection with Grayson Street. Route 1 at this location is classified as a minor arterial and is non-NHS. Traffic volumes are high with a current AADT of 13390, with 4% heavy trucks (536 heavy trucks per day). The 18-kip Equivalent Single Axle Loads (ESAL's) for a 20-year design period are 1,708,200.

The proposed scope of work includes widening for additional lanes, drainage improvements, and pavement structure improvements. The project is located in an urban area with a mix of commercial and residential properties, and a cemetery along the northbound lane. The immediate surrounding topography is considered flat.

Site Evaluation

A site visit was done to evaluate the existing pavement structure condition, to identify the types of pavement distress, to confirm as-built plan information, to note geological features, and to establish the preliminary subsurface investigation program.

The existing pavement is approximately 32' total width (12-foot travel lanes and a southbound 8-foot paved shoulder), with a 5-foot wide gravel shoulder on the northbound side of the roadway. The pavement is moderately to severely distressed throughout the project. The primary types of distress are reflective cracking of longitudinal and transverse concrete joints up through the asphalt surface. There is also evidence of reflective "D" cracking (durability cracking). Using coarse aggregate in the concrete mix that is susceptible to freeze-thaw deterioration is the underlying cause of D-cracking. It always is located at the pavement joints, cracks or free edges. Cracking usually begins at the bottom of the slab and moves upward with

time. Therefore, the bottom of the slab may be severely deteriorated before the cracks appear at the surface.

There is currently no ditching or underdrain present at this location. Standing water can be seen on the shoulders after rainstorms and during spring thaw. This standing water is a source of water for the formation of D-cracking and can enter the pavement through surface cracks as well as from the saturated underlying base material.

As-Built Information

As-built plans from 1932 indicate that the roadway was originally constructed with three 10-foot wide, 40-foot long, continuously reinforced concrete slabs. The slabs were constructed at variable thicknesses, ranging from 7" inches thick at the center of the slab, and widening to 7½" thick at the outside of the slabs. The as-built plan sheets indicate that 8" of base gravel was placed under the concrete pavement in this section of Route 1. At some point, the roadway was overlaid with bituminous pavement.

Geology

The Maine Surficial Geology map for the Biddeford Quadrangle shows that the surficial soils at this location are Marine shoreline deposits that consist predominately of sands and gravels. The Soil Survey of York County indicates that the surficial soils are of the Adams series (AgB), which consists of sand and small quantities of silt size particles, with the amount of silt size particles decreasing with depth. Adams soils are well draining, with permeability rates increasing with depth (a function of the decreasing silt size particles). Ponding of water on the surface is common in the late winter. The Soil Survey also has information on the engineering index properties, classifications, and land use considerations. Table 1 summarizes the information from the Soil Survey.

Table 1: Soil Survey Summary

Soil Unit	Unified Classification	AASHTO Classification	Depth to H ₂ O	Depth to Bedrock	Frost Action	Permeability
Adams (AgB)	SM, SP-SM, SW-SM, SP	A-1, A-2, A-3	> 6'	> 6'	Low	6 – 20 in/hr

The Maine Design Freezing Index for this site is approximately 1250. For snow free pavement, the anticipated depth of frost penetration beneath the pavement structure is 68" for sand deposits. Natural soils at this location are considered only slightly frost susceptible, therefore the formation of ice lens and associated frost heaving/thaw weakening damage to the pavement is not probable.

Subsurface Investigations and Lab Testing

Roadway Investigations and Lab Testing

Eight borings were drilled (May 2008) in the roadway to determine the subsurface material types, to confirm the existence of a concrete roadway, to collect representative samples and depths of the existing base/subbase gravels, to identify shallow bedrock, and to identify the depth to groundwater. Borings were drilled to a depth of approximately 5' or refusal, which

ever was encountered first. Pavement cores were also collected at two locations to confirm the HMA and concrete thicknesses, and material quality. No shallow refusals or groundwater were encountered in any borings.

Boring and core information indicates that the pavement structure consists of approximately 3.6" to 6.0" of HMA, 4.8" to 7.2" of concrete pavement, and 16.8" to 25.2" of granular material. A core collected in a joint location at Station 43+25 revealed that the bottom of the slab at that location was severely deteriorated.

Laboratory testing was completed on eight samples to determine the grain size distribution, water content, the Unified (USCS) and AASHTO Classifications, and the Frost Susceptibility Rating of the existing subbase and subgrade.

The subbase samples test results indicate that the existing material has a Unified classification of SM and an AASHTO classification of A-1-B or A-2-4. The existing subbase exceeds the MaineDOT maximum of 7% passing the #200 sieve and therefore does not meet the MaineDOT requirements for base or subbase aggregate.

All subgrade samples tested have a Unified Classification of SP-SM or SM and an AASHTO Classification of A-1-B or A-2-4. The subgrade soils are considered slightly frost susceptible. Test results confirm the soils information in the Soil Survey and on the Surficial Geology map. Testing results indicate that there are higher water contents in the subgrade samples at Stations 50+96 and 63+13. Roadway photographs indicate that water ponds on the surface in this general location.

Table 2 summarizes the subsurface information and lab testing data. Please refer to the detailed boring logs and the lab testing data attached at the end of this report for more specific information.

Table 2: Geotechnical Investigations and Lab Testing Summary-Roadway

Boring No.	Station	Offset (ft)	Drilling Depth (ft)	Depth to water (ft)	Pavement Thickness			Total Pavement Thickness (in)	Subbase Class (USCS & AASHTO)	Subgrade Type
					HMA (in)	Concrete (in)	Subbase (in)			
HB-BIDD-101	63+13	6.4 L	5.0	xxx	3.6	7.2	25.2	36.0	SM / A-2-4	SAND
HB-BIDD-102	56+23	4.1 R	5.0	xxx	4.8	6.0	19.2	30.0	SM / A-1-b	SAND
HB-BIDD-103	52+84	4.1 R	5.0	xxx	4.8	6.0	19.2	30.0	SM / A-1-b	SAND
HB-BIDD-104	50+96	4.2 L	5.0	xxx	4.8	4.8	16.8	26.4	SM / A-2-4	SAND
HB-BIDD-105	48+08	4.8 L	5.0	xxx	4.8	6.0	19.2	30.0	SM / A-1-b	SAND
HB-BIDD-106	46+38	6.4 L	5.0	xxx	6.0	4.8	19.2	30.0	SM / A-2-4	SAND
HB-BIDD-107	43+52	12.4 R	5.0	xxx	6.0	6.0	18.0	30.0	SM / A-2-4	SAND
HB-BIDD-108	40+33	4.5 R	5.0	xxx	6.0	6.0	18.0	30.0	SM / A-2-4	SAND

Drainage Outlet Investigations and Lab Testing

Six borings were drilled off alignment from Station 50+75 to 51+80 for a proposed drainage outlet location and for environmental purposes. Borings HB-BIDD 201 through HB-BIDD-205 were located in a fill area that consisted of tailings and waste soils from the Biddeford Wal-Mart construction project several years ago. All borings were drilled to 30' (+/-) below the existing ground surface, or to refusal, whichever was encountered first. The materials encountered included sand, gravel, silt, clay, asphalt, brick, and rock fragments. Refusal was encountered at a few locations and based on the drill bit response, the drillers believe that refusal was on boulder sized material and not bedrock. Boulder sized tailings are visible at the edge of the fill area, so it is assumed that the refusal was on similar sized pieces of rock. Native soils encountered below the fill consist primarily of sand with small amounts of gravel. Groundwater was encountered in one boring at an elevation 136.8' (corresponds to 28.2' b.g.s). This elevation was measured during the drilling process and probably does not represent a stabilized groundwater elevation. Wet soils were encountered within some of the fill material, therefore the drainage capabilities of the fill is expected to be variable.

One boring (HB-BIDD-206) was drilled in what is believed to be native soils at Station 50+60 and approximately 434.4' to the northwest of Route 1. This boring was drilled to a depth of 12' below the existing ground surface. Soils at this location consist of sand with small amounts of gravel and silt. Groundwater was encountered at elevation of 133.7' (8.8' b.g.s.) Again, this depth was measured during the drilling process and probably does not represent a stabilized groundwater level. The Soil Survey of York County indicates that the surficial soils at this location are of the Colton series (CoB), which consists primarily of sand and gravel. Colton soils typically have a very rapid permeability rate. As per the Soil Survey, there is a hazard of groundwater contamination because of the rapid permeability of this soil.

Table 3 summarizes the investigations and lab testing information at the proposed drainage outlet location.

Table 3: Geotechnical Investigations and Lab Testing Summary-Drainage Outlet

Boring No.	Station	Offset (ft)	Drilling Depth (ft)	Depth to refusal (ft)	Depth of fill (ft)	Fill - USCS/AASHTO Classification	Natural soil - USCS/AASHTO Classification	Depth to water (ft)	Comments
HB-BIDD-201	50+79.3	201.7 R	31.5		14	SW-SM, A-1-b	SP/A-3	28.2	g.w. elev. 136.2"
HB-BIDD-202	51+35	220.4 R	27		23	ML, A-4	SP-SM/ A-3		wet soils @ 10'
HB-BIDD-203	51+79.8	239.5 R	32		29	SM, A-1-b	SP-SM/ A-1-b		wet soils @ 10'
HB-BIDD-204	51+15.5	300.1 R	15.8	15.8	15.8	GM, A-2-4			
HB-BIDD-205	50+74.5	322.1 R	17.1	17.1	17.1	ML, A-4			wet soils @ 5'
HB-BIDD-206	50+60	434.4 R	12				SM, SP-SM/A-1-b	8.8	g.w. elev. 133.7'

Design Considerations

Pavement Structure

The D-cracking in the existing concrete pavement is considered medium to high severity, and it is expected that the underside of the concrete is highly deteriorated at joint locations. The pavement core in photo C-2 shows the deterioration at the bottom of the slab. D-cracking is a

non-repairable materials issue and will eventually result in slab disintegration and loss of support for traffic loadings. The existing subbase does not meet the MaineDOT requirements for base or subbase aggregate. Removing the existing concrete pavement and underlying gravel and constructing a new 30" thick pavement structure is recommended.

Subgrade

The subgrade soils consist primarily of sand with varying amounts of silt. This soil type should provide excellent foundation support for the pavement structure. Based on the boring information and correlations to Soil Support Values, the recommended Subgrade Resilient Modulus (Mr) value to use for the pavement design is 4800 psi. Testing results indicate that there are higher water contents in the subgrade samples at Stations 50+96 and 63+13.

Bedrock

No shallow refusals were encountered in the borings therefore bedrock excavation is not expected on this project. Geology maps also indicate that there is no shallow bedrock at this location.

Drainage

The existing underlying natural soils have good drainage properties and the permeability increases as the depth below the surface increases. No shallow groundwater issues are expected. Since the surface soils may have a lower permeability rate, positive drainage of the pavement structure is recommended to prolong pavement service life. Surface water should be removed either by ditching or by a closed drainage system.

Construction Considerations

Soil Survey maps indicate that the existing natural soils tend to cave when excavated, therefore trenches for underdrain and cross pipes may be difficult to keep open. If groundwater is encountered in deeper excavations, dewatering may be necessary to keep the trench in the dry and the soils stable.

Attachments:

Project Location Map

Project Pavement Photo's

As-built Plans

Maine Surficial Geology Map (Biddeford Quadrangle)

Soil Survey of York County

Design Freezing Index/Frost Depth Chart

Boring Logs

Pavement Core Photo's

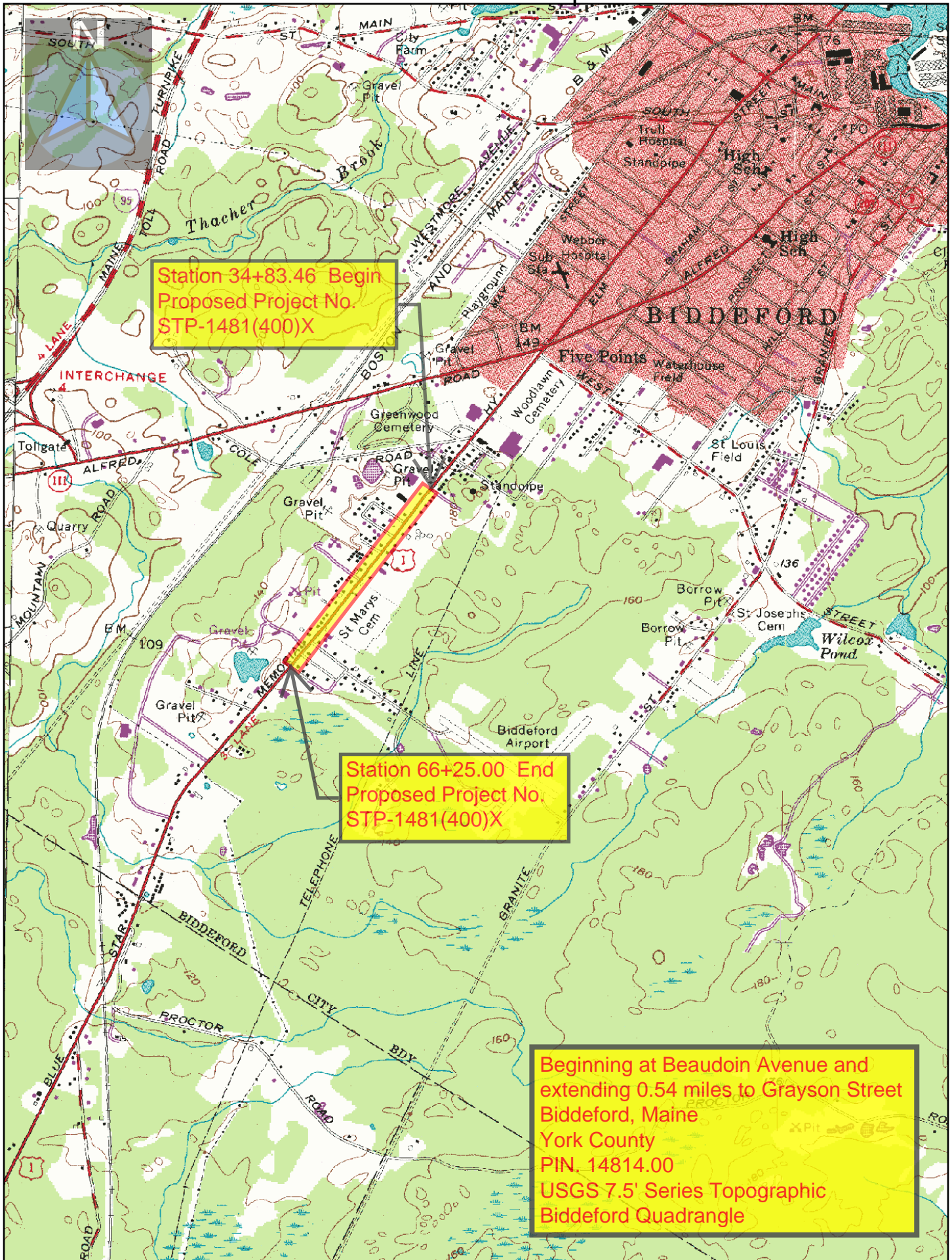
Laboratory Testing Summary Sheet

Grain Size Curves

Subgrade Resilient Modulus Charts

Geoplans

Location Map

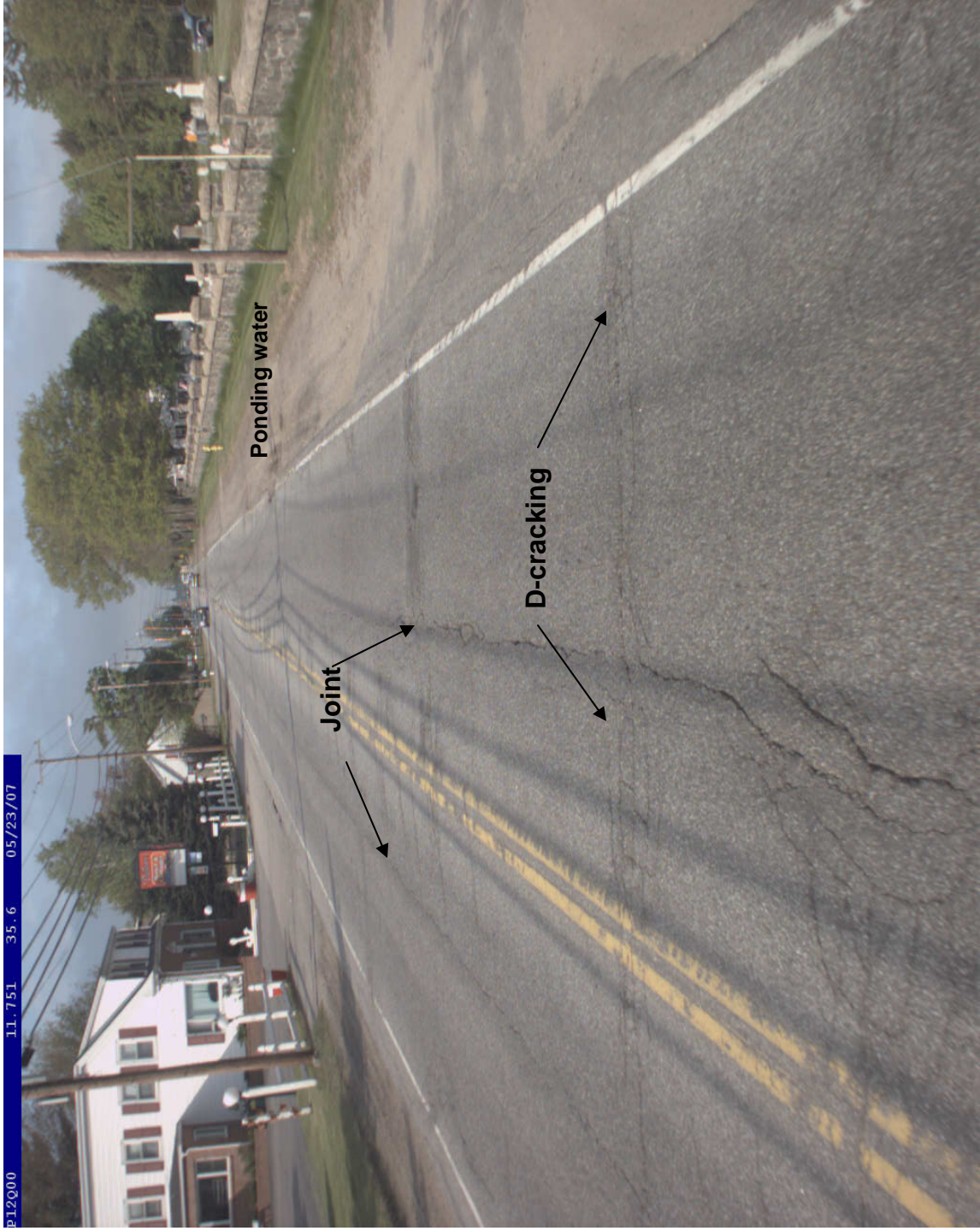


Map Scale 1:24000

The Maine Department of Transportation provides this publication for information only. Reliance upon this information is at user risk. It is subject to revision and may be incomplete depending upon changing conditions. The Department assumes no liability if injuries or damages result from this information. This map is not intended to support emergency dispatch. Road names used on this map may not match official road names.

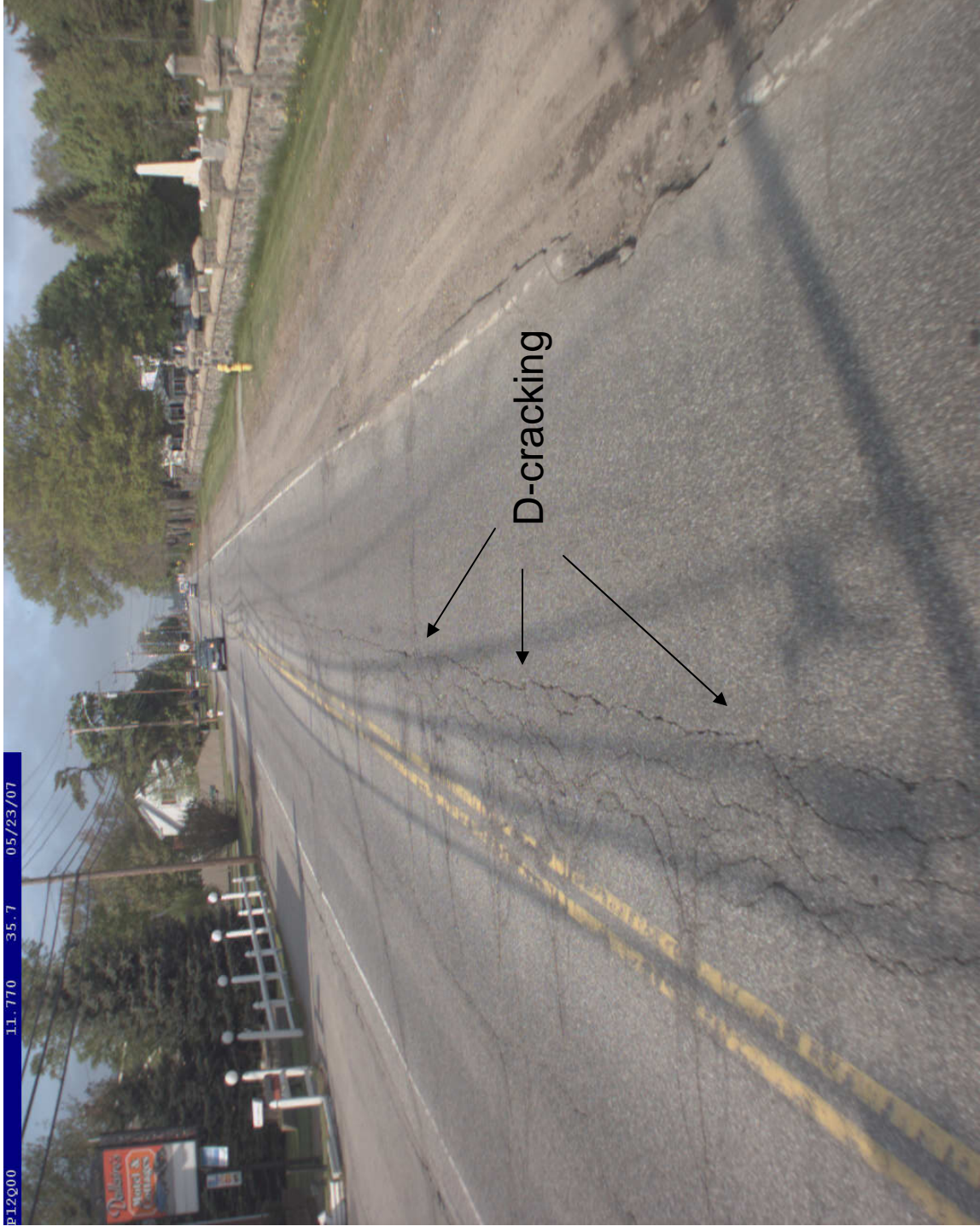
Station 58+00

PI12000 11.751 35.6 05/23/07



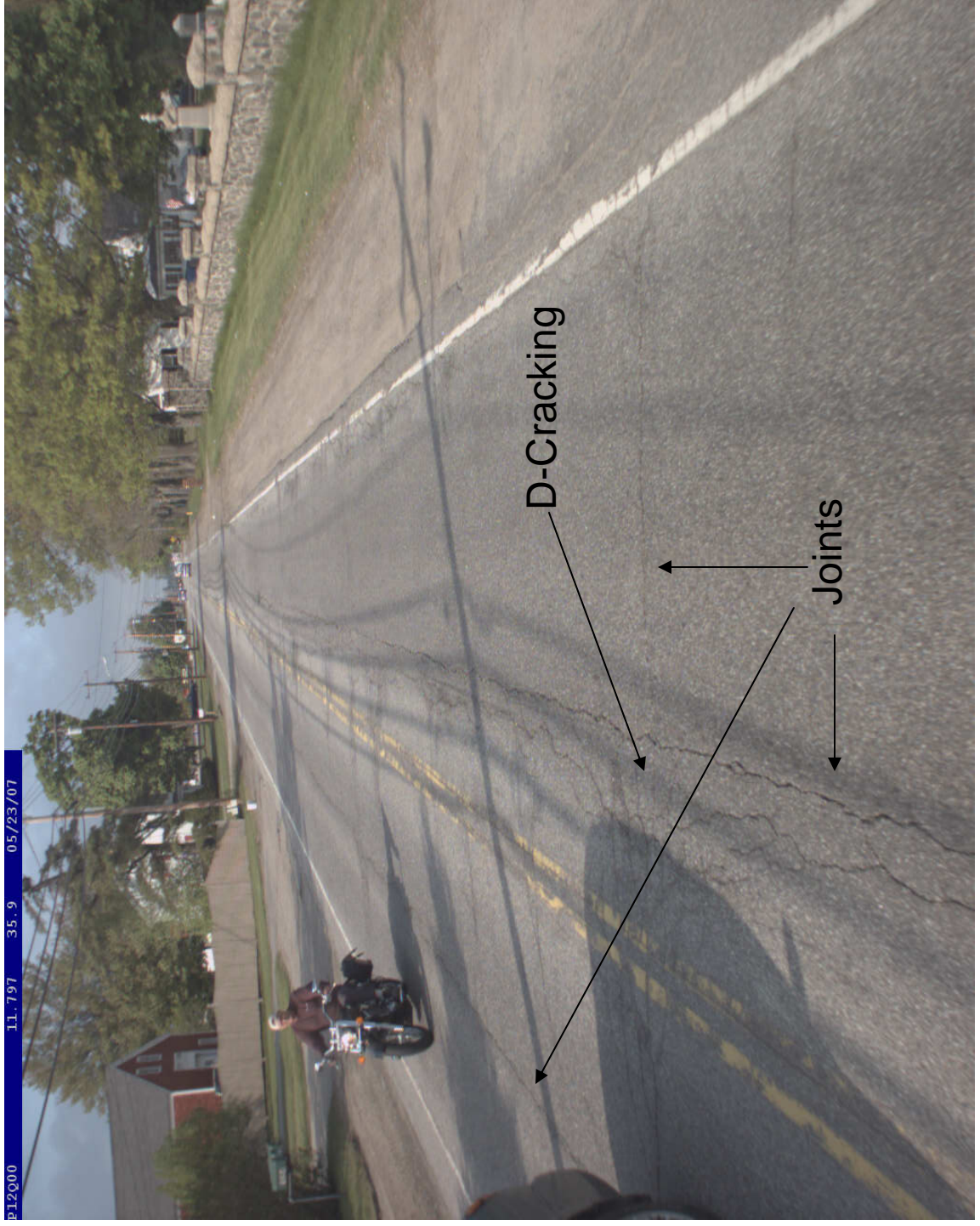
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Station 54+00

PI2000 11.797 35.9 05/23/07



Station 52+00



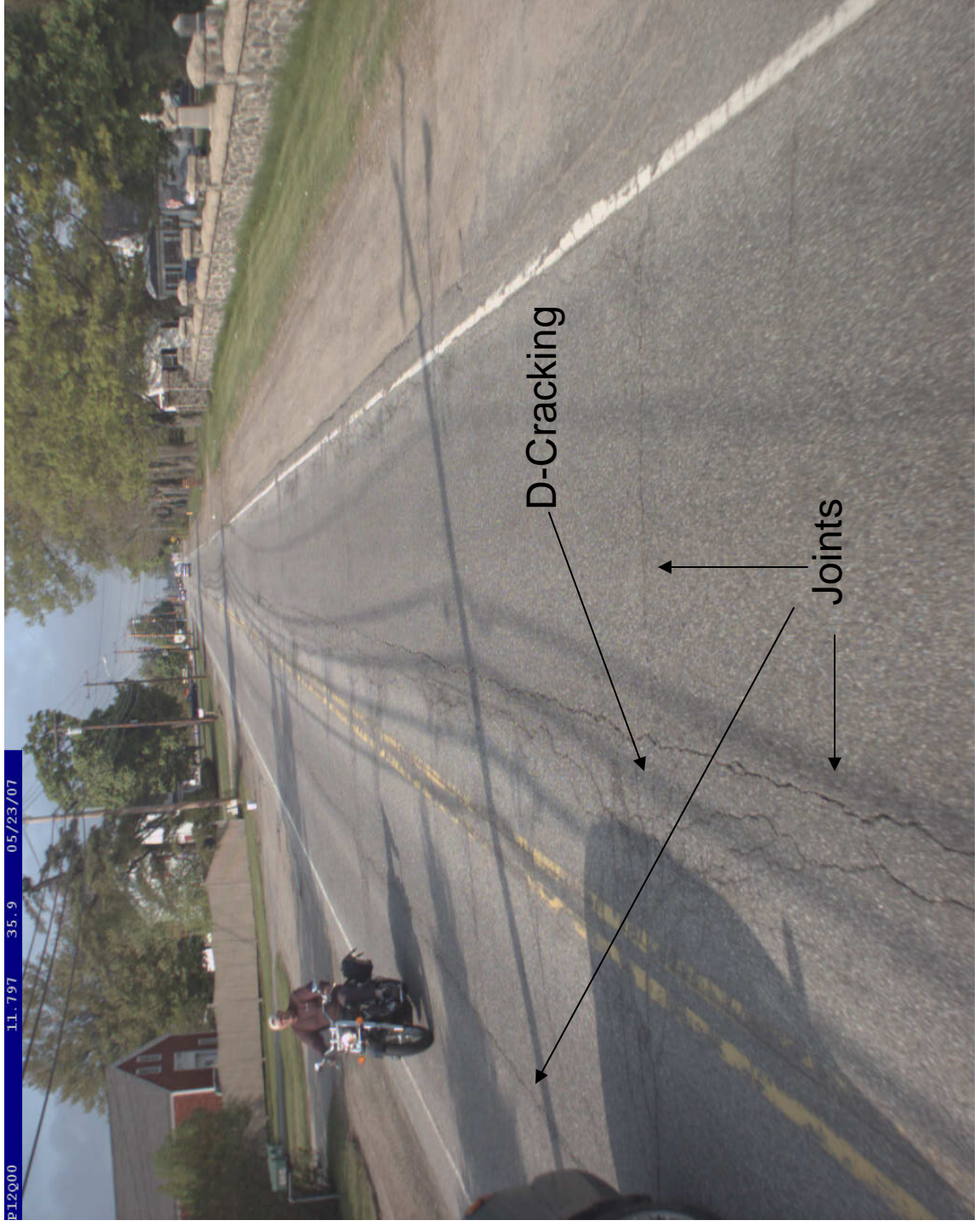
Station 41+00

P12000 12.046 32.9 05/23/07



Station 54+00

PI2000 11.797 35.9 05/23/07



Station 52+00



Station 41+00

P12000 12.046 32.9 05/23/07



DURABILITY CRACKING (“D” CRACKING)

Description

Closely spaced crescent-shaped hairline cracking pattern.

Occurs adjacent to joints, cracks, or free edges; initiating in slab corners. Dark coloring of the cracking pattern and surrounding area.

How to Measure

Record number of slabs with “D” cracking and square meters of area affected at each severity level. The slab and affected area severity rating is based on the highest severity level present for at least 10 percent of the area affected.

Severity Levels

LOW

“D” cracks are tight, with no loose or missing pieces, and no patching is in the affected area.

MODERATE

“D” cracks are well-defined, and some small pieces are loose or have been displaced.

HIGH

“D” cracking has a well-developed pattern, with a significant amount of loose or missing material. Displaced pieces, up to 0.1 m², may have been patched.

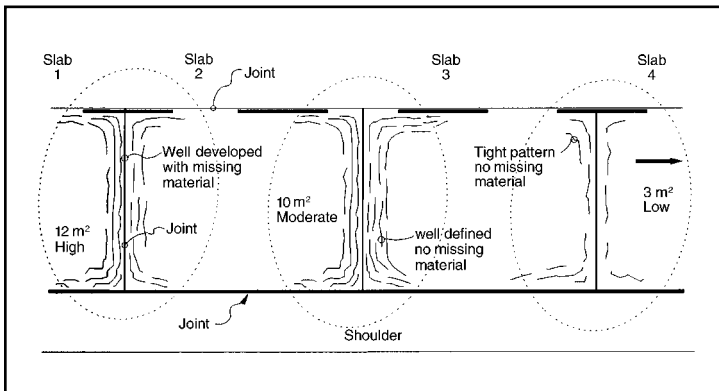


FIGURE 51
Distress Type JCP 2—Durability Cracking (“D” Cracking)



FIGURE 53
Distress Type JCP 2—High Severity “D” Cracking with Loose and Missing Material



FIGURE 52
Distress Type JCP 2—Moderate Severity “D” Cracking with Well-Defined Pattern

Route 1 (Elm Street) – Northbound
Station 61+00



Route 1 (Elm Street) – Northbound
Station 53+00



Route 1 (Elm Street) – Northbound
Station 49+00



STATE OF MAINE
STATE HIGHWAY COMMISSION

PLAN AND PROFILE
STATE HIGHWAY ^{RP A} 119
NORTH KENNEBUNKPORT
AND
BIDDEFORD
YORK COUNTY

FEDERAL AID PROJECT NO. 101A

TOTAL LENGTH 6032 MILES

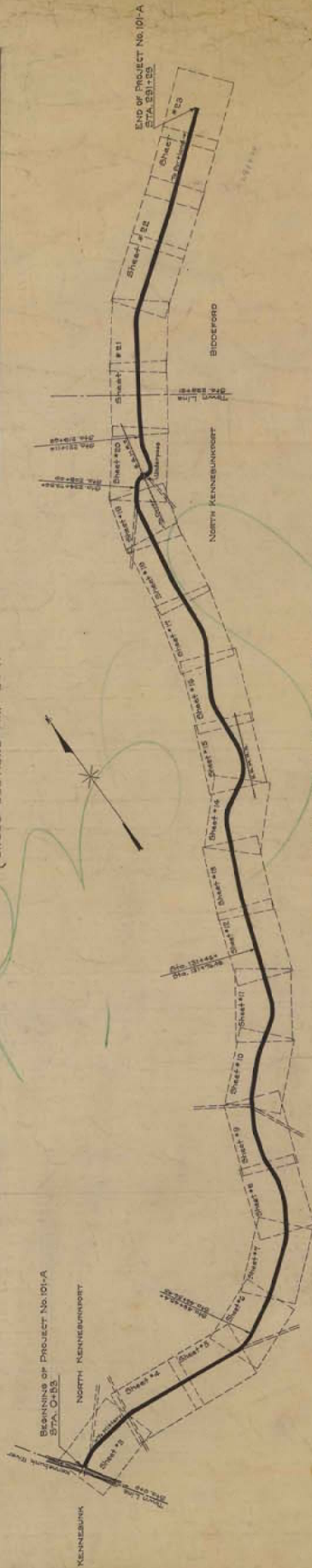
PLAN 1 IN. = 50 FT.
PROFILE 1/8" IN. = 5 FT.
CROSS SECTIONS 1 IN. = 5 FT.

CONVENTIONAL SIGNS

STATE OR NATIONAL LINE	SURVEY LINE
COUNTY LINE	CONCRETE
UNFENCED PROPERTY	TRIVETRY POLE
FENCE	POWER POLE
FRONT OF WAY LINE	TILL POLE
RIGHT OF WAY	RAILROAD
ROADWAY	STONE WALL
RETAINING WALL	

INDEX OF SHEETS

SHEET NO.	TITLE PAGE	STA.
1	TYPICAL SECTIONS	0+53-291+29
2	PLAN AND PROFILE	0+53-291+29
3-23	CROSS-SECTIONS	0+53-291+29
24-52	SMOOTH	0+53-291+29
53	SPECIAL DETAILS	0+53-291+29



KEY MAP STATE HIGHWAY 119 WELLS TO BIDDEFORD
Approx. Scale: 1 in. = 10 mi.

APPROVED:
U. S. BUREAU OF PUBLIC ROADS

APPROVED:
MAINE STATE HIGHWAY COMMISSION

Charles W. ...
William ...
Charles W. ...
Frank ...

A16

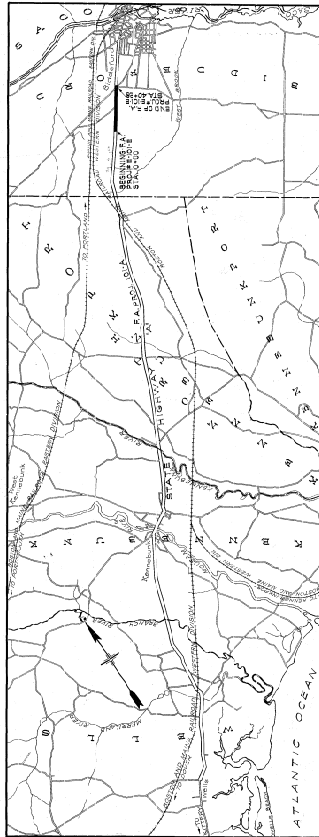
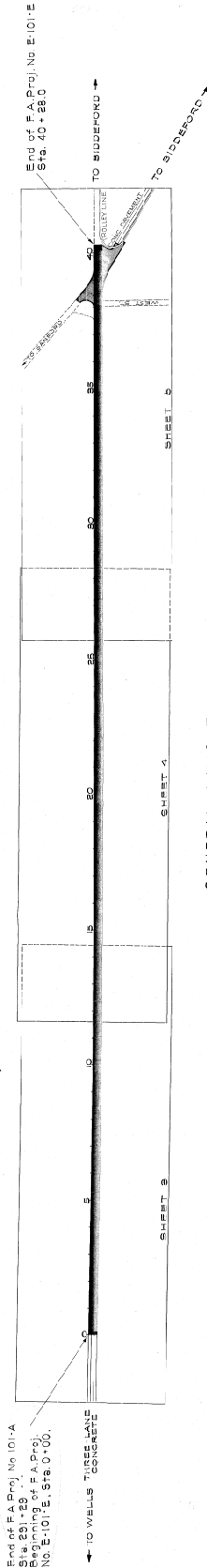
STATE OF MAINE STATE HIGHWAY COMMISSION

PLAN AND PROFILE STATE HIGHWAY PP A 99 **BIDDEFORD** YORK COUNTY FEDERAL AID PROJECT NO. E-101-E

TOTAL LENGTH 0.762 MILES
 PLAN 1" = 50 FT.
 PROFILE 1" = 50 FT.
 SCALES { HOR. 1" = 50 FT.
 { VER. 1" = 5 FT.
 { CROSS SECTIONS 1" = 5 FT.

CONVENTIONAL SIGNS	
STATE OR NATIONAL LINE	
COUNTY LINE	
TOWN LINE	
UNIMPROVED PROPERTY	
FENCE	
RIGHT OF WAY LINE	
TRAVELED WAY	
RAILROAD	
RETAINING WALL	
SURVEY LINE	
CULVERT	
DROP INLET	
POWER POLE	
TEL. POLE	
MARSH	
TREES	
STONE WALL	

INDEX OF SHEETS	
SHEET NO.	TITLE PAGE
1	TYPICAL SECTIONS
2	PLAN AND PROFILE
3-6	CROSS-SECTIONS
7-13	BRIDGES
14	SPECIAL DETAILS



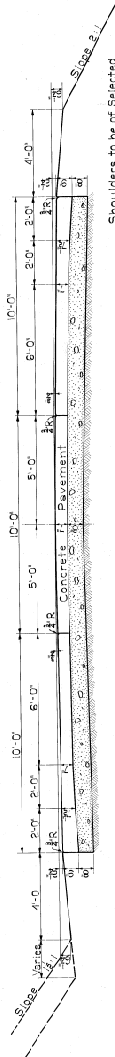
Note: All work contemplated under this contract to be governed by, and in conformity with, the specifications added March 21, 1955, except as modified on this plan.

APPROVED:
 MAINE STATE HIGHWAY COMMISSION
Edward J. [Signature]
 Chief Engineer

APPROVED:
 U.S. BUREAU OF PUBLIC ROADS
 DISTRICT ENGINEER
Ward V. [Signature]
 Chief Engineer

APPROVED:
 U.S. BUREAU OF PUBLIC ROADS
 DISTRICT ENGINEER
William D. [Signature]
 Chief Engineer

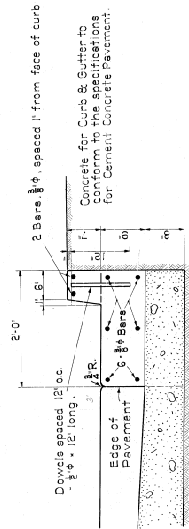
STANDARD SECTION 30' CONCRETE PAVEMENT



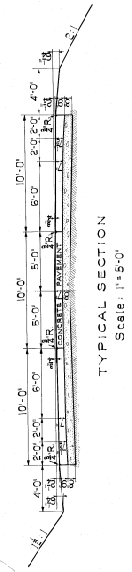
8" GRAVEL BASE
 Cement Concrete Pavement - 66.46 Cu. Yds per 100 Lin. Ft.
 8" Gravel Base Course - 81.66 Cu. Yds per 100 Lin. Ft.
 Gravel Base may be omitted subject to the opinion of the Engineer, soil conditions are suitable.

Location and depth of ditch to depend on local conditions.

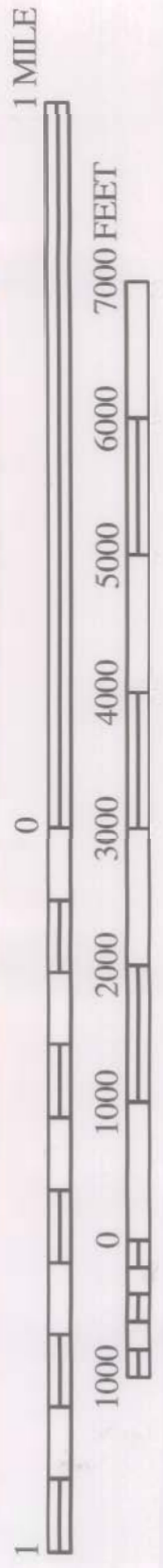
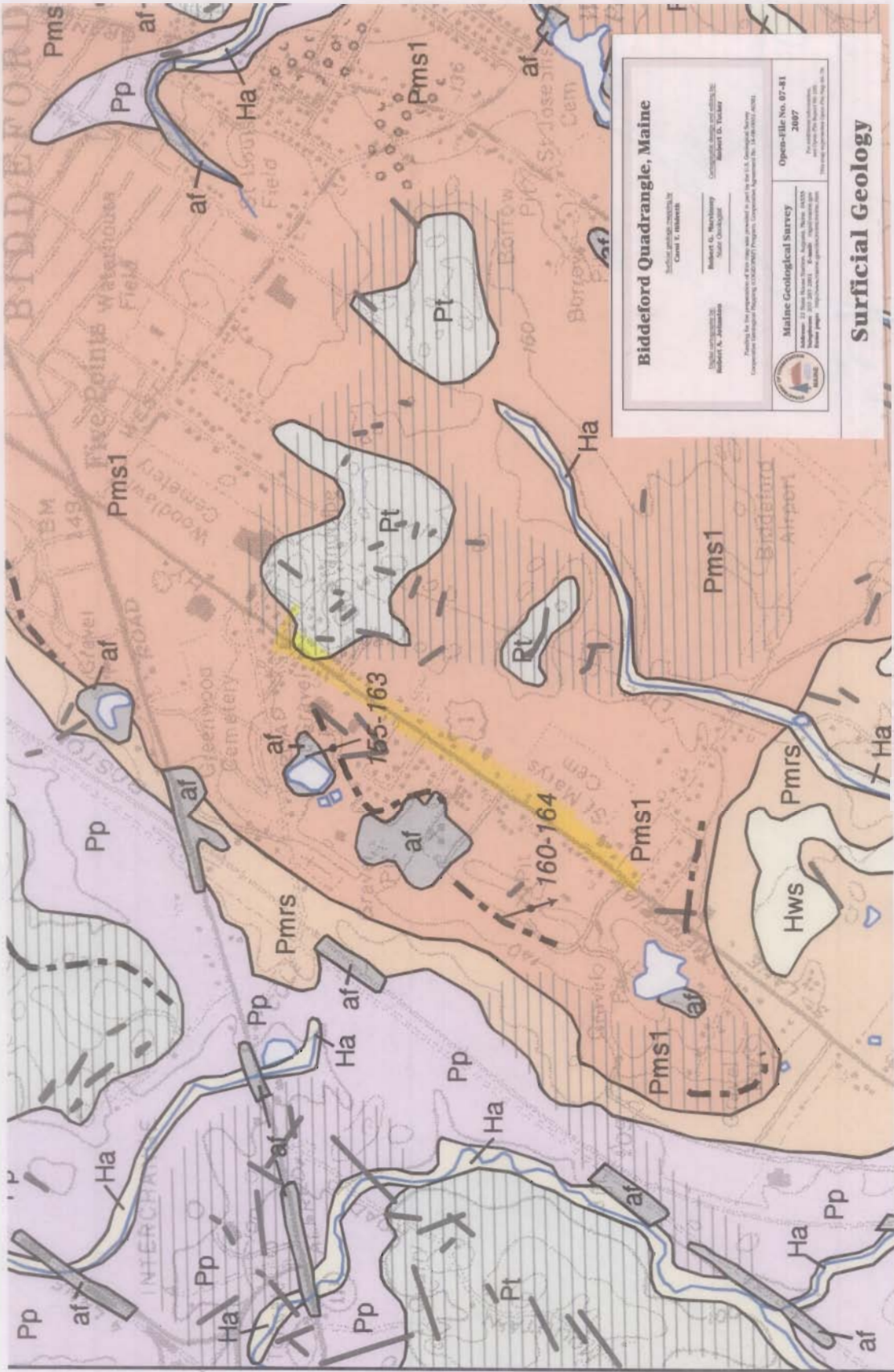
ESTIMATE OF QUANTITIES				
ITEM	DESCRIPTION	QUANTITY	UNIT	REMARKS
12A	Earth Excavation	7.765	Cu Yds	
13	Excavation for Structures	3.715	Cu Yds	
13	Gravel Base Course	4.316	Cu Yds	
30	Cement Concrete Pavement	2.654	Cu Yds	
34A	Placing Reinfor for Pavement	159.666	Lbs.	
42A	Laying 6" Vitrified Clay Piles	4.4	Lin. Ft.	
42C	Laying 15" Vitrified Clay Piles	2.4	Lin. Ft.	
42D	Laying 18" Vitrified Clay Piles	1.906	Lin. Ft.	
42E	Catch Basins (Sticks)	27	Each	
50	Cobble Stone Gutter	65.5	Sq Yds	
55	Concrete Curb & Gutter	125	Lin. Ft.	



DETAIL
CURB & GUTTER
 Scale: 1"=1'-0"



TYPICAL SECTION
 Scale: 1"=5'-0"



USES OF SURFICIAL GEOLOGY MAPS

A surficial geology map shows all the loose materials such as till (commonly called hardpan), sand and gravel, or clay, which overlie solid ledge (bedrock). Bedrock outcrops and areas of abundant bedrock outcrops are shown on the map, but varieties of the bedrock are not distinguished (refer to bedrock geology map). Most of the surficial materials are deposits formed by glacial and deglacial processes during the last stage of continental glaciation, which began about 25,000 years ago. The remainder of the surficial deposits are the products of postglacial geologic processes, such as river floodplains, or are attributed to human activity, such as fill or other land-modifying features.

The map shows the areal distribution of the different types of glacial features, deposits, and landforms as described in the map explanation. Features such as striations and moraines can be used to reconstruct the movement and position of the glacier and its margin, especially as the ice sheet melted. Other surficial features include shorelines and deposits of glacial lakes or the glacial sea, now long gone from the site. This glacial geologic history of the quadrangle is useful to the larger understanding of past earth climate, and how our region of the world underwent recent geologically significant climatic and environmental changes. We may then be able to use this knowledge in anticipation of future similar changes for long-term planning efforts, such as coastal development or waste disposal.

Surficial geology maps are often best used in conjunction with related maps such as surficial materials maps or significant sand and gravel aquifer maps for anyone wanting to know what lies beneath the land surface. For example, these maps may aid in the search for water supplies, or economically important deposits such as sand and gravel for aggregate or clay for bricks or pottery. Environmental issues such as the location of a suitable landfill site or the possible spread of contaminants are directly related to surficial geology. Construction projects such as locating new roads, excavating foundations, or siting new homes may be better planned with a good knowledge of the surficial geology of the site. Refer to the list of related publications below.

OTHER SOURCES OF INFORMATION

1. Hildreth, C. T., 1999, Surficial geology of the Biddeford 7.5-minute quadrangle, York County, Maine: Maine Geological Survey, Open-File Report 99-109, 6 p.
2. Hildreth, C. T., 1998, Surficial materials of the Biddeford quadrangle, Maine: Maine Geological Survey, Open-File Map 98-183.
3. Neil, C. D., 1998, Significant sand and gravel aquifers of the Biddeford quadrangle, Maine: Maine Geological Survey, Open-File Map 98-149.
4. Thompson, W. B., 1979, Surficial geology handbook for coastal Maine: Maine Geological Survey, 68 p. (out of print)
5. Thompson, W. B., and Borns, H. W., Jr., 1985, Surficial geologic map of Maine: Maine Geological Survey, scale 1:500,000.
6. Thompson, W. B., Crossen, K. J., Borns, H. W., Jr., and Anderson, B. G., 1989, Glaciomarine deltas of Maine and their relation to late Pleistocene-Holocene crustal movements, in Anderson, W. A., and Borns, H. W., Jr. (eds.), Neotectonics of Maine: Maine Geological Survey, Bulletin 40, p. 43-67.

Marine regressive sand deposits - Massive to stratified and cross-stratified, well-sorted sand. Generally has gradational basal contact with Pt. Thickness 0.5 to 5 m. Deposited during regressive phase of marine submergence.

Presumpscot Formation - Massive to laminated, gray and blue-gray (weathering brown) silt and silty clay. Locally may contain boulders, sand and gravel. Occurs as blanket deposit over bedrock and older glacial sediments. Variable thickness of 1-20 m. Deposited during period of late-glacial submergence.

Till - Gray to gray-brown poorly sorted mixture of silt, sand, pebbles, cobbles, and boulders. Forms a blanket deposit over bedrock, and is inferred to underlie younger sediments where not exposed at surface. Thin over topographic bedrock highs; thickers in topographic low areas, averages 1-5 m in thickness.

Bedrock - Rock units not distinguished. Individual outcrops not shown in areas of poor access. Ruled pattern indicates areas where surficial materials are thin (less than 1-2 m) and bedrock exposures are abundant. Areas of bedrock exposure (gray areas) are mapped in part from direct observation and in part from aerial photos.

Contact

Marine strandline - Defined by beach or base of wave-cut cliff.

Abandoned stream channel - Channel inferred to have been eroded by post-glacial stream during marine offlap. Arrow indicates inferred direction of flow.

Glacial Striation - Includes striations, grooves, crag-and-tail, sand related ice-flow indicators on bedrock outcrops. Dot to center of arrow is point of observation. Arrowhead omitted where ice-flow direction is unknown. Flag indicates older trend.

Crossbeds - Arrow indicates average direction and dip of cross-bedding in glacioluvial deposits. Tip of arrow is at point of observation.

Marine fossil locality - Indicates site where marine fossils were located.

Area of many large boulders

*NOTE: Wetland symbols followed by "T" indicate areas where peat deposits probably do not constitute a significant commercial resource, either because they are thin (< 1.5 m), or they have an ash content greater than 25 percent. Symbols followed by "P" indicate peat deposits that are thicker (generally > 1.5 m), with ash content less than 25 percent, and thus may be suitable for commercial applications.

Artificial fill - Artificially emplaced materials of nearly any composition, man-made or natural, areas filled may be either man-made or natural, depressions, includes dumps, landfills and areas where the surface has been so altered by construction that the natural landscape has been obliterated - such as in city centers. Thickness variable.

Stream alluvium - Fine sand, silt, and clay, with some gravel and organic matter in places. Deposited in flood plains of modern streams. Extent of alluvium approximates area of potential flooding. Thickness of deposits variable. In places merges with wetlands deposits.

Landslide - Recently slumped clay-silt deposits of the Presumpscot Formation on the banks of Moors Brook where the bank is a nearly vertical cliff about 15-20 feet high; each landslide is bounded by an arcuate fault scarp about 100 feet long, and extends a maximum of about 30 to 50 feet into the cliff; the toe of each landslide is being swiftly eroded by the brook. Three such landslides were found.

Wetland, swamp* - Peat, silt, clay, and sand. Poorly drained area with variable tree cover, often with standing water. Thickness variable.

Wetland, freshwater marsh* - Peat, silt, clay, and sand. Poorly drained freshwater grassland, often with standing water and cattails. Thickness variable.

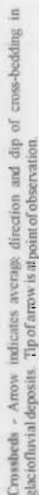
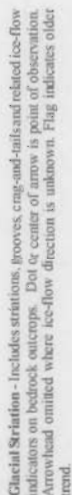
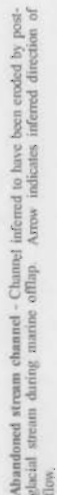
Wetland, salt marsh* - Peat, silt, clay, and sand. Coastal marsh subject to tidal flooding and containing salt marsh grasses, 0.5 to 2m thick, where 1 m or more thick, bottom part commonly peat rich.

Marine shoreline deposit (beach) - Sand and/or gravel, and minor silt. Developed along the present coast, 0.5 to 5 m thick. May include sand dunes in places.

Sand dunes - Sand with minor silt and gravel in places. Developed primarily along the present shoreline as part of barrier beach complexes, but two small deposits were found inland, 0.5 to 5 m thick.

Marine nearshore deposits - Thin, discontinuous deposits of sand, gravel, silt, clay, and reworked till overlying bedrock and till. Formed in shallow marine waters where glacial sediments were reworked by ocean waves and currents during regressive phase of late-glacial marine submergence. Average thickness probably less than 2 m. Subdivided into units 1 and 2 on the basis of elevation [Pm1 is above the 120-foot sea level stand of unit Pms2, and Pm2 is below that level.]

Marine shoreline deposits - Predominantly sand and gravel. Consists of beach deposits formed during stillstands of relative sea level in regressive phase of marine submergence. Thickness variable, less than 3 m to more than 10 m. Pms1 represents deposits that accumulated at stands of 160+ and 140+ ft, combined Pms2, a stand of 120- ft. Pms3, combined stands of 80+ and 60+ ft, and Pms4 (mapped only in the Biddeford Pool quad), a sea-level stand of 40- ft.



W.F. Reid Jr.

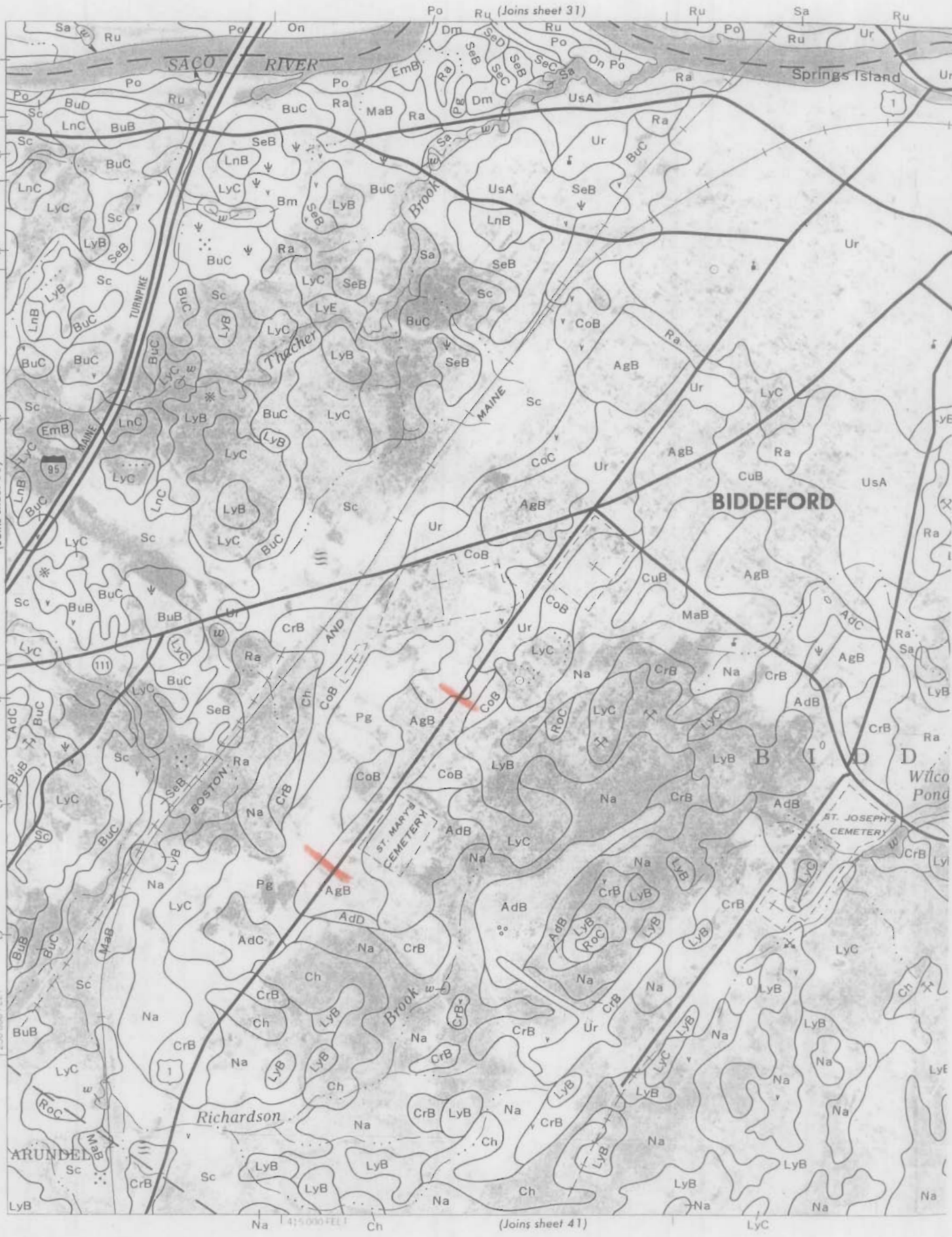
RAC -

SOIL SURVEY OF

York County Maine



United States Department of Agriculture, Soil Conservation Service
in cooperation with the Maine Agricultural Experiment Station
and the Maine Soil and Water Conservation Commission



(Joins sheet 35)

(Joins sheet 41)

BIDDEFORD

Richardson

ARUNDEL

ST. JOSEPH'S CEMETERY

ST. MARY'S CEMETERY

Wilcox Pond

Na 1 45000 FEET

Although this soil is mostly wooded, droughtiness and very low natural fertility limit productivity. Machinery operation on this soil is difficult because of the steep slopes. Logging roads and skid trails that are constructed on the contour help to reduce erosion.

The steep slopes make this soil poorly suited for most urban uses. The hazard of erosion at construction sites makes it necessary that removal of vegetation be held to a minimum and that a temporary plant cover be established as soon as possible. The rapid permeability of the soil causes a hazard of ground-water contamination from septic disposal systems. This soil is used as a source of poorly graded sand.

The capability subclass is VII_s.

AgB—Adams-Urban land complex, 0 to 8 percent slopes. This complex consists of areas of nearly level and gently sloping, excessively drained Adams soils and urbanized areas generally on plains and deltas. Much of the acreage of the Adams soils has been altered by grading for streets, housing, commercial buildings, and similar uses. Areas of the complex range from 10 to 200 acres. The complex consists of about 50 percent Adams soils, 40 percent urbanized areas, and 10 percent included soils. The soils and urban areas are in such an intricate pattern that it was not practical to map them separately.

Typically, undisturbed areas of the Adams soils have a surface layer of very dark grayish brown loamy sand about 7 inches thick. The subsoil is 11 inches thick. It is brown to dark brown loamy sand in the upper part and yellowish brown sand in the lower part. The substratum is light yellowish brown sand and coarse sand to a depth of 60 inches or more.

Included with this complex in mapping are small areas of Colton and Croghan soils. Also included are small areas of Adams soils with slopes of 8 to 15 percent.

The Adams soils in this complex have rapid or very rapid permeability. Surface runoff on the Adams soils is slow.

Most undisturbed areas of this complex consist of Adams soils between streets, houses, apartment buildings, or commercial buildings and in yards and playgrounds. The areas are generally less than 3 acres.

The Adams soils are well suited as a site for houses and commercial buildings. Ponding on the surface late in the winter is a concern in the nearly level areas. The Adams soils are poorly suited for grasses, trees, shrubs, and vegetable gardens because of their sandy texture and droughtiness.

An onsite investigation is needed to determine the suitability of this complex for any proposed use.

The unit is not assigned to a capability subclass.

AIB—Allagash very fine sandy loam, 3 to 8 percent slopes. This soil is gently sloping, well drained, and

deep. It is generally on the tops of plains and terraces. Slopes are less than 400 feet long. Most areas of this soil are oval and range from 3 to 40 acres.

Typically, the surface layer is brown to dark brown very fine sandy loam 7 inches thick. The subsoil is 13 inches thick. The upper part is yellowish brown very fine sandy loam, and the lower part is brownish yellow and light olive brown fine sandy loam. The substratum is stratified light yellowish brown loamy fine sand and light olive brown sand to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Colton and Madawaska soils. Also included are small areas of Allagash soils with slopes of less than 3 percent. Included areas make up about 10 to 15 percent of this unit.

This Allagash soil has moderately rapid permeability to a depth of about 20 inches and rapid permeability at a depth of more than 20 inches. Surface runoff is medium. The available water capacity is moderate, and the natural fertility is low. The depth to bedrock is generally 5 feet or more. Unless limed, the surface layer is very strongly acid.

Most areas of this soil are used for cultivated crops. Some areas are wooded.

This soil is suited to cultivated crops such as corn. Controlling erosion and providing irrigation are major management concerns. Maintaining the organic matter content of the soil will help to improve tilth, increase available water capacity, and reduce runoff.

The soil is suited to pasture, but prevention of overgrazing during dry periods, the timely application of fertilizer and lime, and pasture rotation are major management needs.

This soil is suited to woodland. The available moisture and rooting depth of the soil are generally adequate for trees.

The soil is generally suitable as a site for housing and septic tank disposal. Contamination of ground water, however, is a hazard caused by the rapid permeability in the substratum.

The capability subclass is II_e.

AIC—Allagash very fine sandy loam, 8 to 15 percent slopes. This soil is sloping, well drained, and deep. It is generally on the sides of plains and terraces. Slopes are less than 200 feet long. Most areas of this soil are elongated or oval and range from 3 to 15 acres.

Typically, the surface layer is brown to dark brown very fine sandy loam 7 inches thick. The subsoil is 13 inches thick. The upper part is yellowish brown very fine sandy loam, and the lower part is brownish yellow and light olive brown fine sandy loam. The substratum is stratified light yellowish brown loamy fine sand and light olive brown sand to a depth of 60 inches or more.

Included with this soil in mapping are small areas of Colton soils and small areas of Allagash soils with

TABLE 14.--ENGINEERING INDEX PROPERTIES AND CLASSIFICATIONS

[The symbol < means less than; > means more than. Absence of an entry indicates that data were not estimated.
NP = nonplastic]

Soil name and map symbol	Depth	USDA texture	Classification		Frag-ments > 3 inches	Percentage passing sieve number--				Liquid limit	Plas-ticity index
			Unified	AASHTO		4	10	40	200		
	In				Pct					Pct	
AdB, AdC, AdD----- Adams	0-3	Loamy sand-----	SM, SP-SM	A-1, A-2, A-3, A-4	0	95-100	95-100	45-85	5-40	---	NP
	3-18	Loamy sand, sand, loamy fine sand.	SM, SP-SM	A-1, A-2, A-3, A-4	0	95-100	95-100	35-95	5-40	---	NP
	18-60	Sand, coarse sand.	SP-SM, SW-SM, SP	A-1, A-2, A-3	0-1	90-100	70-100	20-90	0-10	---	NP
AgB*: Adams-----	0-3	Loamy sand-----	SM, SP-SM	A-1, A-2, A-3, A-4	0	95-100	95-100	45-85	5-40	---	NP
	3-18	Loamy sand, sand, loamy fine sand.	SM, SP-SM	A-1, A-2, A-3, A-4	0	95-100	95-100	35-95	5-40	---	NP
	18-60	Sand, coarse sand.	SP-SM, SW-SM, SP	A-1, A-2, A-3	0-1	90-100	70-100	20-90	0-10	---	NP
Urban land.											
AlB, AlC----- Allagash	0-7	Very fine sandy loam.	SM, ML	A-4, A-5	0	95-100	95-100	65-100	40-90	<44	NP-9
	7-20	Fine sandy loam, loam.	SM, ML	A-2, A-4	0	95-100	75-100	50-95	30-75	---	NP
	20-38	Fine sand, loamy fine sand, sand.	SM, SP-SM	A-2, A-1, A-3	0	85-100	75-100	35-80	5-35	---	NP
	38-60	Stratified loamy fine sand to very gravelly sand.	SP, SM, SW	A-1, A-2, A-3	0-10	70-100	25-100	10-75	0-30	---	NP
Ba*. Beaches											
BcB, BcC, BcD----- Becket	0-6	Fine sandy loam	SM	A-2, A-4	0-15	85-95	55-90	35-75	20-50	---	---
	6-23	Fine sandy loam, sandy loam, gravelly sandy loam.	SM	A-2, A-4	5-15	70-90	60-85	50-75	25-40	---	---
	23-60	Gravelly loamy sand, gravelly loamy fine sand, gravelly sandy loam.	SM, SP-SM, GM, GP-GM	A-2	5-15	60-85	55-75	25-70	10-30	---	---

See footnote at end of table.

TABLE 15.--PHYSICAL AND CHEMICAL PROPERTIES OF SOILS

[The symbol < means less than; > means more than. Entries under "Erosion factors--T" apply to the entire profile. Entries under "Organic matter" apply only to the surface layer. Absence of an entry indicates that data were not available or were not estimated]

Soil name and map symbol	Depth	Clay <2mm		Moist bulk density G/cm ³	Permeability In/hr	Available water capacity In/in	Soil reaction pH	Shrink-swell potential	Erosion factors		Organic matter Pct
		In	Pct						K	T	
AdB, AdC, AdD Adams	0-3	0-5	1.10-1.40	6.0-20	0.05-0.10	4.5-5.5	Low-----	0.17	5	1-4	
	3-18	0-5	1.25-1.55	6.0-20	0.04-0.08	4.5-5.5	Low-----	0.17			
	18-60	0-5	1.45-1.65	>20	0.03-0.04	4.5-6.0	Low-----	0.17			
AgB*: Adams	0-3	0-5	1.10-1.40	6.0-20	0.05-0.10	4.5-5.5	Low-----	0.17	5	1-4	
	3-18	0-5	1.25-1.55	6.0-20	0.04-0.08	4.5-5.5	Low-----	0.17			
	18-60	0-5	1.45-1.65	>20	0.03-0.04	4.5-6.0	Low-----	0.17			
Urban land.											
AlB, AlC Allagash	0-7	3-13	0.95-1.25	2.0-6.0	0.16-0.22	4.5-6.5	Low-----	0.28	3	2-8	
	7-20	2-12	1.20-1.50	2.0-6.0	0.08-0.24	4.5-6.5	Low-----	0.28			
	20-38	2-5	1.35-1.65	6.0-20	0.06-0.18	4.5-6.5	Low-----	0.28			
	38-60	1-4	1.40-1.70	6.0-20	0.01-0.10	4.5-6.5	Low-----	0.28			
Ba*. Beaches											
BcB, BcC, BcD Becket	0-6	3-8	0.90-1.20	0.6-2.0	0.10-0.23	4.5-6.5	Low-----	0.20	3	3-7	
	6-23	3-8	1.20-1.50	0.6-2.0	0.05-0.16	5.1-6.5	Low-----	0.28			
	23-60	1-4	1.65-1.80	0.06-0.6	0.03-0.09	5.1-6.5	Low-----	0.17			
BeB, BeC, BeD Becket	0-2	3-8	0.90-1.20	0.6-2.0	0.10-0.23	4.5-6.5	Low-----	0.20	3	---	
	2-23	3-8	1.20-1.50	0.6-2.0	0.05-0.16	5.0-6.5	Low-----	0.28			
	23-60	1-4	1.65-1.80	0.06-0.6	0.03-0.09	5.0-6.5	Low-----	0.17			
Bm Biddeford	14-0	---	0.10-0.30	2.0-6.0	0.20-0.43	5.1-6.5	-----	---	---	---	
	0-5	20-50	0.90-1.20	0.2-0.6	0.24-0.34	5.1-7.3	Low-----	---			
	5-36	35-55	1.60-1.80	<0.2	0.13-0.23	5.6-7.8	Moderate----	---			
	36-60	35-55	1.70-1.95	<0.2	0.06-0.16	6.1-7.8	Moderate----	---			
BrB*: Brayton	0-5	6-12	0.90-1.20	0.6-6.0	0.10-0.20	4.5-6.5	Low-----	0.28	3	2-8	
	5-11	6-12	1.40-1.70	0.6-6.0	0.08-0.17	4.5-6.5	Low-----	0.24			
	11-60	6-12	1.70-2.00	<0.2	0.01-0.05	5.6-7.3	Low-----	0.24			
Westbury	0-4	3-12	0.90-1.20	0.6-2.0	0.08-0.16	3.6-6.0	Low-----	0.24	3	2-8	
	4-23	3-12	1.40-1.70	0.6-2.0	0.07-0.15	3.6-6.0	Low-----	0.24			
	23-36	3-12	1.70-2.00	0.06-0.2	0.02-0.06	4.5-6.0	Low-----	0.24			
	36-60	3-12	1.70-2.00	0.06-0.2	0.02-0.06	5.1-7.3	Low-----	0.24			
BsB*: Brayton	0-5	6-12	0.90-1.20	0.6-6.0	0.08-0.17	4.5-6.5	Low-----	0.24	3	---	
	5-11	6-12	1.40-1.70	0.6-6.0	0.08-0.17	4.5-6.5	Low-----	0.24			
	11-60	6-12	1.70-2.00	<0.2	0.01-0.05	5.6-7.3	Low-----	0.24			
Westbury	0-4	3-12	0.90-1.20	0.6-2.0	0.08-0.16	3.6-6.0	Low-----	0.24	3	2-8	
	4-23	3-12	1.40-1.70	0.6-2.0	0.07-0.15	3.6-6.0	Low-----	0.24			
	23-36	3-12	1.70-2.00	0.06-0.2	0.02-0.06	4.5-6.0	Low-----	0.24			
	36-60	3-12	1.70-2.00	0.06-0.2	0.02-0.06	5.1-7.3	Low-----	0.24			
BuB, BuC, BuD Buxton	0-7	15-30	0.90-1.20	0.2-2.0	0.18-0.28	4.5-6.5	Low-----	0.28	3	4-7	
	7-19	20-40	1.20-1.55	0.2-0.6	0.13-0.23	4.5-6.5	Low-----	0.49			
	19-60	35-55	1.75-1.95	<0.2	0.06-0.16	5.6-7.3	Moderate----	0.49			
Ch Chocorua	0-32	---	<0.30	0.6-6.0	0.20-0.25	3.6-4.5	-----	---	---	---	
	32-60	---	<0.30	>6.0	0.01-0.11	4.5-6.0	-----	---	---	---	

See footnote at end of table.

TABLE 16.--SOIL AND WATER FEATURES

[The definitions of "flooding" and "water table" in the Glossary explain terms such as "rare," "brief," "apparent," and "perched." The symbol < means less than; > means more than. Absence of an entry indicates that the feature is not a concern]

Soil name and map symbol	Hydrologic group	Flooding			High water table			Bedrock		Risk of corrosion	
		Frequency	Duration	Months	Depth	Kind	Months	Depth	Potential frost action	Uncoated steel	Concrete
AdB, AdC, AdD----- Adams	A	None-----	---	---	Fe >6.0	---	---	In >60	Low-----	Low-----	High.
AgB*: Adams----- Urban land.	A	None-----	---	---	>6.0	---	---	>60	Low-----	Low-----	High.
AlB, AlC----- Allagash	B	None-----	---	---	>6.0	---	---	>60	Low-----	Low-----	High.
Ba*: Beaches											
BcB, BcC, BcD----- Becket	C	None-----	---	---	2.0-3.0	Perched	Nov-Mar	>60	Moderate---	Low-----	Moderate.
BeB, BeC, BeD----- Becket	C	None-----	---	---	2.0-3.0	Perched	Nov-Mar	>60	Moderate---	Low-----	Moderate.
Bm----- Biddeford	D	None-----	---	---	+1-0.5	Perched	Nov-Aug	>60	High-----	High-----	Moderate.
BrB*: Brayton-----	C	None-----	---	---	0.0-1.5	Perched	Nov-May	>60	High-----	High-----	Moderate.
Westbury-----	C	None-----	---	---	0.5-1.5	Perched	Nov-May	>60	High-----	Moderate	High.
BsB*: Brayton-----	C	None-----	---	---	0.0-1.5	Perched	Nov-May	>60	High-----	High-----	Moderate.
Westbury-----	C	None-----	---	---	0.5-1.5	Perched	Nov-May	>60	High-----	Moderate	High.
BuB, BuC, BuD----- Buxton	C	None-----	---	---	1.0-3.0	Perched	Nov-May	>60	High-----	High-----	Moderate.
Ch----- Chocorua	D	Common-----	Very long	Nov-May	0-0.5	Apparent	Jan-Dec	>60	High-----	Moderate	High.
CoB, CoC, CoD, CoE----- Colton	A	None-----	---	---	>6.0	---	---	>60	Low-----	Low-----	High.
CrB----- Croghan	B	None-----	---	---	1.5-2.0	Apparent	Nov-May	>60	Moderate---	Low-----	High.
CuB*: Croghan----- Urban land.	B	None-----	---	---	1.5-2.0	Apparent	Nov-May	>60	Moderate---	Low-----	High.

See footnote at end of table.

TABLE 10.--BUILDING SITE DEVELOPMENT

[Some terms that describe restrictive soil features are defined in the Glossary. See text for definitions of "slight," "moderate," and "severe." Absence of an entry indicates that the soil was not rated]

Soil name and map symbol	Shallow excavations	Dwellings without basements	Dwellings with basements	Small commercial buildings	Local roads and streets	Lawns and landscaping
AdB----- Adams	Severe: outbanks cave.	Slight-----	Slight-----	Moderate: slope.	Slight-----	Severe: droughty, too sandy.
AdC----- Adams	Severe: outbanks cave.	Moderate: slope.	Moderate: slope.	Severe: slope.	Moderate: slope.	Severe: droughty, too sandy.
AdD----- Adams	Severe: slope, outbanks cave.	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope, droughty, too sandy.
AgB*: Adams	Severe: outbanks cave.	Slight-----	Slight-----	Moderate: slope.	Slight-----	Severe: droughty, too sandy.
Urban land.						
AlB----- Allagash	Severe: outbanks cave.	Slight-----	Slight-----	Moderate: slope.	Slight-----	Slight.
AlC----- Allagash	Severe: outbanks cave.	Moderate: slope.	Moderate: slope.	Severe: slope.	Moderate: slope.	Moderate: slope.
Ba*. Beaches						
BoB----- Becket	Moderate: wetness.	Moderate: frost action, wetness.	Moderate: wetness.	Moderate: frost action, slope.	Moderate: frost action.	Moderate: small stones.
BoC----- Becket	Moderate: wetness, slope.	Moderate: frost action, slope.	Moderate: wetness, slope.	Severe: slope.	Moderate: frost action, slope.	Moderate: small stones, slope.
BoD----- Becket	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.
BeB----- Becket	Moderate: large stones, wetness.	Moderate: frost action, wetness.	Moderate: large stones, wetness.	Moderate: frost action, slope.	Moderate: frost action.	Moderate: large stones.
BeC----- Becket	Moderate: large stones, slope.	Moderate: frost action, slope.	Moderate: large stones, slope.	Severe: slope.	Moderate: frost action, slope.	Moderate: large stones, slope.
BeD----- Becket	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.	Severe: slope.
Bm----- Biddeford	Severe: wetness, too clayey.	Severe: wetness, low strength.	Severe: wetness, low strength.	Severe: wetness, low strength.	Severe: wetness, low strength.	Severe: wetness, excess humus.
BrB*: Brayton	Severe: wetness.	Severe: wetness, frost action.	Severe: wetness.	Severe: wetness, frost action.	Severe: wetness, frost action.	Moderate: wetness.
Westbury-----	Severe: wetness.	Severe: wetness, frost action.	Severe: wetness.	Severe: wetness, frost action.	Severe: frost action, wetness.	Moderate: wetness.

See footnote at end of table.

TABLE 12.--CONSTRUCTION MATERIALS

[Some terms that describe restrictive soil features are defined in the Glossary. See text for definitions of "good," "fair," and "poor." Absence of an entry indicates that the soil was not rated]

Soil name and map symbol	Roadfill	Sand	Gravel	Topsoil
AdB, AdC----- Adams	Good-----	Good-----	Unsuited: excess fines.	Poor: too sandy.
AdD----- Adams	Fair: slope.	Good-----	Unsuited: excess fines.	Poor: slope, too sandy.
AgB*: Adams----- Urban land.	Good-----	Good-----	Unsuited: excess fines.	Poor: too sandy.
AlB----- Allagash	Good-----	Good-----	Unsuited: excess fines.	Good.
AlC----- Allagash	Good-----	Good-----	Unsuited: excess fines.	Fair: slope.
Ba*. Beaches				
BcB, BcC----- Becket	Fair: frost action.	Poor: excess fines.	Poor: excess fines.	Poor: small stones.
BcD----- Becket	Fair: frost action, slope.	Poor: excess fines.	Poor: excess fines.	Poor: slope, small stones.
BeB, BeC----- Becket	Fair: frost action.	Poor: excess fines.	Poor: excess fines.	Poor: large stones.
BeD----- Becket	Fair: slope, frost action.	Poor: excess fines.	Poor: excess fines.	Poor: large stones, slope.
Bm----- Biddeford	Poor: wetness, low strength.	Unsuited: excess fines.	Unsuited: excess fines.	Poor: wetness, thin layer, too clayey.
BrB*: Brayton----- Westbury-----	Poor: wetness, frost action.	Unsuited: excess fines.	Unsuited: excess fines.	Poor: small stones, wetness.
	Poor: frost action.	Unsuited: excess fines.	Unsuited: excess fines.	Poor: small stones.
BsB*: Brayton----- Westbury-----	Poor: wetness, frost action.	Unsuited: excess fines.	Unsuited: excess fines.	Poor: large stones, wetness.
	Poor: frost action.	Unsuited: excess fines.	Unsuited: excess fines.	Poor: large stones.
BuB----- Buxton	Poor: frost action.	Unsuited: excess fines.	Unsuited: excess fines.	Fair: too clayey.
BuC----- Buxton	Poor: frost action.	Unsuited: excess fines.	Unsuited: excess fines.	Fair: slope, too clayey.

See footnote at end of table.

TABLE 14.--ENGINEERING INDEX PROPERTIES AND CLASSIFICATIONS--Continued

Soil name and map symbol	Depth In	USDA texture	Classification		Frag- ments > 3 inches Pct	Percentage passing sieve number--				Liquid limit Pct	Plas- ticity index
			Unified	AASHTO		4	10	40	200		
BsB*: Westbury-----	0-4	Very stony fine sandy loam.	SM, ML, GM	A-2, A-4, A-1	5-10	55-80	50-75	30-75	15-70	<15	NP-4
	4-23	Gravelly loam, silt loam, gravelly sandy loam.	SM, GM, ML	A-2, A-4, A-1	0-5	55-95	50-90	30-90	15-80	<15	NP-4
	23-36	Gravelly sandy loam, very gravelly fine sandy loam, loam.	SM, GM, GW-GM, ML	A-1, A-2, A-4	0-5	40-90	35-85	20-80	10-65	<15	NP-4
	36-60	Gravelly sandy loam, very gravelly fine sandy loam, loam.	GM, GW-GM, SM, ML	A-1, A-2, A-4	0-5	40-90	35-85	20-80	10-65	<15	NP-4
BuB, BuC, BuD----- Buxton	0-7	Silt loam-----	ML, MH	A-4, A-6, A-7, A-5	0	98-100	95-100	95-100	85-100	36-55	5-20
	7-19	Silt loam, silty clay loam.	ML, CL, CL-ML	A-4, A-6, A-7, A-5	0	98-100	95-100	95-100	85-100	25-55	5-20
	19-60	Silty clay, silty clay loam, clay.	CL, CL-ML, ML	A-6, A-4	0	98-100	95-100	95-100	90-100	25-40	5-15
Ch----- Chocorua	0-32	Peat	Pt	A-8	0	---	---	---	---	---	---
	32-60	Gravelly sand, loamy sand, loamy fine sand.	SP, SM	A-1, A-3	0	100	60-100	30-80	0-30	---	NP
CoB, CoC, CoD, CoE----- Colton	0-10	Gravelly loamy coarse sand.	SM, SP, GW, GM	A-1, A-2, A-3	5-20	30-80	25-75	25-60	2-25	---	NP
	10-18	Gravelly loamy sand, very gravelly sand, cobbly sand.	SM, GM, SP, GP	A-1, A-2, A-3	5-20	30-80	25-75	20-50	2-20	---	NP
	18-60	Very gravelly sand, very cobbly sand.	GP, SP, GW, SW	A-1	10-45	20-55	15-50	10-30	0-5	---	NP
CrB----- Croghan	0-7	Loamy sand-----	SM, SP-SM, SW-SM	A-1, A-3, A-4, A-2	0	95-100	95-100	45-80	5-40	---	NP
	7-28	Sand, loamy sand, loamy fine sand.	SM, SP-SM, SW-SM	A-1, A-2, A-3, A-4	0	90-100	85-100	45-80	5-40	---	NP
	28-60	Sand, loamy sand	SM, SP-SM, SW-SM	A-1, A-2, A-3	0	90-100	85-100	45-75	5-30	---	NP

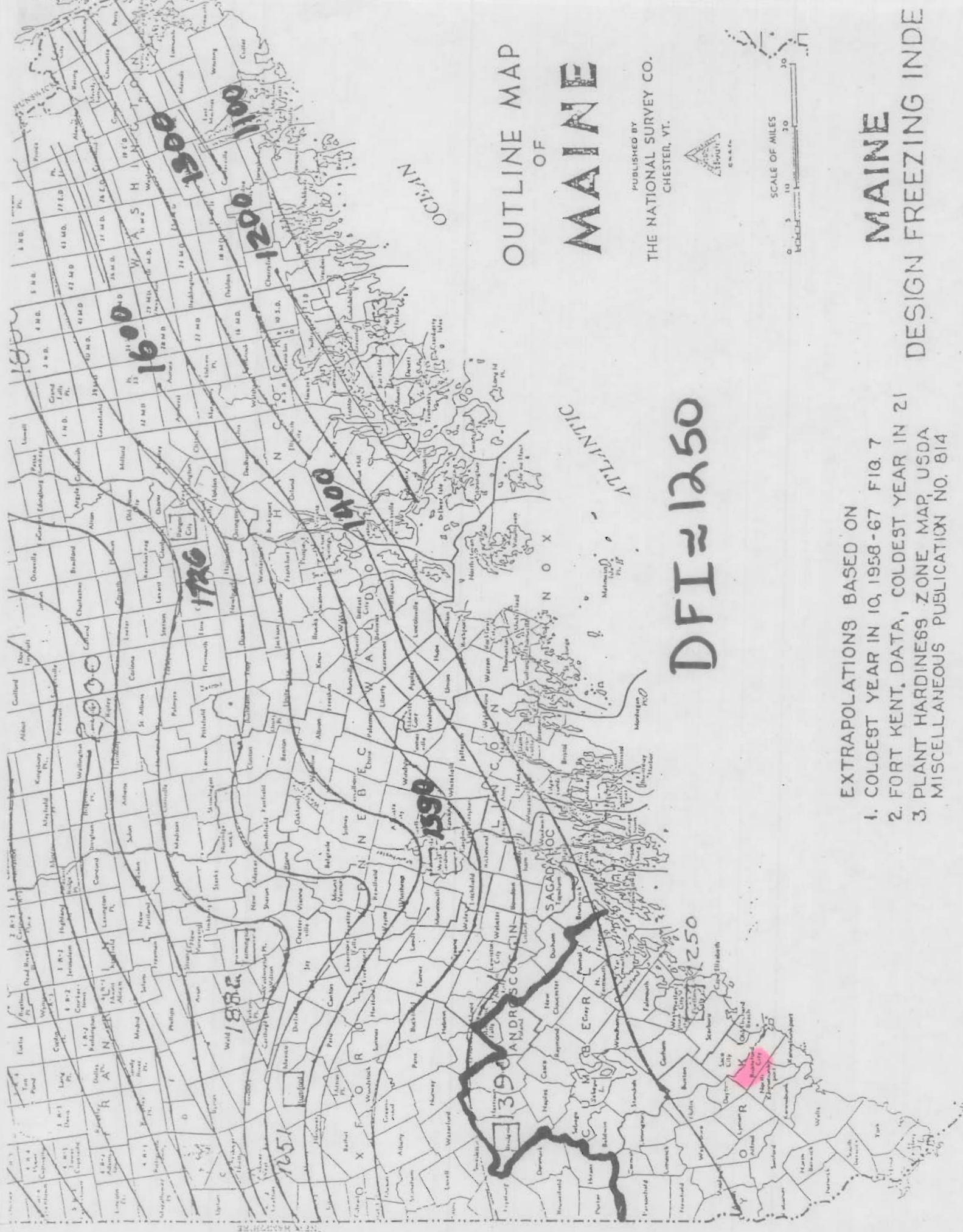
drainage area

See footnote at end of table.

TABLE 15.--PHYSICAL AND CHEMICAL PROPERTIES OF SOILS--Continued

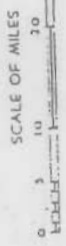
Soil name and map symbol	Depth	Clay <2mm	Moist bulk density	Permeability	Available water capacity	Soil reaction	Shrink-swell potential	Erosion factors		Organic matter
								K	T	
	In	Pct	G/cm ³	In/hr	In/in	pH			Pct	
CoB, CoC, CoD, CoE Colton	0-10 10-18 18-60	1-5 1-5 0-3	1.10-1.40 1.25-1.55 1.45-1.65	>6.0 >6.0 >20	0.03-0.07 0.02-0.05 0.01-0.02	3.6-5.0 4.5-5.5 4.5-6.0	Low----- Low----- Low-----	0.17 0.17 0.17	3	3-7
<i>drainage area</i> CrB Croghan	0-7 7-28 28-60	0-5 0-5 0-5	1.20-1.50 1.20-1.50 1.20-1.50	6.0-20 >20 >20	0.05-0.09 0.03-0.07 0.03-0.06	4.5-6.0 4.5-6.0 4.5-6.0	Low----- Low----- Low-----	0.17 0.17 0.17	5	2-9
CuB* Croghan	0-7 7-28 28-60	0-5 0-5 0-5	1.20-1.50 1.20-1.50 1.20-1.50	6.0-20 >20 >20	0.05-0.09 0.03-0.07 0.03-0.06	4.5-6.0 4.5-6.0 4.5-6.0	Low----- Low----- Low-----	0.17 0.17 0.17	5	---
Urban land.										
Dm* Dumps										
EmB, EmC Elmwood	0-14 14-20 20-60	5-10 5-12 35-55	1.00-1.30 1.15-1.45 1.50-1.80	2.0-6.0 2.0-6.0 <0.2	0.13-0.20 0.13-0.22 0.12-0.18	4.5-6.0 5.6-6.5 6.1-7.3	Low----- Low----- Moderate-----	0.32 0.32 0.49	3	3-7
HeB, HeC, HeD Hermon	0-6 6-19 19-60	2-6 2-7 1-4	0.95-1.20 1.00-1.30 1.50-1.80	6.0-20 6.0-20 6.0-20	0.10-0.20 0.07-0.14 0.01-0.10	3.6-5.5 3.6-6.0 5.1-6.0	Low----- Low----- Low-----	0.17 0.17 0.17	3	3-7
HmB, HmC, HmD Hermon	0-4 4-19 19-60	2-6 2-7 1-4	0.95-1.20 1.00-1.30 1.50-1.80	6.0-20 6.0-20 6.0-20	0.10-0.20 0.07-0.14 0.01-0.10	3.6-5.5 3.6-6.0 5.1-6.0	Low----- Low----- Low-----	0.17 0.17 0.17	3	---
HnC, HnE Hermon	0-4 4-19 19-60	2-6 2-7 1-4	0.95-1.20 1.00-1.30 1.50-1.80	6.0-20 6.0-20 6.0-20	0.08-0.18 0.07-0.14 0.01-0.10	3.6-5.5 3.6-6.0 5.1-6.0	Low----- Low----- Low-----	0.17 0.17 0.17	3	---
LnB, LnC, LnD Lyman	0-4 4-18 18	2-10 2-10 ---	0.90-1.20 1.20-1.40 ---	2.0-6.0 2.0-6.0 ---	0.11-0.20 0.07-0.16 ---	3.6-6.0 3.6-6.0 ---	Low----- Low----- ---	0.20 0.20 ---	2	1-4
LyB*, LyC*, LyE* Lyman	0-4 4-18 18	2-10 2-10 ---	0.90-1.20 1.20-1.40 ---	2.0-6.0 2.0-6.0 ---	0.11-0.20 0.07-0.16 ---	3.6-6.0 3.6-6.0 ---	Low----- Low----- ---	0.20 0.20 ---	2	1-4
Rock outcrop.										
MaB Madawaska	0-10 10-23 23-60	3-13 2-12 0-5	0.95-1.25 1.20-1.50 1.35-1.65	2.0-6.0 2.0-6.0 6.0-20	0.11-0.25 0.09-0.18 0.02-0.08	4.5-6.0 4.5-6.0 4.5-6.0	Low----- Low----- Low-----	0.28 0.28 0.28	3	3-9
MrB, MrC2, MrD2 Marlow	0-9 9-29 29-60	5-12 5-12 5-12	0.90-1.20 1.20-1.50 1.70-2.00	0.6-6.0 0.6-6.0 0.06-0.6	0.10-0.23 0.06-0.20 0.05-0.12	4.5-6.0 4.5-6.0 4.5-6.0	Low----- Low----- Low-----	0.24 0.43 0.17	3	3-8
MvB, MvC, MvD Marlow	0-2 2-29 29-60	5-12 5-12 5-12	0.90-1.20 1.20-1.50 1.70-2.00	0.6-6.0 0.6-6.0 0.06-6.0	0.10-0.23 0.06-0.20 0.05-0.12	4.5-6.0 4.5-6.0 4.5-6.0	Low----- Low----- Low-----	0.24 0.43 0.17	3	---
Na Naumburg	0-5 5-28 28-60	0-5 0-5 0-5	1.10-1.40 1.25-1.55 1.45-1.65	2.0-6.0 6.0-20 6.0-20	0.05-0.09 0.06-0.08 0.04-0.06	3.6-5.5 3.6-5.5 4.5-6.5	Low----- Low----- Low-----	0.17 0.17 0.17	5	2-7
On Ondawa	0-9 9-30 30-60	0-10 0-10 0-5	1.10-1.40 1.20-1.50 1.20-1.50	2.0-6.0 2.0-6.0 2.0-20	0.12-0.26 0.12-0.22 0.01-0.13	4.5-6.5 4.5-6.5 4.5-6.5	Low----- Low----- Low-----	---	---	3-7

See footnote at end of table.



OUTLINE MAP
OF
MAINE

PUBLISHED BY
THE NATIONAL SURVEY CO.
CHESTER, VT.



MAINE
DESIGN FREEZING INDE

DFI ≈ 1250

- EXTRAPOLATIONS BASED ON
1. COLDEST YEAR IN 10, 1958-67 FIG. 7
 2. FORT KENT, DATA, COLDEST YEAR IN 21
 3. PLANT HARDINESS ZONE MAP, USDA MISCELLANEOUS PUBLICATION NO. 814

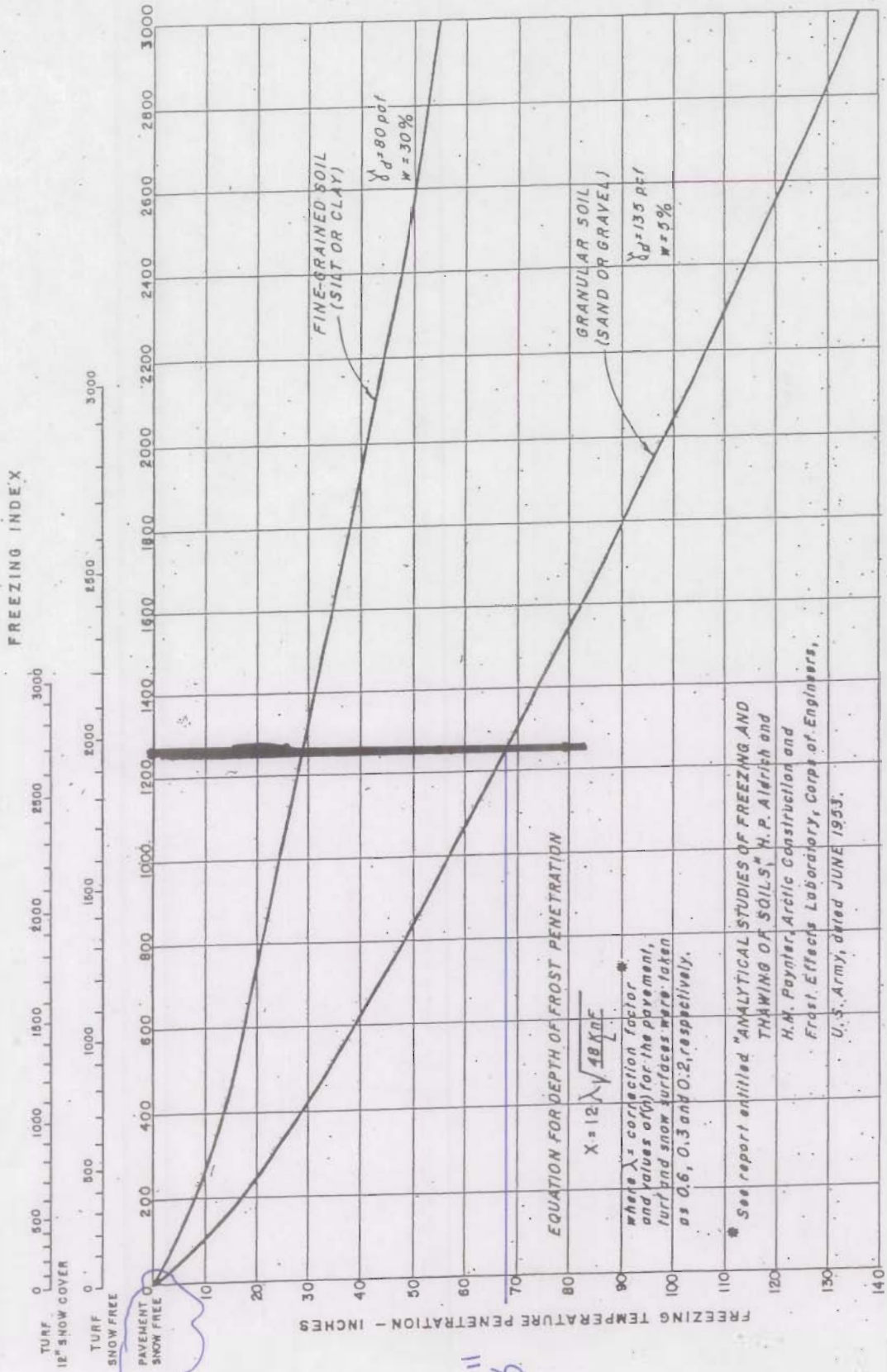


Figure 13-3 RELATIONSHIP BETWEEN FREEZING INDEX AND FREEZING TEMPERATURE PENETRATION FOR VARIOUS SURFACE CONDITIONS FOR GRANULAR AND FINE-GRAINED SOILS.

66

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 63+13, 6.4 Lt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf)
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.	
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows						
0									-0.30		PAVEMENT.		
	S1		1.10 - 3.00						-0.90		CONCRETE.		
									-1.10		Brown, damp, fine to medium SAND, some gravel.	G#207234 A-2-4, SM WC=13.7%	
	S2		3.00 - 5.00						-3.00		Dark brown, moist, fine to medium SAND some silt, trace gravel.		
5									-5.00		Gold, damp, fine to medium SAND, little gravel, trace silt.	G#207235 A-1-b, SP-SM WC=4.6	
25													

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 56+23, 4.1 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf)
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

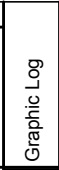
Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	C1		0.00 - 0.40						-0.40		PAVEMENT, (Core sample taken).	
	C1		0.40 - 0.90						-0.90		CONCRETE, (Core sample taken).	
	S3		0.90 - 5.00						-0.90		Light brown, damp, fine to medium SAND, little silt, little gravel.	G#207236 A-1-b, SM WC=4.2%
5									-5.00		Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL	
10												
15												
20												
25												

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 52+84, 4.1 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	S4		0.90 - 5.00						-0.35 -0.90	 PAVEMENT. CONCRETE. Brown, damp, fine to coarse SAND, some silt, little gravel.	G#207237 A-1-b, SM WC=6.2%	
5									-5.00	 Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL		
10												
15												
20												
25												

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 50+96, 4.2 Lt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf)
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	S5		0.80 - 2.20						-0.40		PAVEMENT.	G#207238 A-2-4, SM WC=6.0% G#207239 A-2-4, SM WC=21.5%
									-0.80		CONCRETE.	
	S6		2.20 - 5.00						-2.20		Brown, damp, fine to coarse SAND, some silt, little gravel.	
									-5.00		Brown, moist, fine to medium SAND, some silt, trace gravel.	
5									-5.00	Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL		
10												
15												
20												
25												

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 48+08, 4.8 Lt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test


Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	S7		0.85 - 5.00					SSA	-0.40 -0.85			
5									-5.00	<p style="text-align: center;">Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL</p>		
10												
15												
20												
25												

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 46+38, 6.4 Lt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf)
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	S8		0.90 - 5.00						-0.50 -0.90	 PAVEMENT. CONCRETE. Brown, damp, fine to coarse SAND, little silt, little gravel.	G#207240 A-1-b, SM WC=8.4%	
5								-5.00	Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL			
10												
15												
20												
25												

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.):	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 43+52, 12.4 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: _____ **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0	C2		0.00 - 0.45						-0.45		PAVEMENT, (Core sample taken).	
	C2		0.45 - 1.00						-1.00		CONCRETE, (Core sample taken).	
	S9		1.00 - 5.00						-1.00		Light brown, damp, fine to medium SAND, little gravel, little silt.	G#207241 A-2-4, SM WC=4.1%
5									-5.00		Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL	
10												
15												
20												
25												

Remarks:
Offsets are from Existing Roadway CL.

Driller: MaineDOT	Elevation (ft.): 168.7	Auger ID/OD: 5" Dia.
Operator: E. Giguere/C. Giles	Datum: NAVD 88	Sampler: Off Flights
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: N/A
Date Start/Finish: 5/8/08-5/8/08	Drilling Method: Solid Stem Auger	Core Barrel: N/A
Boring Location: 40+33, 4.5 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample attempt U = Thin Wall Tube Sample R = Rock Core Sample V = Insitu Vane Shear Test SSA = Solid Stem Auger	Definitions: S _u = Insitu Field Vane Shear Strength (psf) T _v = Pocket Torvane Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) S _u (lab) = Lab Vane Shear Strength (psf) WOH = weight of 140lb. hammer WOR = weight of rods. WOC = weight of casing	Definitions: WC = water content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test
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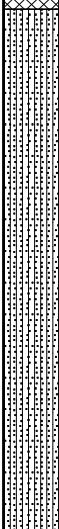
Sample Information										Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-value	Casing Blows	Elevation (ft.)	Graphic Log			
0						SSA	168.25		PAVEMENT.	-0.45	
	S10		1.00 - 5.00				167.70		CONCRETE.	-1.00	
									Light brown, damp, fine to medium SAND, little gravel, little silt.		
5						↓	163.70		Bottom of Exploration at 5.00 feet below ground surface. NO REFUSAL	-5.00	
10											
15											
20											
25											

Remarks:
 Offsets are from Existing Roadway CL.

Driller: Northern Test Boring	Elevation (ft.): 165.0	Auger ID/OD: 2 3/4" / 6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 09:30-10:30	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 50+79.3, 201.7 Rt.	Casing ID/OD: N/A	Water Level*: 28.2 ft bgs.

Hammer Efficiency Factor: 0.678 Hammer Type: Automatic Hydraulic Rope & Cathead

Definitions:
D = Split Spoon Sample R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
MD = Unsuccessful Split Spoon Sample attempt SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
U = Thin Wall Tube Sample HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
MV = Unsuccessful Insitu Vane Shear Test attempt WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0								HSA	164.70		TOPSOIL, (Sod). ————— 0.30	
5	MD	1.2/0	5.00 - 5.10	25(1.2")	---						Failed sample attempt. Cobble from 5.0-5.6 ft bgs.	
10	1D	24/10	10.00 - 12.00	4/3/2/3	5	6					Brown, moist, loose, fine to coarse SAND, some gravel, little silt, (Fill). ————— 14.00	G#239976 A-1-b, SW-SM WC=7.7%
15	2D	24/20	15.00 - 17.00	4/6/9/12	15	17					Brown, damp, medium dense, fine to medium SAND, trace silt, trace gravel, (Native Soil).	G#239977 A-3, SP WC=4.5%
20	3D	24/18	20.00 - 22.00	14/17/17/18	34	38				Similar to above.		
25												

Remarks:
Auto Hammer #283

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS	Project: Route 1, Detention Basin Location: Biddeford, Maine	Boring No.: HB-BIDD-201, B-1 PIN: 14814.00
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Driller: Northern Test Boring	Elevation (ft.): 165.0	Auger ID/OD: 2 1/4" / 6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 09:30-10:30	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 50+79.3, 201.7 Rt.	Casing ID/OD: N/A	Water Level*: 28.2 ft bgs.

Hammer Efficiency Factor: 0.678 **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample attempt V = Insitu Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Insitu Vane Shear Test attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = weight of 140lb. hammer WOR/C = weight of rods or casing WO1P = Weight of one person	S _u = Insitu Field Vane Shear Strength (psf) T _v = Pocket Torvane Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw field SPT N-value Hammer Efficiency Factor = Annual Calibration Value N ₆₀ = SPT N-uncorrected corrected for hammer efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected
		S _u (lab) = Lab Vane Shear Strength (psf) WC = water content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test

Sample Information										Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)				
25												
30	4D	18/18	30.00 - 31.50	20/21/22	43	49		135.00	30.00		Brown, wet, dense, fine to coarse SAND, some gravel, trace silt.	
								133.50	31.50	Bottom of Exploration at 31.50 feet below ground surface. NO REFUSAL		
35												
40												
45												
50												

Remarks:
Auto Hammer #283

Driller: Northern Test Boring	Elevation (ft.): 167.5	Auger ID/OD: 2 3/4"/6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 10:30-11:30	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 51+35, 220.4 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: 0.678 **Hammer Type:** Automatic Hydraulic Rope & Cathead

 Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
 D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
 MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
 U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
 MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
 V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
 MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.	
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows						
0								HSA	167.20		TOPSOIL, (Sod). ————— 0.30		
5													
10	1D	24/18	10.00 - 12.00	3/3/6/8	9	10					Olive-brown, wet, loose, SILT, some sand, trace gravel, (Fill).	G#239978 A-4, ML WC=25.2%	
15													
20	2D	24/18	20.00 - 22.00	4/31/45/9	76	86			147.00			Dark brown, wet, silty, fine to medium SAND, gravel, (Fill). ————— 20.50	
									146.00	Wood layer from 20.5-21.5 ft bgs. ————— 21.50			
25									144.50	————— 23.00			

Remarks:
Auto Hammer #283

Maine Department of Transportation Soil/Rock Exploration Log US CUSTOMARY UNITS	Project: Route 1, Detention Basin Location: Biddeford, Maine	Boring No.: HB-BIDD-202, B-2 PIN: 14814.00
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Driller: Northern Test Boring	Elevation (ft.): 167.5	Auger ID/OD: 2 3/4" / 6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 10:30-11:30	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 51+35, 220.4 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: 0.678 **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
 D = Split Spoon Sample SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
 MD = Unsuccessful Split Spoon Sample attempt HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
 U = Thin Wall Tube Sample RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
 MU = Unsuccessful Thin Wall Tube Sample attempt WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
 V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
 MV = Unsuccessful Insitu Vane Shear Test attempt WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
25	3D	24/16	25.00 - 27.00	11/12/16/19	28	32			140.50	Brown, damp, medium dense, fine to medium SAND, trace silt, trace gravel, (Native Soil). Bottom of Exploration at 27.00 feet below ground surface. NO REFUSAL	G#239980 A-3, SP-SM WC=3.9%	
30												
35												
40												
45												
50												

Remarks:
Auto Hammer #283

Driller: Northern Test Boring	Elevation (ft.): 167.4	Auger ID/OD: 2 3/4" / 6 3/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 12:00-13:00	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 51+79.8, 239.5 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: 0.678 Hammer Type: Automatic Hydraulic Rope & Cathead

Definitions:
D = Split Spoon Sample R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_u(lab) = Lab Vane Shear Strength (psf)
MD = Unsuccessful Split Spoon Sample attempt SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
U = Thin Wall Tube Sample HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
MV = Unsuccessful Insitu Vane Shear Test attempt WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%) * N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing	Blows				
0	1D	24/18	0.00 - 2.00	6/6/8/6	14	16	HSA			Brown, moist, medium dense, fine to coarse SAND, some silt, little gravel, (Fill).	G#239981 A-2-4, SM WC=12.5%	
5	2D	24/12	5.00 - 7.00	3/3/4/4	7	8		161.40		Olive-grey, loose, silty, fine to medium SAND, trace gravel, little clay, (Fill).		
10	3D	24/10	10.00 - 12.00	2/2/2/11	4	5		157.40		Olive-grey, wet, loose, silty, fine to medium SAND, old pavement, trace gravel, (Fill).		
15	4D	24/14	15.00 - 17.00	2/2/3/2	5	6		153.40		Olive, wet, loose, fine to coarse SAND, some silt, little gravel, (Fill).	G#239982 A-1-b, SM WC=14.1%	
20	5D	24/16	20.00 - 22.00	4/3/3/3	6	7		143.40		Similar to above.		
25												

Remarks:
Auto Hammer #283

Driller: Northern Test Boring	Elevation (ft.): 167.4	Auger ID/OD: 2 1/4" / 6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 12:00-13:00	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 51+79.8, 239.5 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: 0.678 **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions: D = Split Spoon Sample MD = Unsuccessful Split Spoon Sample attempt U = Thin Wall Tube Sample MU = Unsuccessful Thin Wall Tube Sample attempt V = Insitu Vane Shear Test, PP = Pocket Penetrometer MV = Unsuccessful Insitu Vane Shear Test attempt	R = Rock Core Sample SSA = Solid Stem Auger HSA = Hollow Stem Auger RC = Roller Cone WOH = weight of 140lb. hammer WOR/C = weight of rods or casing WO1P = Weight of one person	S _u = Insitu Field Vane Shear Strength (psf) T _v = Pocket Torvane Shear Strength (psf) q _p = Unconfined Compressive Strength (ksf) N-uncorrected = Raw field SPT N-value Hammer Efficiency Factor = Annual Calibration Value N ₆₀ = SPT N-uncorrected corrected for hammer efficiency N ₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected
		S _{u(lab)} = Lab Vane Shear Strength (psf) WC = water content, percent LL = Liquid Limit PL = Plastic Limit PI = Plasticity Index G = Grain Size Analysis C = Consolidation Test

Sample Information										Graphic Log	Visual Description and Remarks	Laboratory Testing Results/ AASHTO and Unified Class.
Depth (ft.)	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows	Elevation (ft.)				
25	6D	24/20	25.00 - 27.00	2/2/3/5	5	6		138.40	29.00	Grey-brown, wet, loose, sandy SILT, trace gravel, brick fragments, (Fill).	G#239983 A-4, SM WC=20.8%	
30	7D	24/20	30.00 - 32.00	13/18/25/27	43	49		135.40	32.00	Brown, wet, dense, fine to coarse SAND, trace gravel, trace silt.	G#239984 A-1-b, SP-SM WC=15.0%	
Bottom of Exploration at 32.00 feet below ground surface. NO REFUSAL												
35												
40												
45												
50												

Remarks:
Auto Hammer #283

Driller: Northern Test Boring	Elevation (ft.): 159.0	Auger ID/OD: 2 3/4" / 6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 13:30-14:30	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 50+74.5, 322.1 Rt.	Casing ID/OD: N/A	Water Level*: None Observed

Hammer Efficiency Factor: 0.678 Hammer Type: Automatic Hydraulic Rope & Cathead

Definitions:
D = Split Spoon Sample R = Rock Core Sample S_u = In situ Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
MD = Unsuccessful Split Spoon Sample attempt SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
U = Thin Wall Tube Sample HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
V = In situ Vane Shear Test, PP = Pocket Penetrometer WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
MV = Unsuccessful Insitu Vane Shear Test attempt WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (/6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing Blows					
0								HSA	158.70		TOPSOIL, (Sod). -0.30	G#239986 A-4, ML WC=24.8%
5	1D	24/15	5.00 - 7.00	3/2/4/3	6	7					Olive-brown, wet, loose, SILT, some sand, little gravel, granite fragments, (Fill).	
10	2D	24/10	10.00 - 12.00	2/3/4/3	7	8					Similar to above, (Fill).	
15	3D	24/10	15.00 - 17.00	4/3/4/40	7	8			141.90		Similar to above, (Fill).	
20											Bottom of Exploration at 17.10 feet below ground surface. BOULDER or GRANITE BLOCK REFUSAL -17.10	
25												

Remarks:
Auto Hammer #283

Driller: Northern Test Boring	Elevation (ft.): 142.5	Auger ID/OD: 2 3/4" / 6 1/4"
Operator: Mike/Mike	Datum: NAVD88	Sampler: Standard Split Spoon
Logged By: B. Wilder	Rig Type: CME 45C	Hammer Wt./Fall: 140#/30"
Date Start/Finish: 1/19/11; 14:30-15:30	Drilling Method: Hollow Stem Auger	Core Barrel: N/A
Boring Location: 50+60, 434.4 Rt.	Casing ID/OD: N/A	Water Level*: 8.8 ft bgs.

Hammer Efficiency Factor: 0.678 **Hammer Type:** Automatic Hydraulic Rope & Cathead

Definitions:
D = Split Spoon Sample R = Rock Core Sample S_u = Insitu Field Vane Shear Strength (psf) S_{u(lab)} = Lab Vane Shear Strength (psf)
MD = Unsuccessful Split Spoon Sample attempt SSA = Solid Stem Auger T_v = Pocket Torvane Shear Strength (psf) WC = water content, percent
U = Thin Wall Tube Sample HSA = Hollow Stem Auger q_p = Unconfined Compressive Strength (ksf) LL = Liquid Limit
MU = Unsuccessful Thin Wall Tube Sample attempt RC = Roller Cone N-uncorrected = Raw field SPT N-value PL = Plastic Limit
V = Insitu Vane Shear Test, PP = Pocket Penetrometer WOH = weight of 140lb. hammer Hammer Efficiency Factor = Annual Calibration Value PI = Plasticity Index
MV = Unsuccessful Insitu Vane Shear Test attempt WOR/C = weight of rods or casing N₆₀ = SPT N-uncorrected corrected for hammer efficiency G = Grain Size Analysis
WO1P = Weight of one person N₆₀ = (Hammer Efficiency Factor/60%)*N-uncorrected C = Consolidation Test

Depth (ft.)	Sample Information								Elevation (ft.)	Graphic Log	Visual Description and Remarks	Laboratory Testing Results/AASHTO and Unified Class.
	Sample No.	Pen./Rec. (in.)	Sample Depth (ft.)	Blows (6 in.) Shear Strength (psf) or RQD (%)	N-uncorrected	N ₆₀	Casing	Blows				
0	1D	24/12	0.00 - 2.00	7/12/40/39	52	59	HSA		140.00	Brown, damp, dense, fine to coarse SAND, some gravel, little silt.	G#239987 A-1-b, SM WC=7.2%	
5	2D	24/20	5.00 - 7.00	13/15/16/15	31	35				Light brown, damp, dense, fine to coarse SAND, little gravel, trace silt.	G#239988 A-1-b, SP-SM WC=3.7%	
10	3D	24/18	10.00 - 12.00	7/12/13/13	25	28			130.50	Similar to above, except medium dense.		
										Bottom of Exploration at 12.00 feet below ground surface. NO REFUSAL		

Remarks:
Auto Hammer #283

Pavement Core
Station 56+23, 4.1' R



Pavement Core
Station 43+52, 12.4' R

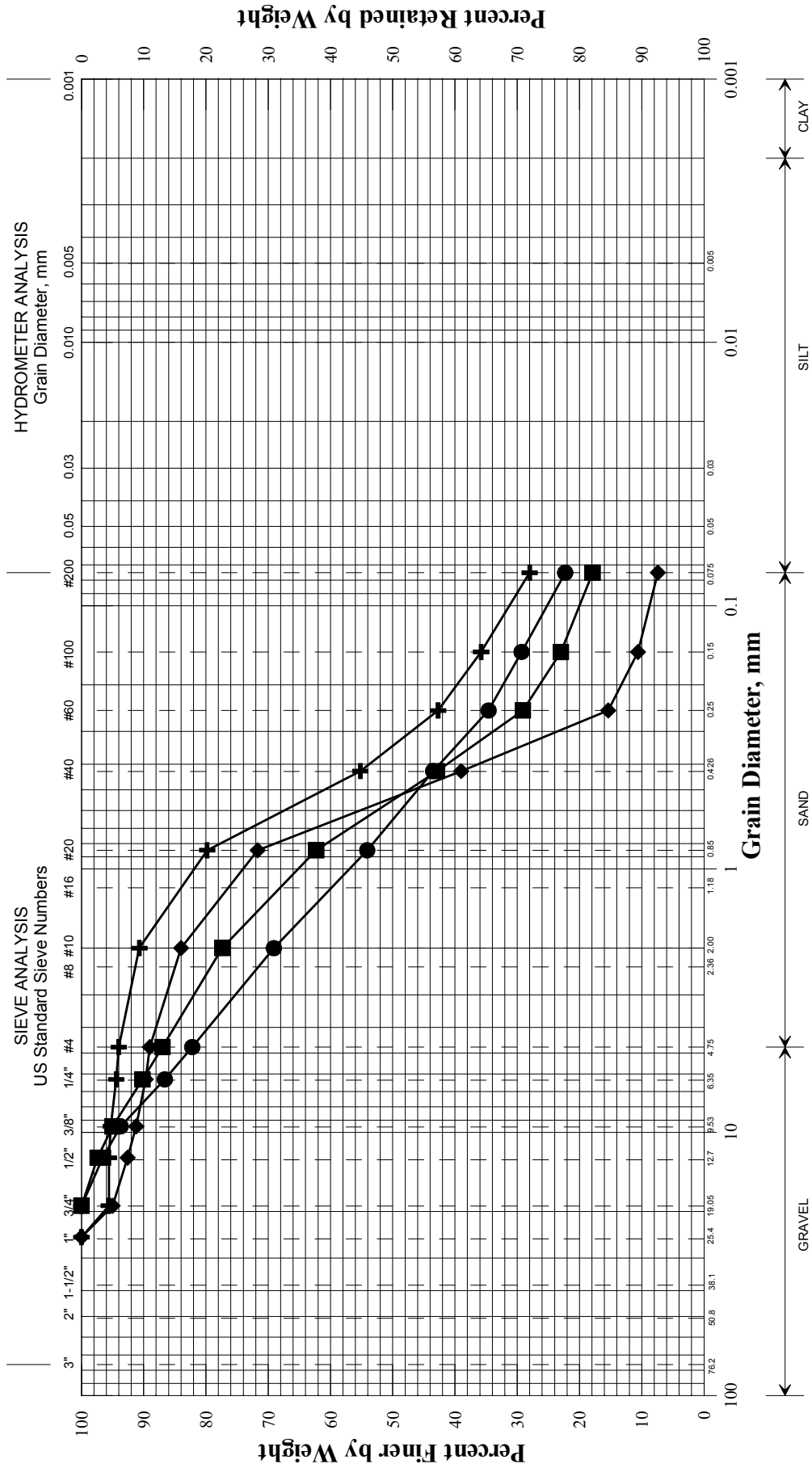


HB-Bidd-107
C2

Biddford, Rt 1 (Elm St)

PIN# 18414.00
6/12/08

State of Maine Department of Transportation
GRAIN SIZE DISTRIBUTION CURVE

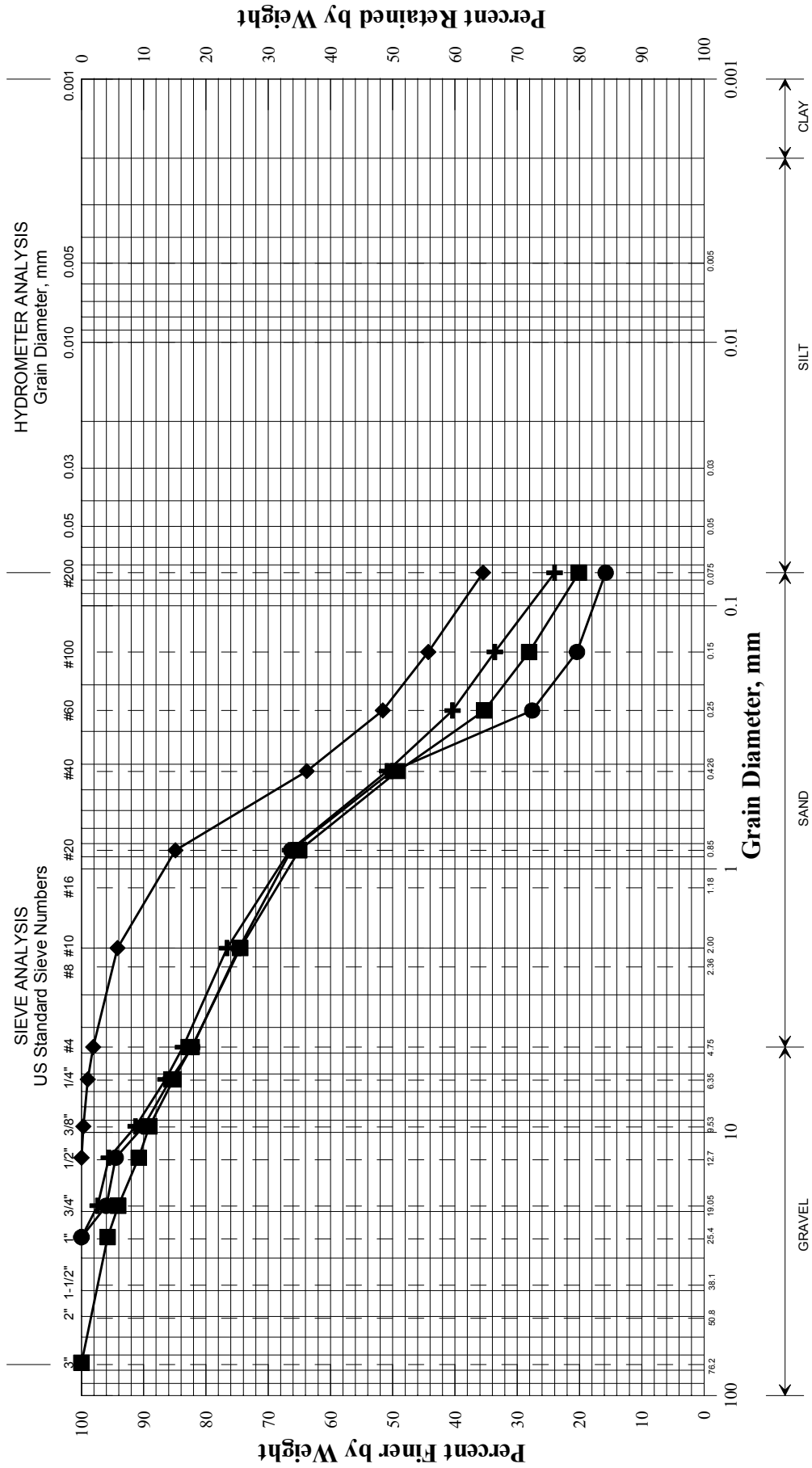


UNIFIED CLASSIFICATION

Boring/Sample No.	Station	Offset, ft	Depth, ft	Description	W, %	LL	PL	PI
+	63+13	6.4 LT	1.1-3.0	SAND, some silt, trace gravel.	13.7			
◆	63+13	6.4 LT	3.0-5.0	SAND, little gravel, trace silt.	4.6			
■	56+23	4.1 RT	0.9-5.0	SAND, little silt, little gravel.	4.2			
●	52+84	4.1 RT	0.9-5.0	SAND, some silt, little gravel.	6.2			
▲								
×								

014814.00	PIN
Biddeford	Town
WHITE, TERRY A	Reported by/Date
6/3/2008	

State of Maine Department of Transportation
GRAIN SIZE DISTRIBUTION CURVE

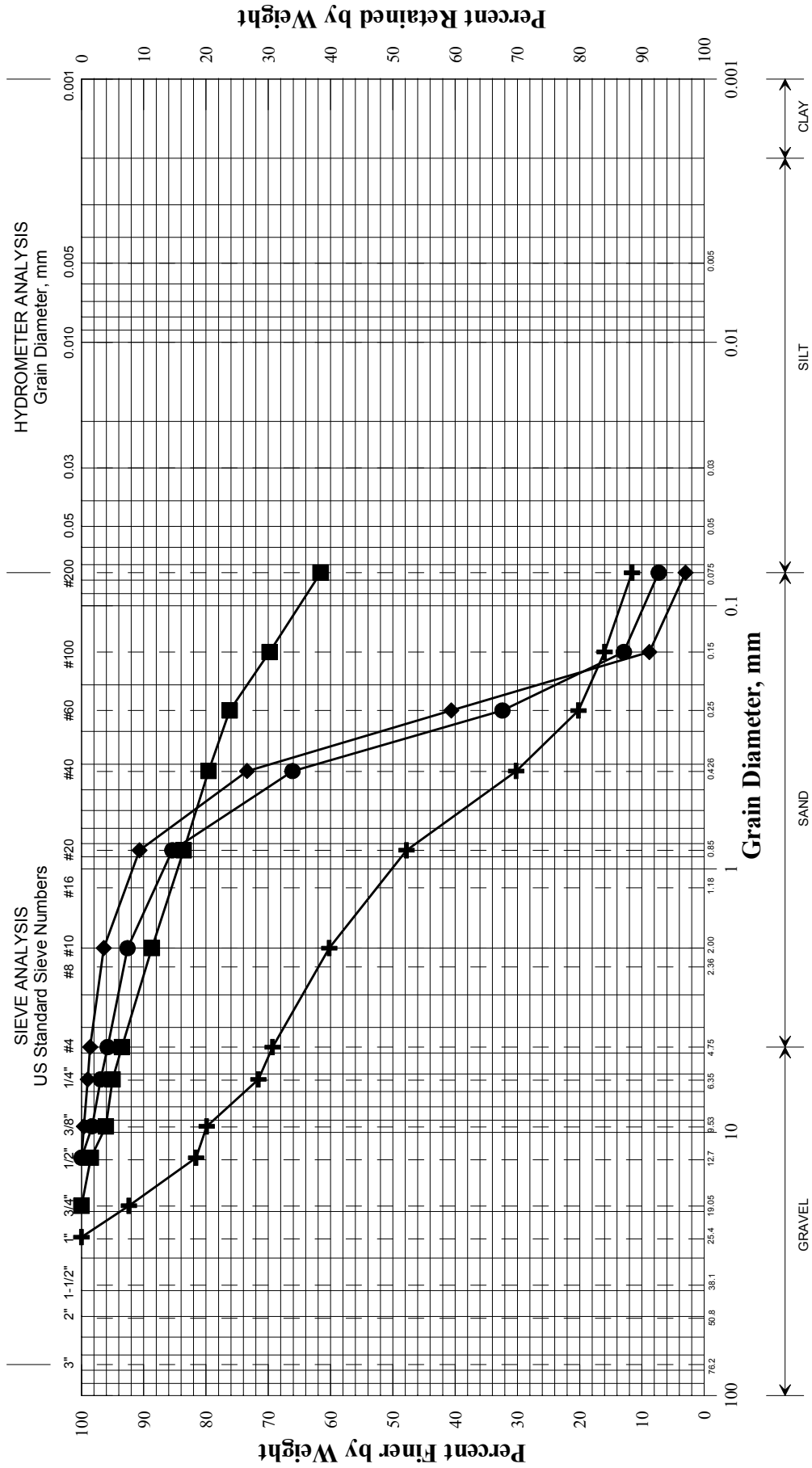


UNIFIED CLASSIFICATION

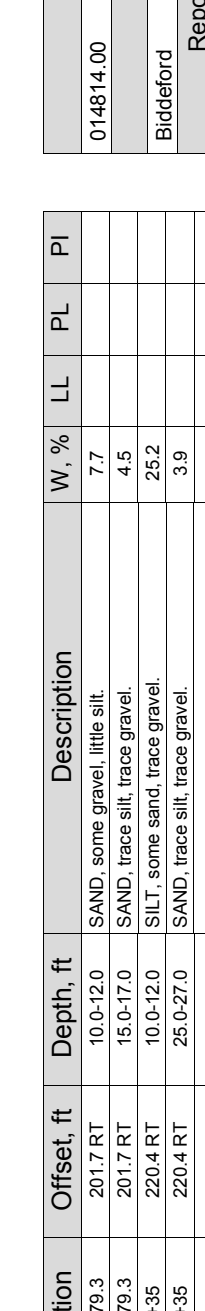
+	Station	50+96	Depth, ft	0.8-2.2	Description	SAND, some silt, little gravel.	W, %	6.0	LL		PL	PI
◆	Station	50+96	Depth, ft	2.2-5.0	Description	SAND, some silt, trace gravel.	W, %	21.5	LL		PL	PI
■	Station	46+38	Depth, ft	0.9-5.0	Description	SAND, little silt, little gravel.	W, %	8.4	LL		PL	PI
●	Station	43+52	Depth, ft	1.0-5.0	Description	SAND, little gravel, little silt.	W, %	4.1	LL		PL	PI
×	Station		Depth, ft		Description		W, %		LL		PL	PI

+	Boring/Sample No.	HB-BIDD-104/S5	Station	50+96	Offset, ft	4.2 LT	Depth, ft	0.8-2.2	Description	SAND, some silt, little gravel.	W, %	6.0	LL	PL	PI
◆	Boring/Sample No.	HB-BIDD-104/S6	Station	50+96	Offset, ft	4.2 LT	Depth, ft	2.2-5.0	Description	SAND, some silt, trace gravel.	W, %	21.5	LL	PL	PI
■	Boring/Sample No.	HB-BIDD-106/S8	Station	46+38	Offset, ft	6.4 LT	Depth, ft	0.9-5.0	Description	SAND, little silt, little gravel.	W, %	8.4	LL	PL	PI
●	Boring/Sample No.	HB-BIDD-107/S9	Station	43+52	Offset, ft	12.4 RT	Depth, ft	1.0-5.0	Description	SAND, little gravel, little silt.	W, %	4.1	LL	PL	PI
×	Boring/Sample No.		Station		Offset, ft		Depth, ft		Description		W, %		LL	PL	PI

State of Maine Department of Transportation
GRAIN SIZE DISTRIBUTION CURVE



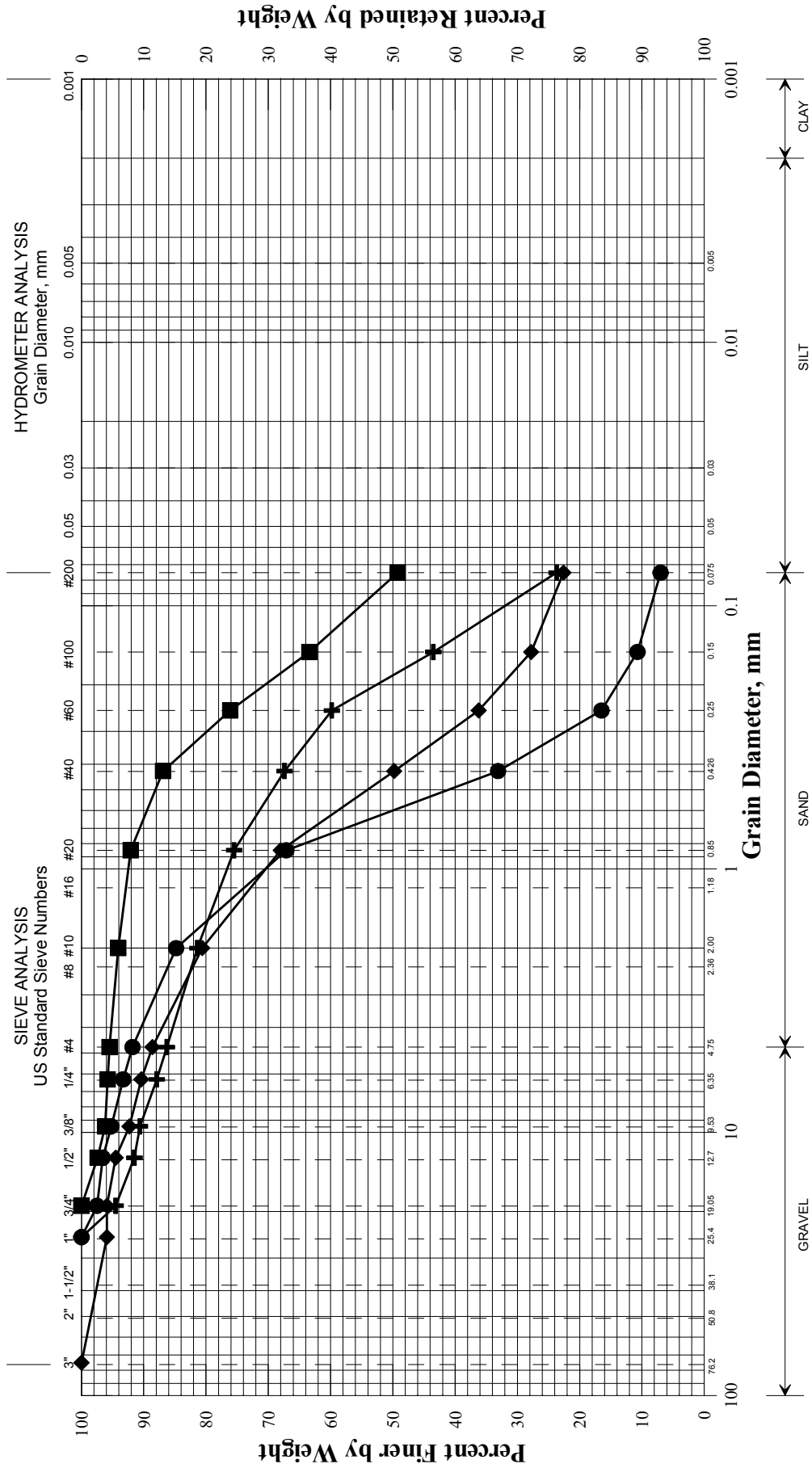
UNIFIED CLASSIFICATION



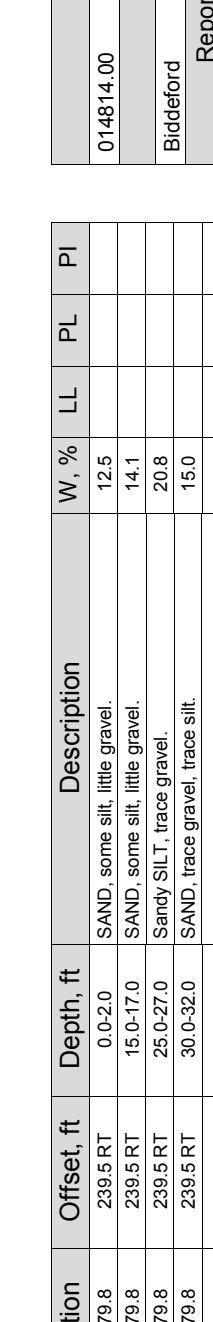
+	Station	50+79.3	Offset, ft	201.7 RT	Depth, ft	10.0-12.0	Description	SAND, some gravel, little silt.	W, %	7.7	LL		PL		PI	
◆	Station	50+79.3	Offset, ft	201.7 RT	Depth, ft	15.0-17.0	Description	SAND, trace silt, trace gravel.	W, %	4.5	LL		PL		PI	
■	Station	51+35	Offset, ft	220.4 RT	Depth, ft	10.0-12.0	Description	SILT, some sand, trace gravel.	W, %	25.2	LL		PL		PI	
●	Station	51+35	Offset, ft	220.4 RT	Depth, ft	25.0-27.0	Description	SAND, trace silt, trace gravel.	W, %	3.9	LL		PL		PI	
×	Station		Offset, ft		Depth, ft		Description		W, %		LL		PL		PI	

	Boring/Sample No.	Station	Offset, ft	Depth, ft	Description	W, %	LL	PL	PI
	HB-BIDD-201/1D	50+79.3	201.7 RT	10.0-12.0	SAND, some gravel, little silt.	7.7			
	HB-BIDD-201/2D	50+79.3	201.7 RT	15.0-17.0	SAND, trace silt, trace gravel.	4.5			
	HB-BIDD-202/1D	51+35	220.4 RT	10.0-12.0	SILT, some sand, trace gravel.	25.2			
	HB-BIDD-202/3D	51+35	220.4 RT	25.0-27.0	SAND, trace silt, trace gravel.	3.9			

State of Maine Department of Transportation
GRAIN SIZE DISTRIBUTION CURVE



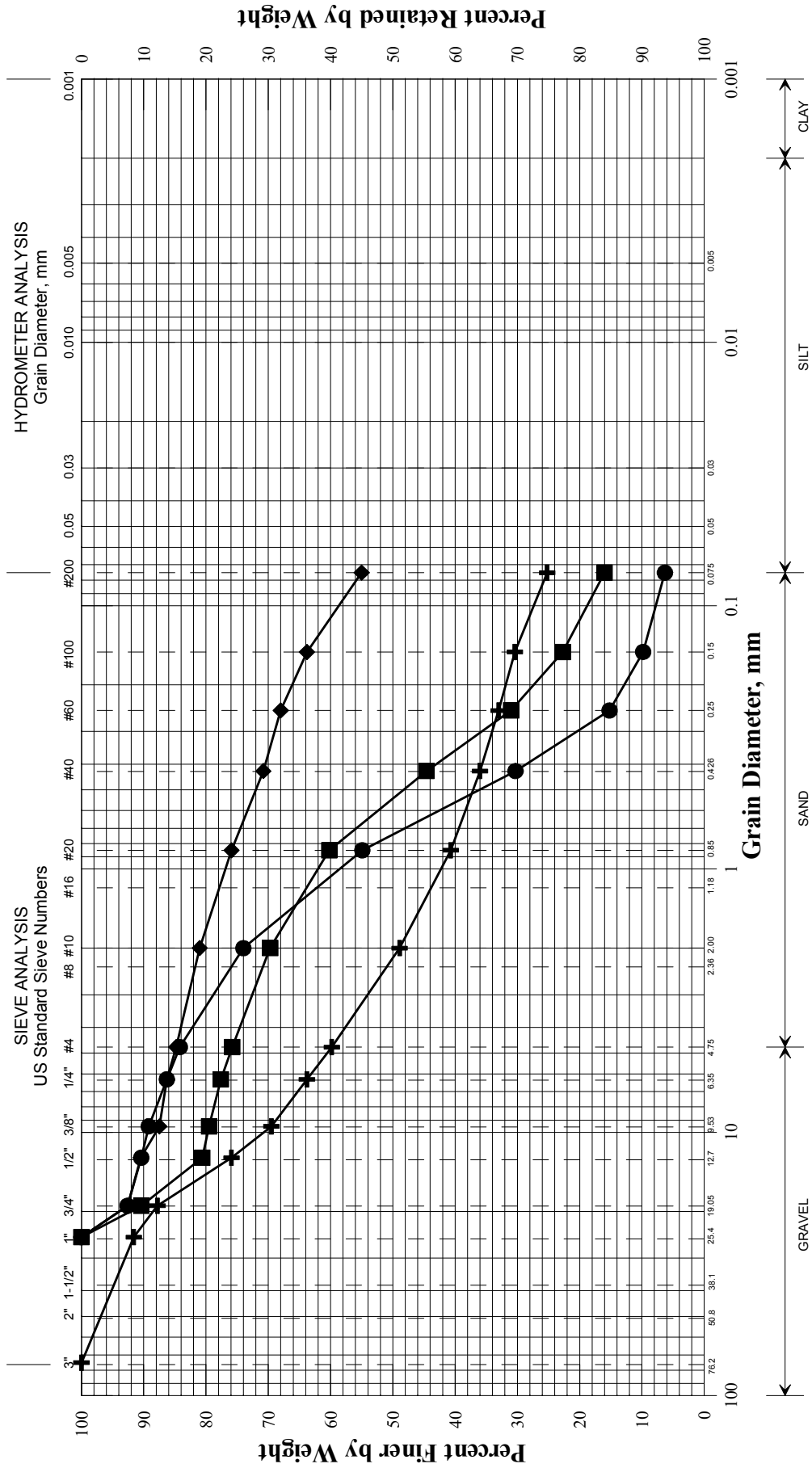
UNIFIED CLASSIFICATION



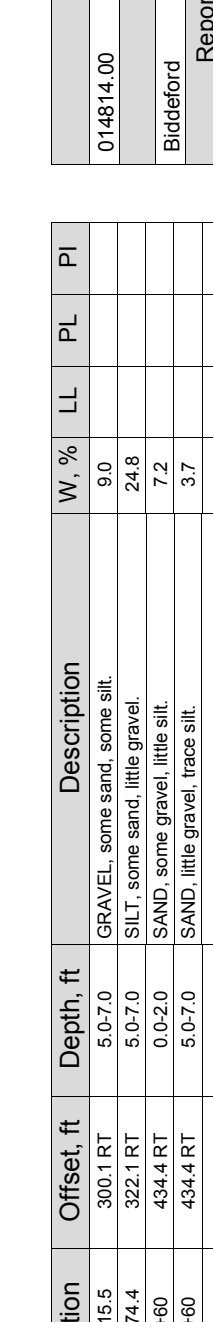
Boring/Sample No.	Station	Offset, ft	Depth, ft	Description	W, %	LL	PL	PI
+	51+79.8	239.5 RT	0.0-2.0	SAND, some silt, little gravel.	12.5			
◆	51+79.8	239.5 RT	15.0-17.0	SAND, some silt, little gravel.	14.1			
■	51+79.8	239.5 RT	25.0-27.0	Sandy SILT, trace gravel.	20.8			
●	51+79.8	239.5 RT	30.0-32.0	SAND, trace gravel, trace silt.	15.0			
▲								
×								

PIN	014814.00
Town	Biddeford
Reported by/Date	WHITE, TERRY A 2/8/2011

State of Maine Department of Transportation
GRAIN SIZE DISTRIBUTION CURVE



UNIFIED CLASSIFICATION



Boring/Sample No.	Station	Offset, ft	Depth, ft	Description	W, %	LL	PL	PI
+ HB-BIDD-204/1D	51+15.5	300.1 RT	5.0-7.0	GRAVEL, some sand, some silt.	9.0			
◆ HB-BIDD-205/1D	50+74.4	322.1 RT	5.0-7.0	SILT, some sand, little gravel.	24.8			
■ HB-BIDD-206/1D	50+60	434.4 RT	0.0-2.0	SAND, some gravel, little silt.	7.2			
● HB-BIDD-206/2D	50+60	434.4 RT	5.0-7.0	SAND, little gravel, trace silt.	3.7			
▲								
×								

PIN	014814.00
Town	Biddeford
Reported by/Date	WHITE, TERRY A 2/8/2011



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
207234	HB-BIDD-101/S1	GEOTECHNICAL (DISTURBED)	5/8/2008	5/23/2008
Sample Type: GEOTECHNICAL Location: OTHER		Station: 63+13 Offset, ft: 6.4 LT Dbfg, ft: 1.1-3.0		
PIN: 014814.00 Town: Biddeford		Sampler: WILDER, BRUCE H		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	95.6
½ in. [12.5 mm]	95.6
⅜ in. [9.5 mm]	95.3
¼ in. [6.3 mm]	94.4
No. 4 [4.75 mm]	94.0
No. 10 [2.00 mm]	90.7
No. 20 [0.850 mm]	79.8
No. 40 [0.425 mm]	55.2
No. 60 [0.250 mm]	42.7
No. 100 [0.150 mm]	35.8
No. 200 [0.075 mm]	28.0

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimblings, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H2O, %
Water Content (T 265), %	
13.7	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN** Date Reported: **5/30/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No. **207235** Boring No./Sample No. **HB-BIDD-101/S2** Sample Description **GEOTECHNICAL (DISTURBED)** Sampled **5/8/2008** Received **5/23/2008**

Sample Type: **GEOTECHNICAL** Location: **OTHER** Station: **63+13** Offset, ft: **6.4** LT Dbfg, ft: **3.0-5.0**

PIN: **014814.00** Town: **Biddeford** Sampler: **WILDER, BRUCE H**

TEST RESULTS

Sieve Analysis (T 27, T 11)

Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	95.0
½ in. [12.5 mm]	92.6
⅜ in. [9.5 mm]	91.2
¼ in. [6.3 mm]	89.7
No. 4 [4.75 mm]	89.0
No. 10 [2.00 mm]	84.0
No. 20 [0.850 mm]	71.7
No. 40 [0.425 mm]	39.0
No. 60 [0.250 mm]	15.4
No. 100 [0.150 mm]	10.6
No. 200 [0.075 mm]	7.4

Direct Shear (T 236)

Shear Angle, °		
Initial Water Content, %		
Normal Stress, psi		
Wet Density, lbs/ft³		
Dry Density, lbs/ft³		
Specimen Thickness, in		

Consolidation (T 216)

Trimming, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests

<u>Liquid Limit @ 25 blows (T 89), %</u>
<u>Plastic Limit (T 90), %</u>
<u>Plasticity Index (T 90), %</u>
<u>Specific Gravity, Corrected to 20°C (T 100)</u>
<u>Loss on Ignition (T 267)</u>
<u>Loss, %</u> <u>H2O, %</u>
<u>Water Content (T 265), %</u>
4.6

Vane Shear Test on Shelby Tubes (Maine DOT)

Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **5/30/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
207236	HB-BIDD-102/S3	<u>GEOTECHNICAL (DISTURBED)</u>	5/8/2008	5/23/2008
Sample Type: GEOTECHNICAL Location: OTHER		Station: 56+23 Offset, ft: 4.1	RT Dbfg, ft: 0.9-5.0	
PIN: 014814.00 Town: Biddeford		Sampler: WILDER, BRUCE H		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	
¾ in. [19.0 mm]	100.0
½ in. [12.5 mm]	97.4
⅜ in. [9.5 mm]	95.0
¼ in. [6.3 mm]	90.2
No. 4 [4.75 mm]	87.0
No. 10 [2.00 mm]	77.4
No. 20 [0.850 mm]	62.3
No. 40 [0.425 mm]	42.9
No. 60 [0.250 mm]	29.1
No. 100 [0.150 mm]	23.0
No. 200 [0.075 mm]	17.9

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimming, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H2O, %
Water Content (T 265), %	
4.2	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **6/2/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
207237	HB-BIDD-103/S4	GEOTECHNICAL (DISTURBED)	5/8/2008	5/23/2008
Sample Type: GEOTECHNICAL Location: OTHER		Station: 52+84	Offset, ft: 4.1 RT Dbfg, ft: 0.9-5.0	
PIN: 014814.00 Town: Biddeford		Sampler: WILDER, BRUCE H		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	
¾ in. [19.0 mm]	100.0
½ in. [12.5 mm]	96.6
⅜ in. [9.5 mm]	93.7
¼ in. [6.3 mm]	86.6
No. 4 [4.75 mm]	82.2
No. 10 [2.00 mm]	69.1
No. 20 [0.850 mm]	54.1
No. 40 [0.425 mm]	43.5
No. 60 [0.250 mm]	34.6
No. 100 [0.150 mm]	29.3
No. 200 [0.075 mm]	22.3

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimmings, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests
<u>Liquid Limit @ 25 blows (T 89), %</u>
<u>Plastic Limit (T 90), %</u>
<u>Plasticity Index (T 90), %</u>
<u>Specific Gravity, Corrected to 20°C (T 100)</u>
<u>Loss on Ignition (T 267)</u>
<u>Loss, %</u> <u>H2O, %</u>
<u>Water Content (T 265), %</u>
6.2

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **6/2/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
207238	HB-BIDD-104/S5	GEOTECHNICAL (DISTURBED)	5/8/2008	5/23/2008
Sample Type: GEOTECHNICAL		Location: OTHER	Station: 50+96	Offset, ft: 4.2 LT Dbfg, ft: 0.8-2.2
PIN: 014814.00		Town: Biddeford	Sampler: WILDER, BRUCE H	

TEST RESULTS

Sieve Analysis (T 27, T 11)

Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	97.4
½ in. [12.5 mm]	95.6
⅜ in. [9.5 mm]	91.3
¼ in. [6.3 mm]	86.5
No. 4 [4.75 mm]	83.7
No. 10 [2.00 mm]	76.6
No. 20 [0.850 mm]	66.5
No. 40 [0.425 mm]	50.9
No. 60 [0.250 mm]	40.4
No. 100 [0.150 mm]	33.6
No. 200 [0.075 mm]	24.0

Direct Shear (T 236)

Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)

Trimming, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests

Liquid Limit @ 25 blows (T 89), %
Plastic Limit (T 90), %
Plasticity Index (T 90), %
Specific Gravity, Corrected to 20°C (T 100)
Loss on Ignition (T 267)
Loss, %
H ₂ O, %
Water Content (T 265), %
6.0

Vane Shear Test on Shelby Tubes (Maine DOT)

Depth taken in tube, ft	3 in.		6 in.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear tons/ft²	Remold tons/ft²	U. Shear tons/ft²	Remold tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **6/2/2008**

Paper Copy: Lab File; Project File; Geotech File



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
207239	HB-BIDD-104/S6	GEOTECHNICAL (DISTURBED)	5/8/2008	5/23/2008
Sample Type: GEOTECHNICAL Location: OTHER		Station: 50+96	Offset, ft: 4.2 LT Dbfg, ft: 2.2-5.0	
PIN: 014814.00 Town: Biddeford		Sampler: WILDER, BRUCE H		

TEST RESULTS

Sieve Analysis (T 27, T 11) Wash Method <b style="color: red;">Procedure A <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 70%;">SIEVE SIZE U.S. [SI]</th> <th style="width: 30%;">% Passing</th> </tr> </thead> <tbody> <tr><td>3 in. [75.0 mm]</td><td></td></tr> <tr><td>1 in. [25.0 mm]</td><td></td></tr> <tr><td>¾ in. [19.0 mm]</td><td></td></tr> <tr><td>½ in. [12.5 mm]</td><td style="text-align: center;">100.0</td></tr> <tr><td>⅜ in. [9.5 mm]</td><td style="text-align: center;">99.7</td></tr> <tr><td>¼ in. [6.3 mm]</td><td style="text-align: center;">99.0</td></tr> <tr><td>No. 4 [4.75 mm]</td><td style="text-align: center;">98.1</td></tr> <tr><td>No. 10 [2.00 mm]</td><td style="text-align: center;">94.2</td></tr> <tr><td>No. 20 [0.850 mm]</td><td style="text-align: center;">84.9</td></tr> <tr><td>No. 40 [0.425 mm]</td><td style="text-align: center;">63.8</td></tr> <tr><td>No. 60 [0.250 mm]</td><td style="text-align: center;">51.6</td></tr> <tr><td>No. 100 [0.150 mm]</td><td style="text-align: center;">44.3</td></tr> <tr><td>No. 200 [0.075 mm]</td><td style="text-align: center;">35.5</td></tr> </tbody> </table>	SIEVE SIZE U.S. [SI]	% Passing	3 in. [75.0 mm]		1 in. [25.0 mm]		¾ in. [19.0 mm]		½ in. [12.5 mm]	100.0	⅜ in. [9.5 mm]	99.7	¼ in. [6.3 mm]	99.0	No. 4 [4.75 mm]	98.1	No. 10 [2.00 mm]	94.2	No. 20 [0.850 mm]	84.9	No. 40 [0.425 mm]	63.8	No. 60 [0.250 mm]	51.6	No. 100 [0.150 mm]	44.3	No. 200 [0.075 mm]	35.5	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="4" style="text-align: center;">Direct Shear (T 236)</th> </tr> </thead> <tbody> <tr><td>Shear Angle, °</td><td></td><td></td><td></td></tr> <tr><td>Initial Water Content, %</td><td></td><td></td><td></td></tr> <tr><td>Normal Stress, psi</td><td></td><td></td><td></td></tr> <tr><td>Wet Density, lbs/ft³</td><td></td><td></td><td></td></tr> <tr><td>Dry Density, lbs/ft³</td><td></td><td></td><td></td></tr> <tr><td>Specimen Thickness, in</td><td></td><td></td><td></td></tr> </tbody> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="6" style="text-align: center;">Consolidation (T 216)</th> </tr> </thead> <tbody> <tr> <td colspan="6" style="text-align: center;">Trimmings, Water Content, %</td> </tr> <tr> <td></td> <td style="text-align: center;">Initial</td> <td style="text-align: center;">Final</td> <td></td> <td style="text-align: center;">Void Ratio</td> <td style="text-align: center;">% Strain</td> </tr> <tr> <td>Water Content, %</td> <td></td> <td></td> <td style="text-align: center;">Pmin</td> <td></td> <td></td> </tr> <tr> <td>Dry Density, lbs/ft³</td> <td></td> <td></td> <td style="text-align: center;">Pp</td> <td></td> <td></td> </tr> <tr> <td>Void Ratio</td> <td></td> <td></td> <td style="text-align: center;">Pmax</td> <td></td> <td></td> </tr> <tr> <td>Saturation, %</td> <td></td> <td></td> <td style="text-align: center;">Cc/C'c</td> <td></td> <td></td> </tr> </tbody> </table> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th colspan="7" style="text-align: center;">Vane Shear Test on Shelby Tubes (Maine DOT)</th> </tr> <tr> <th rowspan="3" style="text-align: center;">Depth taken in tube, ft</th> <th colspan="2" style="text-align: center;">3 In.</th> <th colspan="2" style="text-align: center;">6 In.</th> <th rowspan="3" style="text-align: center;">Water Content, %</th> <th rowspan="3" style="text-align: center;">Description of Material Sampled at the Various Tube Depths</th> </tr> <tr> <th style="text-align: center;">U. 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Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**
Date Reported: **6/2/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
207240	HB-BIDD-106/S8	GEOTECHNICAL (DISTURBED)	5/8/2008	5/23/2008
Sample Type: GEOTECHNICAL Location: OTHER		Station: 46+38	Offset, ft: 6.4 LT Dbfg, ft: 0.9-5.0	
PIN: 014814.00 Town: Biddeford		Sampler: WILDER, BRUCE H		

TEST RESULTS

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Reported by: **FOGG, BRIAN**
Date Reported: **6/2/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
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Sample Type: GEOTECHNICAL Location: OTHER		Station: 43+52	Offset, ft: 12.4 RT Dbfg, ft: 1.0-5.0	
PIN: 014814.00 Town: Biddeford		Sampler: WILDER, BRUCE H		

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Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**
Date Reported: **6/2/2008**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239976	HB-BIDD-201/1D	<u>GEOTECHNICAL (DISTURBED)</u>	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 50+79.3 Offset, ft: 201. RT Dbfg, ft: 10.0-12.0		
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	92.4
½ in. [12.5 mm]	81.6
⅜ in. [9.5 mm]	79.9
¼ in. [6.3 mm]	71.6
No. 4 [4.75 mm]	69.3
No. 10 [2.00 mm]	60.2
No. 20 [0.850 mm]	47.8
No. 40 [0.425 mm]	30.2
No. 60 [0.250 mm]	20.2
No. 100 [0.150 mm]	16.0
No. 200 [0.075 mm]	11.6

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimming, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H ₂ O, %
Water Content (T 265), %	
7.7	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No. **239977** Boring No./Sample No. **HB-BIDD-201/2D** Sample Description **GEOTECHNICAL (DISTURBED)** Sampled **1/19/2011** Received **2/1/2011**
 Sample Type: **GEOTECHNICAL** Location: **OTHER** Station: **50+79.3** Offset, ft: **201. RT Dbfg, ft: 15.0-17.0**
 PIN: **014814.00** Town: **Biddeford** Sampler: **GROSS, KAREN L**

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	
¾ in. [19.0 mm]	
½ in. [12.5 mm]	100.0
⅜ in. [9.5 mm]	99.6
¼ in. [6.3 mm]	99.0
No. 4 [4.75 mm]	98.6
No. 10 [2.00 mm]	96.4
No. 20 [0.850 mm]	90.7
No. 40 [0.425 mm]	73.4
No. 60 [0.250 mm]	40.6
No. 100 [0.150 mm]	8.8
No. 200 [0.075 mm]	3.0

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimblings, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H2O, %
Water Content (T 265), %	
4.5	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239978	HB-BIDD-202/1D	GEOTECHNICAL (DISTURBED)	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 51+35	Offset, ft: 220. RT Dbfg, ft: 10.0-12.0	
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

<p>Sieve Analysis (T 27, T 11)</p> <p>Wash Method Procedure A</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 70%;">SIEVE SIZE U.S. [SI]</th> <th style="width: 30%;">% Passing</th> </tr> </thead> <tbody> <tr><td>3 in. [75.0 mm]</td><td></td></tr> <tr><td>1 in. [25.0 mm]</td><td></td></tr> <tr><td>¾ in. [19.0 mm]</td><td>100.0</td></tr> <tr><td>½ in. [12.5 mm]</td><td>98.5</td></tr> <tr><td>⅜ in. [9.5 mm]</td><td>96.1</td></tr> <tr><td>¼ in. [6.3 mm]</td><td>95.0</td></tr> <tr><td>No. 4 [4.75 mm]</td><td>93.5</td></tr> <tr><td>No. 10 [2.00 mm]</td><td>88.7</td></tr> <tr><td>No. 20 [0.850 mm]</td><td>83.6</td></tr> <tr><td>No. 40 [0.425 mm]</td><td>79.6</td></tr> <tr><td>No. 60 [0.250 mm]</td><td>76.2</td></tr> <tr><td>No. 100 [0.150 mm]</td><td>69.8</td></tr> <tr><td>No. 200 [0.075 mm]</td><td>61.6</td></tr> </tbody> </table>	SIEVE SIZE U.S. [SI]	% Passing	3 in. [75.0 mm]		1 in. [25.0 mm]		¾ in. [19.0 mm]	100.0	½ in. [12.5 mm]	98.5	⅜ in. [9.5 mm]	96.1	¼ in. [6.3 mm]	95.0	No. 4 [4.75 mm]	93.5	No. 10 [2.00 mm]	88.7	No. 20 [0.850 mm]	83.6	No. 40 [0.425 mm]	79.6	No. 60 [0.250 mm]	76.2	No. 100 [0.150 mm]	69.8	No. 200 [0.075 mm]	61.6	<p style="text-align: center;">Direct Shear (T 236)</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr><td>Shear Angle, °</td><td></td><td></td></tr> <tr><td>Initial Water Content, %</td><td></td><td></td></tr> <tr><td>Normal Stress, psi</td><td></td><td></td></tr> <tr><td>Wet Density, lbs/ft³</td><td></td><td></td></tr> <tr><td>Dry Density, lbs/ft³</td><td></td><td></td></tr> <tr><td>Specimen Thickness, in</td><td></td><td></td></tr> </table> <p style="text-align: center;">Consolidation (T 216)</p> <p style="text-align: center;">Trimmings, Water Content, % <input style="width: 100px;" type="text"/></p> <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th></th> <th>Initial</th> <th>Final</th> <th></th> <th>Void Ratio</th> <th>% Strain</th> </tr> </thead> <tbody> <tr><td>Water Content, %</td><td></td><td></td><td>Pmin</td><td></td><td></td></tr> <tr><td>Dry Density, lbs/ft³</td><td></td><td></td><td>Pp</td><td></td><td></td></tr> <tr><td>Void Ratio</td><td></td><td></td><td>Pmax</td><td></td><td></td></tr> <tr><td>Saturation, %</td><td></td><td></td><td>Cc/C'c</td><td></td><td></td></tr> </tbody> </table>	Shear Angle, °			Initial Water Content, %			Normal Stress, psi			Wet Density, lbs/ft³			Dry Density, lbs/ft³			Specimen Thickness, in				Initial	Final		Void Ratio	% Strain	Water Content, %			Pmin			Dry Density, lbs/ft³			Pp			Void Ratio			Pmax			Saturation, %			Cc/C'c			<p>Miscellaneous Tests</p> <p>Liquid Limit @ 25 blows (T 89), %</p> <hr/> <p>Plastic Limit (T 90), %</p> <hr/> <p>Plasticity Index (T 90), %</p> <hr/> <p>Specific Gravity, Corrected to 20°C (T 100)</p> <hr/> <p>Loss on Ignition (T 267)</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td>Loss, %</td> <td>H2O, %</td> </tr> <tr> <td></td> <td></td> </tr> </table> <hr/> <p>Water Content (T 265), %</p> <p style="text-align: center;">25.2</p>	Loss, %	H2O, %		
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Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**
Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239980	HB-BIDD-202/3D	GEOTECHNICAL (DISTURBED)	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 51+35 Offset, ft: 220. RT Dbfg, ft: 25.0-27.0		
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11) Wash Method Procedure A <table style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 70%;">SIEVE SIZE U.S. [SI]</th> <th style="width: 30%;">% Passing</th> </tr> </thead> <tbody> <tr><td>3 in. [75.0 mm]</td><td></td></tr> <tr><td>1 in. [25.0 mm]</td><td></td></tr> <tr><td>¾ in. [19.0 mm]</td><td></td></tr> <tr><td>½ in. [12.5 mm]</td><td style="text-align: center;">100.0</td></tr> <tr><td>⅜ in. [9.5 mm]</td><td style="text-align: center;">98.3</td></tr> <tr><td>¼ in. [6.3 mm]</td><td style="text-align: center;">96.9</td></tr> <tr><td>No. 4 [4.75 mm]</td><td style="text-align: center;">95.8</td></tr> <tr><td>No. 10 [2.00 mm]</td><td style="text-align: center;">92.6</td></tr> <tr><td>No. 20 [0.850 mm]</td><td style="text-align: center;">85.4</td></tr> <tr><td>No. 40 [0.425 mm]</td><td style="text-align: center;">66.1</td></tr> <tr><td>No. 60 [0.250 mm]</td><td style="text-align: center;">32.4</td></tr> <tr><td>No. 100 [0.150 mm]</td><td style="text-align: center;">12.9</td></tr> <tr><td>No. 200 [0.075 mm]</td><td style="text-align: center;">7.3</td></tr> </tbody> </table>	SIEVE SIZE U.S. [SI]	% Passing	3 in. [75.0 mm]		1 in. [25.0 mm]		¾ in. [19.0 mm]		½ in. [12.5 mm]	100.0	⅜ in. [9.5 mm]	98.3	¼ in. [6.3 mm]	96.9	No. 4 [4.75 mm]	95.8	No. 10 [2.00 mm]	92.6	No. 20 [0.850 mm]	85.4	No. 40 [0.425 mm]	66.1	No. 60 [0.250 mm]	32.4	No. 100 [0.150 mm]	12.9	No. 200 [0.075 mm]	7.3	<table style="width: 100%; border-collapse: collapse;"> <tr> <th colspan="6" style="text-align: center; background-color: #e0e0e0;">Direct Shear (T 236)</th> </tr> <tr><td style="width: 40%;">Shear Angle, °</td><td style="width: 10%;"></td><td style="width: 10%;"></td><td style="width: 10%;"></td><td style="width: 10%;"></td><td style="width: 10%;"></td></tr> <tr><td>Initial Water Content, %</td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>Normal Stress, psi</td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>Wet Density, lbs/ft³</td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>Dry Density, lbs/ft³</td><td></td><td></td><td></td><td></td><td></td></tr> <tr><td>Specimen Thickness, in</td><td></td><td></td><td></td><td></td><td></td></tr> <tr> <th colspan="6" style="text-align: center; background-color: #e0e0e0;">Consolidation (T 216)</th> </tr> <tr><td colspan="6" style="text-align: center;">Trimming, Water Content, %</td></tr> <tr> <th style="width: 30%;"></th> <th style="width: 10%;">Initial</th> <th style="width: 10%;">Final</th> <th style="width: 10%;"></th> <th style="width: 10%;">Void Ratio</th> <th style="width: 10%;">% Strain</th> </tr> <tr><td>Water Content, %</td><td></td><td></td><td>Pmin</td><td></td><td></td></tr> <tr><td>Dry Density, lbs/ft³</td><td></td><td></td><td>Pp</td><td></td><td></td></tr> <tr><td>Void Ratio</td><td></td><td></td><td>Pmax</td><td></td><td></td></tr> <tr><td>Saturation, %</td><td></td><td></td><td>Cc/C'c</td><td></td><td></td></tr> <tr> <th colspan="6" style="text-align: center; background-color: #e0e0e0;">Vane Shear Test on Shelby Tubes (Maine DOT)</th> </tr> <tr> <th rowspan="3" style="width: 10%;">Depth taken in tube, ft</th> <th colspan="2" style="width: 15%;">3 In.</th> <th colspan="2" style="width: 15%;">6 In.</th> <th rowspan="3" style="width: 10%;">Water Content, %</th> <th rowspan="3" style="width: 40%;">Description of Material Sampled at the Various Tube Depths</th> </tr> <tr> <th style="width: 5%;">U. Shear</th> <th style="width: 10%;">Remold</th> <th style="width: 5%;">U. Shear</th> <th style="width: 10%;">Remold</th> </tr> <tr> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> </tr> <tr><td colspan="7" style="height: 100px;"></td></tr> </table>	Direct Shear (T 236)						Shear Angle, °						Initial Water Content, %						Normal Stress, psi						Wet Density, lbs/ft³						Dry Density, lbs/ft³						Specimen Thickness, in						Consolidation (T 216)						Trimming, Water Content, %							Initial	Final		Void Ratio	% Strain	Water Content, %			Pmin			Dry Density, lbs/ft³			Pp			Void Ratio			Pmax			Saturation, %			Cc/C'c			Vane Shear Test on Shelby Tubes (Maine DOT)						Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths	U. Shear	Remold	U. Shear	Remold	tons/ft²	tons/ft²	tons/ft²	tons/ft²								Miscellaneous Tests Liquid Limit @ 25 blows (T 89), % Plastic Limit (T 90), % Plasticity Index (T 90), % Specific Gravity, Corrected to 20°C (T 100) Loss on Ignition (T 267) <table style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; text-align: center;">Loss, %</td> <td style="width: 50%; text-align: center;">H2O, %</td> </tr> </table> Water Content (T 265), % <p style="text-align: center; font-weight: bold;">3.9</p>	Loss, %	H2O, %
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Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**
Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239981	HB-BIDD-203/1D	<u>GEOTECHNICAL (DISTURBED)</u>	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 51+79.8 Offset, ft: 239. RT Dbfg, ft: 0.0-2.0		
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	94.5
½ in. [12.5 mm]	91.5
⅜ in. [9.5 mm]	90.6
¼ in. [6.3 mm]	87.9
No. 4 [4.75 mm]	86.3
No. 10 [2.00 mm]	81.4
No. 20 [0.850 mm]	75.5
No. 40 [0.425 mm]	67.4
No. 60 [0.250 mm]	59.8
No. 100 [0.150 mm]	43.5
No. 200 [0.075 mm]	23.7

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimmings, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H2O, %
Water Content (T 265), %	
12.5	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**
Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239982	HB-BIDD-203/4D	<u>GEOTECHNICAL (DISTURBED)</u>	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 51+79.8 Offset, ft: 239. RT Dbfg, ft: 15.0-17.0		
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11) Wash Method <b style="color: red;">Procedure A <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 70%;">SIEVE SIZE U.S. [SI]</th> <th style="width: 30%;">% Passing</th> </tr> </thead> <tbody> <tr><td>3 in. [75.0 mm]</td><td style="text-align: center;">100.0</td></tr> <tr><td>1 in. [25.0 mm]</td><td style="text-align: center;">95.9</td></tr> <tr><td>¾ in. [19.0 mm]</td><td style="text-align: center;">95.9</td></tr> <tr><td>½ in. [12.5 mm]</td><td style="text-align: center;">94.5</td></tr> <tr><td>⅜ in. [9.5 mm]</td><td style="text-align: center;">92.3</td></tr> <tr><td>¼ in. [6.3 mm]</td><td style="text-align: center;">90.4</td></tr> <tr><td>No. 4 [4.75 mm]</td><td style="text-align: center;">88.6</td></tr> <tr><td>No. 10 [2.00 mm]</td><td style="text-align: center;">80.6</td></tr> <tr><td>No. 20 [0.850 mm]</td><td style="text-align: center;">68.0</td></tr> <tr><td>No. 40 [0.425 mm]</td><td style="text-align: center;">49.8</td></tr> <tr><td>No. 60 [0.250 mm]</td><td style="text-align: center;">36.2</td></tr> <tr><td>No. 100 [0.150 mm]</td><td style="text-align: center;">27.8</td></tr> <tr><td>No. 200 [0.075 mm]</td><td style="text-align: center;">22.6</td></tr> </tbody> </table>	SIEVE SIZE U.S. [SI]	% Passing	3 in. [75.0 mm]	100.0	1 in. [25.0 mm]	95.9	¾ in. [19.0 mm]	95.9	½ in. [12.5 mm]	94.5	⅜ in. [9.5 mm]	92.3	¼ in. [6.3 mm]	90.4	No. 4 [4.75 mm]	88.6	No. 10 [2.00 mm]	80.6	No. 20 [0.850 mm]	68.0	No. 40 [0.425 mm]	49.8	No. 60 [0.250 mm]	36.2	No. 100 [0.150 mm]	27.8	No. 200 [0.075 mm]	22.6	<table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr style="background-color: #e0e0e0;"> <th colspan="4" style="text-align: center;">Direct Shear (T 236)</th> </tr> </thead> <tbody> <tr><td style="width: 40%;">Shear Angle, °</td><td style="width: 10%;"></td><td style="width: 10%;"></td><td style="width: 40%;"></td></tr> <tr><td>Initial Water Content, %</td><td></td><td></td><td></td></tr> <tr><td>Normal Stress, psi</td><td></td><td></td><td></td></tr> <tr><td>Wet Density, lbs/ft³</td><td></td><td></td><td></td></tr> <tr><td>Dry Density, lbs/ft³</td><td></td><td></td><td></td></tr> <tr><td>Specimen Thickness, in</td><td></td><td></td><td></td></tr> <tr style="background-color: #e0e0e0;"> <th colspan="4" style="text-align: center;">Consolidation (T 216)</th> </tr> <tr><td colspan="4" style="text-align: center;">Trimming, Water Content, %</td></tr> <tr> <td></td> <td style="text-align: center;">Initial</td> <td style="text-align: center;">Final</td> <td></td> </tr> <tr> <td>Water Content, %</td> <td></td> <td></td> <td style="text-align: center;">Pmin</td> </tr> <tr> <td>Dry Density, lbs/ft³</td> <td></td> <td></td> <td style="text-align: center;">Pp</td> </tr> <tr> <td>Void Ratio</td> <td></td> <td></td> <td style="text-align: center;">Pmax</td> </tr> <tr> <td>Saturation, %</td> <td></td> <td></td> <td style="text-align: center;">Cc/C'c</td> </tr> <tr style="background-color: #e0e0e0;"> <th colspan="6" style="text-align: center;">Vane Shear Test on Shelby Tubes (Maine DOT)</th> </tr> <tr> <th rowspan="3" style="width: 10%;">Depth taken in tube, ft</th> <th colspan="2" style="width: 15%;">3 In.</th> <th colspan="2" style="width: 15%;">6 In.</th> <th rowspan="3" style="width: 10%;">Water Content, %</th> <th rowspan="3" style="width: 40%;">Description of Material Sampled at the Various Tube Depths</th> </tr> <tr> <th style="width: 5%;">U. Shear</th> <th style="width: 10%;">Remold</th> <th style="width: 5%;">U. Shear</th> <th style="width: 10%;">Remold</th> </tr> <tr> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> </tr> <tr><td colspan="7" style="height: 100px;"></td></tr> </tbody> </table>	Direct Shear (T 236)				Shear Angle, °				Initial Water Content, %				Normal Stress, psi				Wet Density, lbs/ft³				Dry Density, lbs/ft³				Specimen Thickness, in				Consolidation (T 216)				Trimming, Water Content, %					Initial	Final		Water Content, %			Pmin	Dry Density, lbs/ft³			Pp	Void Ratio			Pmax	Saturation, %			Cc/C'c	Vane Shear Test on Shelby Tubes (Maine DOT)						Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths	U. Shear	Remold	U. Shear	Remold	tons/ft²	tons/ft²	tons/ft²	tons/ft²								Miscellaneous Tests Liquid Limit @ 25 blows (T 89), % Plastic Limit (T 90), % Plasticity Index (T 90), % Specific Gravity, Corrected to 20°C (T 100) Loss on Ignition (T 267) <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 50%; text-align: center;">Loss, %</td> <td style="width: 50%; text-align: center;">H2O, %</td> </tr> </table> Water Content (T 265), % <p style="text-align: center; font-weight: bold;">14.1</p>	Loss, %	H2O, %
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Comments:

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Reported by: **FOGG, BRIAN** Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239983	HB-BIDD-203/6D	<u>GEOTECHNICAL (DISTURBED)</u>	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 51+79.8 Offset, ft: 239. RT Dbfg, ft: 25.0-27.0		
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	
¾ in. [19.0 mm]	100.0
½ in. [12.5 mm]	97.4
⅜ in. [9.5 mm]	96.2
¼ in. [6.3 mm]	95.8
No. 4 [4.75 mm]	95.5
No. 10 [2.00 mm]	94.1
No. 20 [0.850 mm]	92.1
No. 40 [0.425 mm]	86.9
No. 60 [0.250 mm]	76.1
No. 100 [0.150 mm]	63.4
No. 200 [0.075 mm]	49.2

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft ³			
Dry Density, lbs/ft ³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimming, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft ³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H2O, %
Water Content (T 265), %	
20.8	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft ²	tons/ft ²	tons/ft ²	tons/ft ²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239984	HB-BIDD-203/7D	GEOTECHNICAL (DISTURBED)	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 51+79.8 Offset, ft: 239. RT Dbfg, ft: 30.0-32.0		
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11)

Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	97.5
½ in. [12.5 mm]	96.6
⅜ in. [9.5 mm]	95.2
¼ in. [6.3 mm]	93.3
No. 4 [4.75 mm]	91.8
No. 10 [2.00 mm]	84.8
No. 20 [0.850 mm]	67.1
No. 40 [0.425 mm]	33.1
No. 60 [0.250 mm]	16.5
No. 100 [0.150 mm]	10.7
No. 200 [0.075 mm]	7.0

Direct Shear (T 236)

Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)

Trimblings, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests

<u>Liquid Limit @ 25 blows (T 89), %</u>
<u>Plastic Limit (T 90), %</u>
<u>Plasticity Index (T 90), %</u>
<u>Specific Gravity, Corrected to 20°C (T 100)</u>
<u>Loss on Ignition (T 267)</u>
<u>Loss, %</u> <u>H2O, %</u>
<u>Water Content (T 265), %</u>
15.0

Vane Shear Test on Shelby Tubes (Maine DOT)

Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **2/7/2011**

Paper Copy: Lab File; Project File; Geotech File



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239985	HB-BIDD-204/1D	GEOTECHNICAL (DISTURBED)	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL	Location: OTHER	Station: 51+15.5	Offset, ft: 300.	RT Dbfg, ft: 5.0-7.0
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11)

Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	100.0
1 in. [25.0 mm]	91.6
¾ in. [19.0 mm]	87.8
½ in. [12.5 mm]	75.9
⅜ in. [9.5 mm]	69.5
¼ in. [6.3 mm]	63.8
No. 4 [4.75 mm]	59.8
No. 10 [2.00 mm]	48.9
No. 20 [0.850 mm]	40.7
No. 40 [0.425 mm]	36.0
No. 60 [0.250 mm]	33.0
No. 100 [0.150 mm]	30.4
No. 200 [0.075 mm]	25.2

Direct Shear (T 236)

Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)

Trimmings, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests

Liquid Limit @ 25 blows (T 89), %
Plastic Limit (T 90), %
Plasticity Index (T 90), %
Specific Gravity, Corrected to 20°C (T 100)
Loss on Ignition (T 267)
Loss, % H ₂ O, %
Water Content (T 265), %
9.0

Vane Shear Test on Shelby Tubes (Maine DOT)

Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN**

Date Reported: **2/7/2011**

Paper Copy: Lab File; Project File; Geotech File



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239987	HB-BIDD-206/1D	GEOTECHNICAL (DISTURBED)	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 50+60	Offset, ft: 434. RT Dbfg, ft: 0.0-2.0	
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11) Wash Method <b style="color: red;">Procedure A <table border="1" style="width: 100%; border-collapse: collapse;"> <thead> <tr> <th style="width: 70%;">SIEVE SIZE U.S. [SI]</th> <th style="width: 30%;">% Passing</th> </tr> </thead> <tbody> <tr><td>3 in. [75.0 mm]</td><td></td></tr> <tr><td>1 in. [25.0 mm]</td><td style="text-align: center;">100.0</td></tr> <tr><td>¾ in. [19.0 mm]</td><td style="text-align: center;">90.4</td></tr> <tr><td>½ in. [12.5 mm]</td><td style="text-align: center;">80.6</td></tr> <tr><td>⅜ in. [9.5 mm]</td><td style="text-align: center;">79.5</td></tr> <tr><td>¼ in. [6.3 mm]</td><td style="text-align: center;">77.6</td></tr> <tr><td>No. 4 [4.75 mm]</td><td style="text-align: center;">75.8</td></tr> <tr><td>No. 10 [2.00 mm]</td><td style="text-align: center;">69.7</td></tr> <tr><td>No. 20 [0.850 mm]</td><td style="text-align: center;">60.2</td></tr> <tr><td>No. 40 [0.425 mm]</td><td style="text-align: center;">44.6</td></tr> <tr><td>No. 60 [0.250 mm]</td><td style="text-align: center;">31.0</td></tr> <tr><td>No. 100 [0.150 mm]</td><td style="text-align: center;">22.7</td></tr> <tr><td>No. 200 [0.075 mm]</td><td style="text-align: center;">16.0</td></tr> </tbody> </table>	SIEVE SIZE U.S. [SI]	% Passing	3 in. [75.0 mm]		1 in. [25.0 mm]	100.0	¾ in. [19.0 mm]	90.4	½ in. [12.5 mm]	80.6	⅜ in. [9.5 mm]	79.5	¼ in. 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Shear</th> <th style="text-align: center;">Remold</th> <th style="text-align: center;">U. Shear</th> <th style="text-align: center;">Remold</th> </tr> <tr> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> <th style="text-align: center;">tons/ft²</th> </tr> <tr> <td colspan="7" style="height: 100px;"></td> </tr> </tbody> </table>	Direct Shear (T 236)						Shear Angle, °						Initial Water Content, %						Normal Stress, psi						Wet Density, lbs/ft³						Dry Density, lbs/ft³						Specimen Thickness, in						Consolidation (T 216)						Trimming, Water Content, %							Initial	Final		Void Ratio	% Strain	Water Content, %			Pmin			Dry Density, lbs/ft³			Pp			Void Ratio			Pmax			Saturation, %			Cc/C'c			Vane Shear Test on Shelby Tubes (Maine DOT)						Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths	U. Shear	Remold	U. Shear	Remold	tons/ft²	tons/ft²	tons/ft²	tons/ft²								Miscellaneous Tests <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="text-align: center;">Liquid Limit @ 25 blows (T 89), %</td> </tr> <tr> <td style="text-align: center;">Plastic Limit (T 90), %</td> </tr> <tr> <td style="text-align: center;">Plasticity Index (T 90), %</td> </tr> <tr> <td style="text-align: center;">Specific Gravity, Corrected to 20°C (T 100)</td> </tr> <tr> <td style="text-align: center;">Loss on Ignition (T 267)</td> </tr> <tr> <td style="text-align: center;">Loss, % H2O, %</td> </tr> <tr> <td style="text-align: center;">Water Content (T 265), %</td> </tr> <tr> <td style="text-align: center;">7.2</td> </tr> </table>	Liquid Limit @ 25 blows (T 89), %	Plastic Limit (T 90), %	Plasticity Index (T 90), %	Specific Gravity, Corrected to 20°C (T 100)	Loss on Ignition (T 267)	Loss, % H2O, %	Water Content (T 265), %	7.2
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Comments:

AUTHORIZATION AND DISTRIBUTION

Reported by: **FOGG, BRIAN** Date Reported: **2/7/2011**



GEOTECHNICAL TEST REPORT

Central Laboratory

SAMPLE INFORMATION

Reference No.	Boring No./Sample No.	Sample Description	Sampled	Received
239988	HB-BIDD-206/2D	GEOTECHNICAL (DISTURBED)	1/19/2011	2/1/2011
Sample Type: GEOTECHNICAL Location: OTHER		Station: 50+60	Offset, ft: 434. RT Dbfg, ft: 5.0-7.0	
PIN: 014814.00 Town: Biddeford		Sampler: GROSS, KAREN L		

TEST RESULTS

Sieve Analysis (T 27, T 11)	
Wash Method	
Procedure A	
SIEVE SIZE U.S. [SI]	% Passing
3 in. [75.0 mm]	
1 in. [25.0 mm]	100.0
¾ in. [19.0 mm]	92.6
½ in. [12.5 mm]	90.4
⅜ in. [9.5 mm]	89.2
¼ in. [6.3 mm]	86.3
No. 4 [4.75 mm]	84.2
No. 10 [2.00 mm]	74.0
No. 20 [0.850 mm]	54.9
No. 40 [0.425 mm]	30.3
No. 60 [0.250 mm]	15.2
No. 100 [0.150 mm]	9.8
No. 200 [0.075 mm]	6.3

Direct Shear (T 236)			
Shear Angle, °			
Initial Water Content, %			
Normal Stress, psi			
Wet Density, lbs/ft³			
Dry Density, lbs/ft³			
Specimen Thickness, in			

Consolidation (T 216)					
Trimming, Water Content, %					
	Initial	Final		Void Ratio	% Strain
Water Content, %			Pmin		
Dry Density, lbs/ft³			Pp		
Void Ratio			Pmax		
Saturation, %			Cc/C'c		

Miscellaneous Tests	
Liquid Limit @ 25 blows (T 89), %	
Plastic Limit (T 90), %	
Plasticity Index (T 90), %	
Specific Gravity, Corrected to 20°C (T 100)	
Loss on Ignition (T 267)	
Loss, %	H2O, %
Water Content (T 265), %	
3.7	

Vane Shear Test on Shelby Tubes (Maine DOT)						
Depth taken in tube, ft	3 In.		6 In.		Water Content, %	Description of Material Sampled at the Various Tube Depths
	U. Shear	Remold	U. Shear	Remold		
	tons/ft²	tons/ft²	tons/ft²	tons/ft²		

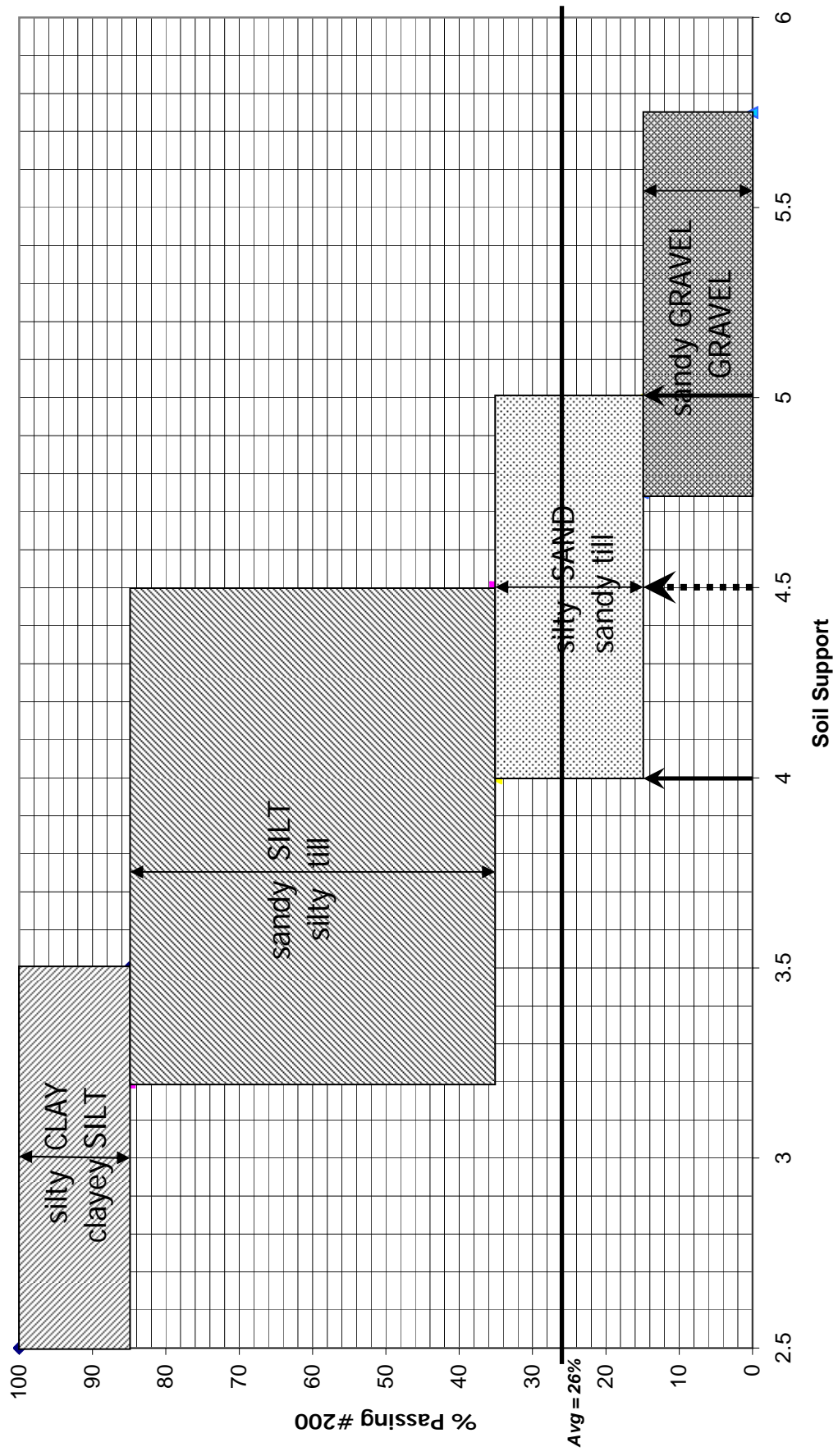
Comments:

AUTHORIZATION AND DISTRIBUTION

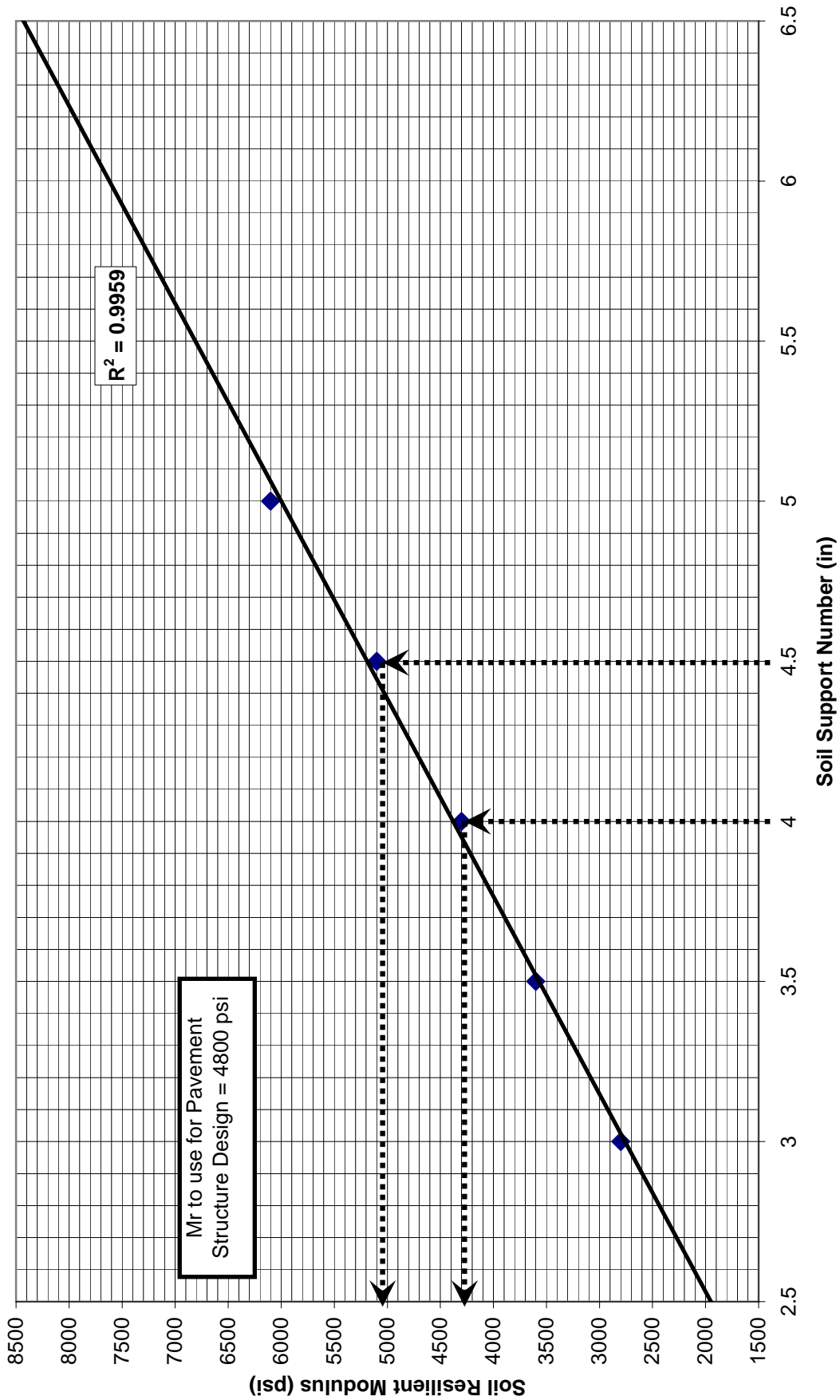
Reported by: **FOGG, BRIAN**

Date Reported: **2/7/2011**

Guidelines for Selection of Soil Support Values for Pavement Design

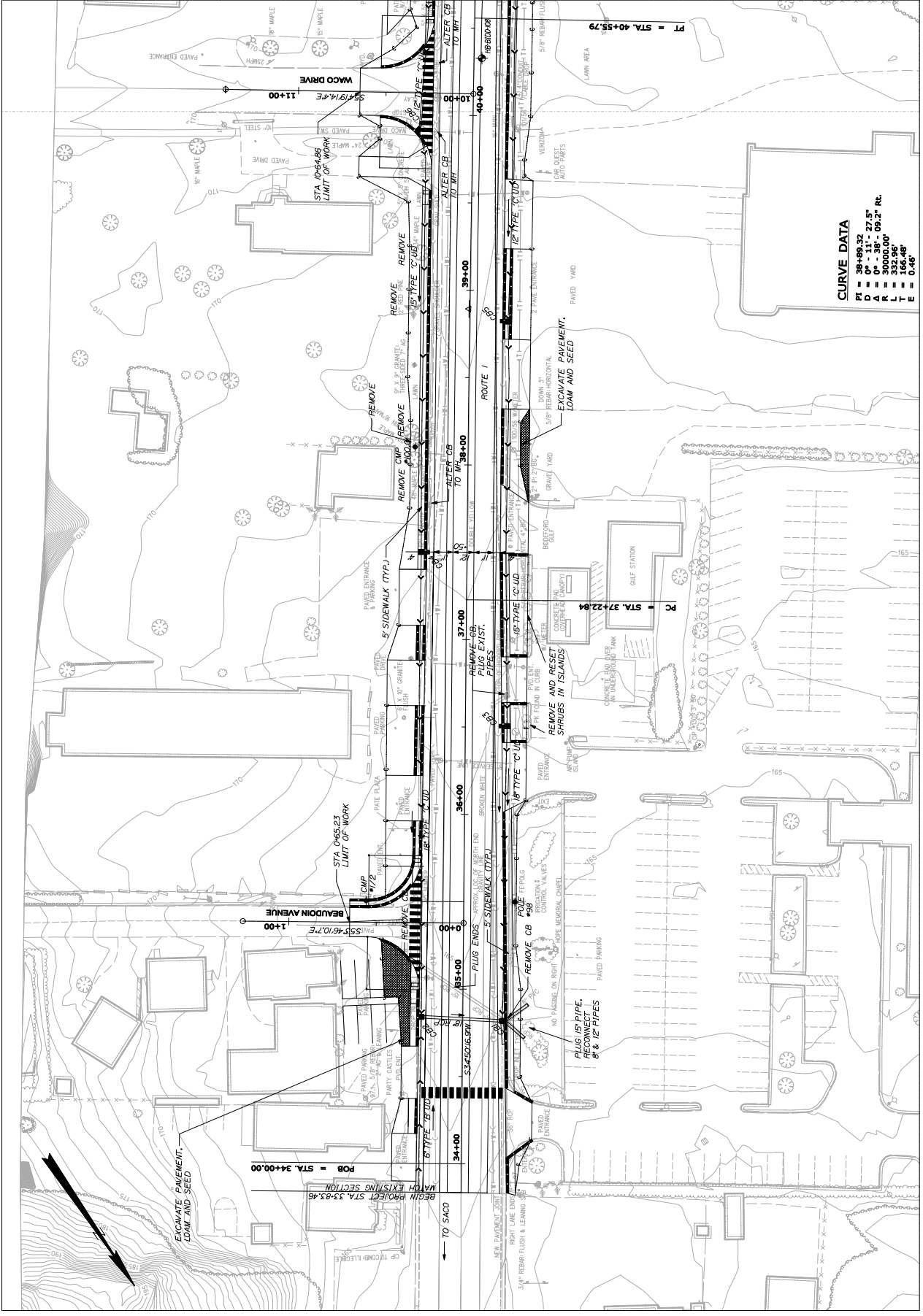


Soil Resilient Modulus for DARWin Design



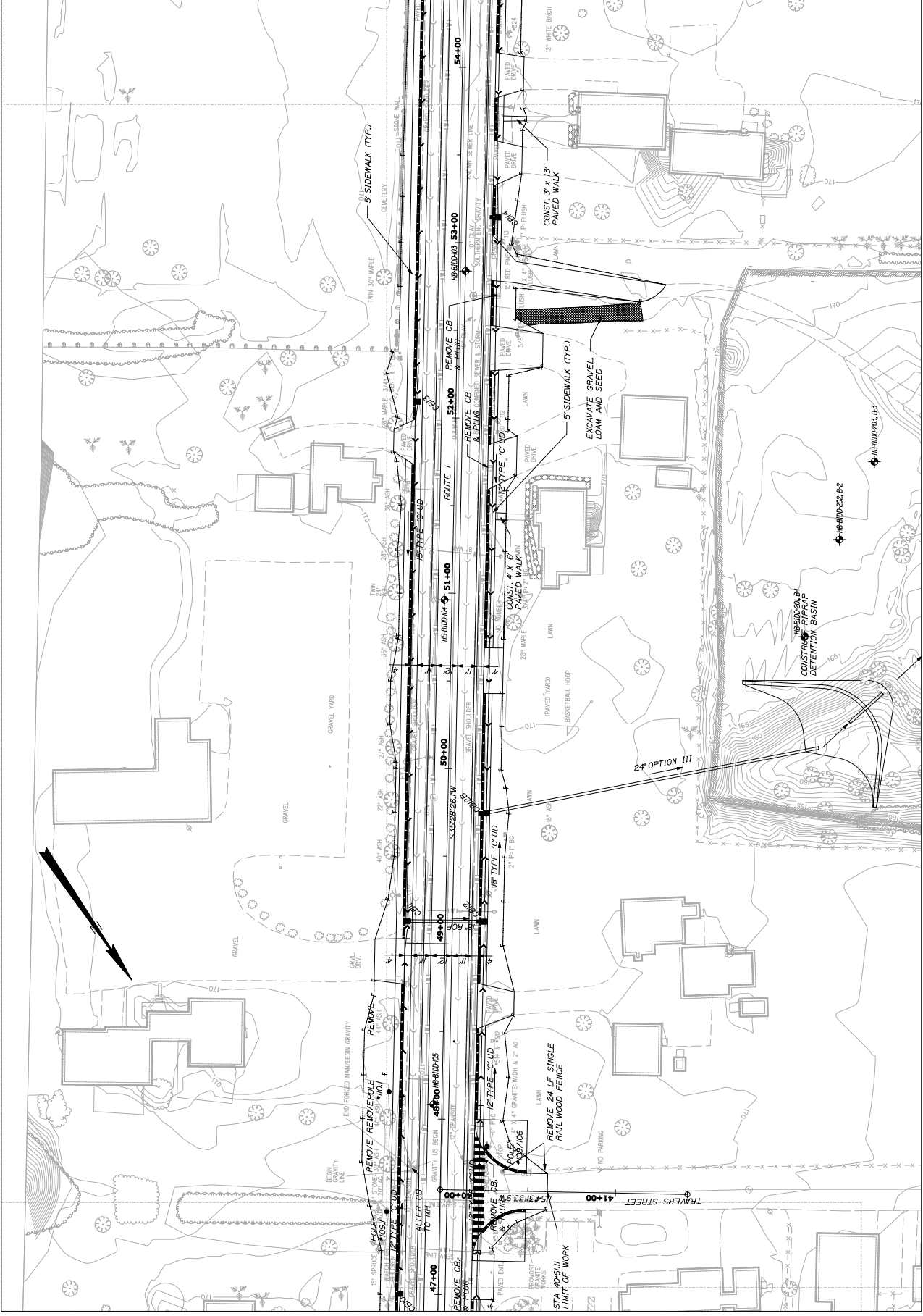
NO.	DATE	BY	DESCRIPTION
1			DESIGN REVIEW
2			CHECKED
3			DESIGNED
4			REVISIONS
5			REVISIONS
6			REVISIONS
7			REVISIONS
8			REVISIONS
9			REVISIONS
10			REVISIONS

BIDDEFORD
ROUTE 1
GEOPANS



CURVE DATA

PI	= 38+489.32
D	= 0° - 11' - 27.5"
A	= 0° - 38' - 05.2" Rt.
L	= 333.00'
T	= 166.48'
E	= 0.46'



PROJ. NUMBER	BY	DATE
14814.00	K.ROSS	AUG 2010
14814.00	WHITE	AUG 2010

CHECKED-REVIEWED	SIGNATURE	DATE
14814.00	[Signature]	[Date]
14814.00	[Signature]	[Date]

REVISIONS	DATE
14814.00	[Date]
14814.00	[Date]

STATE OF MAINE
DEPARTMENT OF TRANSPORTATION
STP-1481(400)X
PIN
14814.00
HIGHWAY PLANS

DATE	BY	DESCRIPTION

BIDDEFORD
ROUTE 1
GEOLANS

SHEET NUMBER
5
OF 6

