# MAINE DEPARTMENT OF TRANSPORTATION
# HIGHWAY PROGRAM
# GEOTECHNICAL SECTION
# AUGUSTA, MAINE

## GEOTECHNICAL DESIGN REPORT

*For the Construction of*

**EAST BAY BRIDGE**
**ROUTE 1**
**PERRY, MAINE**


*Prepared by:*
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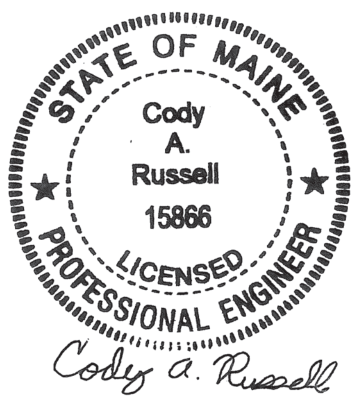



*Reviewed by:*
Cody Russell, P.E.
Senior Geotechnical Engineer



Washington County
WIN 26630.11

Soils Report 2025-32
Bridge No. 6775

August 1, 2025

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## 1.0 INTRODUCTION

The purpose of this Geotechnical Design Report is to present subsurface information and make geotechnical recommendations for the replacement of an existing cross culvert (#88081) on Route 1 in Perry. A subsurface investigation has been completed at the site to evaluate subsurface conditions and to develop geotechnical design and construction recommendations for the replacement structure. This report presents the subsurface information obtained during the subsurface investigation and soil laboratory testing programs and provides design and construction recommendations and geotechnical design parameters for the culvert replacement.

The existing structure consists of an approximately 48-inch diameter, 88-foot long precast concrete pipe culvert. The precast concrete pipe culvert is in poor condition and needs replacement both from an infrastructure and environmental standpoint. Route 1 is a Highway Corridor Priority 2 road.

The proposed replacement structure will be an approximately 14-foot span by 8-foot rise by 83-foot-long precast concrete box culvert. The invert of the proposed culvert is approximately 12.8 feet below the existing road grade at the roadway centerline. The roadway embankment slopes at the proposed culvert inlet and outlet shall be no steeper than 2H:1V to protect against erosion.

## 2.0 GEOLOGIC SETTING

The existing culvert carries an unnamed stream under Route 1 in Perry and is located approximately 0.21 of a mile east of Burby Road as shown on Sheet 1 – Location Map.

According to the Maine Geological Survey (MGS) map titled Surficial Geology of the Eastport Quadrangle, Maine, Open File 75-2 (1975) the surficial soils at the site consist of Presumpscot Formation. Presumpscot Formation consists of silt, clay, and sand.

According to the map titled Bedrock Geologic Map of Maine (1985) published by the MGS, the bedrock in the vicinity of the site consists of mafic to felsic volcanic rocks of the Eastport Formation Mafic to Felsic Volcanic Member.

## 3.0 SUBSURFACE INVESTIGATION

One (1) boring (HB-PER-101) and one (1) probe (HB-PER-102) were drilled for this project on October 26, 2023 by the MaineDOT drill crew using a trailer-mounted drill rig. Exploration locations are shown on Sheet 2 – Boring Location Plan & Interpretive Subsurface Profile. Details and sampling methods used, field data obtained, and soil and groundwater conditions encountered are presented on the Boring Logs in Appendix A.

Boring HB-PEM-101 was drilled using solid stem auger, cased wash boring, and open hole drilling techniques. Soil samples were obtained at 5-foot intervals using Standard Penetration Test (SPT) methods. The MaineDOT drill rig is equipped with an automatic hammer to drive the split spoon. The MaineDOT calibrated automatic hammer delivers approximately 51 percent more energy during driving than the standard rope and cathead system. All N-values discussed in this report are corrected values ($N_{60}$) computed by applying an average energy transfer factor of 0.906 to the raw field N-values. Probe HB-PER-102 was drilled using solid stem auger techniques. No soil samples were obtained in the probe.

The MaineDOT Geotechnical Team member selected the boring and probe locations, drilling methods, designated type and depth of sampling, reviewed field logs for accuracy and identified field and laboratory testing requirements. A NorthEast Transportation Training and Certification (NETTCP) certified Subsurface Investigator logged the subsurface conditions encountered. The boring and probe were located in the field by taping to surveyed site features after completion of the drilling program.

## 4.0 Laboratory Testing

A laboratory testing program was conducted to assist in soil classification, evaluation of engineering properties of the soils and geologic assessment of the project site. Laboratory testing consisted of two (2) standard grain size analyses with natural water content, two (2) standard grain size analyses with hydrometer and natural water content, and two (2) Atterberg Limits tests. The results of the laboratory testing program are discussed in the following section and are included in Appendix B – Laboratory Test Results. Laboratory test information is also shown on the Boring Logs in Appendix A.

## 5.0 Subsurface Conditions

Subsurface conditions encountered in the test boring and probe generally consisted of gravelly sand fill underlain by native silty clay underlain by sandy gravel. An interpretive subsurface profile depicting the generalized soil stratigraphy at the boring location is shown on Sheet 2 – Boring Location Plan & Interpretive Subsurface Profile.

Boring HB-PER-101 was drilled to depth of approximately 22.0 feet below ground surface (bgs) where a refusal surface was encountered. The exact nature of the refusal surface was not determined in the boring. Probe HB-PER-102 was drilled to depth of approximately 20.0 feet bgs without encountering a refusal surface.

The table below summarizes the field and laboratory information obtained in boring HB-PER-101:

| Approx. Depth BGS[1] (feet) | Soil Description | AASHTO[2] Classification | USCS[3] | WC%[4] |
|---|---|---|---|---|
| 0.0 – 8.5 | Fill:<br>Brown, moist to wet, gravelly fine to coarse sand, trace silt. | A-1-a | SW-SM | 5.4 |
| 8.5 – 20.5 | Olive, wet, silty clay, little gravel, trace fine to coarse sand.<br>Cobbles from 18.0 – 18.5 feet bgs. | A-6 | CL | 18.2 to 19.1 |

| | | | | |
|---|---|---|---|---|
| 20.5 – 22.0 | Brown, wet, fine to coarse sandy gravel, trace silt, occasional cobbles. | A-1-a | GW | 3.8 |

[1]BGS = below ground surface
[2]AASHTO = American Association of State Highway and Transportation Officials
[3]USCS = Unified Soil Classification System
[4]WC% = Water content in percent

Two (2) $N_{60}$-values obtained in the gravelly sand fill were 17 blows per foot (bpf) and 42 bpf, indicating that the fill is medium dense to dense in consistency. Two (2) $N_{60}$-values obtained in the native silty clay were 32 bpf and 41 bpf, indicating that the silty clay is hard in consistency.

The following table summarizes the results of Atterberg Limits tests done on two (2) samples of the silty clay:

| Boring No. and Sample No. | Water Content (%) | Liquid Limit | Plastic Limit | Plasticity Index | Liquidity Index |
|---|---|---|---|---|---|
| HB-PER-101 3D | 18.2 | 35 | 22 | 13 | -0.29 |
| HB-PER-101 4D | 19.1 | 34 | 21 | 13 | -0.15 |

Interpretation of these results indicate that the silty clay has medium plasticity. The silty clay in samples 3D and 4D from boring HB-PER-101 are some to heavily overconsolidated.

Groundwater was recorded at depth 4.5 feet bgs in boring HB-PER-101. Groundwater levels can be expected to fluctuate subject to seasonal variations, local soil conditions, topography, precipitation, and construction activity.

# 6.0 GEOTECHNICAL DESIGN AND CONSTRUCTION RECOMMENDATIONS

The following sections discuss geotechnical recommendations for the design and construction of the proposed culvert.

## 6.1 Precast Concrete Box Culvert Design and Construction

The proposed replacement structure will consist of a 14-foot span by 8-foot rise by 83-foot-long precast concrete box culvert. The proposed box culvert shall be designed and constructed in accordance with MaineDOT Standard Specification 534.

The approximate invert of the proposed culvert ranges from an elevation of 19.7 feet at the inlet to 16.6 feet at the outlet with a 3.6% slope. To facilitate fish passage, Habitat Connectivity Design elements will be used inside the precast concrete box culvert as shown on the Streambed Details Sheet in the Plans.

The full nature of the culvert bearing surface will not become evident until the culvert excavation is made. Any cobbles or boulders in excess of 6 inches encountered at the bedding elevation shall be removed and replaced with compacted Granular Borrow Material for Underwater Backfill or Crushed Stone ¾-Inch. Any disturbed soils at the bedding elevation resulting from excavation activities should be removed by hand prior to placement of the bedding material. The prepared subgrade shall be proof rolled using a static roller to visually confirm the prepared subgrade is firm and stable. The exposed subgrade shall be free of ponded water so that bedding material placement and compaction can be completed in the dry.

The proposed structure shall be bedded on a 1-foot-thick layer of Granular Borrow, Material for Underwater Backfill meeting the requirements of MaineDOT Standard Specification 703.19. The soil envelope and backfill shall consist of Standard Specification 703.19 - Granular Borrow with a maximum particle size of 4 inches. The Granular Borrow bedding and backfill material shall be placed in lifts of 6 to 8 inches loose measure and compacted to the manufacturer's specifications or, in the absence of manufacturer's specifications, the bedding and backfill soil shall be compacted to at least 92 percent of the AASHTO T-180 maximum dry density.

### 6.2 Settlement

No settlement issues are anticipated at the site. The proposed precast concrete box culvert is larger than the existing culvert and will result in a net unloading of the site soils at the proposed structure location. Placement of fill soils at the location of the existing structure is not anticipated to exceed the past loading condition of the site soils. Any settlement due to elastic compression of the bedding material will be immediate and negligible.

### 6.3 Bearing Resistance

The factored bearing resistances for the precast concrete box culvert bearing on compacted granular bedding material placed on native soils and/or bedrock at the service and strength limit states are presented in the table below. Supporting calculations in accordance with AASHTO LRFD Bridge Design Specifications 10th Edition 2024 (LRFD) are provided in Appendix C – Calculations.

| Limit State | Resistance Factor $\varphi_b$ | AASHTO LRFD Reference | Factored Bearing Resistance (ksf) |
|---|---|---|---|
| Service | 1.0 | Article 10.5.5.1 | 6.0 |
| Strength | 0.45 | Table 10.5.5.2.2-1 | 14.0 |

### 6.4 Modulus of Subgrade Reaction

A modulus of subgrade reaction ($k_s$) equal to 180 pounds per cubic inch shall be used for the structural design of the box culvert's base slab. Calculations are included in Appendix C – Calculations.

### 6.5 Scour and Riprap

Both the inlet and outlet of the precast concrete box culvert shall be protected against scour with riprap conforming to MaineDOT Standard Specification Section 703.26 Plain and Hand Laid Riprap. Slopes shall be no steeper than 2H:1V on the inlet and outlet end. No specific scour protection recommendations are needed other than armoring with riprap. The riprap on the slopes shall be underlain by a 1-foot layer of protective aggregate cushion consisting of Granular Borrow Material for Underwater Backfill (703.19) that is underlain by a non-woven, Class 1 Erosion Control Geotextile meeting the requirements of MaineDOT Standard Specification 722.03. The toe of the riprap sections shall be keyed into the existing soils 1 foot below the streambed elevation.

### 6.6 Seismic Design Considerations

In conformance with LRFD Article 3.10.1, seismic analysis is not required for buried structures, except where they cross active faults. There are no known active faults in Maine; therefore, seismic analysis is not required.

### 6.7 Construction Considerations

Construction activities may include construction of cofferdams and earth support systems to control stream flow during construction. Construction activities will also include common earth excavation. Construction of the proposed precast concrete box culvert will require deep soil excavation. Earth support systems shall be implemented if laying back slopes is not feasible. It is likely that the use of complex (four-sided) braced excavations with dewatering will be necessary due to the depth of the excavation. If this is the case, adequate embedment into soil will be necessary to allow for the excavation and maintenance of a stable excavation bottom. All earth support systems shall be designed by a Professional Engineer licensed in the State of Maine. Regardless of the method of excavation, all excavations and earth support systems shall meet all applicable OSHA regulations.

The Contractor shall control groundwater and surface water infiltration using temporary ditches, sumps, granular drainage blankets, stone ditch protection or hand-laid riprap with geotextile underlayment to divert groundwater and surface water as needed to maintain a stable excavation and allow work in the dry.

Using the excavated native soils as backfill around the culvert shall not be permitted. The native soils may only be used as common borrow in accordance with MaineDOT Standard Specifications 203 and 703.

The Contractor will have to excavate the existing subbase and subgrade fill soils in the vicinity of the culvert. These materials should not be used to re-base the roadway. Excavated subbase sand and gravel may be used as fill below roadway subgrade level in fill areas provided all other requirements of MaineDOT Standard Specifications 203 and 703 are met.

## 7.0 CLOSURE

This report has been prepared for the use of the MaineDOT Highway Program for specific application to the proposed replacement of an existing cross culvert (#88081) under Route 1 in Perry, Maine in accordance with generally accepted geotechnical and foundation engineering practices. No other intended use or warranty is expressed or implied.

In the event that any changes in the nature, design, or location of the proposed project are planned, this report should be reviewed by a geotechnical engineer to assess the appropriateness of the conclusions and recommendations and to modify the recommendations as appropriate to reflect the changes in design. These analyses and recommendations are based in part upon a limited subsurface investigation at discrete exploratory location completed at the site. If variations from the conditions encountered during the investigation appear evident during construction, it may also become necessary to re-evaluate the recommendations made in this report.

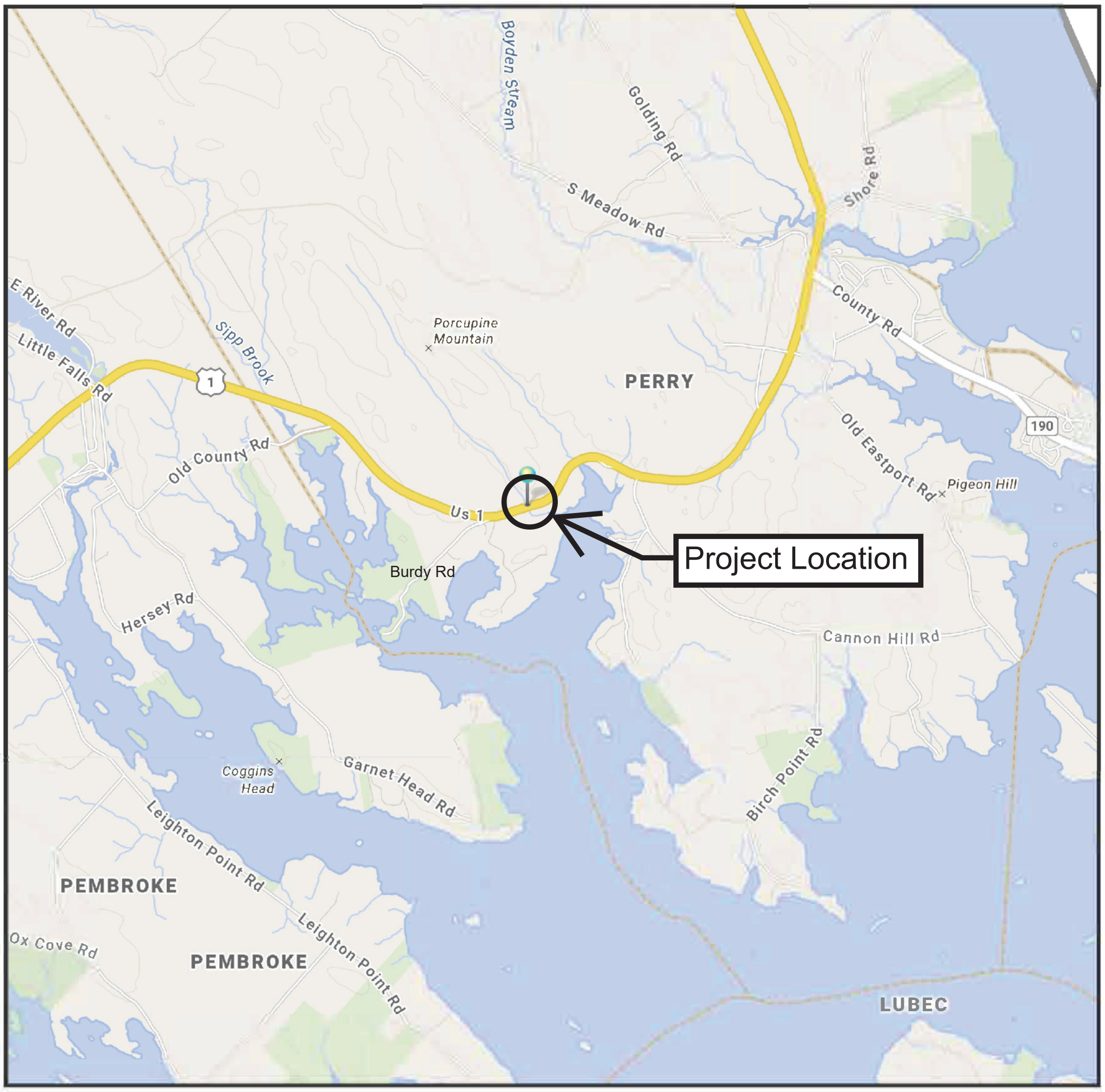
It is recommended that a geotechnical engineer be provided the opportunity for a review of the design and specifications in order that the earthwork and foundation recommendations and construction considerations presented in this report are properly interpreted and implemented in the design and specifications.

**Sheets**

Date: 7/23/2025

Username: Terry.White

# PERRY, MAINE

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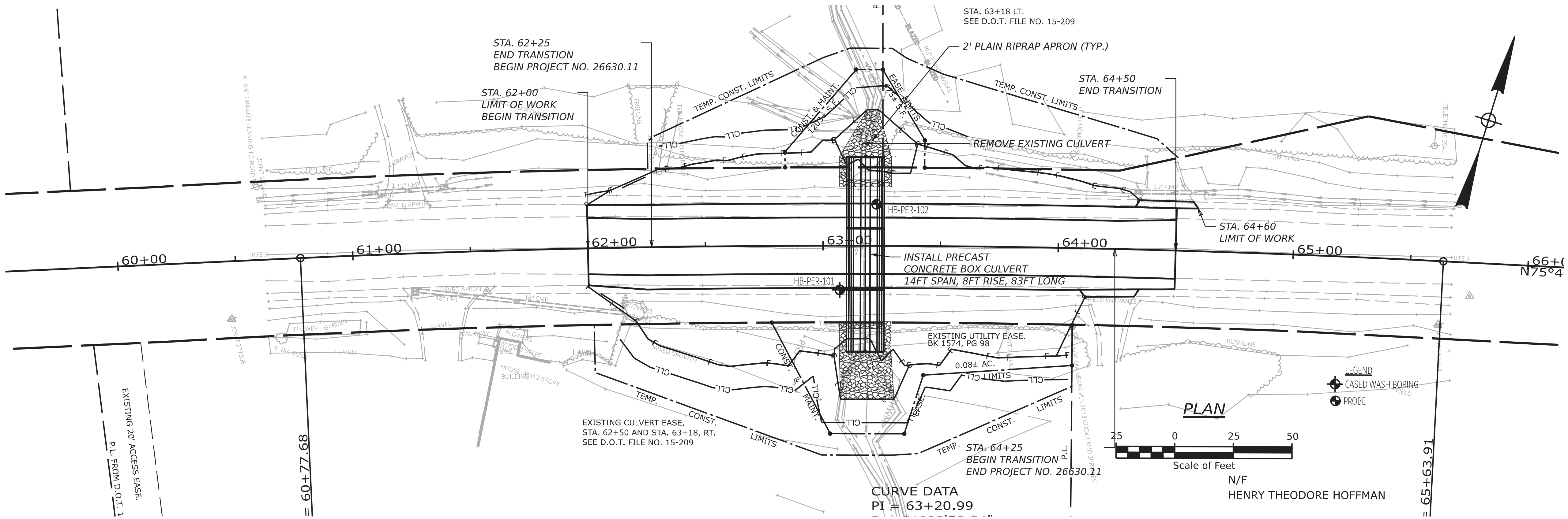
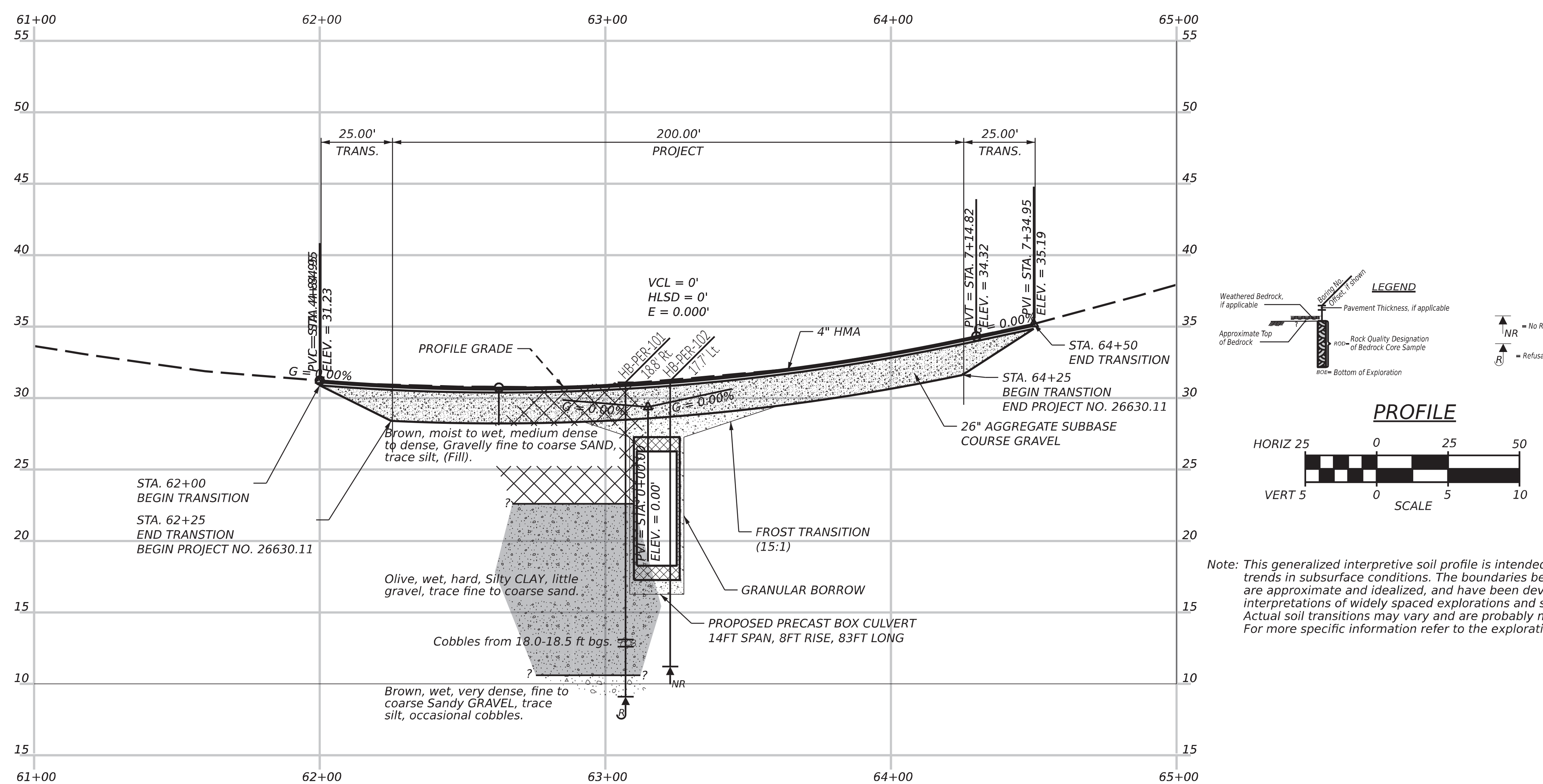
1 Miles

1 inch =1.14 miles

Date: 7/23/2025
Time: 7:47:11 AM

| SHEET NUMBER | PERRY | STATE OF MAINE DEPARTMENT OF TRANSPORTATION |
|---|---|---|
| 1 | U.S. ROUTE 1 | 2663011 |
| OF 2 | LOCATION MAP | WIN 26630.11 HIGHWAY PLANS |




Note: This generalized interpretive soil profile is intended to convey trends in subsurface conditions. The boundaries between strata are approximate and idealized, and have been developed by interpretations of widely spaced explorations and samples. Actual soil transitions may vary and are probably more erratic. For more specific information refer to the exploration logs.

STATE OF MAINE
DEPARTMENT OF TRANSPORTATION

2663011

26630.11

HIGHWAY PLANS

PERRY
U.S. ROUTE 1

BORING LOCATION PLAN &
INTERPRETIVE SUBSURFACE PROFILE

SHEET NUMBER
2
OF 2

Username: Yueh-Ti.Lee
Date: 8/8/2025

Filename: C:\Users\Yueh-Ti.Lee\State of Maine\MaineDOT Work - WIN\26630_11\GEOTECH\PlanProfile_2663011 Proposed GEOTECH.dgn

# Appendix A

Boring Logs

## UNIFIED SOIL CLASSIFICATION SYSTEM

| MAJOR DIVISIONS | | | GROUP SYMBOLS | TYPICAL NAMES |
|---|---|---|---|---|
| COARSE-GRAINED SOILS (more than half of material is larger than No. 200 sieve size) | GRAVELS (more than half of coarse fraction is larger than No. 4 sieve size) | CLEAN GRAVELS (little or no fines) | GW | Well-graded gravels, gravel-sand mixtures, little or no fines. |
| | | | GP | Poorly-graded gravels, gravel sand mixtures, little or no fines. |
| | | GRAVEL WITH FINES (Appreciable amount of fines) | GM | Silty gravels, gravel-sand-silt mixtures. |
| | | | GC | Clayey gravels, gravel-sand-clay mixtures. |
| | SANDS (more than half of coarse fraction is smaller than No. 4 sieve size) | CLEAN SANDS (little or no fines) | SW | Well-graded sands, Gravelly sands, little or no fines |
| | | | SP | Poorly-graded sands, Gravelly sand, little or no fines. |
| | | SANDS WITH FINES (Appreciable amount of fines) | SM | Silty sands, sand-silt mixtures |
| | | | SC | Clayey sands, sand-clay mixtures. |
| FINE-GRAINED SOILS (more than half of material is smaller than No. 200 sieve size) | SILTS AND CLAYS (liquid limit less than 50) | | ML | Inorganic silts and very fine sands, rock flour, Silty or Clayey fine sands, or Clayey silts with slight plasticity. |
| | | | CL | Inorganic clays of low to medium plasticity, Gravelly clays, Sandy clays, Silty clays, lean clays. |
| | | | OL | Organic silts and organic Silty clays of low plasticity. |
| | SILTS AND CLAYS (liquid limit greater than 50) | | MH | Inorganic silts, micaceous or diatomaceous fine Sandy or Silty soils, elastic silts. |
| | | | CH | Inorganic clays of high plasticity, fat clays. |
| | | | OH | Organic clays of medium to high plasticity, organic silts. |
| | HIGHLY ORGANIC SOILS | | Pt | Peat and other highly organic soils. |

**Desired Soil Observations (in this order, if applicable):**

Color (Munsell color chart)
Moisture (dry, damp, moist, wet)
Density/Consistency (from above right hand side)
Texture (fine, medium, coarse, etc.)
Name (Sand, Silty Sand, Clay, etc., including portions - trace, little, etc.)
Gradation (well-graded, poorly-graded, uniform, etc.)
Plasticity (non-plastic, slightly plastic, moderately plastic, highly plastic)
Structure (layering, fractures, cracks, etc.)
Bonding (well, moderately, loosely, etc., )
Cementation (weak, moderate, or strong)
Geologic Origin (till, marine clay, alluvium, etc.)
Groundwater level

## MODIFIED BURMISTER SYSTEM

| Descriptive Term | Portion of Total (%) |
|---|---|
| trace | 0 - 10 |
| little | 11 - 20 |
| some | 21 - 35 |
| adjective (e.g. Sandy, Clayey) | 36 - 50 |

## TERMS DESCRIBING DENSITY/CONSISTENCY

**Coarse-grained soils** (more than half of material is larger than No. 200 sieve): Includes (1) clean gravels; (2) Silty or Clayey gravels; and (3) Silty, Clayey or Gravelly sands. Density is rated according to standard penetration resistance (N-value).

| Density of Cohesionless Soils | Standard Penetration Resistance N-Value (blows per foot) |
|---|---|
| Very loose | 0 - 4 |
| Loose | 5 - 10 |
| Medium Dense | 11 - 30 |
| Dense | 31 - 50 |
| Very Dense | > 50 |

**Fine-grained soils** (more than half of material is smaller than No. 200 sieve): Includes (1) inorganic and organic silts and clays; (2) Gravelly, Sandy or Silty clays; and (3) Clayey silts. Consistency is rated according to undrained shear strength as indicated.

| Consistency of Cohesive soils | SPT N-Value (blows per foot) | Approximate Undrained Shear Strength (psf) | Field Guidelines |
|---|---|---|---|
| Very Soft | WOH, WOR, WOP, <2 | 0 - 250 | Fist easily penetrates |
| Soft | 2 - 4 | 250 - 500 | Thumb easily penetrates |
| Medium Stiff | 5 - 8 | 500 - 1000 | Thumb penetrates with moderate effort |
| Stiff | 9 - 15 | 1000 - 2000 | Indented by thumb with great effort |
| Very Stiff | 16 - 30 | 2000 - 4000 | Indented by thumbnail |
| Hard | >30 | over 4000 | Indented by thumbnail with difficulty |

**Rock Quality Designation (RQD):**

$$RQD\ (\%) = \frac{\text{sum of the lengths of intact pieces of core* > 4 inches}}{\text{length of core advance}}$$

*Minimum NQ rock core (1.88 in. OD of core)

**Rock Quality Based on RQD**

| Rock Quality | RQD (%) |
|---|---|
| Very Poor | ≤25 |
| Poor | 26 - 50 |
| Fair | 51 - 75 |
| Good | 76 - 90 |
| Excellent | 91 - 100 |

**Desired Rock Observations (in this order, if applicable):**

Color (Munsell color chart)
Texture (aphanitic, fine-grained, etc.)
Rock Type (granite, schist, sandstone, etc.)
Hardness (very hard, hard, mod. hard, etc.)
Weathering (fresh, very slight, slight, moderate, mod. severe, severe, etc.)
Geologic discontinuities/jointing:
- -dip (horiz - 0-5 deg., low angle - 5-35 deg., mod. dipping - 35-55 deg., steep - 55-85 deg., vertical - 85-90 deg.)
- -spacing (very close - <2 inch, close - 2-12 inch, mod. close - 1-3 feet, wide - 3-10 feet, very wide >10 feet)
- -tightness (tight, open, or healed)
- -infilling (grain size, color, etc.)

Formation (Waterville, Ellsworth, Cape Elizabeth, etc.)
RQD and correlation to rock quality (very poor, poor, etc.)
ref: ASTM D6032 and FHWA NHI-16-072 GEC 5 - Geotechnical Site Characterization, Table 4-12
Recovery (inch/inch and percentage)
Rock Core Rate (X.X ft - Y.Y ft (min:sec))

***Maine Department of Transportation***
***Geotechnical Section***
**Key to Soil and Rock Descriptions and Terms**
Field Identification Information

**Sample Container Labeling Requirements:**

| | |
|---|---|
| WIN | Blow Counts |
| Bridge Name / Town | Sample Recovery |
| Boring Number | Date |
| Sample Number | Personnel Initials |
| Sample Depth | |

| Maine Department of Transportation<br>Soil/Rock Exploration Log<br>US CUSTOMARY UNITS | Project: Route 1 Large Culvert Replacement<br>Location: Perry, Maine | Boring No.: HB-PER-101<br>WIN: 26630.11 |
|---|---|---|

| | | | | | |
|---|---|---|---|---|---|
| **Driller:** | MaineDOT | **Elevation (ft.)** | 31.1 | **Auger ID/OD:** | 5" Solid Stem |
| **Operator:** | Daggett/Andrle | **Datum:** | NAVD88 | **Sampler:** | Standard Split Spoon |
| **Logged By:** | B. Wilder | **Rig Type:** | CME 45C | **Hammer Wt./Fall:** | 140#/30" |
| **Date Start/Finish:** | 10/26/2023; 09:00-12:00 | **Drilling Method:** | Cased Wash Boring | **Core Barrel:** | N/A |
| **Boring Location:** | 63+07.1, 18.8 ft Rt. | **Casing ID/OD:** | NW-3" | **Water Level*:** | 4.5 ft bgs. |
| **Hammer Efficiency Factor:** | 0.906 | **Hammer Type:** | Automatic ☒ Hydraulic ☐ Rope & Cathead ☐ | | |

Definitions:
D = Split Spoon Sample
MD = Unsuccessful Split Spoon Sample Attempt
U = Thin Wall Tube Sample
MU = Unsuccessful Thin Wall Tube Sample Attempt
V = Field Vane Shear Test, PP = Pocket Penetrometer
MV = Unsuccessful Field Vane Shear Test Attempt
R = Rock Core Sample
SSA = Solid Stem Auger
HSA = Hollow Stem Auger
RC = Roller Cone
WOH = Weight of 140lb. Hammer
WOR/C = Weight of Rods or Casing
WO1P = Weight of One Person
$S_u$ = Peak/Remolded Field Vane Undrained Shear Strength (psf)
$S_{u(lab)}$ = Lab Vane Undrained Shear Strength (psf)
$q_p$ = Unconfined Compressive Strength (ksf)
N-uncorrected = Raw Field SPT N-value
Hammer Efficiency Factor = Rig Specific Annual Calibration Value
$N_{60}$ = SPT N-uncorrected Corrected for Hammer Efficiency
$N_{60}$ = (Hammer Efficiency Factor/60%)*N-uncorrected
$T_v$ = Pocket Torvane Shear Strength (psf)
WC = Water Content, percent
LL = Liquid Limit
PL = Plastic Limit
PI = Plasticity Index
G = Grain Size Analysis
C = Consolidation Test

| Depth (ft.) | Sample No. | Pen./Rec. (in.) | Sample Depth (ft.) | Blows (/6 in.) Shear Strength (psf) or RQD (%) | N-uncorrected | $N_{60}$ | Casing Blows | Elevation (ft.) | Graphic Log | Visual Description and Remarks | Laboratory Testing Results/ AASHTO and Unified Class. |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 1D | 24/12 | 0.00 - 2.00 | 14/14/14/9 | 28 | 42 | SSA | | | Brown, moist, dense, Gravelly fine to coarse SAND, trace silt, (Fill). | G#379694<br>A-1-a, SW-SM<br>WC=5.4% |
| | 2D | 24/14 | 4.00 - 6.00 | 7/7/4/3 | 11 | 17 | | | | Brown, wet, medium dense, Gravelly fine to coarse SAND, trace silt, (Fill). | |
| 5 | | | | | | | | | | | |
| | | | | | | | | 22.6 | | 8.5 | |
| 10 | 3D | 24/12 | 10.00 - 12.00 | 13/11/10/10 | 21 | 32 | 39 | | | Olive, wet, hard, Silty CLAY, little gravel, trace fine to coarse sand. | G#379695<br>A-6, CL<br>WC=18.2%<br>LL=35<br>PL=22<br>PI=13 |
| | | | | | | | 37 | | | | |
| | | | | | | | 55 | | | | |
| | | | | | | | 118 | | | | |
| | | | | | | | 109 | | | | |
| 15 | 4D | 24/20 | 15.00 - 17.00 | 9/12/15/21 | 27 | 41 | OPEN HOLE | | | Olive, wet, hard, Silty CLAY, trace fine sand. | G#379696<br>A-6, CL<br>WC=19.1%<br>LL=34<br>PL=21<br>PI=13 |
| | | | | | | | | | | Cobble from 18.0-18.5 ft bgs. | |
| 20 | 5D | 9.6/5 | 20.50 - 21.30 | 38/50(3.6") | --- | | | 10.6 | | 20.5<br>Brown, wet, very dense, fine to coarse Sandy GRAVEL, trace silt.<br>Roller Coned ahead to 22.0 ft bgs, cobbles and gravel. | G#379697<br>A-1-a, GW<br>WC=3.8% |
| | | | | | | | | 9.1 | | 22.0<br>**Bottom of Exploration at 22.0 feet below ground surface.**<br>Possible REFUSAL, very dense. | |
| 25 | | | | | | | | | | | |

**Remarks:**

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

# Maine Department of Transportation

Soil/Rock Exploration Log
US CUSTOMARY UNITS

| | | | | | |
|---|---|---|---|---|---|
| **Project:** | Route 1 Large Culvert Replacement | | | **Boring No.:** | HB-PER-102 |
| **Location:** | Perry, Maine | | | **WIN:** | 26630.11 |
| **Drilling Contractor:** | MaineDOT | **Elevation (ft.)** | 31.2 | **Auger ID/OD:** | 5" Dia. |
| **Operator:** | Daggett/Andrle | **Datum:** | NAVD88 | **Sampler:** | N/A |
| **Logged By:** | B. Wilder | **Rig Type:** | CME 45C | **Hammer Wt./Fall:** | N/A |
| **Date Start/Finish:** | 10/26/2023-10/26/2023 | **Drilling Method:** | Solid Stem Auger | **Core Barrel:** | N/A |
| **Boring Location:** | 63+22.7, 17.7 ft Lt. | **Casing ID/OD:** | N/A | **Water Level*:** | None Observed |

Definitions: D = Spilt Spoon Sample
S = Sample off Auger Flights
B = Bucket Sample off Auger Flights
MD = Unsuccessful Split Spoon Sample Attempt
U = Thin Wall Tube Sample
MV = Unsuccessful Field Vane Shear Test Attempt
V = Field Vane Shear Test, PP= Pocket Penetrometer
MU = Unsuccessful Thin Wall Tube Sample Attempt
R = Rock Core Sample
SSA = Solid Stem Auger
HSA = Hollow Stem Auger
RC = Roller Cone
WOH = Weight of 140lb. Hammer
WOR/C = Weight of Rods or Casing
WO1P = Weight of 1 Person
$S_u$ = Peak/Remolded Field Vane Undrained Shear Strength (psf)
$S_{u(lab)}$ = Lab Vane Undrained Shear Strength (psf)
$q_p$ = Unconfined Compressive Strength (ksf)
N-value = Raw Field SPT N-value
$T_v$ = Pocket Torvane Shear Strength (psf)
WC = Water Content, percent ≅ = Similar or Equal too
LL = Liquid Limit
PL = Plastic Limit
PI = Plasticity Index
G = Grain Size Analysis
C = Consolidation Test

| Depth (ft.) | Sample No. | Pen./Rec. (in.) | Sample Depth (ft.) | Blows (/6 in.) Shear Strength (psf) or RQD (%) | N-value | Casing Blows | Elevation (ft.) | Graphic Log | Visual Description and Remarks | Laboratory Testing Results/ AASHTO and Unified Class. |
|---|---|---|---|---|---|---|---|---|---|---|
| 0 | | | | | | SSA | | | Probe, no material samples taken. | |
| 20 | | | | | | | 11.2 | | 20.0 **Bottom of Exploration at 20.0 feet below ground surface.** NO REFUSAL | |

**Remarks:**

Stratification lines represent approximate boundaries between soil types; transitions may be gradual.

* Water level readings have been made at times and under conditions stated. Groundwater fluctuations may occur due to conditions other than those present at the time measurements were made.

# <u>Appendix B</u>

Laboratory Test Results

State of Maine - Department of Transportation

## Laboratory Testing Summary Sheet

# Town(s): Perry    Work Number: 26630.11

| Boring & Sample Identification Number | Station (Feet) | Offset (Feet) | Depth (Feet) | Reference Number | G.S.D.C. Sheet | W.C. % | L.L. | P.I. | Classification | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | Unified | AASHTO | Frost |
| HB-PER-101, 1D | 63+07.1 | 18.8 Rt. | 0.0-2.0 | 379694 | 1 | 5.4 | | | SW-SM | A-1-a | 0 |
| HB-PER-101, 3D | 63+07.1 | 18.8 Rt. | 10.0-12.0 | 379695 | 1 | 18.2 | 35 | 13 | CL | A-6 | III |
| HB-PER-101, 4D | 63+07.1 | 18.8 Rt. | 15.0-17.0 | 379696 | 1 | 19.1 | 34 | 13 | CL | A-6 | III |
| HB-PER-101, 5D | 63+07.1 | 18.8 Rt. | 20.5-21.3 | 379697 | 1 | 3.8 | | | GW | A-1-a | 0 |

**Classification of these soil samples is in accordance with AASHTO Classification System M-145-40. This classification is followed by the "Frost Susceptibility Rating" from zero (non-frost susceptible) to Class IV (highly frost susceptible). The "Frost Susceptibility Rating" is based upon the MaineDOT and Corps of Engineers Classification Systems.**

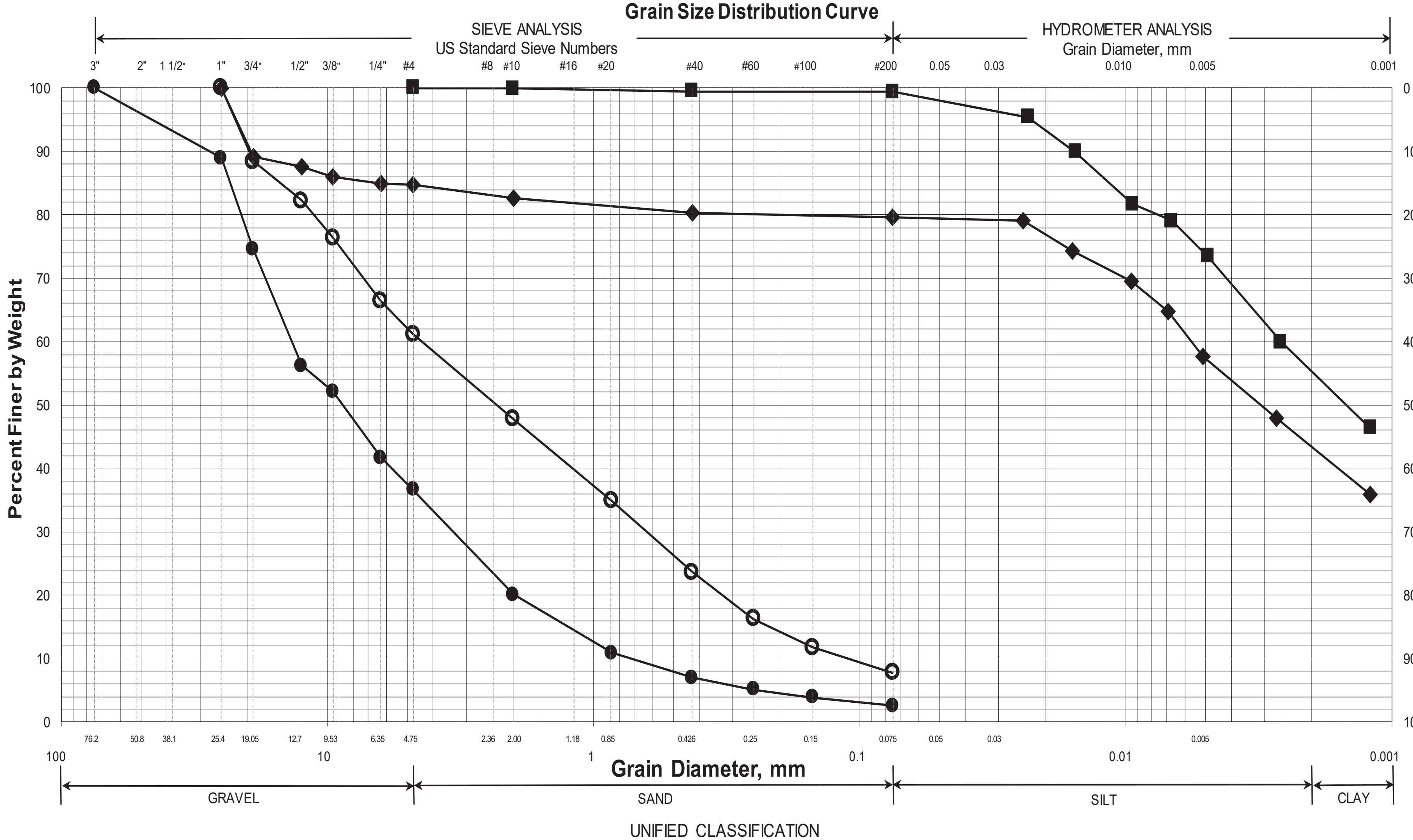
GSDC = Grain Size Distribution Curve as determined by AASHTO T 88-93 (1996) and/or ASTM D 422-63 (Reapproved 1998)

WC = water content as determined by AASHTO T 265-93 and/or ASTM D 2216-98

LL = Liquid limit as determined by AASHTO T 89-96 and/or ASTM D 4318-98    NP = Non Plastic

PI = Plasticity Index as determined by AASHTO 90-96 and/or ASTM D4318-98

# Maine Department of Transportation
## Grain Size Distribution Curve




| | Boring/Sample No. | Station | Offset, ft | Depth, ft | Description | WC, % | LL | PL | PI |
|---|---|---|---|---|---|---|---|---|---|
| ○ | HB-PER-101/1D | 63+07.1 | 18.8 RT | 0.0-2.0 | Gravelly SAND, trace silt. | 5.4 | | | |
| ◆ | HB-PER-101/3D | 63+07.1 | 18.8 RT | 10.0-12.0 | Silty CLAY, little gravel, trace sand. | 18.2 | 35 | 22 | 13 |
| ■ | HB-PER-101/4D | 63+07.1 | 18.8 RT | 15.0-17.0 | Silty CLAY, trace sand. | 19.1 | 34 | 21 | 13 |
| ● | HB-PER-101/5D | 63+07.1 | 18.8 RT | 20.5-21.3 | Sandy GRAVEL, trace silt. | 3.8 | | | |
| ▲ | | | | | | | | | |
| × | | | | | | | | | |

| WIN | |
|---|---|
| 026630.11 | |
| Town | |
| Perry | |
| Reported by/Date | |
| WHITE, TERRY A | 5/7/2025 |

**SHEET 1**

# <u>Appendix C</u>

Calculations

# Bearing Resistance - Existing Soils:

## Part 1 - Service Limit State

**Nominal and factored Bearing Resistance - Box Culvert on Silty Clay**

**Presumptive Bearing Resistance for Service Limit State ONLY**

Reference: AASHTO LRFD Bridge Design Specifications 10th Edition 2024
Table C10.6.2.5.1-1 Presumptive Bearing Resistances for Spread Footings at the Service Limit State Modified after US Department of Navy (1982)

Type of Bearing Material: Silty Clay (CL)

Based on N-values, soils are hard near the bearing elevation

Density In Place: very stiff to hard

Bearing Resistance: Ordinary Range (ksf) 4 to 8

Recommended Value of Use: $q_{nom} := 6 \cdot ksf$

Resistance factor at the **service limit state** = 1.0 (LRFD Article 10.5.5.1) $\phi_{service\_bc} := 1.0$

$q_{factored\_service\_bc} := q_{nom} \cdot \phi_{service\_bc}$ $q_{factored\_service\_bc} = 6 \cdot ksf$

*Note: This bearing resistance is settlement limited (1 inch) and applies only at the service limit state.*

## Part 2 - Strength Limit State

**Nominal and factored Bearing Resistance - Box Culvert on Silty Clay**

Reference: AASHTO LRFD Bridge Design Specifications 10th Edition 2024 - Article 10.6.3.1

Assumptions:

1. The box will be founded at ~ Elev 19.70 feet

   Bottom of Construction will be 2 feet below box invert $D_{footing} := 2.0 \cdot ft$

2. Assumed parameters for fill soils:

   Saturated unit weight: $\gamma_s := 125 \cdot pcf$

   Internal friction angle: $\phi_{ns} := 32 \cdot deg$

   Undrained shear strength: $c_{ns} := 0 \cdot psf$

3. Box Culvert parameters

   Width of box culvert, B $B_{box} := 14 \cdot ft$

   Length of box culvert, L $L_{box} := 83 \cdot ft$

Nominal Bearing Resistance per LRFD Equation 10.6.3.1.2a-1

$q_n$=c$N_{cm}$+γ$D_f$$N_{qm}$$C_{wq}$+0.5γ B$N_{γm}$$C_{wγ}$

Bearing Capacity Factors - LRFD Table 10.6.3.1.2a-1

For ϕ=32 deg $N_c := 35.5$ $N_q := 23.2$ $N_\gamma := 30.2$

Shape Correction Factors LRFD Table 10.6.3.1.2a.-3

for ϕ=32 degrees

$$s_c := 1 + \left(\frac{B_{box}}{L_{box}}\right)\left(\frac{N_q}{N_c}\right) \qquad s_c = 1.11$$

$$s_\gamma := 1 - 0.4\left(\frac{B_{box}}{L_{box}}\right) \qquad s_\gamma = 0.9325$$

$$s_q := 1 + \left(\frac{B_{box}}{L_{box}} \cdot \tan(\phi_{ns})\right) \qquad s_q = 1.11$$

Load Inclination Factors:
Assume all are 1.0 (LRFD Article C10.6.3.1.2a)

$i_c := 1.0$ $i_q := 1.0$ $i_\gamma := 1.0$

Depth Correction Factor

$$d_q := 1 + 2 \cdot \tan(\phi_{ns}) \cdot (1 - \sin(\phi_{ns}))^2 \cdot \tan\left(\frac{D_{footing}}{B_{box}}\right)^{-1} \qquad d_q = 2.92$$

LRFD Eq. 10.6.3.1.2a-10

$N_{cm} := N_c \cdot s_c \cdot i_c$ $N_{cm} = 39.4133$ LRFD Eq. 10.6.3.1.2a-2

$N_{qm} := N_q \cdot s_q \cdot d_q \cdot i_q$ $N_{qm} = 74.88$ LRFD Eq. 10.6.3.1.2a-3

$N_{\gamma m} := N_\gamma \cdot s_\gamma \cdot i_\gamma$ $N_{\gamma m} = 28.16$ LRFD Eq. 10.6.3.1.2a-4

Coefficients for Groundwater Depths LRFD Table 10.6.3.1.2a-2

Depth the water table: $D_w := 4.5 \cdot ft$ $C_{wq} := 1.0$ $C_{w\gamma} := 0.5$

$$q_{nominal} := c_{ns} \cdot N_{cm} + \gamma_s \cdot D_{footing} \cdot N_{qm} \cdot C_{wq} + 0.5(\gamma_s)B_{box} \cdot N_{\gamma m} \cdot C_{w\gamma}$$

$$q_{nominal} = 31 \cdot ksf$$

**Factored Bearing Resistance for Strength Limit State**

Resistance Factor: $\phi_b := 0.45$ LRFD Table 10.5.5.2.2-1

$$q_{factored} := q_{nominal} \cdot \phi_b$$

$$q_{factored} = 14 \cdot ksf$$

Recommend a limiting factored bearing resistance of 14 ksf for the Strength Limit State.

## Modulus of Subgrade Reaction:

Reference: Foundation Analysis and Design 5th Edition JE Bowles Section 9-6

Width of box culvert, B $B_{box} = 14\ ft$

Length of box culvert, L $L_{box} = 83\ ft$

Thickness of box culvert, t $t_{box} := 12 \cdot in$ assumed

Depth of box, D $D_{box} := 12.8 \cdot ft$

Bearing Resistance: $q_{factored\_service\_bc} = 6 \cdot ksf$ Calculated above

Modulus of Elasticity: Site soils at bearing elevation are Silty Clay. Use values for Clay (hard)
From Bowles Table 2-8 Modulus Es for Hard Clay, ranges from 1044 - 2089 ksf

Use: Modulus of Elasticity, Es $E_s := 1560 \cdot ksf$

Poisson's Ratio: Site conditions at bearing elevation are Silty Clay. Use values for Clay (hard)
From Bowles Table 2-7 Poisson's Ration μ for Saturated Clay ranges from 0.4 - 0.5

Use: Possion's Ratio, μ $\mu := 0.5$

$$E_{prime\_s} := \frac{1 - \mu^2}{E_s} \qquad E_{prime\_s} = 0.000481 \cdot \frac{ft^2}{kip}$$

Analyze corner:

Take H as 5*B as recommended in Bowles Chapter 5

$$H_{inf} := \frac{5 \cdot B_{box}}{B_{box}} \qquad H_{inf} = 5$$ N in Table 5-2

$$\frac{L_{box}}{B_{box}} = 5.9286$$ M in Table 5-2

From Table 5-2 for N=5 and M=5.93

$I_1 := 0.548$

$I_2 := 0.119$

by interpolation

Determine Steinbrenner influence factor - Bowles Section 5-6:

$$I_s := I_1 + \left[\frac{1 - (2 \cdot \mu)}{1 - \mu}\right] \cdot I_2 \qquad I_s = 0.548$$

Determine Influence factor for footing depth - Bowles Figure 5-7

Depth ratio: $\frac{D_{box}}{B_{box}} = 0.9143$ $\frac{L_{box}}{B_{box}} = 5.9286$ $\mu = 0.5$ $I_F := 0.86$

Calculate modulus of subgrade reaction - Bowles Eq. 9-7

$$k_s := \frac{1}{B_{box} \cdot E_{prime\_s} \cdot I_s \cdot I_F}$$ Bowles Eq. 9-7

$$k_s = 182 \cdot pci$$

Recommend Modulus of Subgrade Reaction of 180 pci