STORMWATER MANAGEMENT SYSTEM

Prepared for the

CENTRAL MAINE POWER COMPANY FICKETT ROAD SUBSTATION



Location

Fickett Road Pownal, ME

Owner

Central Maine Power Company 83 Edison Drive Augusta, Maine 04336

Prepared by



11733 Chesterdale Road Cincinnati, OH 45246 (513) 326-1500 September 2017

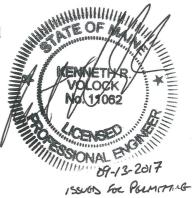


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INTRODUCTION

Central Maine Power Company (CMP) is proposing to construct a new electrical substation as part of the New England Clean Energy Connect (NECEC) Project. The new station will be built on Fickett Road in the town of Pownal in Cumberland County, Maine and will be named the Fickett Road Substation.

Runoff from the proposed electrical substation flows south to Runaround Brook, and then heads north into Runaround Pond. Runaround Pond is listed as a Lake Most at Risk from New Development in Maine Department of Environmental Protection (MeDEP) Chapter 502. The pond then discharges to Runaround Brook, then Chandler Brook, heading downstream to Royal River, then southeast where it discharges into the Atlantic Ocean.

Fickett Road Substation

The existing conditions and proposed grading plans for the proposed Fickett Road Substation are included with this submission as sheets 1077-003-001 SH 001 General Site Plan Existing Conditions and 1077-003-001 SH 002 General Site Plan Proposed Conditions, respectively. The layout of proposed equipment within the yard is shown on SK-FICK-GL Conceptual General Location Plan.

The proposed substation will sit on a 19.61 acre parcel of land that is a mix of flat terrain, steep hills, forest, shrubs and low lying wetlands and includes an existing electric transmission line corridor. The proposed station footprint will be approximately 3.75 acres and will consist of roof top and concrete foundation impervious and evenly graded 3/4" to 1.5" stone for the remainder of the station pad. The access roads leading to the station from the north and east will consist of gravel. The project will consist of a total developed area of 4.87 acres, of which, 3.90 acres will be impervious. The site will be sloped to drain to the south, honoring the existing drainage patterns to the extent practicable. Site stormwater runoff will be treated with a grassed underdrain soil filter, while the stoned yard areas are considered to be treated in place.

Permitting Requirements

The Fickett Road Substation is part of the larger NECEC Project currently being undertaken by CMP. The project is submitted as a whole to the MeDEP for permitting purposes.

The project will require a Stormwater Management Permit and a Site Location of Development Permit because more than 3 acres will be stripped or graded and not revegetated within one year, and because the project will occupy more than 20 acres of land. The project will be required to meet the Basic, General, and Flooding Standards as described in MeDEP Chapter 500. As a result of the Fickett Road Substation discharging to Runaround Brook the project is also required to meet the Chapter 500 Phosphorous Standard. The standards will be met using several erosion and sedimentation control and permanent stormwater management Best Management Practices (BMPs).

BASIC STANDARD

The proposed project will disturb more than one acre of land, requiring compliance with the Basic Standard as described in MeDEP Chapter 500 Section 4B. In order to meet the Basic Standard, the proposed project will be required to address the following:

- Erosion and Sedimentation Control
- Inspection and Maintenance
- Housekeeping

Erosion and Sedimentation Control

Exhibit 14-1 of the Site Law Application contains the manual "Central Maine Power Company - Environmental Guidelines for Construction and Maintenance Activities on Transmission Line and Substation Projects". This manual addresses general erosion and sedimentation control measures used in many previous transmission and substation projects and has been reviewed and approved by MeDEP. The manual was developed to be consistent with the Maine Erosion and Sediment Control Practices Field Guide for Contractors, 2015, and MeDEP's Chapter 500.

Specific erosion and sedimentation control BMPs for the Fickett Road Substation project are indicated on sheet 1077-003-004 SH 001 Erosion and Sediment Control Plan. Details of the measures proposed are shown on sheet 1077-003-005 SH 003 Site Details 3 and sheet 1077-003-005 SH 004 Site Details 4. Sheet 1077-003-005 SH 005 Site Details 5 presents a plan for implementing these measures at the site.

Inspection and Maintenance

CMP will ensure that a qualified design engineer inspects the construction site periodically to verify that the stormwater BMPs are constructed in accordance with the plans and specifications shown on the design drawings, and, as needed, during any period when construction activity affecting the stormwater management system occurs, until the site is permanently stabilized. Inspection and Maintenance procedures for the proposed substation are described below. BMP Inspection & Maintenance Checklists and BMP Inspection & Maintenance Logs for each site have been enclosed in Appendix A. The BMP Inspection & Maintenance Checklists outline the inspection frequency/requirements and maintenance/cleanout thresholds for each BMP measure. The enclosed BMP Inspection & Maintenance Logs include specific inspection guidelines for each BMP measure and are the documentation portion of this Plan.

Scheduled Inspections

Prior to completion of construction, CMP shall designate a CMP Supervisor and personnel or a contractor as the Site Inspector for each substation. Inspection requirements for each individual BMP measure are specified on the Inspection & Maintenance Checklists in Appendix A.

• QUARTERLY: Inspections of stormwater conveyance, control and treatment measures at each Site are to be performed on a quarterly basis throughout the year. Inspections during winter months may encounter snow and ice cover, frozen ground, snow embankments, dormant vegetation, etc. In these cases, the inspector must use his/her best judgment

- interpreting these inspection and maintenance requirements, in order to meet both the stated objectives and the intent of the Plan. The inspection should prevent problems and plan for maintenance in advance of the spring thaw (removing snow piles if they obstruct drainage paths, repairing any damage from snow plows, frost heaves, etc.).
- <u>FOLLOW-UP</u>: Additional follow-up inspections will be performed, as needed, depending on the results of routine inspections and site conditions, under the direction of the CMP Supervisor.

As-Needed Maintenance

Maintenance is to be performed on an as-needed basis, in accordance with recommendations made by the Site Inspector. Routine maintenance will include the immediate repair of eroded channels or gullies; reseeding or sodding of bare ground; removal of trash, leaves and sediment; and control of vegetation. Maintenance issues associated with specific areas and stormwater facilities at each Site are identified on the Inspection & Maintenance Checklists in Appendix A. Disposal of all sediment, debris, and waste shall be in accordance with Maine Solid Waste Management Rules, Chapter 400.

5-Year Re-Certification

CMP will certify the following to the MeDEP within three months of the expiration of each five-year interval from the date of issuance of the permit:

- All areas of the project site have been inspected for areas of erosion, and appropriate steps have been taken to permanently stabilize these areas.
- All aspects of the stormwater control system have been inspected for damage, wear, and malfunction, and appropriate steps have been taken to repair or replace the facilities.
- The erosion and stormwater maintenance plan for the site is being implemented as written, or modifications of the plan have been submitted to and approved by the department, and the maintenance log is being maintained.

Housekeeping

Housekeeping entails the control or elimination of pollution not specifically related to soil erosion such as spill prevention, dust control, litter removal and dewatering. Housekeeping is addressed within the narrative and on sheet 1077-003-005 SH 005 Site Details 5 for the Fickett Road Substation.

PHOSPHORUS STANDARD

The Fickett Road substation discharges to Runaround Pond and will add more than 20,000 square feet of impervious surface within the watershed of a Lake Most at Risk. For this reason the project is required to meet the MeDEP Chapter 500 Phosphorus Standard. In order to meet the Phosphorus Standard, the project needs to reduce the amount of phosphorus released from the site to calculated allowable levels for the parcel. Phosphorus Worksheet 1 was used to calculate the allowable phosphorus load from the parcel, also known as the phosphorous Budget. Following establishment of

the phosphorous Budget, pre-treatment phosphorous loading from the site and loading from the site following implementation of on site BMPs is calculated using Worksheet 2. For the proposed condition, phosphorous Worksheet 2 was used to calculate post-developed phosphorous export loads from the site. Worksheets 1 and 2 can be found in Appendix C.

Stormwater Treatment BMPs

Crushed Stone Substation Surface

MeDEP has provided yard construction requirements that allow for reduced *Export Coefficients* and *Treatment Factors* to be applied to the substation's stone surface for treatment related to meeting the Phosphorous Standard. In email correspondence following MeDEP's 2008 letter MeDEP has indicated that phosphorous loading and phosphorous removal associated with the station pad may be calculating using an *Export Coefficient* of 0.30 and a *Treatment Factor* of 0.10 for the *Crushed Stone Substation Surface*. The email correspondence can be found in Appendix B.

Grassed Underdrain Soil Filter

Runoff from the vegetated developed area along the west side of the station pad will be treated in a Grassed Underdrain Soil Filter. Pretreatment will be accomplished by flowing runoff through a vegetated swale and into a pre-treatment forebay before entering the filter area. Additionally, areas of the station pad and the rooftop surfaces within the pad will be treated within the Soil Filter following treatment within the crushed stone.

The Grassed Underdrain Soil Filter is comprised of an 18"-thick layer of a silty sand and organic material mix. The underdrain system consists of 6" perforated pipe within a 12"-thick layer of underdrain material. The filter is proposed partially within an existing wetland and within areas believed to have elevated groundwater conditions. An impermeable liner has been incorporated into the filter to allow for proper dewatering and prevent oversaturation of the filter media by groundwater prior to rain events. A detail of the underdrained soil filter is shown on sheet 1077-003-003 SH 001 Stormwater Treatment Plan. Underdrained soil filter sizing calculations are provided in Appendix C.

Stormwater Treatment Calculations

In addition to using the station stone as a BMP, a downstream Soil Filter is proposed to further reduce post developed phosphorous exports from the site by providing primary treatment for developed areas surrounding the pad and by further treating runoff from the stone pad as part of a two-tier treatment train utilizing the *Crushed Stone Substation Surface* treatment with a downstream soil filter. For parts of the site (pad, rooftops) utilizing the two-tier treatment train, a calculated Treatment Factor of 0.05 was used.

Export Coefficients for the proposed surfaces were used to calculate pre-treatment loading and Treatment Factors for the proposed BMPs were used to calculate load reductions and subsequent post-developed phosphorous export loads. As shown in Worksheet 1, the Budget for the parcel was calculated to be 0.426 pounds per year and as seen in Worksheet 2, a post developed, post treatment phosphorous export load of 0.418 is achieved.

Typical sizing of Soil Filters for adherence to the Phosphorous Standard requires that the filter have capacity to contain the standard water quality volume (BMP $_{ST}$) which is the volume required for adherence to the General Standard, plus additional volume calculated using a prescribed Treatment Factor. The BMP $_{ST}$ volume plus the additional phosphorous treatment volume requirement constitute the total volume capacity required for BMPs used to meet the Phosphorous Standard and is known as BMP $_{TF}$. The Fickett Road substation yard is self-treating and does not require additional BMPs for adherence to the General Standard, therefore the soil filter was sized to have capacity for the difference between the BMP $_{ST}$ and BMP $_{TF}$ for areas of the yard plus the full BMP $_{TF}$ for developed landscaped areas outside the yard that are not treated for the general standard within the yard stone. Appendix C contains calculations for sizing the soil filter based on these parameters.

The hydraulic modeling report for the entire project site is also included with this submission in Appendix C. The calculations were developed using USDA TR-55 methodology. The model results in Appendix C illustrate how the site drainage and stormwater management infrastructure will function during the 2-, 10- and 25- year storms. The report also contains the hydrologic calculations for the project. The modeling results were used to confirm that adequate water quality volume (WQV) will be provided below the required 18" depth for the Grassed Underdrain Soil Filter.

FLOODING STANDARD

The project is required to meet the MeDEP Chapter 500 Flooding Standard; the addition of over 3 acres of impervious area requires a decrease in peak stormwater runoff as a result of the proposed development. The site is situated entirely within existing HSG Type D soils. Pre-developed and postdeveloped Curve Numbers for the project can be found in Appendix C and on the project drainage area maps (Sheets 1077-003-003 SH 002 and SH 003). The MeDEP letter describing the construction requirements that allow the General Standard requirements to be met for the yards within the *Crushed* Stone Substation Surface also prescribes allotted Curve Numbers for use when calculating runoff from the stone section. Pre-Developed Curve Numbers for the project site depicted on the drainage area maps indicate existing Curve Numbers ranging from 73 to 77. MeDEP prescribes a developed Curve Number for the stone station surface over HSG Type D soils of 60. As existing drainage patterns have been maintained to the extent practicable, the sizes and times of concentration have not been significantly altered with this project. Due to the decreased Curve Numbers across the stone station pad (CN decreased to 60 for these areas), post-development peak flows were calculated to be less than or relatively equal to the pre-development peak flows without the need for on-site stormwater attenuation. Tables 1 and 2 show the pre- and post-development peak flows at each analysis point. Tables 3 through 5 show the comparisons between the pre-developed and postdeveloped peak flow rates

Table 1 - Pre-Developed Peak Flow Rates

Analysis Point	2-Year Flow Rate (CFS)	10-Year Flow Rate (CFS)	25-Year Flow Rate (CFS)
А	2.25	5.70	7.51
В	3.98	10.12	13.36
С	0.27	0.66	0.86
D	0.13	0.30	0.38

Table 2 - Post-Developed Peak Flow Rates

Analysis Point	2-Year Flow Rate (CFS)	10-Year Flow Rate (CFS)	25-Year Flow Rate (CFS)	Peak 2-Year Flow Rate at Outfall (If Subsheds Present)	Peak 10- Year Flow Rate at Outfall (If Subsheds Present)	Peak 25- Year Flow Rate at Outfall (If Subsheds Present)
А	2.33	5.71	7.47	N/A	N/A	N/A
B1	1.30	4.05	5.55	2.06	5.73	7.71
B2	1.84	5.14	6.91	2.00	5.75	7.71
С	0.15	0.37	0.48	N/A	N/A	N/A
D	0.13	0.30	0.38	N/A	N/A	N/A

Table 3 – Flow Rate Comparison, 2-Year

Analysis Point	PRE 2-Year Flow Rate (CFS)	POST 2-Year Flow Rate (CFS)	Change in Peak Flow Rate (CFS)
Α	2.25	2.33	0.08
В	3.98	2.06	(1.92)
С	0.27	0.15	(0.12)
D	0.13	0.13	0.00

Table 4 – Flow Rate Comparison, 10-Year

Analysis Point	PRE 10-Year Flow Rate (CFS)	POST 10-Year Flow Rate (CFS)	Change in Peak Flow Rate (CFS)
Α	5.70	5.71	0.01
В	10.12	5.73	(4.39)
C	0.66	0.37	(0.29)
D	0.30	0.30	0.00

Table 5 – Flow Rate Comparison, 25-Year

Analysis Point	PRE 25-Year Flow Rate (CFS)	POST 25-Year Flow Rate (CFS)	Change in Peak Flow Rate (CFS)
Α	7.51	7.47	(1.04)
В	13.36	7.71	(5.65)
С	0.86	0.48	(0.38)
D	0.38	0.38	0.00

Access Road Culvert Sizing

An approximately 200' long gravel access drive is proposed extending from Fickett Road to the proposed substation pad. The road will be graded to slope longitudinally downward to a low point between the station pad and Fickett Road and will be graded to have a 2% minimum cross slope to carry stormwater runoff from the road surface. Surface runoff from areas upstream of the new access

drive currently flow within a poorly defined ditch along Fickett Road and will be required to pass beneath the road via a proposed 15" reinforced concrete culvert.

The culvert is expected to serve a drainage area of approximately 0.68 acres having a runoff Curve Number of 75 and with a time of concentration of 5 minutes. The drainage area hydrology was modeled in AutoDesk's Storm and Sanitary Analysis program to develop post-developed peak flow rates to the culvert in the 2-, 10- and 25-year storm events. Hydraulic analysis of the culvert was completed using AutoDesk's Hydraflow Express analysis tool to confirm flow capacity and check for flooding. Hydrologic model outputs including peak flow rates can be found in Appendix C in the *Proposed Conditions Hydraulic/Hydrologic Report*. The *Culvert Report* in Appendix C demonstrates the anticipated performance of the culvert during a 25-year event including flow regime and hydraulic grade line elevations at both upstream and downstream ends.

CONCLUSION

The NECEC Project will require a Stormwater Management Permit, and will be required to meet the Basic, Phosphorous and Flooding Standards as described in MeDEP Chapter 500. The Basic Standard shall be met at the Fickett Road Substation through Erosion and Sedimentation Control, Inspection and Maintenance, and Housekeeping, as described in this narrative and the attached checklists, logs and plans. The Flooding Standards shall be met at the Fickett Road Substation by using the MeDEP approved substation yard stone section, as illustrated on the attached stormwater treatment plans. The proposed culvert beneath the new access drive has been sized to prevent flooding of the road during the 25-year storm event. The Phosphorus Standard shall be met using the MeDEP approved substation yard section and a Grassed Underdrain Soil Filter.



APPENDIX A-1: BMP INSPECTION & MAINTENANCE CHECKLIST

BMP MEASURE	INSPECTION REQUIREMENTS*	MAINTENANCE/CLEANOUT THRESHOLDS
	Inspect swale for accumulated sediment, debris and other obstructions.	Clean as needed and dispose of properly.
	Inspect swales for evidence of erosion, gullies, or slumping of the side slopes.	Repair and re-seed as necessary. Consult engineer if problem persists. Areas of persistent erosion may need to be armored.
Vegetated Swales	Inspect swales for bare ground/sparse vegetation.	Re-seed as necessary. Soil may need to be scarified if compacted soils are present.
	Monitor vegetative growth.	Mow vegetation in swales to roughly six inches at least once and no more than two times a year. To be performed between June 15 th and August 30 th .
	Inspect check dams to ensure the center is lower than the edges.	Repair as necessary.
Check Dams	Inspect check dams for stone displacement, erosion, concentrated flow or channelization.	Repair any damaged areas. Consult engineer if problem persists.
	Inspect check dams for accumulated sediment, debris or other obstructions.	Clean as needed and dispose of properly. Sediment must be removed before it exceeds one half the original height of the check dam.
Revegetated Areas	Inspect revegetated areas for evidence of erosion, concentrated flow, or channelization.	Repair and re-seed as necessary. Consult engineer if problem persists. Areas of concentrated flow where rills and gullies are present may need to be armored
	Inspect revegetated areas for bare ground/sparse vegetation.	Re-seed as necessary. Soil may need to be scarified if compacted soils are present.
	Inspect access road shoulder for accumulated sand/sediment.	Remove sand/sediment as necessary.
Gravel Access Roads	Inspect grade on access road and shoulder to ensure stormwater is not impeded by accumulation of materials or false ditches.	Repair grade as necessary.
	Inspect access road to ensure that there is no rutting, wash-boarding, frost heaves, potholes, or ponding occurring.	Repair by replacing gravel and re-grading as necessary.

^{*}Inspections are to be performed on a monthly basis with additional follow-up inspections and maintenance as needed.

APPENDIX A-1: BMP INSPECTION & MAINTENANCE CHECKLIST

Central Maine Power Company – Merrill Road Substation Lewiston, Maine

BMP MEASURE	INSPECTION REQUIREMENTS*	MAINTENANCE/CLEANOUT THRESHOLDS
	Inspect entering swale, basin and outlet structure for accumulated sediment, debris and other obstructions.	Clean as needed and dispose of properly.
	Inspect filter for evidence of erosion, gullies, or slumping of the side slopes.	Repair and re-seed as necessary. Consult engineer if problem persists. Areas of persistent erosion may need to be armored.
Grassed Underdrained Soil Filter	Inspect filter for bare ground/sparse vegetation.	Re-seed as necessary. Soil may need to be scarified if filter media becomes compacted.
	Monitor vegetative growth.	Mow vegetation in impoundment to roughly six inches at least once and no more than two times a year. To be performed between June 15 th and August 30 th .
Crushed Stone Substation Surface	Inspect crushed stone areas for accumulated sand/sediment.	Remove sand/sediment as necessary.
	Inspect substation surface to ensure that there is no ponding occurring.	Repair by re-grading as necessary.

^{*}Inspections are to be performed on a monthly basis with additional follow-up inspections and maintenance as needed.

APPENDIX A-2: BMP INSPECTION & MAINTENANCE LOG

BMP MEASURE (Refer to Appendix B-1 & the O&M Plan)	Inspect	tor(s):		Inspection Type: Monthly [] Follow-up []	Photos Taken: Yes [] No []	Date:
VEGETATED SWALES Swale along Northwesterly side of yard	YES*	NO	INITIALS	OBSERVATIONS	CORRECTIVE ACTIONS/REPAIR ACTIVITY	DATE COMPLETED & BY WHOM (Refer to any contractor service logs)
Is there an accumulation of sediment, debris and/or other obstructions?						
2. Is there any evidence of erosion, gullies or slumping of the side slopes?						
3. Are there areas of bare ground or sparse vegetation?						
4. Has vegetation been mowed to a length roughly 6" this year?						
CHECK DAMS		_				
Check Dams in Swales						
1. Are the edges of the check dams higher than the center?						
2. Is there any evidence of stone displacement, erosion, concentrated flow or channelization?						
3. Is there an accumulation of sediment, debris and/or other obstructions?						

APPENDIX A-2: BMP INSPECTION & MAINTENANCE LOG

BMP MEASURE (Refer to Appendix B-1 & the O&M Plan)	Inspect	or(s):		Inspection Type: Monthly [] Follow-up []	Photos Taken: Yes [] No []	Date:
	YES*	NO	INITIALS	OBSERVATIONS	CORRECTIVE ACTIONS/REPAIR ACTIVITY	DATE COMPLETED & BY WHOM (Refer to any contractor service logs)
REVEGETATED AREAS						
Revegetated Areas along Access Road						
1. Is there any evidence of erosion, concentrated flow or channelization?						
2. Are there areas of bare ground or sparse vegetation?						
Revegetated Areas on all sides of the station						
1. Is there any evidence of erosion, concentrated flow or channelization?						
2. Are there areas of bare ground or sparse vegetation?						
GRAVEL ACCESS ROADS				_		_
Access Road to Entrance						
 Is there an accumulation of sand and/or sediment in the road shoulder? 						
2. Does the grade across the road section allow stormwater to drain off the roadway?						
3. Are there any signs of rutting, wash-boarding, frost heaves, potholes or ponding?						

APPENDIX A-2: BMP INSPECTION & MAINTENANCE LOG

BMP MEASURE (Refer to Appendix B-1 & the O&M Plan)	Inspect	or(s):		Inspection Type: Monthly [] Follow-up []	Photos Taken: Yes [] No []	Date:
GRASSED UNDERDRAINED SOIL FILTER West side of station yard and north of Access Road	YES*	NO	INITIALS	OBSERVATIONS	CORRECTIVE ACTIONS/REPAIR ACTIVITY	DATE COMPLETED & BY WHOM (Refer to any contractor service logs)
Is there an accumulation of sand and/or sediment in the swale or basin?						-
2. Is there any evidence of erosion, gullies or slumping of the side slopes?						
3. Are there areas of bare ground or sparse vegetation?						
CRUSHED STONE SUBSTATION SURFACE						
Fenced-in area of the Substation and aprons 1. Is there an accumulation of sand/sediment in crushed stone areas?						



STATE OF MAINE DEPARTMENT OF ENVIRONMENTAL PROTECTION

JUN 1 1 2008



DAVID P. LITTELL COMMISSIONER

June 5, 2008

Roy Koster Central Maine Power 83 Edison Drive Augusta, ME 04336

RE:

DEP Stormwater Management Regulations and how they apply to Central Maine Power Company Substations and Switchyards

Dear Mr. Koster:

I am writing to provide clarification on how substations and switchyards designed by Central Maine Power Company (CMP) can meet DEP Stormwater Management rules, Chapter 500 and the Site Location of Development Law. This letter supersedes a previous DEP letter on this subject dated February 29, 2008 and is a follow-up to further discussions between CMP and DEP staff.

Based on the report prepared by John Simon of Balance Engineering, dated March 8, 2008, regarding the stormwater runoff coefficient at CMP substations and switchyards, the required gravel fill and surface nature of these structures performs differently than most common construction practices and a modeling variance will be allowed for CMP substations and switchyards as follows:

When Flooding Standard requirements apply to a CMP project, modeling must demonstrate that peak runoff from the substation structure does not exceed predevelopment flow rates at the property line. Because of the permeability plus storage within the gravel fill and roughness of the crushed rock surface, the curve number (CN) specified in John Simon's report (March 2008) may be used for the substation area. As reported, a CN of 55 may be used for substations and switchyards that are built on areas that are mapped as HSG "A", "B", and "C", and a CN of 60 must be used when the area is mapped as HSG "D" for the HydroCAD model. However, all impervious surfaces will have to be added for an averaged curve number.

The General Standards of Chapter 500 (water quality) will be considered as met by the CMP substation/switchyard design specifications as long as the structure includes the typical CMP substation profile overlaying the natural ground surface. The soil layers within the CMP substation profile consist of 4 inches of crushed stone, 50:50 mix of 1.5" and 0.75" diameter stone overlaying 18 inches or more of gravel fill, MDOT 703.06 Type A. Saturation within the granular fill will detain and provide treatment for the one-inch design standard under that requirement. Groundwater can never be any higher than 18 inches below the top of the gravel fill. Other treatment considerations will need to be provided for all impervious structures anticipated on the substation and switchyard and for the roadway.

The <u>Basic Standards</u> of Chapter 500 (erosion and sedimentation control, inspection and maintenance, and housekeeping) will be met by the standard CMP substation and switchyard design specification and erosion control/construction plan as developed by CMP for each Stormwater Management application. These are minimum erosion control measures that will need to be maintained until the site is fully stabilized. However, based on site and weather conditions during construction, additional erosion control measures may be needed.

While there are several ways to approach the design standards discussed above, these must be considered the minimum requirements in meeting the Stormwater Management and Site Location of Development Laws. However, in some situations where the local hydrology and site conditions warrant more resource protection, additional BMPs may be required. Also, the access drive and associated roadside swales are included in the disturbed area for permitting purposes and the treatment of these areas must be addressed separately from the substation or switchyard and be treated with standard practices. The natural hydrology of these areas will need to be maintained and will have to meet all applicable standards as established in Chapter 500 (page 11, Section 5).

I hope this addresses your request and will make the DEP permitting process more straight forward. If you have further questions, please contact Marianne Hubert at (207) 287-4140.

Sincerely,

Don Witherill, Director

Watershed Management Division

Bureau of Land and Water Quality

Cc:

Marianne Hubert, PE, DEP program manager

Andy Fisk, DEP L&W Bureau Director

Dan Butler, PE, TRC Gerry Mirabile, CMP **From:** Gungor, Kerem [mailto:Kerem.Gungor@maine.gov]

Sent: Wednesday, August 23, 2017 1:57 PM

To: Volock, Kenny

Subject: RE: CMP Substation Yard Treatment Clarifications

Hi Kenny,

Here are my answers:

Is there a point at which we can no longer consider the concrete and roof area within a substation to be treated through the 4" stone and 18" MDOT Type "A" gravel station yard section?

I took into account the storage volume provided by the underlying 18" gravel layer for Coopers Mill substation minor revision I reviewed. Same approach can be followed for NECEC:

Storage Volume Provided for Treatment (cf) = (Substation Yard Area excluding the impervious surfaces (sf)) x 2 ft x 0.3 (assumed porosity for the substation yard profile)

Storage Volume Required for the Treatment of the Impervious Surfaces (cf) = Impervious surface (i.e. concrete, roof) (sf) x (1/12) (ft) (one-inch storage requirement for the impervious surfaces)

Therefore, one unit area of stone yard can treat up to 7 unit areas of impervious area (I would recommend staying on the conservative side, not going this far). You do not need to provide additional treatment for the roof at Merrill Road substation.

How is the station yard section considered when it comes to phosphorous treatment? Considering the storage volume and structure of the station yard, I would use the minimum treatment factor, **0.1** as given for the infiltration measures in **Table 4.1** of the Phosphorus Control Manual. For the concrete surfaces and roof, you can use the export factor of **0.5 lb/ac/yr**. For the substation yard, the export factor of **0.3 lb/ac/yr** can be used.

Please let me know if you have any more questions.

Best,

Kerem Gungor, Ph.D., P.E.
Environmental Engineer, Central Maine Region
Bureau of Land Resources | Land Division
Maine Department of Environmental Protection
(207) 446-3915 | kerem.gungor@maine.gov

From: <u>kenny.volock@powereng.com</u> [<u>mailto:kenny.volock@powereng.com</u>]

Sent: Wednesday, August 23, 2017 12:03 PM

To: Gungor, Kerem

Subject: CMP Substation Yard Treatment Clarifications

Kerem,

Thank you for your input regarding stormwater management and erosion control during the NECEC Pre-Application last Thursday. I do have a couple follow-up questions that I would like some clarification on:

Is there a point at which we can no longer consider the concrete and roof area within a substation to be treated through the 4" stone and 18" MDOT Type "A" gravel station yard section?

Since we typically call for 6" of stone, I've always assumed the extra 2" of stone is what provided the additional water quality volume for the roof and concrete areas. Depending on what you use for porosity of the stone (0.3 to 0.4), you would have 0.6" to 0.8" available, enough for 0.6 acres to 0.8 acres of roof/concrete per acre of stone yard. This equates to 37.5% to 44.4% roof/concrete area.

A typical substation yard has only around 2% to 5% roof/concrete area, so it is negligible. However, at Merrill Road, with a very large building, that percentage could approach 30%. I would like to know, prior to submission, if we will be able to consider the runoff from the building roof as treated by the yard, or if we will need to make separate provisions.

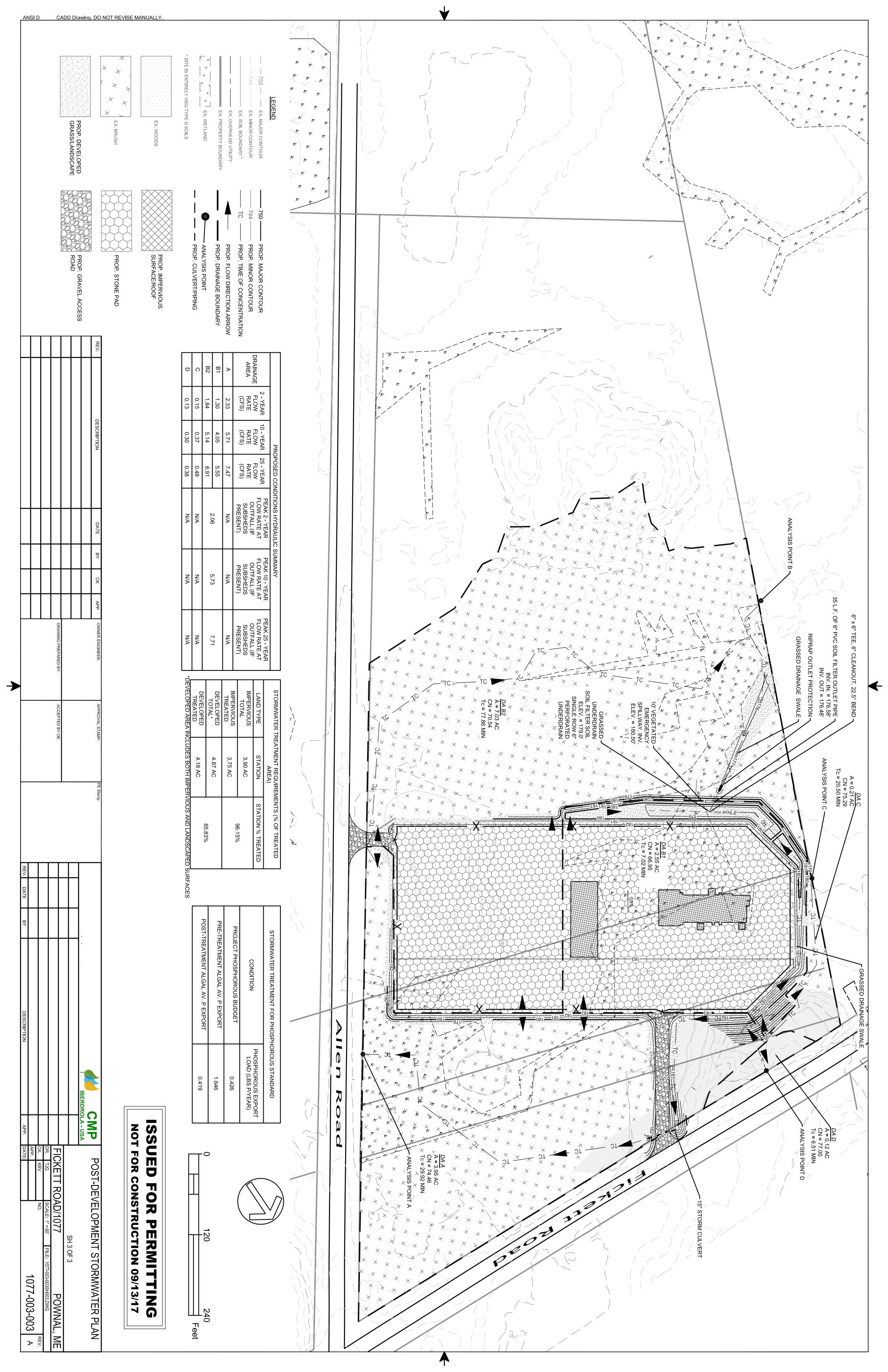
How is the station yard section considered when it comes to phosphorous treatment?

The 2008 letter from MeDEP to CMP discusses the Flooding and General Standards, but does not discuss the Phosphorous Standard. Can we assume the yard to have the same base treatment factor of 0.4 as the other BMPs? Or is there some other base treatment factor we should be using?

Any input you could provide in resolving these two outstanding issues would be greatly appreciated.







Project Name:		Fickett Road Substation			
Lake Watershed:		Runaround Pond			
Town: Durham					
Standard Calculations					
Watershee	d per acre phosphor	us budget (Appendix C)	PAPB	0.025	lbs P/acre/year
To	otal acreage of deve	lopment parcel:	TA	19.61	acres
	NWI wetland a	acreage:	WA	2.41	acres
	Steep slope a	creage:	SA	0.166	acres
		Project acreage: A = TA - (WA+ SA)	Α	17.034	acres
Project Phosphorus Budge	et: PPB = P x A		PPB	0.42585	lbs P/year
<u> </u>					
table in Appendix C), calculate a	than the threshold aci	reage for the small watershed threshold (SWT ng the analysis below and use this value if it is			
If Project Acreage (A) is greater table in Appendix C), calculate a Small Watershed Threshold	than the threshold aci				
If Project Acreage (A) is greater table in Appendix C), calculate a Small Watershed Threshold	than the threshold aci		less than th	he the Standard	d Calculation PPE
f Project Acreage (A) is greater able in Appendix C), calculate a Small Watershed Threshold Project acreage:	than the threshold aci an alternative PPB usin (Appendix C):		less than the	ne the Standard	d Calculation PPE
If Project Acreage (A) is greater table in Appendix C), calculate a Small Watershed Threshold Project acreage: Allowable increase in town's	than the threshold act an alternative PPB usin (Appendix C): share of annual pho	ng the analysis below and use this value if it is	SWT A	N/A N/A	acres
If Project Acreage (A) is greater table in Appendix C), calculate a Small Watershed Threshold Project acreage: Allowable increase in town's Area available for developments	than the threshold act an alternative PPB usin (Appendix C): share of annual pho ent (Appendix C):	ng the analysis below and use this value if it is	SWT A FC	N/A N/A N/A	acres acres lbs P/year
of Project Acreage (A) is greater table in Appendix C), calculate a Small Watershed Threshold Project acreage: Allowable increase in town's Area available for developmentation of A to AAD (R=A/AAD)	than the threshold act an alternative PPB usin (Appendix C): share of annual pho ent (Appendix C):	ng the analysis below and use this value if it is	SWT A FC AAD	N/A N/A N/A N/A N/A	acres acres lbs P/year
If Project Acreage (A) is greater table in Appendix C), calculate a Small Watershed Threshold Project acreage: Allowable increase in town's Area available for development Ratio of A to AAD (R=A/AAD Project Phosphorus Budge	than the threshold act an alternative PPB usin (Appendix C): share of annual pho ent (Appendix C):	ng the analysis below and use this value if it is	SWT A FC AAD	N/A N/A N/A N/A N/A	acres acres lbs P/year

Worksheet 2

Pre-PPE and Post-PPE Calculations
Calculate phosphorus export from development for before and after treatment
Use as many sheets as needed for each development type (commercial, roads, residential lots, etc.)

Project name: Fickett Substation Development type: __Commercial____ Sheet # ____

Land Surface Type or Lot #(s) with description	Acres or # of lots	Export Coefficient from Table 3.1 Table 3.2	Pre- treatment Algal Av. P Export (Ibs P/year)	from	Post- treatment Algal Av. P Export (Ibs P/year)	Description of BMPs
Impervious Roofs	0.24	0.5	0.12	0.05	0.006	Stone yard to Soil Filter
Stone Station Pad	1.58	0.3	0.474	0.1	0.0474	Stone Yard
Concrete Foundations	0.05	0.5	0.025	0.1	0.0025	Stone Yard
Stone Station Pad to Soil Filter	1.88	0.3	0.564	0.05	0.0282	Stone yard to Soil Filter
Gravel Road Outside Station	0.15	0.5	0.075	1	0.075	N/A
Landscaped Treated	0.43	0.4	0.172	0.25	0.043	Soil Filter
Landscaped Untreated	0.54	0.4	0.216	1	0.216	N/A
		Total Pre-PPE (Ibs P/year)	1.646	Total PostPPE (lbs P/year)	0.4181	

	Calculations for Grassed Underdrain Soil Filter								
*B	*Based upon MeDEP Stormwater BMPs Chapter 7.1 - Grassed Underdrain Soil Filters and Phosphorus Control Manual								
Land Type	Area (AC.)	BMP _{ST} = WQv Required, General Standard ¹ , (CU.FT.)	Treatment Factor (TF) ²	BMP _{TF} = WQv Required, Phosphorus Standard + General Standard ³ , (CU.FT.)	(00.11.)	Total WQv Required (Impervious and Pervious) (CU.FT.)	WQv Provided @ 18" Depth, (CU.FT.)		
Impervious Catchment	2.07	7,514.10	0.25	12,022.56	4,508.46	5,507.44	8,354.00		
Pervious Developed Catchment	0.43	624.36	0.25	998.98	998.98				

¹ The General Standard has been met by providing the required BMP_{ST} Water Quality volume within the MeDEP approved station pad stone section.

² The Treatment Factor used to upsize the required Stanard Treatment volume in order to meet the Phosphorous Standard.

 $^{^3}$ The Water Quality volume required to meet the General and Phosphorous Standards, calculated using the Maine Storm Water Management Design Manual - Phosphorus Control Manual, Section 4.3: BMP_{TF}=0.4*(BMP_{ST}/TF)

⁴ The Water Quality volume required to meet the Phosphorouse Standard for areas where the General Standard has already been met within the MeDEP approved station pad stone section.

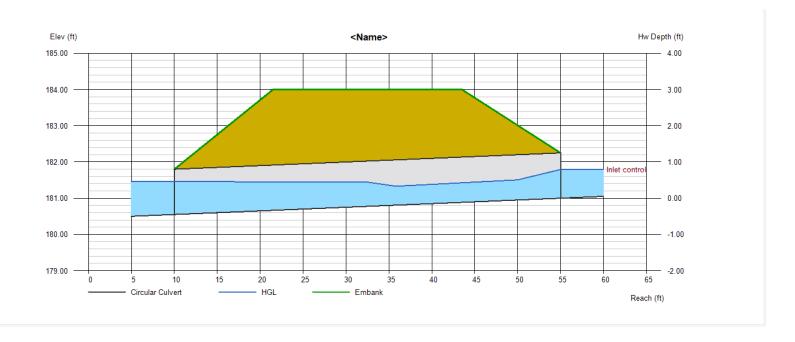
Culvert Report

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Wednesday, Sep 13 2017

Circular Culvert

Invert Elev Dn (ft)	= 180.55	Calculations	
Pipe Length (ft)	= 45.00	Qmin (cfs)	= 2.03
Slope (%)	= 1.00	Qmax (cfs)	= 2.03
Invert Elev Up (ft)	= 181.00	Tailwater Elev (ft)	= (dc+D)/2
Rise (in)	= 15.0		
Shape	= Circular	Highlighted	
Span (in)	= 15.0	Qtotal (cfs)	= 2.03
No. Barrels	= 1	Qpipe (cfs)	= 2.03
n-Value	= 0.015	Qovertop (cfs)	= 0.00
Culvert Type	Circular Concrete	Veloc Dn (ft/s)	= 2.12
Culvert Entrance	= Groove end projecting (C)	Veloc Up (ft/s)	= 3.75
Coeff. K,M,c,Y,k	= 0.0045, 2, 0.0317, 0.69, 0.2	HGL Dn (ft)	= 181.46
		HGL Up (ft)	= 181.57
Embankment		Hw Elev (ft)	= 181.79
Top Elevation (ft)	= 184.00	Hw/D (ft)	= 0.63
Top Width (ft)	= 22.00	Flow Regime	= Inlet Control
Crest Width (ft)	= 20.00		



Project Description

File Name Existing Conditions.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Aug 10, 2017	00:00:00
End Analysis On	Aug 11, 2017	00:00:00
Start Reporting On	Aug 10, 2017	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qt
Rain Gages	1
Subbasins	4
Nodes	4
Junctions	0
Outfalls	4
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	0
Channels	0
Pipes	0
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County	Period	Rainfall Depth (inches)	
1	Rain Gage-01	Time Series	TS-02	Cumulative	inches	Maine	Cumberland (Southeast)	2	3.00	SCS Type III 24-hr

Subbasin Summary

	Area	Weighted		Total		Peak	Time of
ID		Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
		Number			Volume		
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
A	3.70	73.41	3.00	0.88	3.25	2.25	0 00:23:04
В	8.76	73.22	3.00	0.87	7.61	3.98	0 00:43:24
С	0.35	74.60	3.00	0.94	0.33	0.27	0 00:15:12
D	0.12	77.00	3.00	1.07	0.13	0.13	0 00:06:30

Subbasin Hydrology

Subbasin: A

Input Data

Area (ac)	3.70
Weighted Curve Number	73.41
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	2011	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.38	D	77.00
Brush, Good	3.32	D	73.00
Composite Area & Weighted CN	3.70		73.41

Time of Concentration

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$

Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation:

V = 16.1345 * (Sf^0.5) (unpaved surface)
V = 20.3282 * (Sf^0.5) (paved surface)
V = 15.0 * (Sf^0.5) (grassed waterway surface)
V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
V = 7.0 * (Sf^0.5) (short grass pasture surface)
V = 5.0 * (Sf^0.5) (woodland surface)
V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
Tr = 16 f (V) / (3600 ser/hr)

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$

R = Aq/Wp

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

n = Manning's roughness

New England Clean Energy Connect Project Fickett Road Station

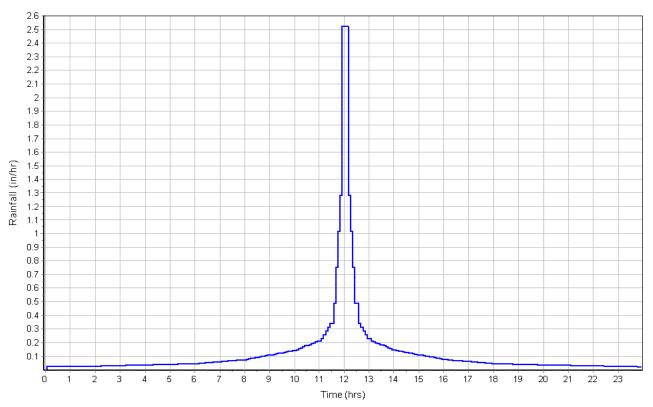
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	14.36	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.12	0.00	0.00
Computed Flow Time (min) :	13.94	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	625	0.00	0.00
Slope (%):	.582	0.00	0.00
Surface Type :	Grassed waterway	Unpaved	Unpaved
Velocity (ft/sec):	1.14	0.00	0.00
Computed Flow Time (min):	9.14	0.00	0.00
Total TOC (min)23.08			

Subbasin Runoff Results

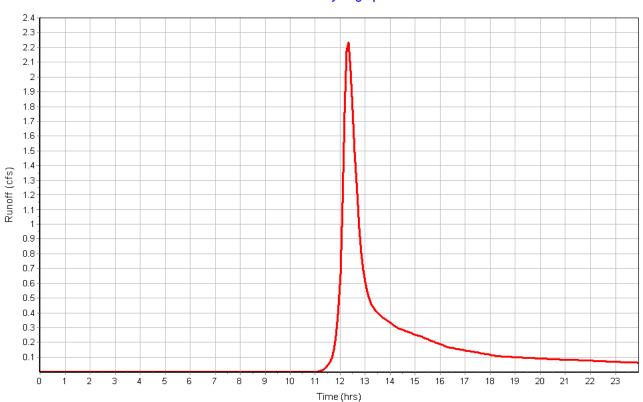
Total Rainfall (in)	3.00
Total Runoff (in)	0.88
Peak Runoff (cfs)	2.25
Weighted Curve Number	73.41
Time of Concentration (days hh:mm:ss)	0 00:23:05

Subbasin : A

Rainfall Intensity Graph



Runoff Hydrograph



Subbasin : B

Input Data

Area (ac)	8.76
Weighted Curve Number	73.22
Rain Gage ID	Rain Gage-01

Composite Curve Number

iiposite oui ve ivuilibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Brush, Good	8.27	D	73.00
Woods, Good	0.49	D	77.00
Composite Area & Weighted CN	8.76		73.22

Time of Concentration

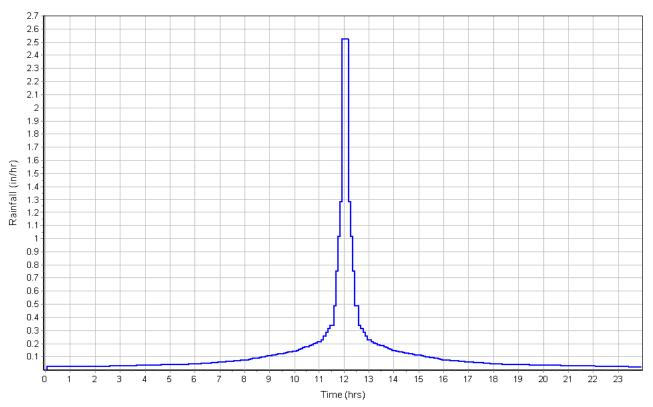
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.6	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	4.25	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.07	0.00	0.00
Computed Flow Time (min):	22.69	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	758	0.00	0.00
Slope (%):	.758	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	0.61	0.00	0.00
Computed Flow Time (min):	20.71	0.00	0.00
Total TOC (min)43.40			

Subbasin Runoff Results

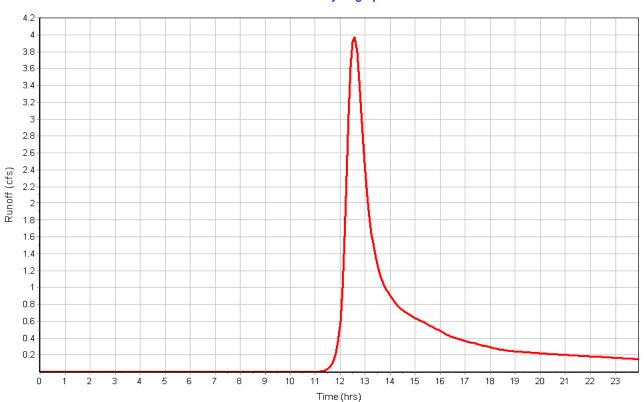
Total Rainfall (in)	
Peak Runoff (cfs)	3.98
Time of Concentration (days hh:mm:ss)	

Subbasin : B

Rainfall Intensity Graph



Runoff Hydrograph



Subbasin : C

Input Data

Area (ac)	0.35
Weighted Curve Number	74.60
Rain Gage ID	Rain Gage-01

Composite Curve Number

nposite Curve Number			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.03	D	77.00
Woods, Good	0.04	D	77.00
Brush, Good	0.08	D	73.00
Brush, Good	0.13	D	73.00
Woods, Good	0.07	D	77.00
Composite Area & Weighted CN	0.35		74.60

Time of Concentration

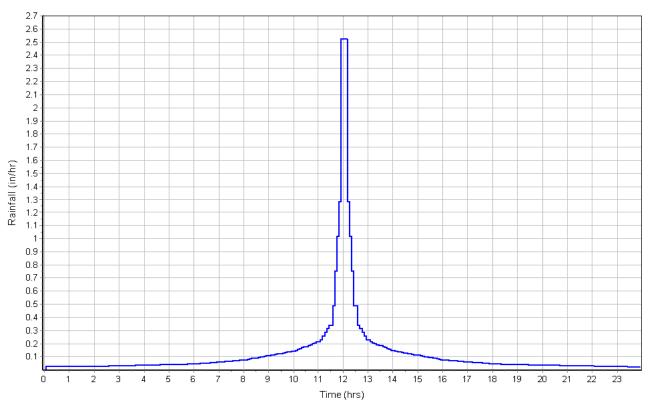
	0.1	0.1	
	Subarea	Subarea Subare	ea
Sheet Flow Computations	Α	B C	
Manning's Roughness :	.4	0.00 0.00	_
Flow Length (ft):	87	0.00 0.00	i
Slope (%):	10.35	0.00 0.00	,
2 yr, 24 hr Rainfall (in):	3.00	0.00 0.00	i
Velocity (ft/sec):	0.14	0.00 0.00	1
Computed Flow Time (min):	10.28	0.00 0.00)
	Subarea	Subarea Subare	ea
Shallow Concentrated Flow Computations	Α	в с	
Flow Length (ft):	313	0.00 0.00	_
Slope (%):	2.3	0.00 0.00	i
Surface Type :	Grass pasture	Unpaved Unpav	ed
Velocity (ft/sec):	1.06	0.00 0.00	i
Computed Flow Time (min):	4.92	0.00 0.00	,
Total TOC (min)15.20			

Subbasin Runoff Results

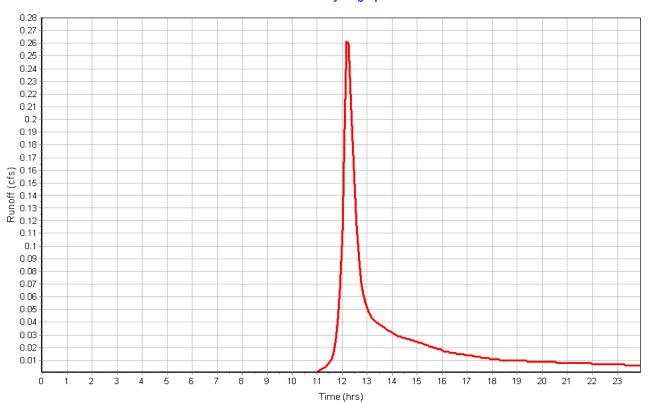
Total Rainfall (in)	3.00
Total Runoff (in)	0.94
Peak Runoff (cfs)	0.27
Weighted Curve Number	74.60
Time of Concentration (days hh:mm:ss)	0 00:15:12

Subbasin : C

Rainfall Intensity Graph



Runoff Hydrograph



Subbasin : D

Input Data

Area (ac)	0.12
Weighted Curve Number	77.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

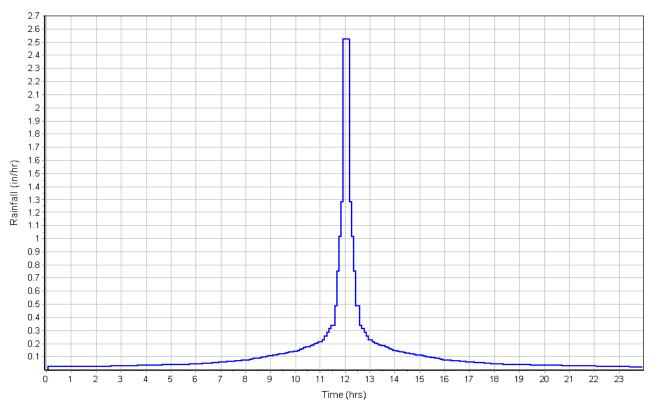
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	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Composite Area & Weighted CN	0.12		77.00

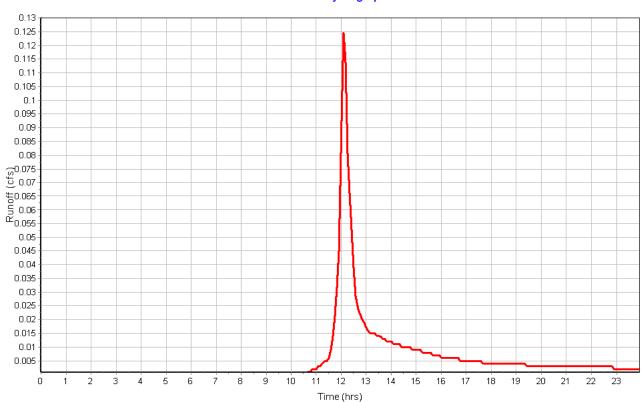
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.4	0.00	0.00
Flow Length (ft):	36	0.00	0.00
Slope (%):	5.55	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.09	0.00	0.00
Computed Flow Time (min):	6.51	0.00	0.00
Fotal TOC (min)6.51			

Total Rainfall (in)	3.00
Total Runoff (in)	1.07
Peak Runoff (cfs)	0.13
Weighted Curve Number	77.00
Time of Concentration (days hh:mm:ss)	0.00:06:31

Subbasin : D





Project Description

File Name Existing Conditions.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Aug 10, 2017	00:00:00
End Analysis On	Aug 11, 2017	00:00:00
Start Reporting On	Aug 10, 2017	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qty
Rain Gages	1
Subbasins	4
Nodes	4
Junctions	0
Outfalls	4
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	0
Channels	0
Pipes	0
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County		Period	Rainfall Depth (inches)	Rainfall Distribution
1	Rain Gage-01	Time Series	TS-10	Cumulative	inches	Maine	Cumberland (Southeast)	10	4.70	SCS Type III 24-hr

Subbasin Summary

Subbasin ID	Area	Weighted Curve			Total Runoff		Time of Concentration
		Number			Volume		
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
A	3.70	73.41	4.70	2.08	7.70	5.70	0 00:23:04
В	8.76	73.22	4.70	2.07	18.10	10.12	0 00:43:24
С	0.35	74.60	4.70	2.18	0.76	0.66	0 00:15:12
D	0.12	77.00	4.70	2.37	0.28	0.30	0 00:06:30

Δτρο

Soil Curve

Subbasin Hydrology

Subbasin: A

Input Data

Area (ac)	3.70
Weighted Curve Number	73.41
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Alca	3011	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.38	D	77.00
Brush, Good	3.32	D	73.00
Composite Area & Weighted CN	3.70		73.41

Time of Concentration

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$

Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation:

V = 16.1345 * (Sf^0.5) (unpaved surface)
V = 20.3282 * (Sf^0.5) (paved surface)
V = 15.0 * (Sf^0.5) (grassed waterway surface)
V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
V = 7.0 * (Sf^0.5) (short grass pasture surface)
V = 5.0 * (Sf^0.5) (woodland surface)
V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
Tr = 16 f (V) / (3600 ser/hr)

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$

R = Aq/Wp

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

n = Manning's roughness

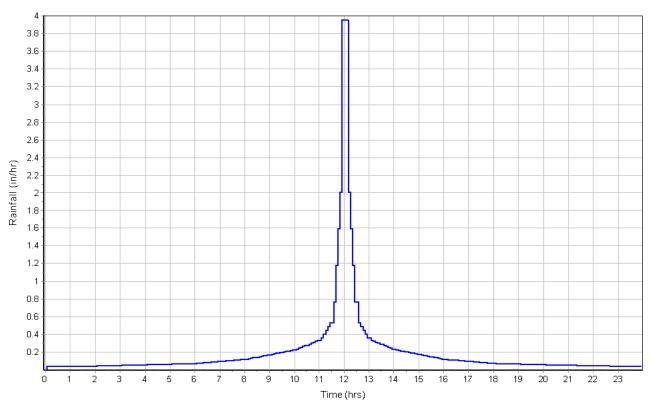
10 - Year Storm

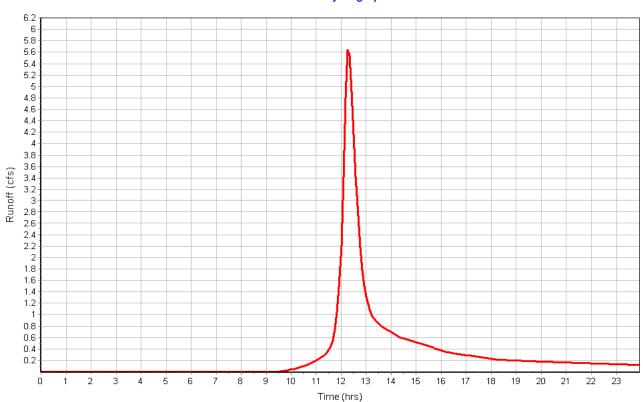
New England Clean Energy Connect Project Fickett Road Station

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	14.36	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.12	0.00	0.00
Computed Flow Time (min):	13.94	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Subarea A	Subarea B	Subarea C
Shallow Concentrated Flow Computations Flow Length (ft) :			
•	Α	В	С
Flow Length (ft):	A 625	0.00 0.00	0.00 0.00
Flow Length (ft): Slope (%):	A 625 .582	0.00 0.00	0.00 0.00
Flow Length (ft) : Slope (%) : Surface Type :	A 625 .582 Grassed waterway	8 0.00 0.00 Unpaved	0.00 0.00 Unpaved

Total Rainfall (in)	4.70
Total Runoff (in)	2.08
Peak Runoff (cfs)	5.70
Weighted Curve Number	73.41
Time of Concentration (days hh:mm:ss)	0 00:23:05

Subbasin : A





Subbasin : B

Input Data

Area (ac)	8.76
Weighted Curve Number	73.22
Rain Gage ID	Rain Gage-01

Composite Curve Number

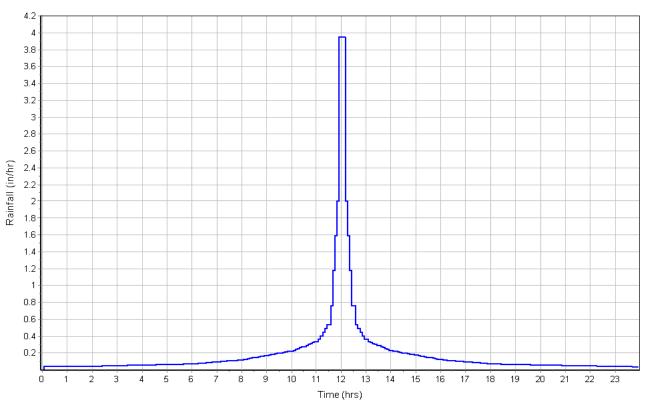
nposite Curve Number			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Brush, Good	8.27	D	73.00
Woods, Good	0.49	D	77.00
Composite Area & Weighted CN	8.76		73.22

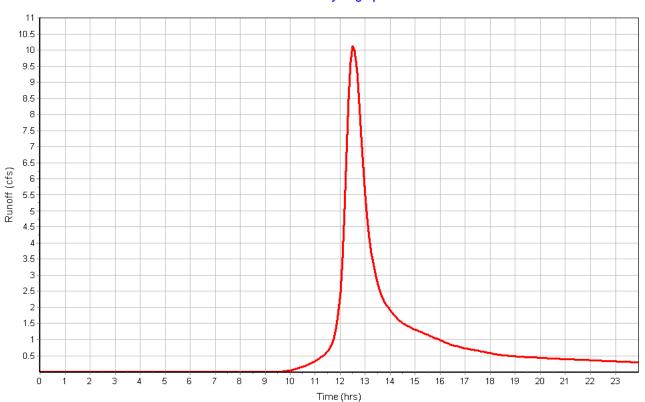
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.6	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	4.25	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.07	0.00	0.00
Computed Flow Time (min):	22.69	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	758	0.00	0.00
Slope (%):	.758	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	0.61	0.00	0.00
Computed Flow Time (min):	20.71	0.00	0.00
Total TOC (min)43.40			

Total Rainfall (in)	4.70
Total Runoff (in)	2.07
Peak Runoff (cfs)	10.12
Weighted Curve Number	73.22
Time of Concentration (days hh:mm:ss)	0.00.43.24

Subbasin : B





Subbasin : C

Input Data

Area (ac)	0.35
Weighted Curve Number	74.60
Rain Gage ID	Rain Gage-01

Composite Curve Number

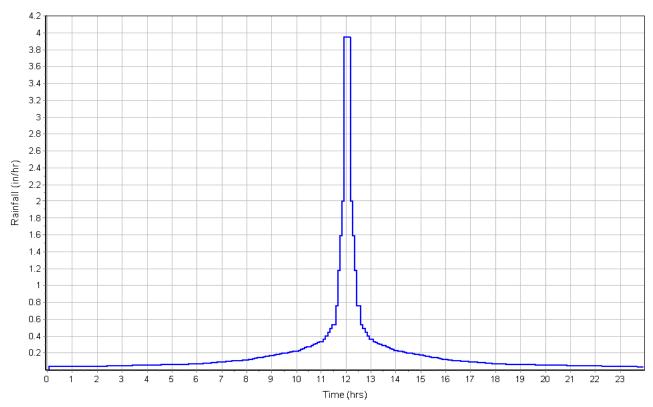
nposite Curve Number			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.03	D	77.00
Woods, Good	0.04	D	77.00
Brush, Good	0.08	D	73.00
Brush, Good	0.13	D	73.00
Woods, Good	0.07	D	77.00
Composite Area & Weighted CN	0.35		74.60

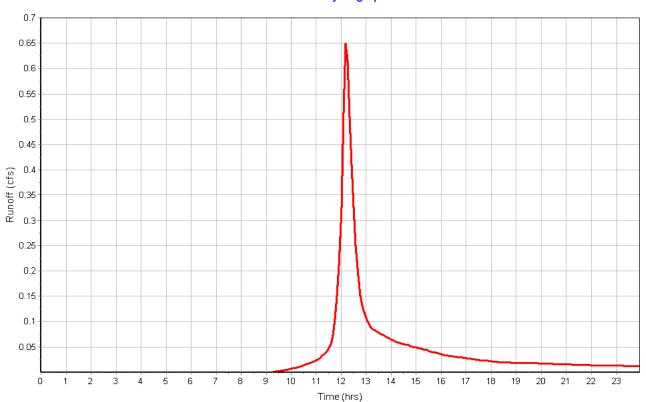
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	87	0.00	0.00
Slope (%):	10.35	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.14	0.00	0.00
Computed Flow Time (min):	10.28	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	313	0.00	0.00
Slope (%):	2.3	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	1.06	0.00	0.00
Computed Flow Time (min):	4.92	0.00	0.00
Total TOC (min)15.20			

Total Rainfall (in)	4.70
Total Runoff (in)	2.18
Peak Runoff (cfs)	0.66
Weighted Curve Number	74.60
Time of Concentration (days hh:mm:ss)	0 00:15:12

Subbasin : C





Subbasin : D

Input Data

Area (ac)	0.12
Weighted Curve Number	77.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

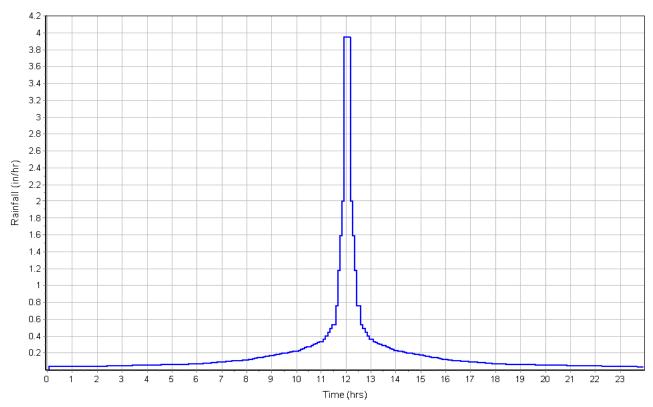
iposite oui ve ivanibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Composite Area & Weighted CN	0.12		77.00

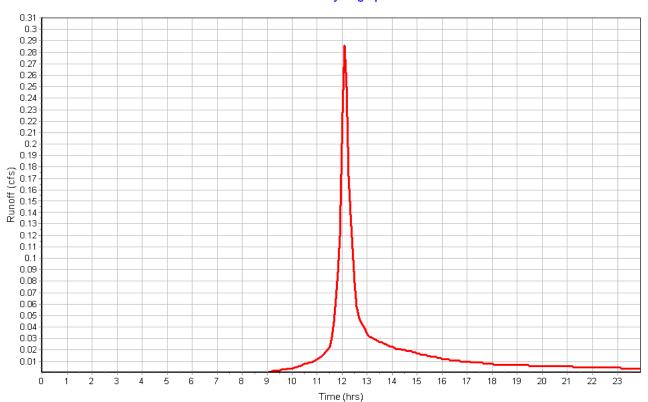
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	36	0.00	0.00
Slope (%):	5.55	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.09	0.00	0.00
Computed Flow Time (min):	6.51	0.00	0.00
Total TOC (min)6.51			

Total Rainfall (in)	4.70
Total Runoff (in)	2.37
Peak Runoff (cfs)	0.30
Weighted Curve Number	77.00
Time of Concentration (days hh:mm:ss)	0 00:06:31

Subbasin : D





Project Description

File Name Existing Conditions.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Aug 10, 2017	00:00:00
End Analysis On	Aug 11, 2017	00:00:00
Start Reporting On	Aug 10, 2017	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

(Qt
Rain Gages	1
Subbasins	4
Nodes	4
Junctions (0
Outfalls	4
Flow Diversions (0
Inlets (0
Storage Nodes (0
Links(0
Channels (0
Pipes (0
Pumps (0
Orifices	0
Weirs (0
Outlets (0
Pollutants	0
Land Uses	0

Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County	Period	Rainfall Depth (inches)	
1	Rain Gage-01	Time Series	TS-25	Cumulative	inches	Maine	Cumberland (Southeast)	25	5.50	SCS Type III 24-hr

Subbasin Summary

	Area	Weighted					Time of
ID		Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
		Number			Volume		
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
A	3.70	73.41	5.50	2.72	10.05	7.51	0 00:23:04
В	8.76	73.22	5.50	2.70	23.65	13.36	0 00:43:24
С	0.35	74.60	5.50	2.82	0.99	0.86	0 00:15:12
D	0.12	77.00	5.50	3.04	0.37	0.38	0 00:06:30

Subbasin Hydrology

Subbasin: A

Input Data

Area (ac)	3.70
Weighted Curve Number	73.41
Rain Gage ID	Rain Gage-01

Composite Curve Number

•	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.38	D	77.00
Brush, Good	3.32	D	73.00
Composite Area & Weighted CN	3.70		73.41

Time of Concentration

TOC Method: SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$

Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation:

V = 16.1345 * (Sf^0.5) (unpaved surface)
V = 20.3282 * (Sf^0.5) (paved surface)
V = 15.0 * (Sf^0.5) (grassed waterway surface)
V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
V = 7.0 * (Sf^0.5) (short grass pasture surface)
V = 5.0 * (Sf^0.5) (woodland surface)
V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
Tr = 16 f (V) / (3600 ser/hr)

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

Channel Flow Equation :

 $V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n$

R = Aq/Wp

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

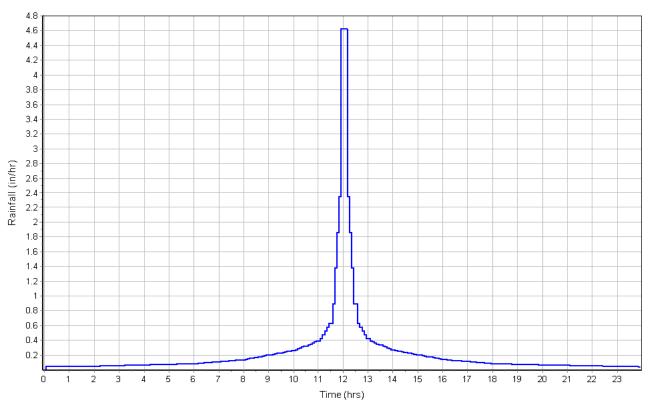
n = Manning's roughness

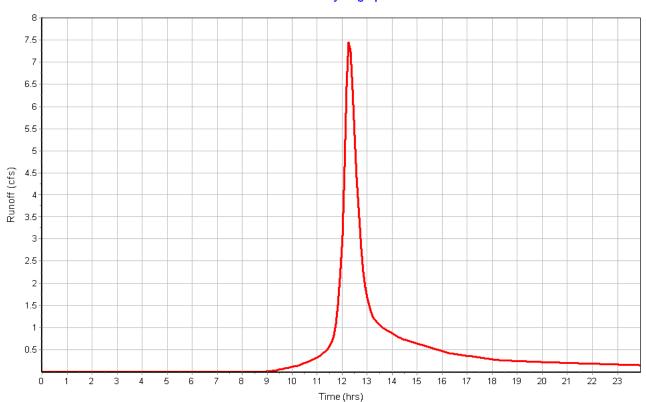
New England Clean Energy Connect Project Fickett Road Station

	Subarea	Subarea	Subarea
Sheet Flow Computations	A	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	14.36	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.12	0.00	0.00
Computed Flow Time (min) :	13.94	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
			0
Flow Length (ft):	625	0.00	0.00
Flow Length (ft) : Slope (%) :			
5 ()	625	0.00	0.00
Slope (%):	625 .582	0.00	0.00
Slope (%): Surface Type:	625 .582 Grassed waterway	0.00 0.00 Unpaved	0.00 0.00 Unpaved

Total Rainfall (in)	5.50
Total Runoff (in)	2.72
Peak Runoff (cfs)	7.51
Weighted Curve Number	73.41
Time of Concentration (days hh:mm:ss)	0 00:23:05

Subbasin : A





Subbasin : B

Input Data

Area (ac)	8.76
Weighted Curve Number	73.22
Rain Gage ID	Rain Gage-01

Composite Curve Number

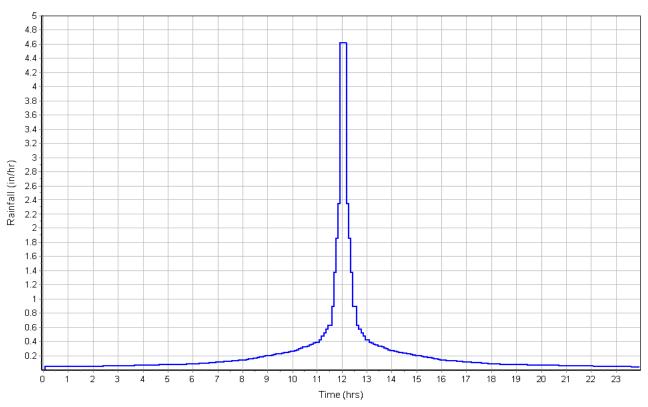
nposite Curve Number			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Brush, Good	8.27	D	73.00
Woods, Good	0.49	D	77.00
Composite Area & Weighted CN	8.76		73.22

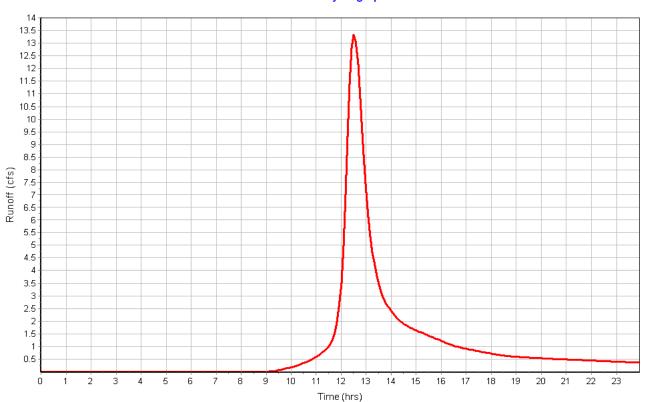
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	4.25	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.07	0.00	0.00
Computed Flow Time (min):	22.69	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	758	0.00	0.00
Slope (%):	.758	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	0.61	0.00	0.00
Computed Flow Time (min):	20.71	0.00	0.00
Total TOC (min)43.40			

Total Rainfall (in)	5.50
Total Runoff (in)	2.70
Peak Runoff (cfs)	13.36
Weighted Curve Number	73.22
Time of Concentration (days hh:mm:ss)	0 00:43:24

Subbasin : B





Subbasin : C

Input Data

Area (ac)	0.35
Weighted Curve Number	74.60
Rain Gage ID	Rain Gage-01

Composite Curve Number

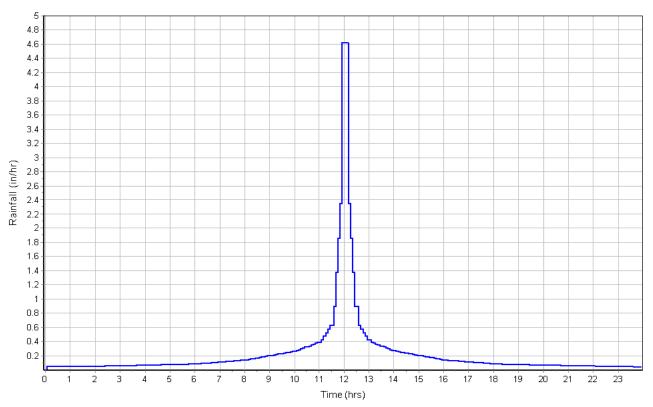
nposite Curve Number				
	Area	Soil	Curve	
Soil/Surface Description	(acres)	Group	Number	
Woods, Good	0.03	D	77.00	
Woods, Good	0.04	D	77.00	
Brush, Good	0.08	D	73.00	
Brush, Good	0.13	D	73.00	
Woods, Good	0.07	D	77.00	
Composite Area & Weighted CN	0.35		74.60	

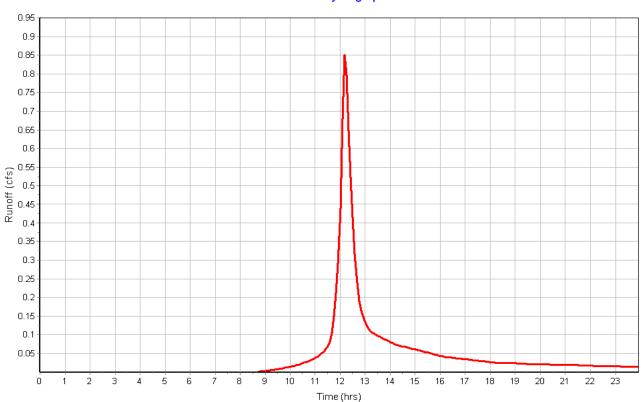
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	87	0.00	0.00
Slope (%):	10.35	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.14	0.00	0.00
Computed Flow Time (min):	10.28	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	313	0.00	0.00
Slope (%):	2.3	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	1.06	0.00	0.00
Computed Flow Time (min):	4.92	0.00	0.00
Total TOC (min)15.20			

Total Rainfall (in)	5.50
Total Runoff (in)	2.82
Peak Runoff (cfs)	0.86
Weighted Curve Number	74.60
Time of Concentration (days hh:mm:ss)	0 00:15:12

Subbasin : C





Subbasin: D

Input Data

Area (ac)	0.12
Weighted Curve Number	77.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

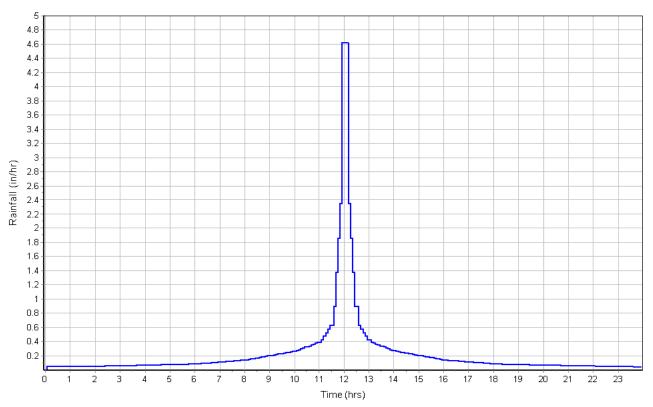
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Composite Area & Weighted CN	0.12		77.00

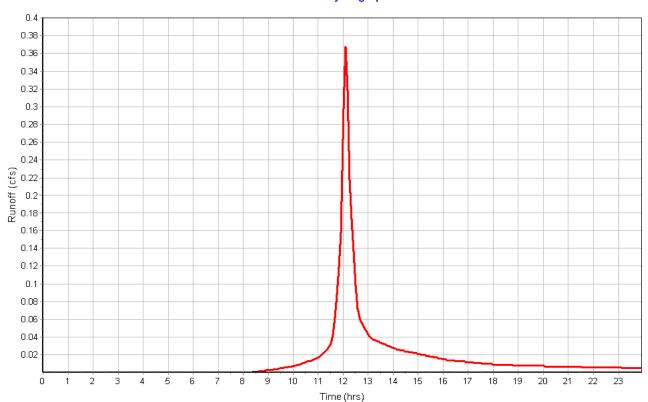
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	36	0.00	0.00
Slope (%):	5.55	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.09	0.00	0.00
Computed Flow Time (min):	6.51	0.00	0.00
Total TOC (min)6.51			

Total Rainfall (in)	5.50
Total Runoff (in)	3.04
Peak Runoff (cfs)	0.38
Weighted Curve Number	77.00
Time of Concentration (days hh:mm:ss)	0 00:06:31

Subbasin : D





Project Description

File Name Proposed Conditions_SMT.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Aug 15, 2017	00:00:00
End Analysis On	Aug 17, 2017	00:00:00
Start Reporting On	Aug 15, 2017	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qt
Rain Gages	1
Subbasins	6
Nodes	7
Junctions	2
Outfalls	5
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	2
Channels	0
Pipes	2
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County	Period	Rainfall Depth (inches)	
1	Rain Gage-01	Time Series	TS-02	Cumulative	inches	Maine	Cumberland (Southeast)	2	3.00	SCS Type III 24-hr

Subbasin Summary

Subbasin	Area	Weighted	Total	Total	Total	Peak	Time of
ID		Curve	Rainfall	Runoff	Runoff	Runoff	Concentration
		Number			Volume		
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
A	3.95	74.46	3.00	0.93	3.68	2.33	0 00:29:55
B-1	2.55	66.95	3.00	0.58	1.49	1.30	0 00:07:01
B-2	7.03	70.54	3.00	0.74	5.20	1.84	0 01:17:51
С	0.21	75.29	3.00	0.98	0.20	0.15	0 00:20:30
CulvertDrainageArea	0.68	75.00	3.00	0.96	0.65	0.67	0 00:05:00
D	0.12	77.00	3.00	1.07	0.13	0.13	0 00:06:30

Node Summary

Element	Element	Invert	Peak
ID	Type	Elevation	Inflow

		(ft)	(cfs)
CulvertInlet	Junction	181.00	0.64
Out_B1andB2	Junction	176.00	2.06
CulvertOutlet	Outfall	180.35	0.64
OUT-A	Outfall	180.00	2.31
OUT-B	Outfall	176.00	2.06
OUT-C	Outfall	178.00	0.15
OUT-D	Outfall	190.82	0.12

New England Clean Energy 2 - Year Storm
Connect Project
Fickett Road Station

Link Summary

Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow	Peak Flow
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Velocity	Depth
		Node			Elevation E	Elevation							
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)	(ft/sec)	(ft)
Direct_to_OutE	Pipe -	Out_B1andB2	OUT-B	1715.96	0.00	0.00	0.0000	0.000	0.0150	2.06	0.00	0.00	0.00
Link-03	Pipe	CulvertInlet	CulvertOutlet	45.00	181.00	180.55	1.0000	15.000	0.0150	0.64	5.60	3.04	0.29

Subbasin Hydrology

Subbasin: A

Input Data

Area (ac)	3.95
Weighted Curve Number	74.46
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.33	D	77.00
Gravel roads	0.10	D	91.00
> 75% grass cover, Good	0.38	D	80.00
Brush, Good	3.14	D	73.00
Composite Area & Weighted CN	3.95		74.46

Time of Concentration

TOC Method : SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$

Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation :

V = 16.1345 * (Sf^0.5) (unpaved surface) V = 20.3282 * (Sf^0.5) (paved surface) V = 15.0 * (Sf^0.5) (grassed waterway surface) V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)

V = 9.0 * (Sf^0.5) (really bare & utilities startace)
V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
V = 7.0 * (Sf^0.5) (short grass pasture surface)
V = 5.0 * (Sf^0.5) (woodland surface)

V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

Channel Flow Equation :

V = (1.49 * (R^(2/3)) * (Sf^0.5)) / n

R = Aq / Wp Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

n = Manning's roughness

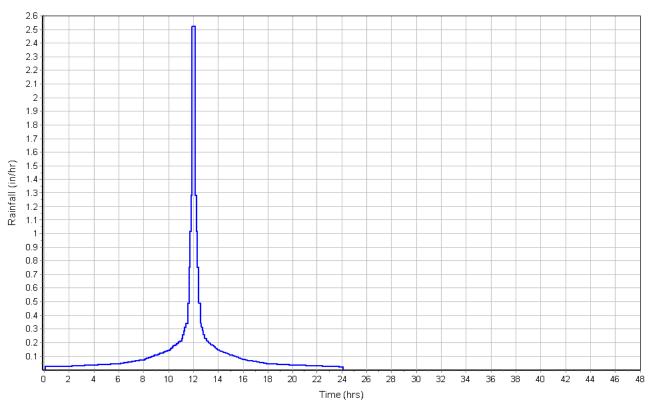
2 - Year Storm

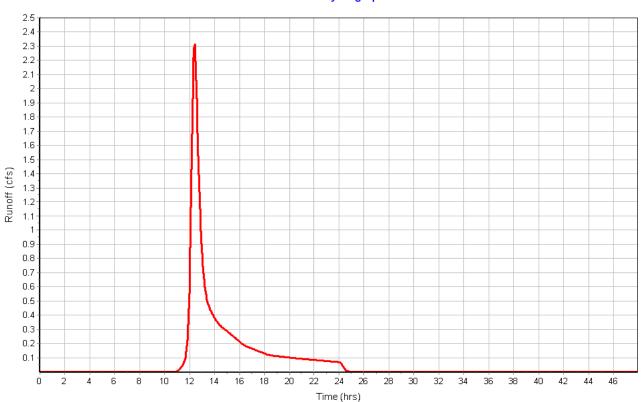
New England Clean Energy Connect Project Fickett Road Station

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	45	0.00	0.00
Slope (%):	50	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.23	0.00	0.00
Computed Flow Time (min) :	3.23	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	264	574	0.00
Slope (%):	.76	.35	0.00
Surface Type :	Grassed waterway	Grass pasture	Unpaved
Velocity (ft/sec):	1.31	0.41	0.00
Computed Flow Time (min):	3.36	23.33	0.00
Total TOC (min)29.92			

Total Rainfall (in)	3.00
Total Runoff (in)	0.93
Peak Runoff (cfs)	2.33
Weighted Curve Number	74.46
Time of Concentration (days hh:mm:ss)	0 00:29:55

Subbasin : A





Subbasin: B-1

Input Data

Area (ac)	2.55
Weighted Curve Number	66.95
Rain Gage ID	Rain Gage-01

Composite Curve Number

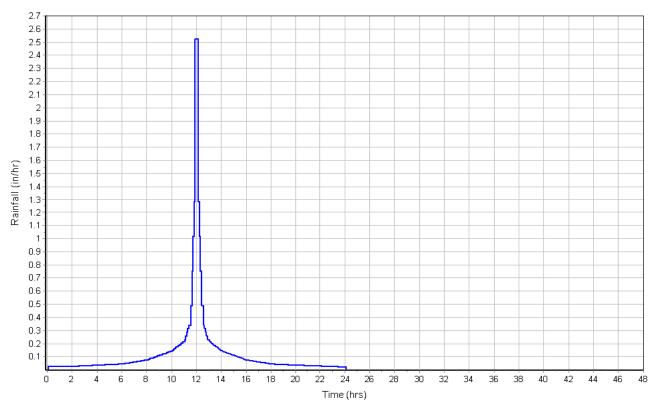
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Gravel-Pad	1.88	D	60.00
Rooftops	0.24	D	98.00
> 75% grass cover, Good	0.43	D	80.00
Composite Area & Weighted CN	2.55		66.95

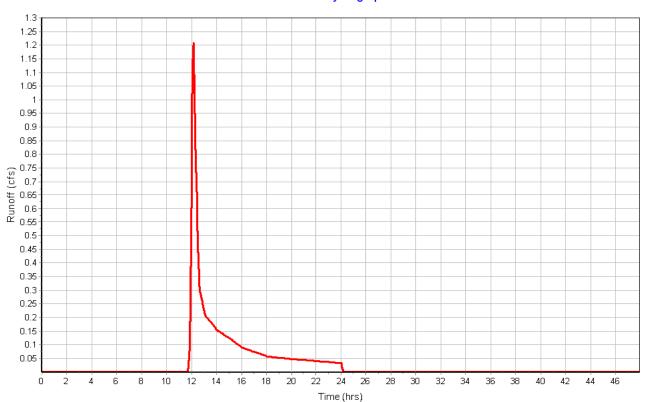
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	38	0.00	0.00
Slope (%):	50	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.22	0.00	0.00
Computed Flow Time (min):	2.82	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	385	0.00	0.00
Slope (%):	1.04	0.00	0.00
Surface Type :	Grassed waterway	Grass pasture rass pasture	
Velocity (ft/sec):	1.53	0.00	0.00
Computed Flow Time (min):	4.19	0.00	0.00
Total TOC (min)7.02			

Total Rainfall (in)	3.00
Total Runoff (in)	0.58
Peak Runoff (cfs)	1.30
Weighted Curve Number	66.95
Time of Concentration (days hh:mm:ss)	0 00:07:01

Subbasin : B-1





Subbasin : B-2

Input Data

Area (ac)	7.03
Weighted Curve Number	
Rain Gage ID	Rain Gage-01

Composite Curve Number

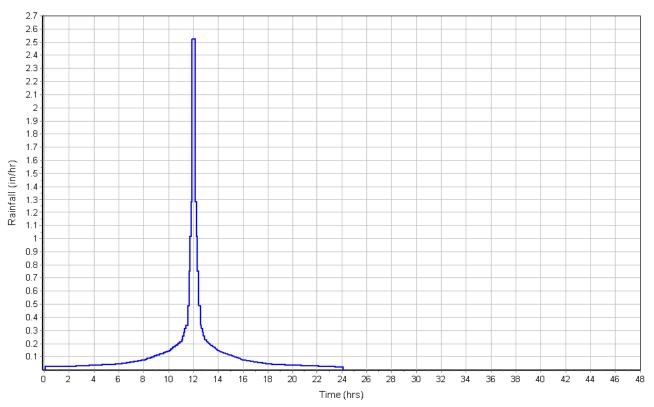
nposite Curve Number			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Brush, Good	5.19	D	73.00
Gravel roads	0.05	D	91.00
> 75% grass cover, Good	0.16	D	80.00
Gravel_Pad	1.58	D	60.00
ConcreteFoundations	0.05	D	98.00
Composite Area & Weighted CN	7.03		70.54

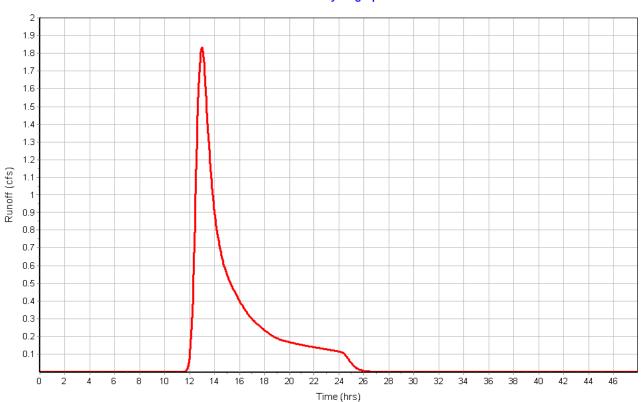
Time of Concentration

Sheet Flow Computations Manning's Roughness: Flow Length (ft): Slope (%): 2 yr, 24 hr Rainfall (in): Velocity (ft/sec): Computed Flow Time (min):	Subarea	Subarea	Subarea
	A	B	C
	.4	0.00	0.00
	100	0.00	0.00
	.25	0.00	0.00
	3.00	0.00	0.00
	0.03	0.00	0.00
	50.95	0.00	0.00
Shallow Concentrated Flow Computations Flow Length (ft): Slope (%): Surface Type: Velocity (ft/sec):	Subarea	Subarea	Subarea
	A	B	C
	791	0.00	0.00
	.5	0.00	0.00
	Grass pasture	Unpaved	Unpaved
	0.49	0.00	0.00
Computed Flow Time (min) : Total TOC (min)77.86	26.90	0.00	0.00

Total Rainfall (in)	3.00
Total Runoff (in)	0.74
Peak Runoff (cfs)	1.84
Weighted Curve Number	70.54
Time of Concentration (days hh:mm:ss)	0 01:17:52

Subbasin : B-2





Subbasin : C

Input Data

Area (ac)	0.21
Weighted Curve Number	75.29
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Brush, Good	0.09	D	73.00
Composite Area & Weighted CN	0.21		75.29

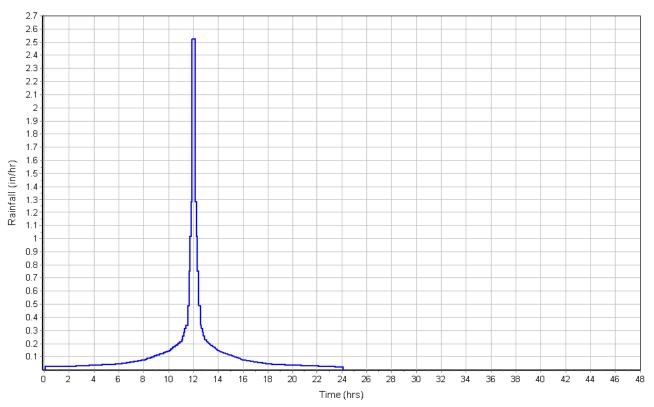
Time of Concentration

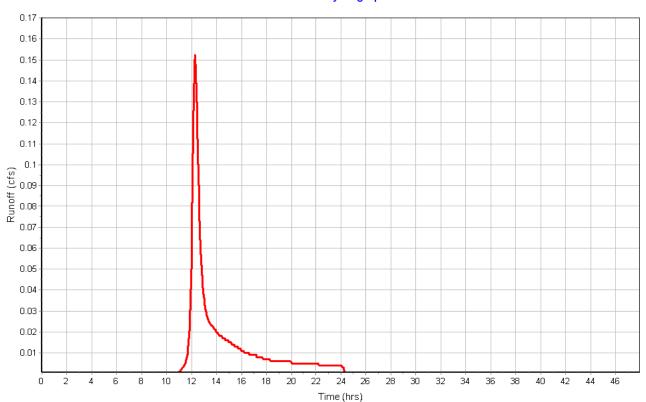
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	80	0.00	0.00
Slope (%):	4.31	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.07	0.00	0.00
Computed Flow Time (min):	18.88	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	A	В	С
Flow Length (ft):	182	0.00	0.00
Slope (%):	7.1	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	1.87	0.00	0.00
Computed Flow Time (min):	1.62	0.00	0.00
Total TOC (min)20.50			

Total Rainfall (in)	3.00
Total Runoff (in)	
Peak Runoff (cfs)	0.15
Weighted Curve Number	
Time of Concentration (days hh:mm:ss)	0.00-20-30

Subbasin : C

Rainfall Intensity Graph





New England Clean Energy Connect Project Fickett Road Station

Subbasin : CulvertDrainageArea

Input Data

Area (ac)	0.68
Weighted Curve Number	75.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.68	-	75.00
Composite Area & Weighted CN	0.68		75.00

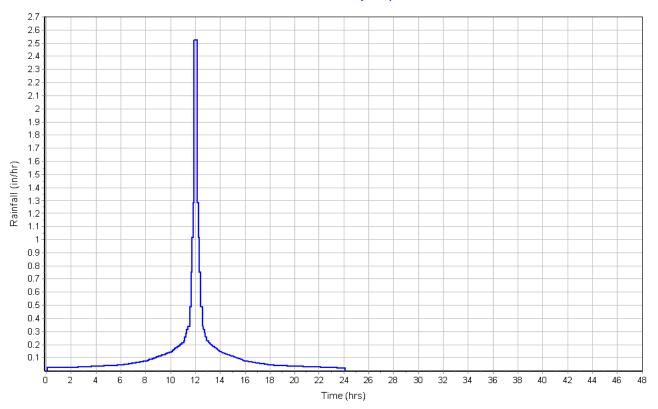
Time of Concentration

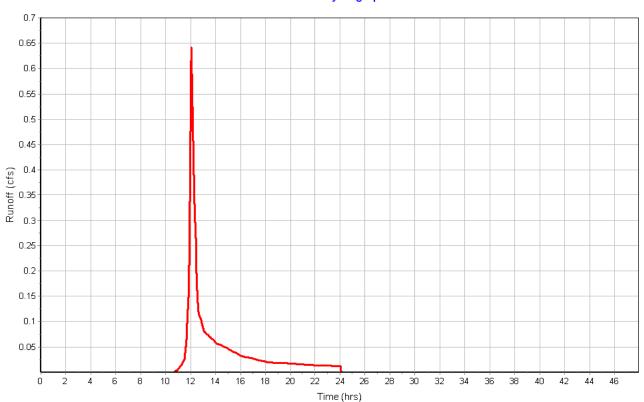
User-Defined TOC override (minutes): 5

Total Rainfall (in)	3.00
Total Runoff (in)	0.96
Peak Runoff (cfs)	0.67
Weighted Curve Number	75.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

Subbasin : CulvertDrainageArea

Rainfall Intensity Graph





Subbasin : D

Input Data

Area (ac)	0.12
Weighted Curve Number	77.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Composite Area & Weighted CN	0.12		77.00

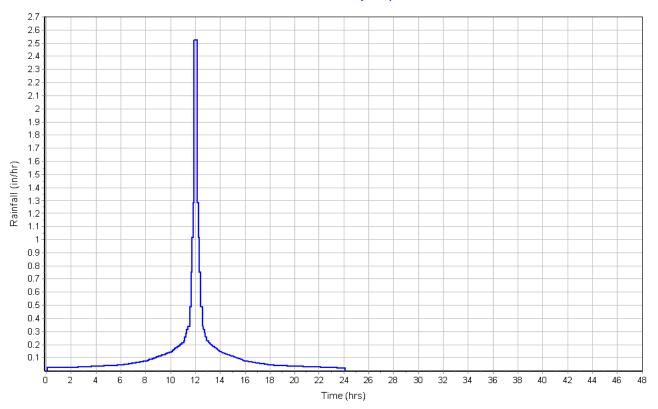
Time of Concentration

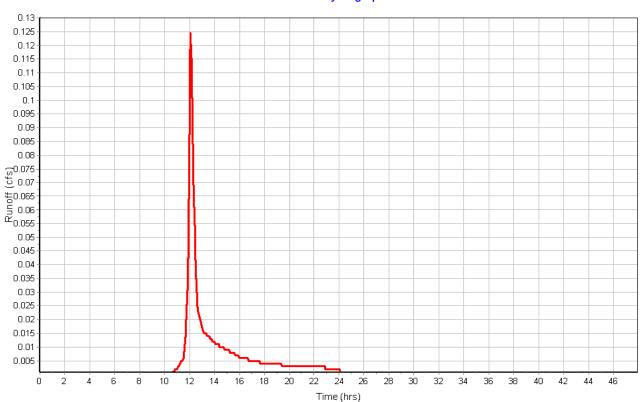
Sheet Flow Computations	Subarea A	Subarea B	Subarea C
Manning's Roughness:	.4	0.00	0.00
Flow Length (ft):	36	0.00	0.00
Slope (%):	5.55	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.09	0.00	0.00
Computed Flow Time (min):	6.51	0.00	0.00
Total TOC (min)6.51			

Total Rainfall (in)	3.00
Total Runoff (in)	1.07
Peak Runoff (cfs)	0.13
Weighted Curve Number	77.00
Time of Concentration (days hh:mm:ss)	0 00:06:31

Subbasin : D

Rainfall Intensity Graph





New England Clean Energy Connect Project Fickett Road Station

Junction Input

Element	Invert	Ground/Rim
ID	Elevation	(Max)
		Elevation
	(ft)	(ft)
CulvertInlet	181.00	184.00
Out B1andB2	176 00	6.00

Junction Results

Element ID		Max HGL Elevation Attained	Max HGL Depth Attained	Min Freeboard Attained	Average HGL Elevation Attained	Time of Max HGL Occurrence
0.1	(cfs)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)
CulvertInlet Out_B1andB2	0.64 2.06	181.29 176.00	0.29 0.00	2.71 0.00	181.02 176.00	0 12:10 0 00:00

Pipe Input

Element ID	Length	Inlet Invert	Outlet Invert	Average Pipe Slope Shape	Pipe Diameter or		Manning's Roughness	
				Elevation Elevation		Height		Ü
	(ft)	(ft)	(ft)	(%)	(in)	(in)		
Direct_to_OutB	1715.96	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150	
Link-03	45.00	181.00	180.55	1.0000 CIRCULAR	15.000	15.000	0.0150	

Pipe Results

Element	Peak	Time of	Design Flow	Peak Flow	Peak Flow
ID	Flow	Peak Flow	Capacity	Velocity	Depth
		Occurrence			
	(cfs)	(days hh:mm)	(cfs)	(ft/sec)	(ft)
Direct_to_OutB	2.06	0 13:00	0.00	0.00	0.00
Link-03	0.64	0 12:10	5.60	3.04	0.29

Project Description

File Name Proposed Conditions_SMT.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Aug 15, 2017	00:00:00
End Analysis On	Aug 17, 2017	00:00:00
Start Reporting On	Aug 15, 2017	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qt
Rain Gages	1
Subbasins	6
Nodes	7
Junctions	2
Outfalls	5
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	2
Channels	0
Pipes	2
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County	Period	Rainfall Depth (inches)	Rainfall Distribution
1	Rain Gage-01	Time Series	TS-10	Cumulative	inches	Maine	Cumberland (Southeast)	10	4.70	SCS Type III 24-hr

Subbasin Summary

Subbasin ID	Area	Weighted Curve	Total Rainfall	Total Runoff	Total Runoff	Peak Runoff	Time of Concentration
.5		Number	- tannan		Volume		00.1001.1141.011
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
A	3.95	74.46	4.70	2.16	8.55	5.71	0 00:29:55
B-1	2.55	66.95	4.70	1.59	4.06	4.05	0 00:07:01
B-2	7.03	70.54	4.70	1.86	13.05	5.14	0 01:17:51
С	0.21	75.29	4.70	2.23	0.47	0.37	0 00:20:30
CulvertDrainageArea	0.68	75.00	4.70	2.21	1.50	1.58	0 00:05:00
D	0.12	77.00	4.70	2.37	0.28	0.30	0 00:06:30

Node Summary

Element	Element	Invert	Peak
ID	Type	Elevation	Inflow

		(ft)	(cfs)
CulvertInlet	Junction	181.00	1.54
Out_B1andB2	Junction	176.00	5.73
CulvertOutlet	Outfall	180.35	1.53
OUT-A	Outfall	180.00	5.67
OUT-B	Outfall	176.00	5.73
OUT-C	Outfall	178.00	0.37
OUT-D	Outfall	190.82	0.29

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Connect Project
Fickett Road Station

Link Summary

Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow	Peak Flow
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Velocity	Depth
		Node			Elevation	Elevation							
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)	(ft/sec)	(ft)
Direct_to_OutB	Pipe	Out_B1andB2	OUT-B	1715.96	0.00	0.00	0.0000	0.000	0.0150	5.73	0.00	0.00	0.00
Link-03	Pipe	CulvertInlet	CulvertOutlet	45.00	181.00	180.55	1.0000	15.000	0.0150	1.53	5.60	3.89	0.45

Subbasin Hydrology

Subbasin: A

Input Data

Area (ac)	3.95
Weighted Curve Number	74.46
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.33	Ď	77.00
Gravel roads	0.10	D	91.00
> 75% grass cover, Good	0.38	D	80.00
Brush, Good	3.14	D	73.00
Composite Area & Weighted CN	3.95		74.46

Time of Concentration

TOC Method : SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$

Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation :

V = 16.1345 * (Sf^0.5) (unpaved surface) V = 20.3282 * (Sf^0.5) (paved surface) V = 15.0 * (Sf^0.5) (grassed waterway surface) V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)

V = 9.0 * (Sf^0.5) (cultivated straight rows surface) V = 7.0 * (Sf^0.5) (short grass pasture surface)

 $V = 5.0 * (Sf^0.5)$ (woodland surface)

V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

Channel Flow Equation :

V = (1.49 * (R^(2/3)) * (Sf^0.5)) / n

R = Aq / Wp Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

n = Manning's roughness

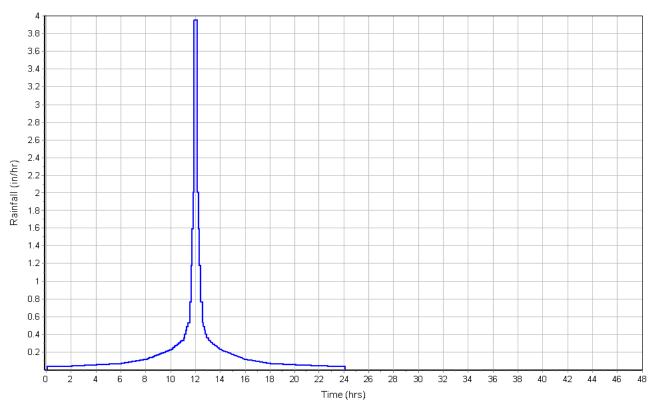
New England Clean Energy Connect Project Fickett Road Station

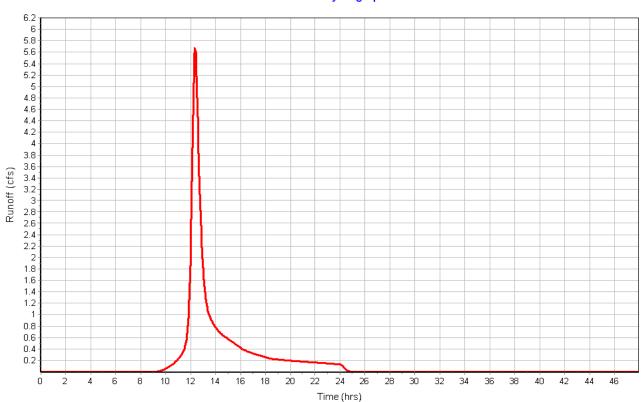
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	45	0.00	0.00
Slope (%):	50	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.23	0.00	0.00
Computed Flow Time (min):	3.23	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	264	574	0.00
Slope (%):	.76	.35	0.00
Surface Type :	Grassed waterway	Grass pasture	Unpaved
Velocity (ft/sec):	1.31	0.41	0.00
Computed Flow Time (min):	3.36	23.33	0.00
Total TOC (min)29.92			

Total Rainfall (in)	4.70
Total Runoff (in)	2.16
Peak Runoff (cfs)	5.71
Weighted Curve Number	74.46
Time of Concentration (days hh:mm:ss)	0 00:29:55

Subbasin : A

Rainfall Intensity Graph





Subbasin: B-1

Input Data

Area (ac)	2.55
Weighted Curve Number	66.95
Rain Gage ID	Rain Gage-01

Composite Curve Number

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	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Gravel-Pad	1.88	D	60.00
Rooftops	0.24	D	98.00
> 75% grass cover, Good	0.43	D	80.00
Composite Area & Weighted CN	2.55		66.95

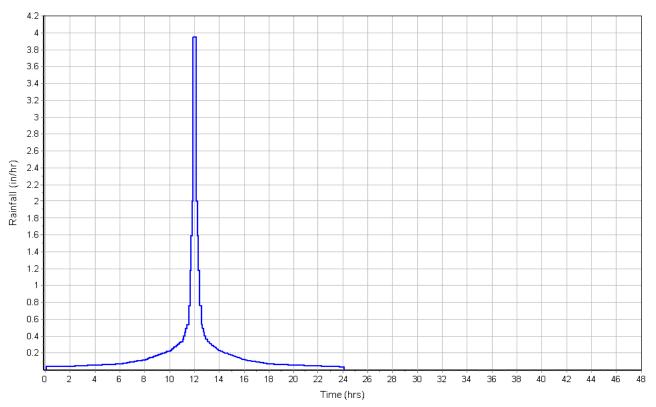
Time of Concentration

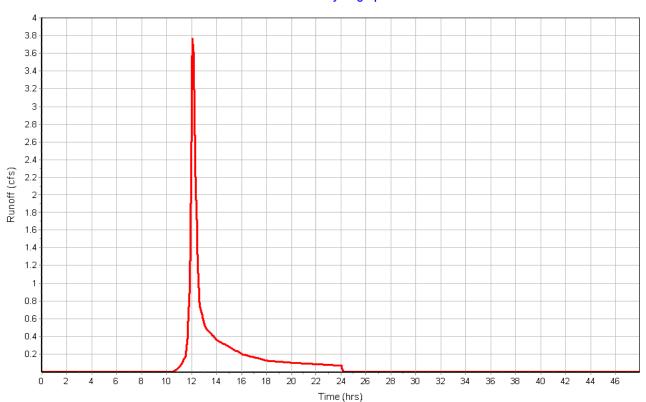
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.4	0.00	0.00
Flow Length (ft):	38	0.00	0.00
Slope (%):	50	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.22	0.00	0.00
Computed Flow Time (min):	2.82	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	385	0.00	0.00
Slope (%):	1.04	0.00	0.00
Surface Type :	Grassed waterway	Grass pasture	e rass pasture
Velocity (ft/sec):	1.53	0.00	0.00
Computed Flow Time (min):	4.19	0.00	0.00
Total TOC (min)			

Total Rainfall (in)	4.70
Total Runoff (in)	1.59
Peak Runoff (cfs)	4.05
Weighted Curve Number	66.95
Time of Concentration (days hh:mm:ss)	0 00:07:01

Subbasin : B-1

Rainfall Intensity Graph





Subbasin : B-2

Input Data

Area (ac)	7.03
Weighted Curve Number	70.54
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Brush, Good	5.19	D	73.00
Gravel roads	0.05	D	91.00
> 75% grass cover, Good	0.16	D	80.00
Gravel_Pad	1.58	D	60.00
ConcreteFoundations	0.05	D	98.00
Composite Area & Weighted CN	7.03		70.54

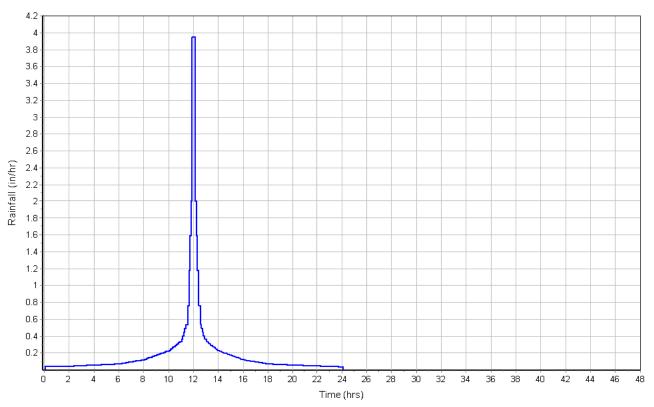
Time of Concentration

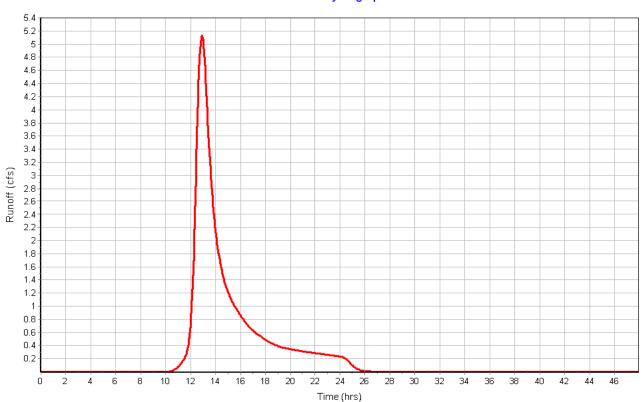
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.4	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	.25	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.03	0.00	0.00
Computed Flow Time (min):	50.95	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	791	0.00	0.00
Slope (%):	.5	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	0.49	0.00	0.00
Computed Flow Time (min):	26.90	0.00	0.00
Total TOC (min)77.86			

Total Rainfall (in)	4.70
Total Runoff (in)	1.86
Peak Runoff (cfs)	5.14
Weighted Curve Number	70.54
Time of Concentration (days hh:mm:ss)	0 01:17:52

Subbasin : B-2

Rainfall Intensity Graph





Subbasin : C

Input Data

Area (ac)	0.21
Weighted Curve Number	75.29
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Brush, Good	0.09	D	73.00
Composite Area & Weighted CN	0.21		75.29

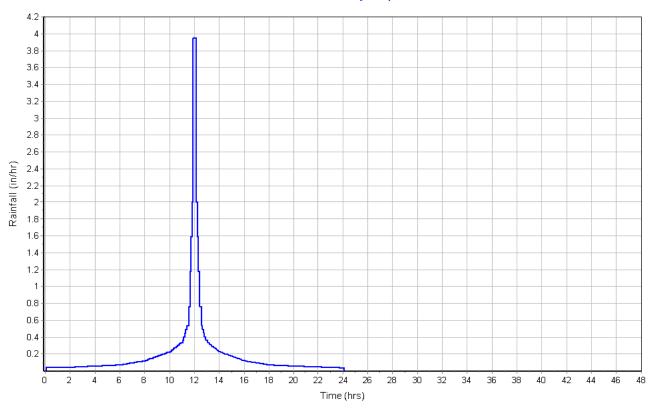
Time of Concentration

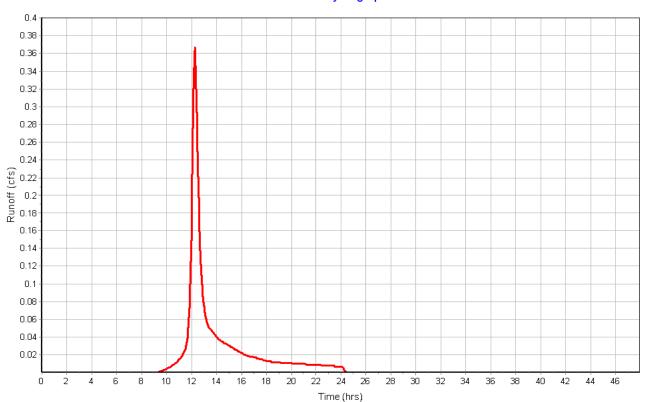
	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	80	0.00	0.00
Slope (%):	4.31	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.07	0.00	0.00
Computed Flow Time (min):	18.88	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	A	В	С
Flow Length (ft):	182	0.00	0.00
Slope (%):	7.1	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	1.87	0.00	0.00
Computed Flow Time (min):	1.62	0.00	0.00
Total TOC (min)20.50			

Total Rainfall (in)	4.70
Total Runoff (in)	2.23
Peak Runoff (cfs)	0.37
Weighted Curve Number	75.29
Time of Concentration (days hh:mm:ss)	0 00:20:30

Subbasin : C

Rainfall Intensity Graph





New England Clean Energy Connect Project Fickett Road Station

Subbasin : CulvertDrainageArea

Input Data

Area (ac)	0.68
Weighted Curve Number	75.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
-	0.68	-	75.00
Composite Area & Weighted CN	0.68		75.00

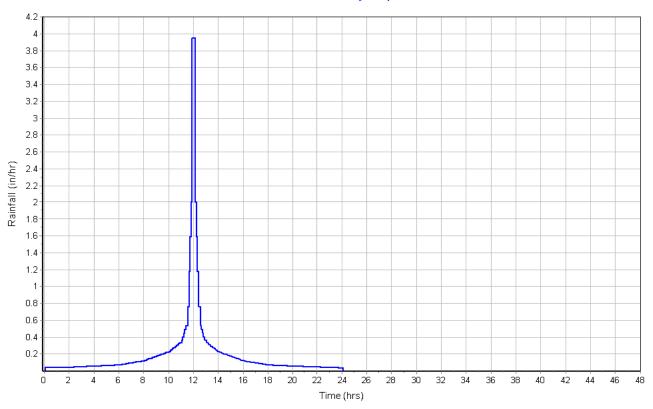
Time of Concentration

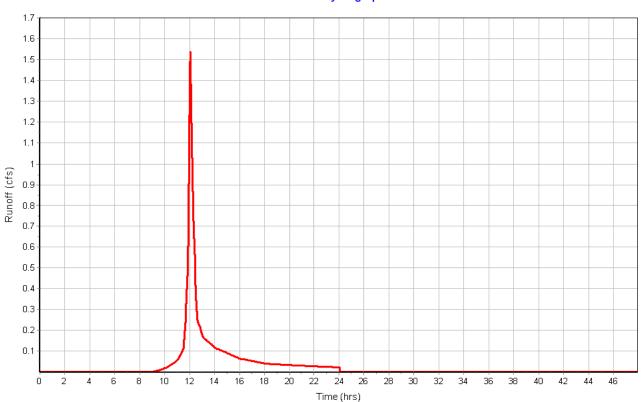
User-Defined TOC override (minutes): 5

Total Rainfall (in)	4.70
Total Runoff (in)	2.21
Peak Runoff (cfs)	1.58
Weighted Curve Number	75.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

Subbasin : CulvertDrainageArea

Rainfall Intensity Graph





Subbasin : D

Input Data

Area (ac)	0.12
Weighted Curve Number	77.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

iiposite cui ve ivuilibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Composite Area & Weighted CN	0.12		77.00

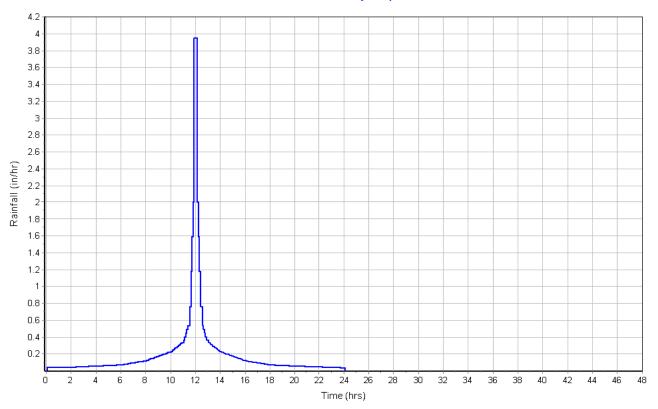
Time of Concentration

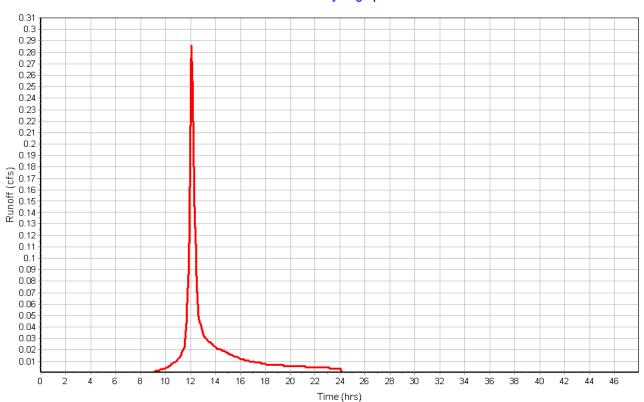
Sheet Flow Computations Manning's Roughness: Flow Length (ft): Slope (%): 2 yr, 24 hr Rainfall (in): Velocity (ft/sec): Computed Flow Time (min):	Subarea A .4 .36 5.55 3.00 0.09 6.51	Subarea B 0.00 0.00 0.00 0.00 0.00 0.00	Subarea C 0.00 0.00 0.00 0.00 0.00 0.00
Total TOC (min)6.51	0.51	0.00	0.00

Total Rainfall (in)	4.70
Total Runoff (in)	2.37
Peak Runoff (cfs)	0.30
Weighted Curve Number	77.00
Time of Concentration (days hh:mm:ss)	0 00:06:31

Subbasin : D

Rainfall Intensity Graph





Junction Input

Element	Invert	Ground/Rim
ID	Elevation	(Max)
		Elevation
	(ft)	(ft)
CulvertInlet	181.00	184.00
Out_B1andB2	176.00	6.00

Junction Results

Element ID		Max HGL Elevation Attained		Min Freeboard Attained	Average HGL Elevation Attained	Time of Max HGL Occurrence
	(cfs)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)
CulvertInlet	1.54	181.45	0.45	2.55	181.03	0 12:10
Out_B1andB2	5.73	176.00	0.00	0.00	176.00	0 00:00

Pipe Input

Element	Length	Inlet	Outlet	Average Pipe	Pipe	Pipe	Manning's
ID		Invert	Invert	Slope Shape	Diameter or	Width	Roughness
	1	Elevation	Elevation		Height		
	(ft)	(ft)	(ft)	(%)	(in)	(in)	
Direct_to_OutB	1715.96	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150
Link-03	45.00	181.00	180.55	1.0000 CIRCULAR	15.000	15.000	0.0150

Proposed Conditions Hydraulic/Hydrologic Report

Pipe Results

Element	Peak	Time of	Design Flow	Peak Flow	Peak Flow
ID	Flow	Peak Flow	Capacity	Velocity	Depth
		Occurrence			
	(cfs)	(days hh:mm)	(cfs)	(ft/sec)	(ft)
Direct_to_OutB	5.73	0 13:00	0.00	0.00	0.00
Link-03	1.53	0 12:10	5.60	3.89	0.45

Project Description

File Name Proposed Conditions_SMT.SPF

Project Options

Flow Units	CFS
Elevation Type	Elevation
Hydrology Method	SCS TR-55
Time of Concentration (TOC) Method	SCS TR-55
Link Routing Method	Kinematic Wave
Enable Overflow Ponding at Nodes	YES
Skip Steady State Analysis Time Periods	NO

Analysis Options

Start Analysis On	Aug 15, 2017	00:00:00
End Analysis On	Aug 17, 2017	00:00:00
Start Reporting On	Aug 15, 2017	00:00:00
Antecedent Dry Days	0	days
Runoff (Dry Weather) Time Step	0 01:00:00	days hh:mm:ss
Runoff (Wet Weather) Time Step	0 00:05:00	days hh:mm:ss
Reporting Time Step	0 00:05:00	days hh:mm:ss
Routing Time Step	30	seconds

Number of Elements

	Qt
Rain Gages	1
Subbasins	6
Nodes	7
Junctions	2
Outfalls	5
Flow Diversions	0
Inlets	0
Storage Nodes	0
Links	2
Channels	0
Pipes	2
Pumps	0
Orifices	0
Weirs	0
Outlets	0
Pollutants	0
Land Uses	0

Rainfall Details

SN	Rain Gage ID	Data Source	Data Source ID	Rainfall Type	Rain Units	State	County	Period	Rainfall Depth (inches)	
1	Rain Gage-01	Time Series	TS-25	Cumulative	inches	Maine	Cumberland (Southeast)	25	5.50	SCS Type III 24-hr

Subbasin Summary

Subbasin	Area	Weighted	Total	Total	Total	Peak	Time of
ID		Number	Rainiaii	Runon	Runoff Volume	Runoii	Concentration
		Number			volume		
	(ac)		(in)	(in)	(ac-in)	(cfs)	(days hh:mm:ss)
A	3.95	74.46	5.50	2.81	11.10	7.47	0 00:29:55
B-1	2.55	66.95	5.50	2.16	5.50	5.55	0 00:07:01
B-2	7.03	70.54	5.50	2.46	17.30	6.91	0 01:17:51
С	0.21	75.29	5.50	2.89	0.61	0.48	0 00:20:30
CulvertDrainageArea	0.68	75.00	5.50	2.86	1.94	2.03	0 00:05:00
D	0.12	77.00	5.50	3.04	0.37	0.38	0 00:06:30

Node Summary

Element	Element	Invert	Peak
ID	Type	Elevation	Inflow

		(ft)	(cfs)
CulvertInlet	Junction	181.00	1.99
Out_B1andB2	Junction	176.00	7.71
CulvertOutlet	Outfall	180.35	1.98
OUT-A	Outfall	180.00	7.44
OUT-B	Outfall	176.00	7.71
OUT-C	Outfall	178.00	0.48
OUT-D	Outfall	190.82	0.37

Link Summary

Element	Element	From	To (Outlet)	Length	Inlet	Outlet	Average	Diameter or	Manning's	Peak	Design Flow	Peak Flow	Peak Flow
ID	Type	(Inlet)	Node		Invert	Invert	Slope	Height	Roughness	Flow	Capacity	Velocity	Depth
		Node			Elevation	Elevation							
				(ft)	(ft)	(ft)	(%)	(in)		(cfs)	(cfs)	(ft/sec)	(ft)
Direct_to_OutB	Pipe	Out_B1andB2	OUT-B	1715.96	0.00	0.00	0.0000	0.000	0.0150	7.71	0.00	0.00	0.00
Link-03	Pipe	CulvertInlet	CulvertOutlet	45.00	181.00	180.55	1.0000	15.000	0.0150	1.98	5.60	4.17	0.51

Subbasin Hydrology

Subbasin: A

Input Data

Area (ac)	3.95
Weighted Curve Number	74.46
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.33	D	77.00
Gravel roads	0.10	D	91.00
> 75% grass cover, Good	0.38	D	80.00
Brush, Good	3.14	D	73.00
Composite Area & Weighted CN	3.95		74.46

Time of Concentration

TOC Method : SCS TR-55

Sheet Flow Equation :

 $Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))$

Where:

Tc = Time of Concentration (hr)

n = Manning's roughness

Lf = Flow Length (ft)

P = 2 yr, 24 hr Rainfall (inches)

Sf = Slope (ft/ft)

Shallow Concentrated Flow Equation :

V = 16.1345 * (Sf^0.5) (unpaved surface) V = 20.3282 * (Sf^0.5) (paved surface) V = 15.0 * (Sf^0.5) (grassed waterway surface) V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)

V = 9.0 * (Sf^0.5) (really bare & utilities startace)
V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
V = 7.0 * (Sf^0.5) (short grass pasture surface)
V = 5.0 * (Sf^0.5) (woodland surface)

V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)

Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

Channel Flow Equation :

V = (1.49 * (R^(2/3)) * (Sf^0.5)) / n

R = Aq / Wp Tc = (Lf / V) / (3600 sec/hr)

Where:

Tc = Time of Concentration (hr)

Lf = Flow Length (ft)

R = Hydraulic Radius (ft)

Aq = Flow Area (ft²)

Wp = Wetted Perimeter (ft)

V = Velocity (ft/sec)

Sf = Slope (ft/ft)

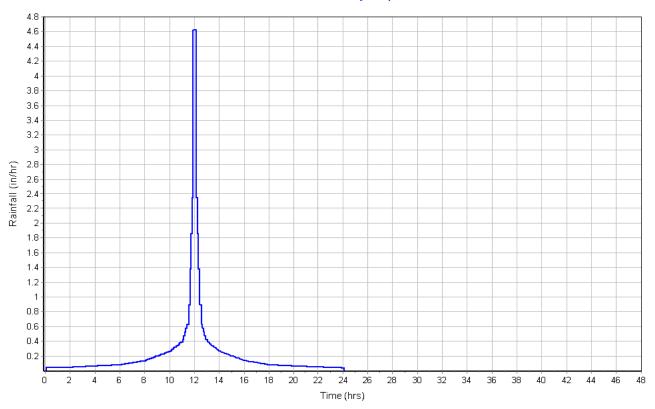
n = Manning's roughness

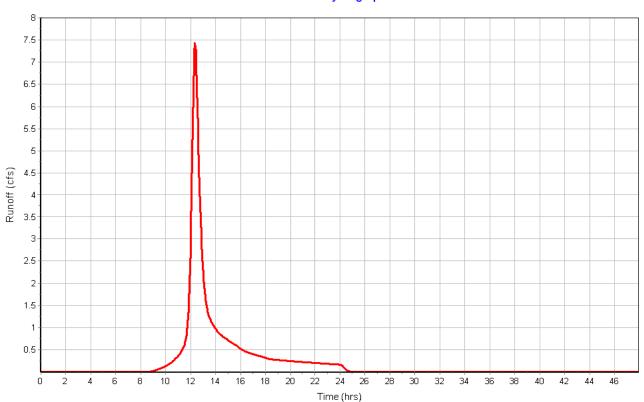
New England Clean Energy Connect Project Fickett Road Station

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	45	0.00	0.00
Slope (%):	50	0.00	0.00
2 yr, 24 hr Rainfall (in):	3.00	0.00	0.00
Velocity (ft/sec):	0.23	0.00	0.00
Computed Flow Time (min) :	3.23	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	264	574	0.00
Slope (%):	.76	.35	0.00
Surface Type :	Grassed waterway	Grass pasture	Unpaved
Velocity (ft/sec):	1.31	0.41	0.00
Computed Flow Time (min) :	3.36	23.33	0.00
Total TOC (min)29.92			

Total Rainfall (in)	5.50
Total Runoff (in)	2.81
Peak Runoff (cfs)	7.47
Weighted Curve Number	74.46
Time of Concentration (days hh:mm:ss)	0 00:29:55

Subbasin : A





Subbasin: B-1

Input Data

Area (ac)	2.55
Weighted Curve Number	66.95
Rain Gage ID	Rain Gage-01

Composite Curve Number

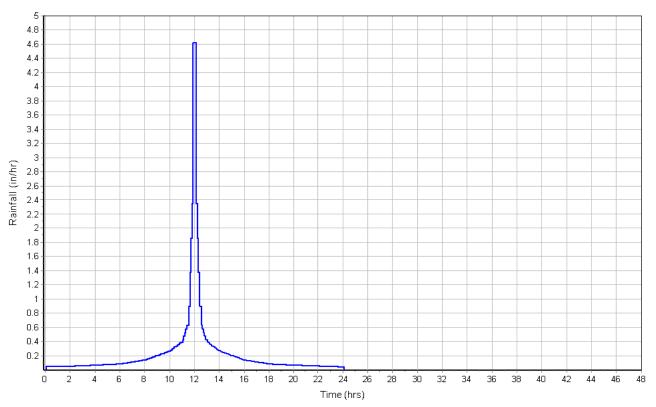
Area	Soil	Curve
(acres)	Group	Number
1.88	D	60.00
0.24	D	98.00
0.43	D	80.00
2.55		66.95
	(acres) 1.88 0.24 0.43	(acres) Group 1.88 D 0.24 D 0.43 D

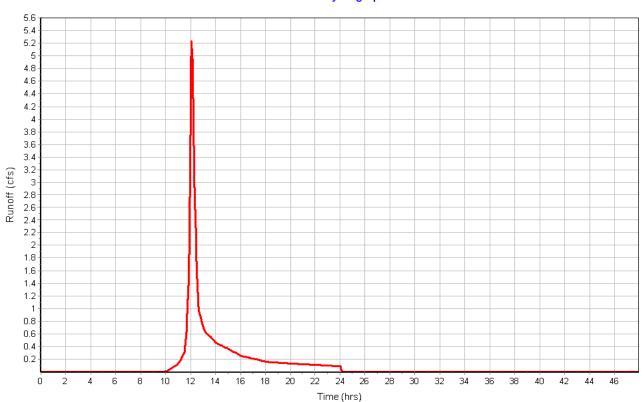
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.4	0.00	0.00
Flow Length (ft):	38	0.00	0.00
Slope (%):	50	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.22	0.00	0.00
Computed Flow Time (min):	2.82	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	385	0.00	0.00
Slope (%):	1.04	0.00	0.00
Surface Type :	Grassed waterway	Grass pastur	e rass pasture
Velocity (ft/sec) :	1.53	0.00	0.00
Computed Flow Time (min) :	4.19	0.00	0.00
Total TOC (min)			

Total Rainfall (in)	5.50
Total Runoff (in)	2.16
Peak Runoff (cfs)	5.55
Weighted Curve Number	66.95
Time of Concentration (days hh:mm:ss)	0 00:07:01

Subbasin : B-1





Subbasin : B-2

Input Data

Area (ac)	7.03
Weighted Curve Number	70.54
Rain Gage ID	Rain Gage-01

Composite Curve Number

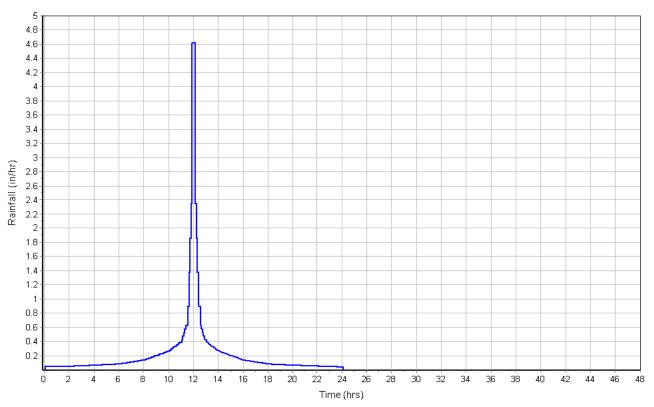
iposite curve Number			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Brush, Good	5.19	D	73.00
Gravel roads	0.05	D	91.00
> 75% grass cover, Good	0.16	D	80.00
Gravel_Pad	1.58	D	60.00
ConcreteFoundations	0.05	D	98.00
Composite Area & Weighted CN	7.03		70.54

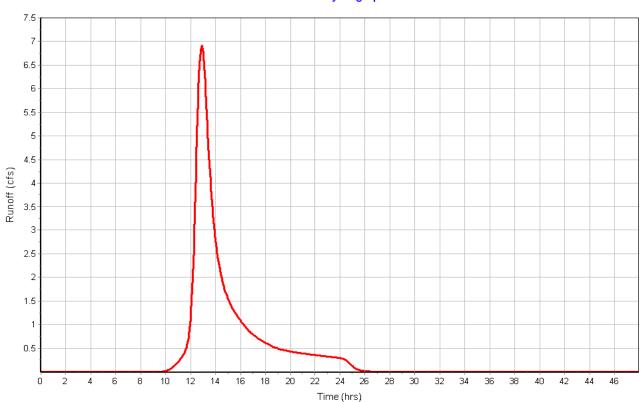
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness :	.4	0.00	0.00
Flow Length (ft):	100	0.00	0.00
Slope (%):	.25	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.03	0.00	0.00
Computed Flow Time (min):	50.95	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	Α	В	С
Flow Length (ft):	791	0.00	0.00
Slope (%):	.5	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	0.49	0.00	0.00
Computed Flow Time (min):	26.90	0.00	0.00
Total TOC (min)77.86			

Total Rainfall (in)	5.50
Total Runoff (in)	2.46
Peak Runoff (cfs)	6.91
Weighted Curve Number	
Time of Concentration (days hh:mm:ss)	0 01:17:52

Subbasin : B-2





Subbasin : C

Input Data

Area (ac)	0.21
Weighted Curve Number	75.29
Rain Gage ID	Rain Gage-01

Composite Curve Number

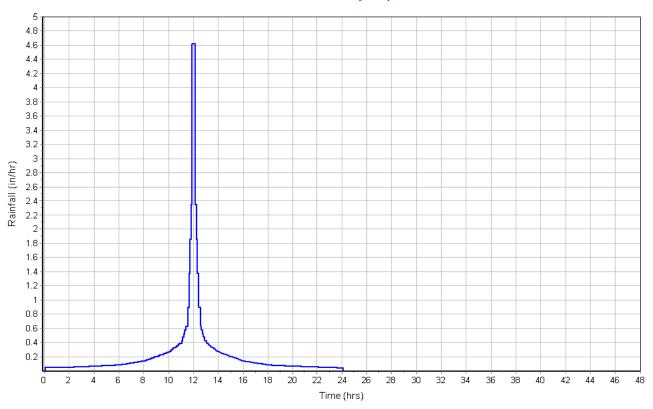
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Brush, Good	0.09	D	73.00
Composite Area & Weighted CN	0.21		75.29

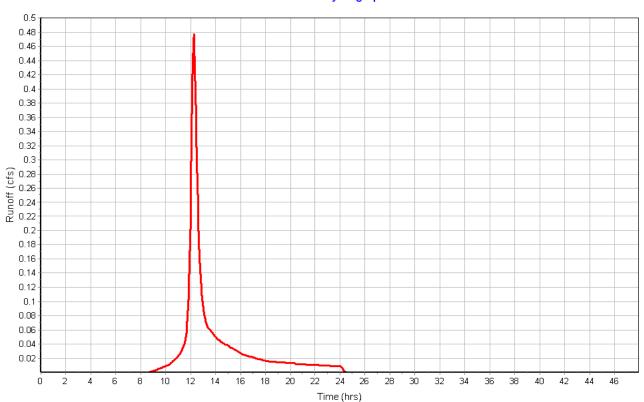
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	A	В	С
Manning's Roughness :	.6	0.00	0.00
Flow Length (ft):	80	0.00	0.00
Slope (%):	4.31	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.07	0.00	0.00
Computed Flow Time (min):	18.88	0.00	0.00
	Subarea	Subarea	Subarea
Shallow Concentrated Flow Computations	A	В	С
Flow Length (ft):	182	0.00	0.00
Slope (%):	7.1	0.00	0.00
Surface Type :	Grass pasture	Unpaved	Unpaved
Velocity (ft/sec):	1.87	0.00	0.00
Computed Flow Time (min):	1.62	0.00	0.00
Total TOC (min)20.50			

Total Rainfall (in)	5.50
Total Runoff (in)	2.89
Peak Runoff (cfs)	0.48
Weighted Curve Number	75.29
Time of Concentration (days hh:mm:ss)	0 00:20:30

Subbasin : C





New England Clean Energy Connect Project Fickett Road Station

Subbasin : CulvertDrainageArea

Input Data

Area (ac)	0.68
Weighted Curve Number	75.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
=	0.68	-	75.00
Composite Area & Weighted CN	0.68		75.00

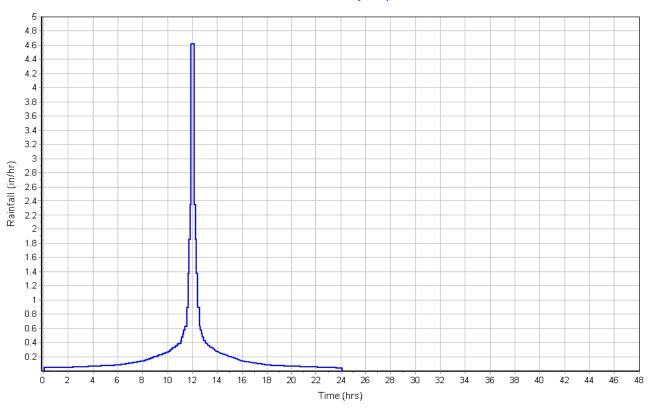
Time of Concentration

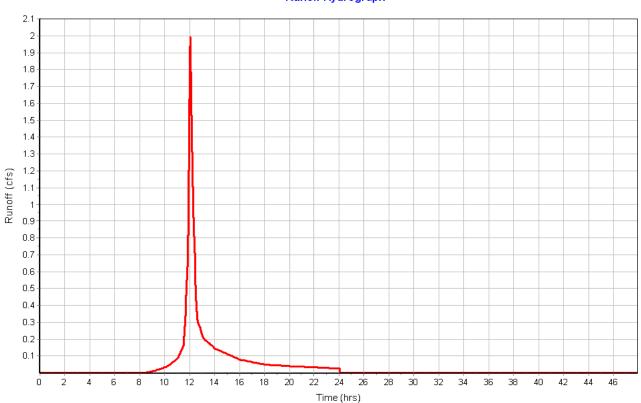
User-Defined TOC override (minutes): 5

Total Rainfall (in)	5.50
Total Runoff (in)	2.86
Peak Runoff (cfs)	2.03
Weighted Curve Number	75.00
Time of Concentration (days hh:mm:ss)	0 00:05:00

Subbasin : CulvertDrainageArea

Rainfall Intensity Graph





Subbasin : D

Input Data

Area (ac)	0.12
Weighted Curve Number	77.00
Rain Gage ID	Rain Gage-01

Composite Curve Number

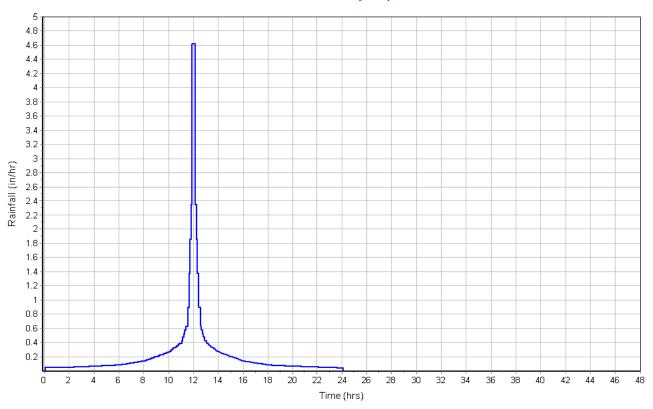
iiposite Cui ve ivallibei			
	Area	Soil	Curve
Soil/Surface Description	(acres)	Group	Number
Woods, Good	0.12	D	77.00
Composite Area & Weighted CN	0.12		77.00

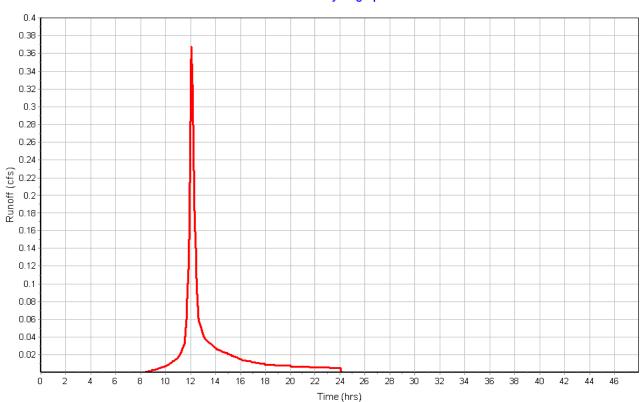
Time of Concentration

	Subarea	Subarea	Subarea
Sheet Flow Computations	Α	В	С
Manning's Roughness:	.4	0.00	0.00
Flow Length (ft):	36	0.00	0.00
Slope (%):	5.55	0.00	0.00
2 yr, 24 hr Rainfall (in) :	3.00	0.00	0.00
Velocity (ft/sec):	0.09	0.00	0.00
Computed Flow Time (min):	6.51	0.00	0.00
Total TOC (min)6.51			

Total Rainfall (in)	5.50
Total Runoff (in)	
Peak Runoff (cfs)	0.38
Weighted Curve Number	77.00
Time of Concentration (days hh:mm:ss)	0 00:06:3

Subbasin : D





Junction Input

Element	Invert	Ground/Rim
ID	Elevation	(Max)
		Elevation
	(ft)	(ft)
CulvertInlet	181.00	184.00
Out_B1andB2	176.00	6.00

Junction Results

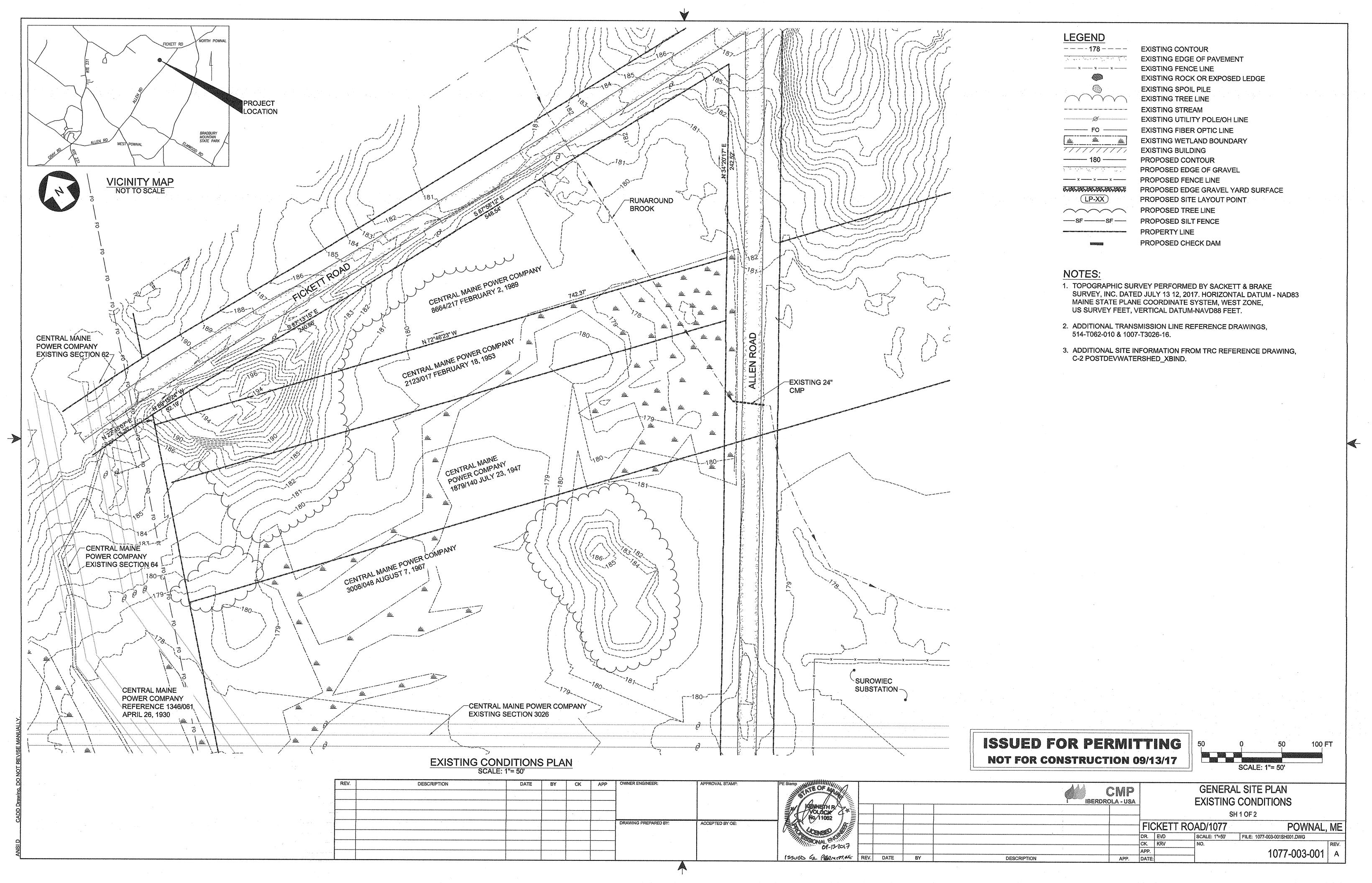
Element ID		Max HGL Max HGL Elevation Depth Attained Attained		Min Freeboard Attained		Time of Max HGL Occurrence
CulvertInlet Out B1andB2	(cfs)	(ft)	(ft)	(ft)	(ft)	(days hh:mm)
	1.99	181.52	0.52	2.48	181.04	0 12:10
	7.71	176.00	0.00	0.00	176.00	0 00:00

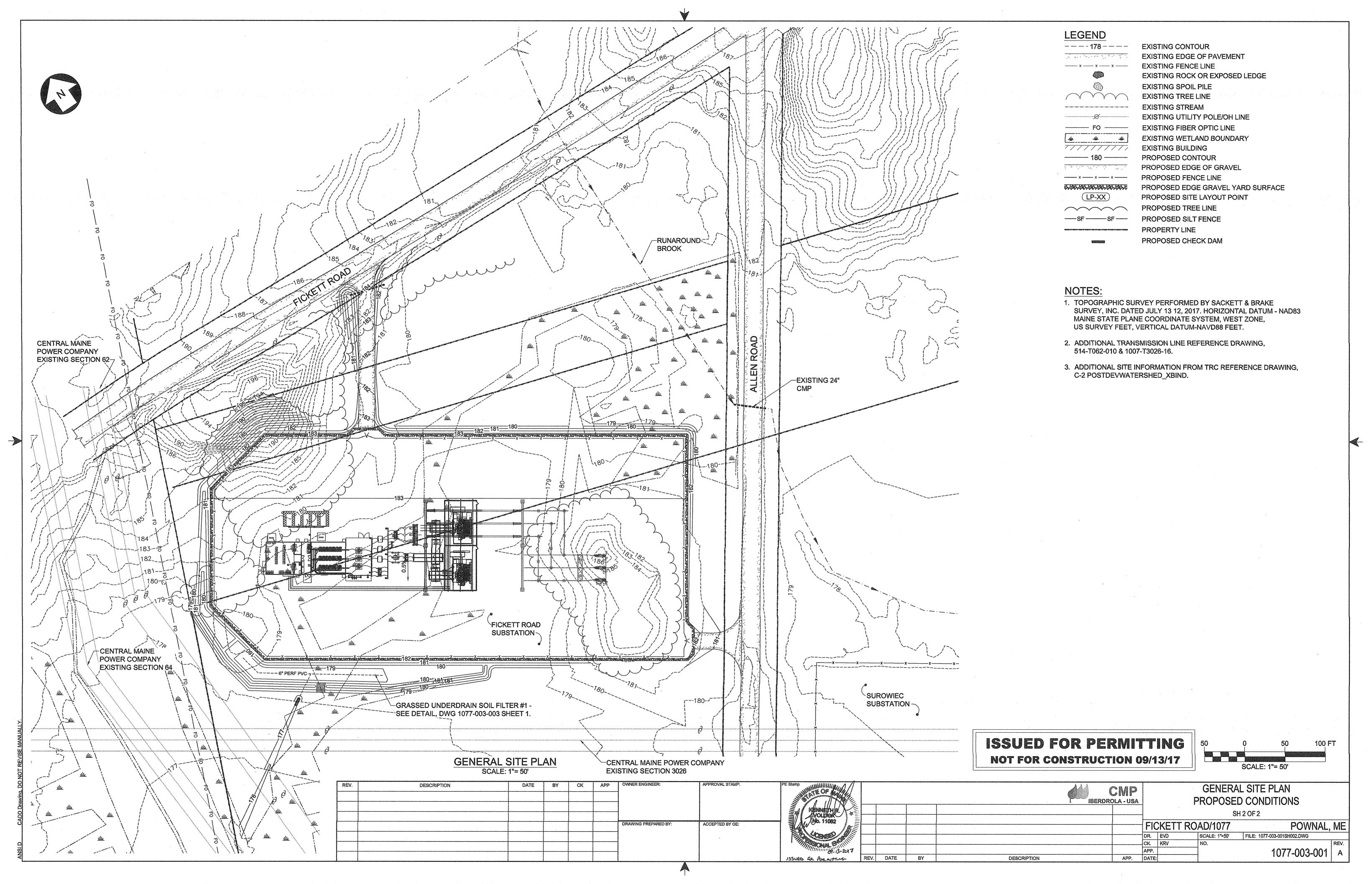
Pipe Input

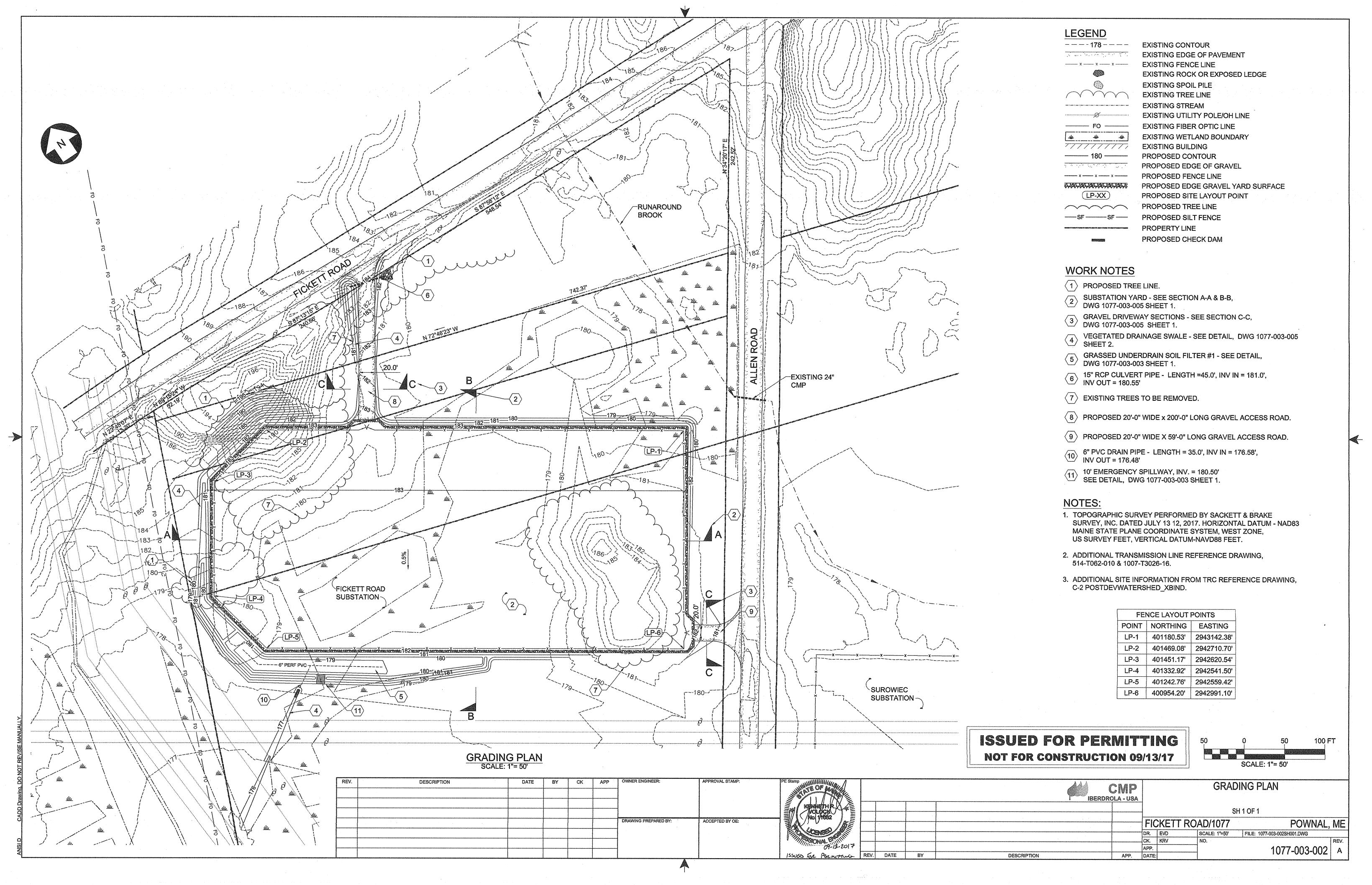
Element	Length	Inlet	Outlet	Average Pipe	Pipe	Pipe	Manning's
ID		Invert	Invert	Slope Shape	Diameter or	Width	Roughness
	1	Elevation	Elevation		Height		
	(ft)	(ft)	(ft)	(%)	(in)	(in)	
Direct_to_OutB	1715.96	0.00	0.00	0.0000 Dummy	0.000	0.000	0.0150
Link-03	45.00	181.00	180.55	1.0000 CIRCULAR	15.000	15.000	0.0150

Pipe Results

Element	Peak	Time of	Design Flow	Peak Flow	Peak Flow
ID	Flow	Peak Flow	Capacity	Velocity	Depth
		Occurrence			·
	(cfs)	(days hh:mm)	(cfs)	(ft/sec)	(ft)
Direct_to_OutB	7.71	0 12:55	0.00	0.00	0.00
Link-03	1.98	0 12:10	5.60	4.17	0.51







FILTER NOTES:

- 1. UNDERDRAIN PIPES SHALL BE SCH. 40 PVC, ENDS OF UNDERDRAIN PIPING SHALL BE PLUGGED WITH PIPE FITTINGS, PIPE JOINTS SHALL BE FULLY GLUED.
- 2. COMPACT EMBANKMENT MATERIAL TO 93% OF MAXIMUM DENSITY AS DETERMINED BY ASTM D1557.
- 3. FILTER BED & SIDE SLOPES SHALL BE SEEDED USING "NEW ENGLAND CONSERVATION/WILDLIFE MIX" FROM NEW ENGLAND WETLAND PLANTS, INC.OF AMHERST, MA. OR APPROVED EQUAL (APPLICATION RATE 25#/ACRE).
- 4. MDOT 703.22 UNDERDRAIN BACKFILL MATERIAL, TYPE B SPECIFICATIONS.

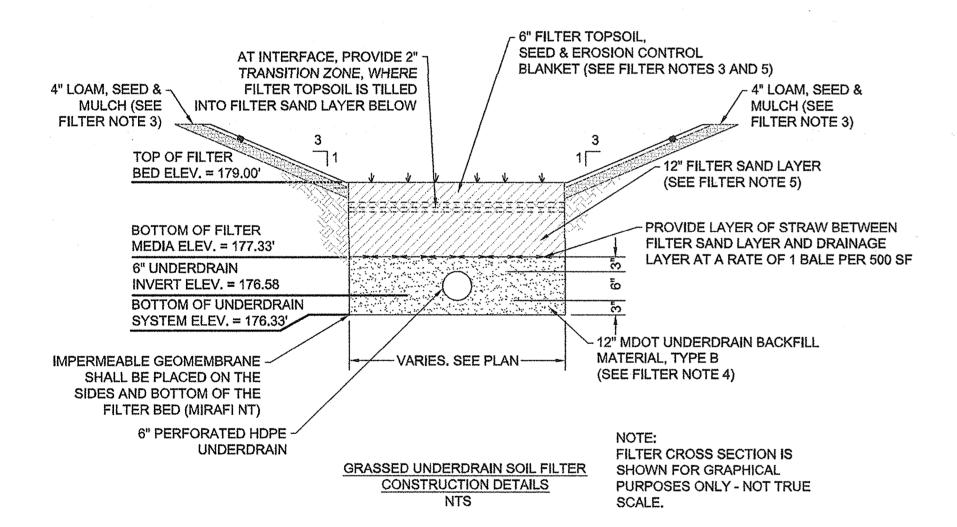
SIEVE	BY WEIGHT
1	90 - 100
1/2	75 - 100
#4	50 - 100
#20	15 - 80
#50	0 - 15
#200	0-5

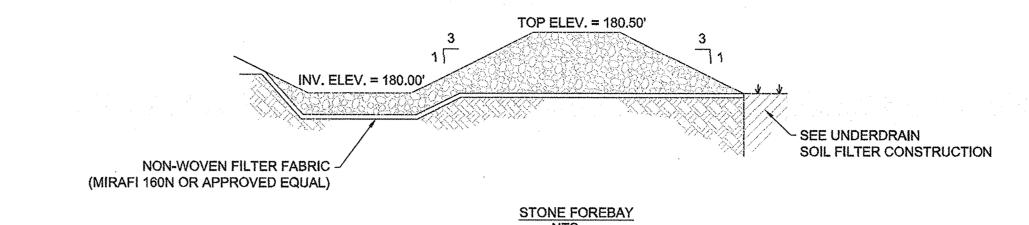
- 5. FILTER MEDIA MATERIALS:
- 5.1. FILTER TOPSOIL LAYER: A 6-INCH LAYER OF LOAMY TOPSOIL SUCH AS USDA SANDY LOAM TOPSOIL WITH 5-8% HUMIFIED ORGANIC MATTER, SCREENED TOPSOIL FROM THE SITE MAY BE APPROPRIATE BUT SHALL BE TESTED FOR ORGANIC CONTENT. ORGANIC MATTER (SUCH AS SUPERHUMUS OR EQUIVALENT) MAY BE ADDED IF NECESSARY, PROVIDED THAT THE RESULTING TEXTURE IS SUITABLE. SEE EROSION CONTROL DETAILS FOR EROSION CONTROL BLANKET INSTALLATION REQUIREMENTS.
- 5.2, FILTER SAND LAYER: A 12-INCH LAYER OF LOAMY COARSE SAND.

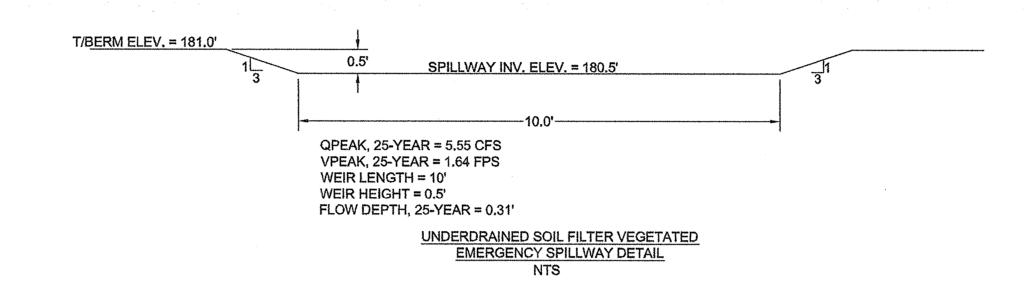
FILTER CONSTRUCTION INSPECTION AND TESTING NOTES:

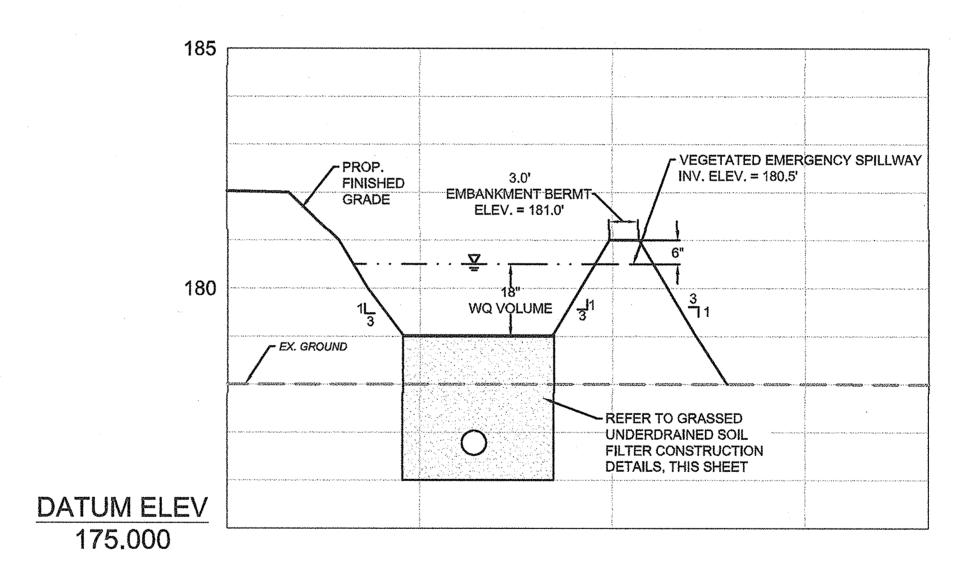
- 1. INSPECTION OF THE FILTER BASIN SHALL BE PROVIDED FOR EACH PHASE OF CONSTRUCTION BY THE DESIGN ENGINEER WITH REQUIRED REPORTING TO THE MAINE DEP.
- 2. AT A MINIMUM INSPECTIONS WILL OCCUR:
- 2.1. AFTER PRELIMINARY CONSTRUCTION OF THE FILTER GRADES AND ONCE THE UNDERDRAIN PIPES ARE INSTALLED BUT NOT BACKFILLED;
- 2.2. AFTER THE DRAINAGE LAYER IS CONSTRUCTED AND PRIOR TO THE INSTALLATION OF THE FILTER SAND LAYER;
- 2.3. AFTER FILTER SAND LAYER IS CONSTRUCTED AND PRIOR TO THE INSTALLATION OF THE FILTER TOPSOIL LAYER; 2.4. AFTER THE FILTER TOPSOIL LAYER HAS BEEN INSTALLED AND SEEDED; AND
- 2.5. AFTER ONE YEAR TO INSPECT HEALTH OF THE VEGETATION AND MAKE CORRECTIONS.
- 3. THE CONTRACTOR SHALL PROVIDE SUBMITTALS FOR EACH COMPONENT OF THE FILTER MEDIA, IDENTIFYING THE SOURCE.
- 4. ALL MATERIAL USED FOR THE CONSTRUCTION OF THE FILTER BASIN WILL BE APPROVED BY THE DESIGN ENGINEER, AFTER TESTS BY A CERTIFIED LABORATORY
- SHOW THAT THEY ARE PASSING MAINE DEP SPECIFICATIONS.

 5. THE CONTRACTOR SHALL SUBMIT SAMPLES OF EACH TYPE OF MATERIAL TO BE USED FOR THE MIVED BY THE MEDIA AND SAMPLES OF THE UNDERDRAIN REDDING
- 5. THE CONTRACTOR SHALL SUBMIT SAMPLES OF EACH TYPE OF MATERIAL TO BE USED FOR THE MIXED FILTER MEDIA AND SAMPLES OF THE UNDERDRAIN BEDDING MATERIAL. SAMPLES MUST BE A COMPOSITE OF THREE DIFFERENT LOCATIONS (GRABS) FROM THE STOCKPILE OR PIT FACE. SAMPLE SIZE REQUIRED WILL BE DETERMINED BY THE TESTING LABORATORY.
- 6. THE CONTRACTOR SHALL PERFORM, OR HAVE PERFORMED, A SIEVE ANALYSIS CONFORMING TO ASTM C138 ON EACH TYPE OF THE SAMPLE MATERIAL. ALL MATERIALS SHALL HAVE A CLAY CONTENT OF LESS THAN 2% AS DETERMNED BY HYDROMETER GRAIN SIZE ANALYSIS.
- 7. THE CONTRACTOR SHALL PERFORM, OR HAVE PERFORMED, A PERMEABILITY TEST ON THE SOIL FILTER MEDIA MATERIALS CONFORMING TO ASTM D2434 WITH THE MIXTURE COMPACTED TO 90 92% OF MAXIMUM DRY DENSITY BASED ON ASTM D698.









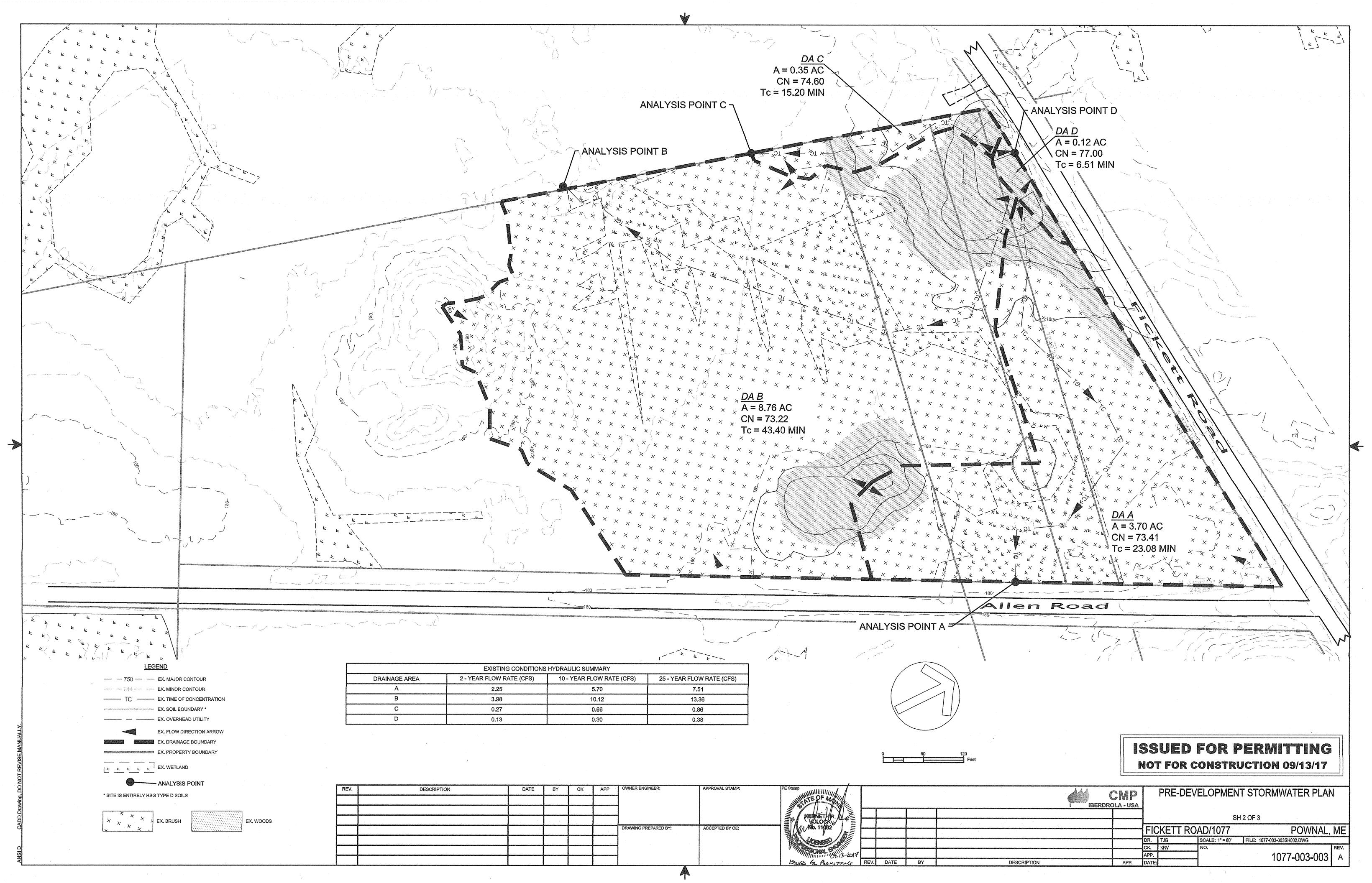
GRASSED UNDERDRAIN SOIL FILTER
VEGETATED EMERGENCY SPILLWAY SECTION

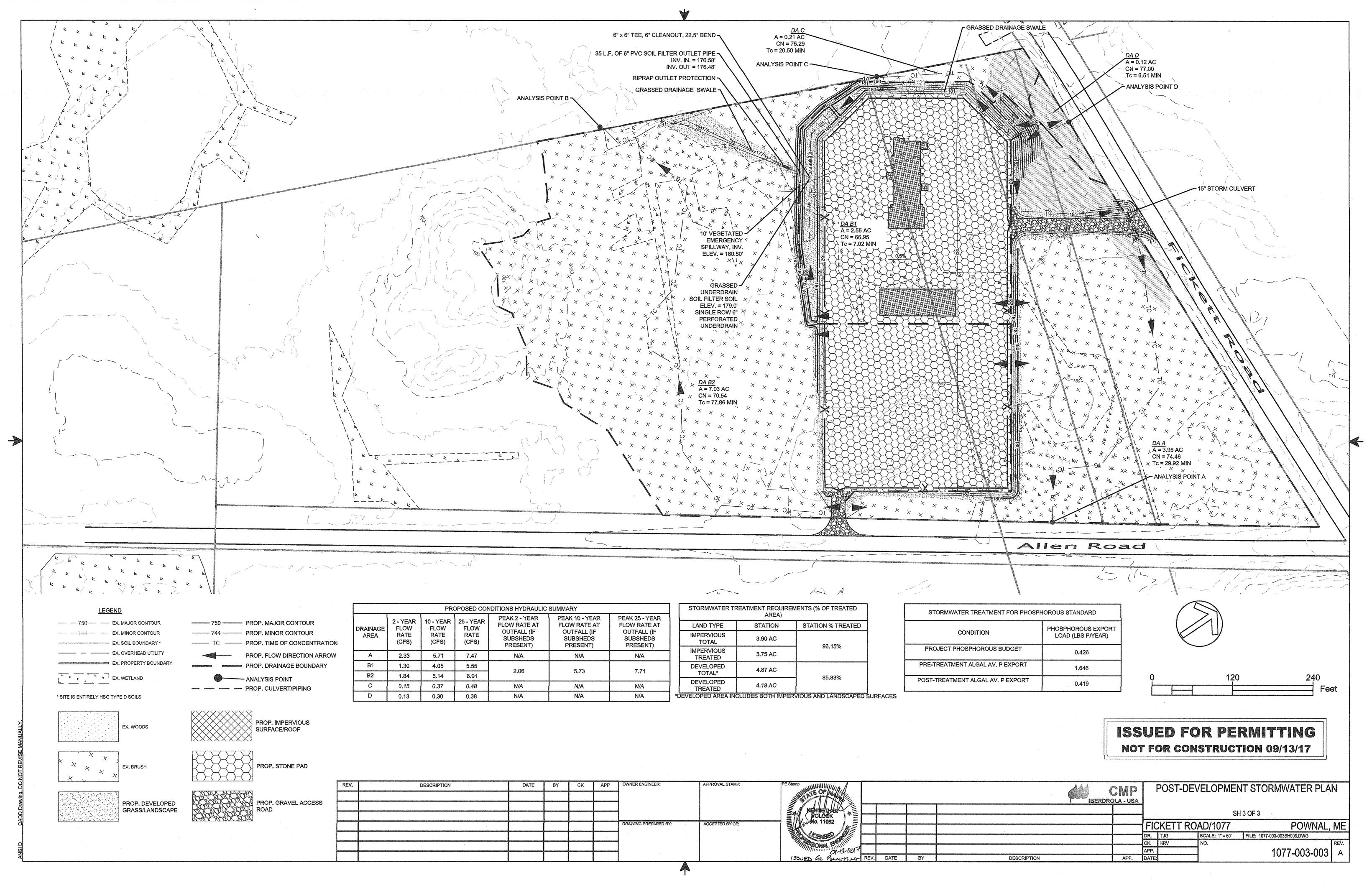
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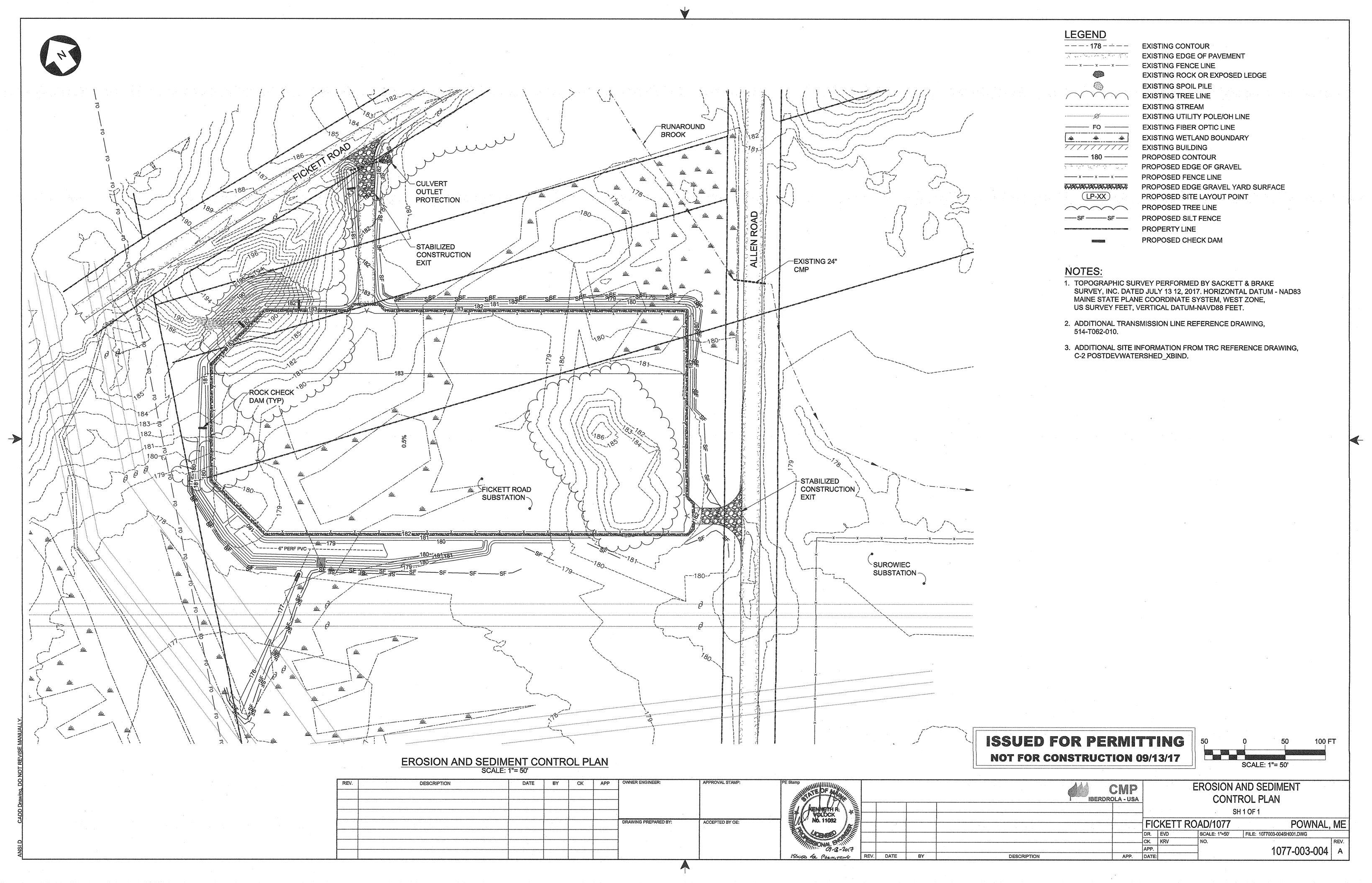
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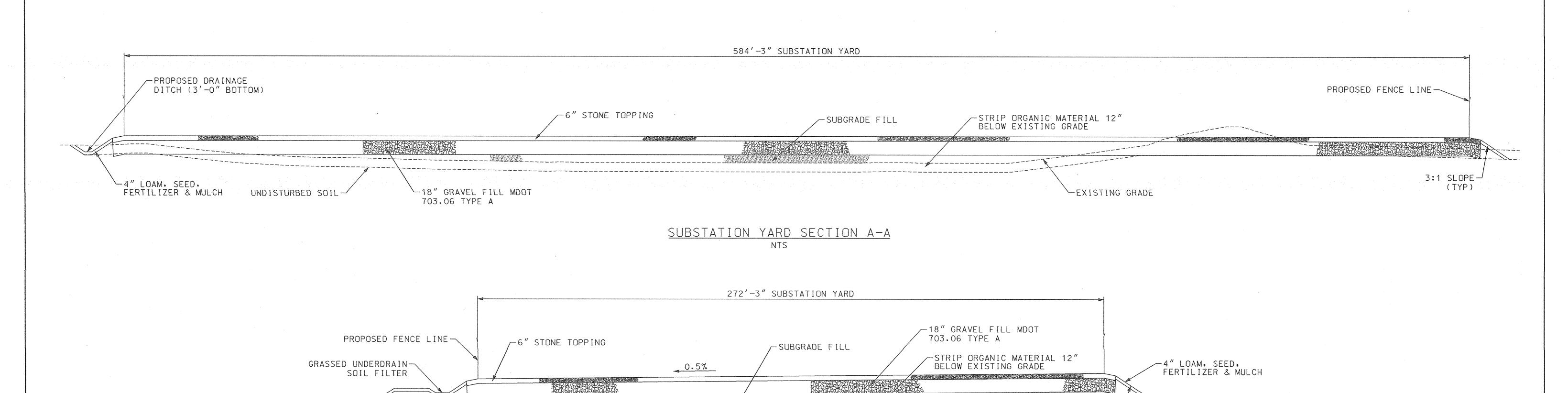
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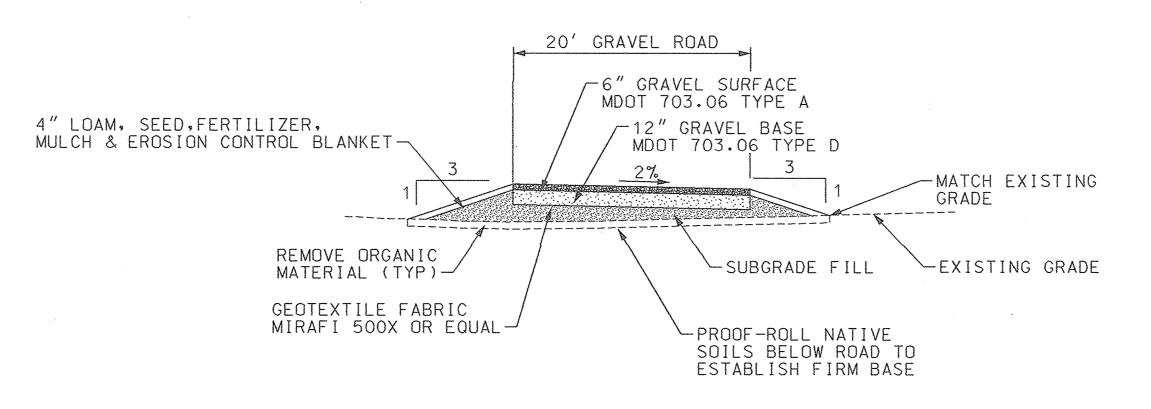






SUBSTATION YARD SECTION B-B

UNDISTURBED SOIL-



GRAVEL ACCESS ROAD SECTION C-C

NOTES:

3:1 SLOPE-(TYP)

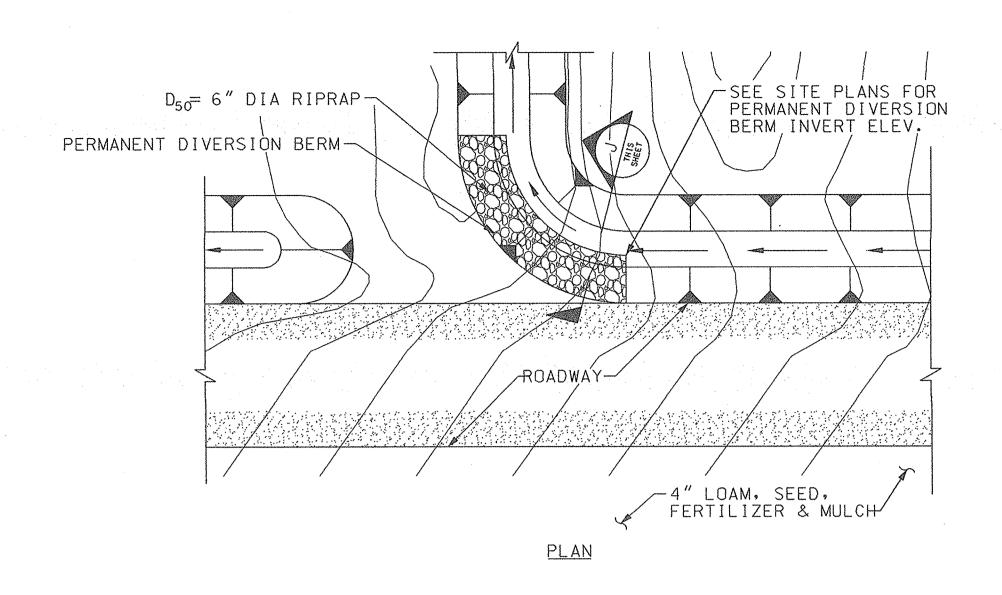
LEXISTING GRADE

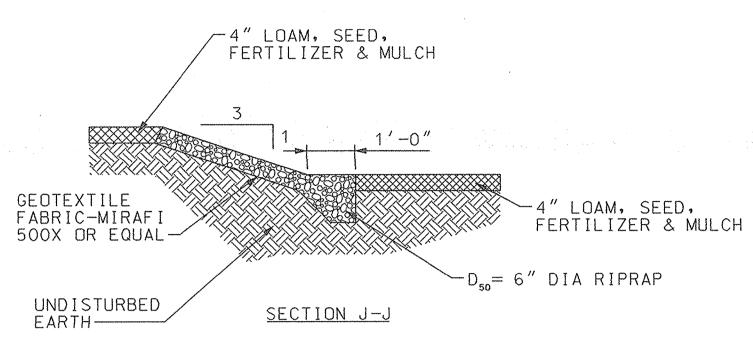
1. FILL SLOPES SHALL BE CONSTRUCTED AS LEVEL BENCHES WHICH ARE OVERBUILT TO FACILITATE COMPACTION. THE FINAL SLOPE FACE SHALL BE CONSTRUCTED BY CUTTING BACK INTO THE COMPACTED CORE.

2. WHERE GREATER THAN 4'-0" OF FILL IS REQUIRED, SUBSTATION YARD SHALL BE FILLED TO 4'-0" BELOW GRADES SHOWN ON THE GRADING PLAN WITH SUBGRADE FILL. FROM 4'-0" BELOW TO GRADE, FILL SHALL BE GRAVEL BORROW.

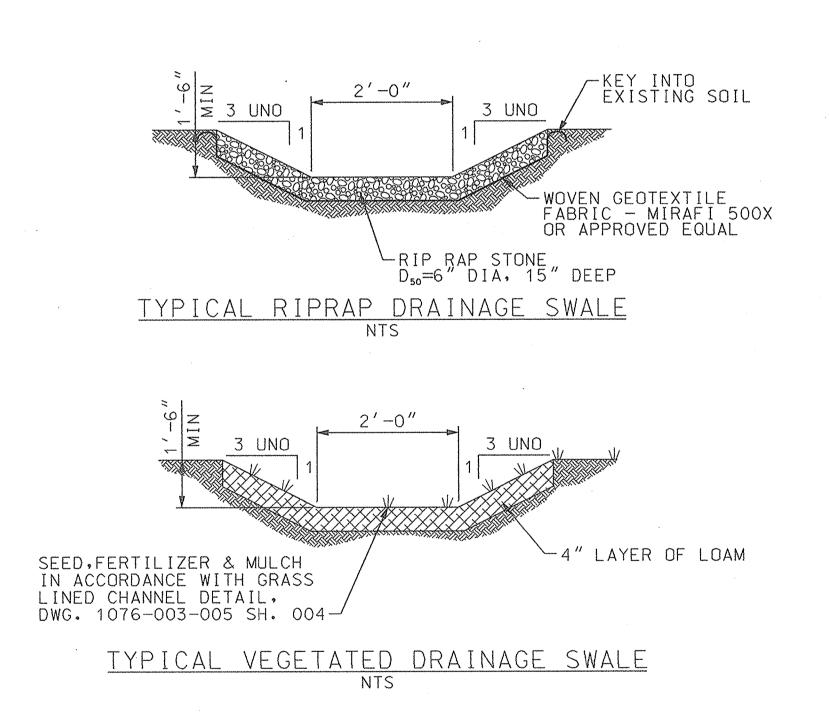
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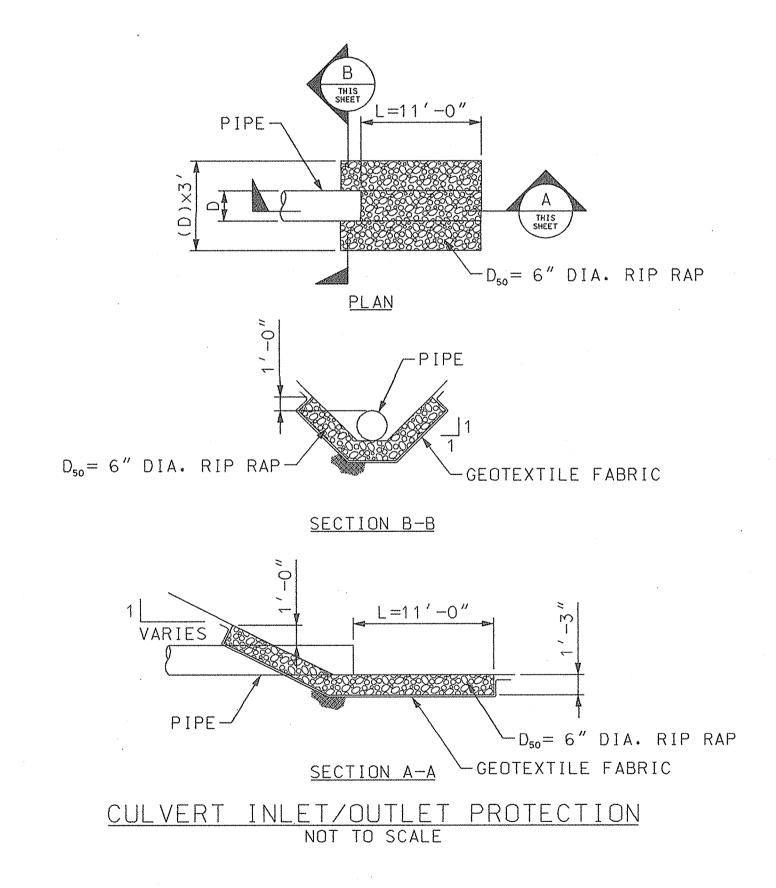
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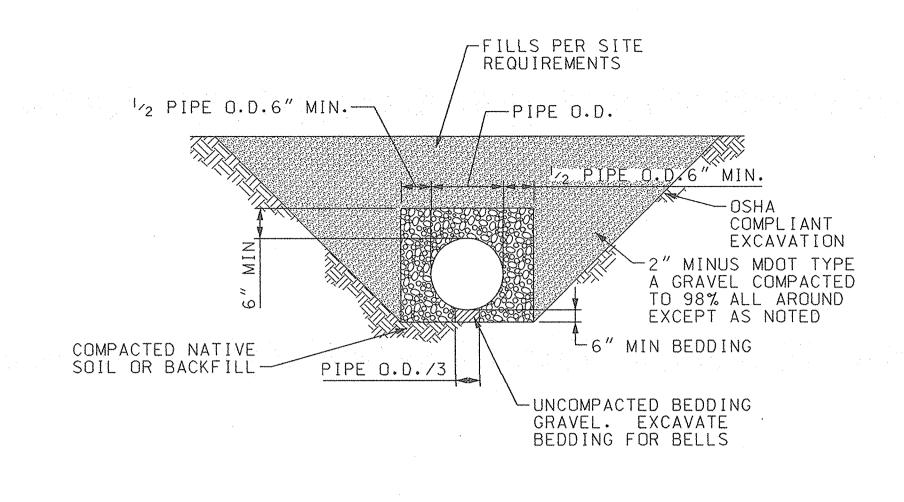




PERMANENT DIVERSION BERM DETAIL NTS



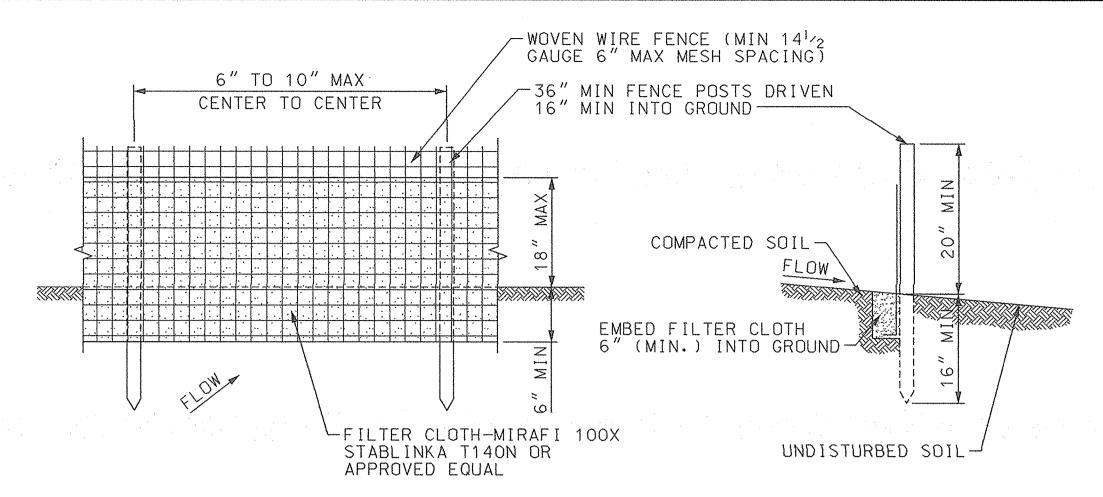




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ELEVATION

- 1. WOVEN WIRE FENCE TO BE FASTENED TO FENCE POSTS WITH WIRE TIES OR STAPLES.
- 2. FILTER CLOTH TO BE FASTENED SECURELY TO WOVEN WIRE FENCE WITH TIES SPACED EVERY 24" AT TOP AND MIDSECTION.
- 3. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER THEY SHALL BE OVERLAPPED BY 6" AND FOLDED.
- 4. MAINTENANCE SHALL BE PERFORMED AS NEEDED AND MATERIAL REMOVED WHEN BUILD-UP REACHES 1/3 THE HEIGHT OF THE FENCE.

1'-0" MIN ON UPSTREAM SIDE

EROSION CONTROL SOIL/BARK MIX: SHALL CONSIST OF SHREDDED BARK, STUMP GRINDINGS, COMPOSTED BARK OR FLUME GRIT AND BARK, STUMP GRINDINGS, COMPOSTED BARK OR FLUME GRIT AND FRAGMENTED WOOD GENERATED FROM WATER-FLUME LOG HANDLING SYSTEMS. THE MIX SHALL CONFORM TO THE FOLLOWING:

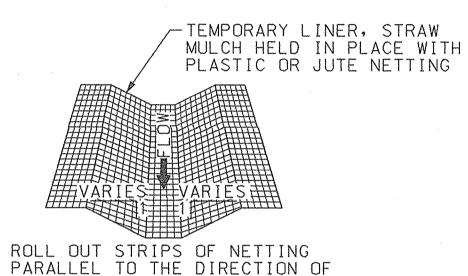
- 1. pH 5.0 TO 8.0.
 2. SCREEN SIZE: 6" 100% PASSING

 3/4" 70% TO 85% PASSING

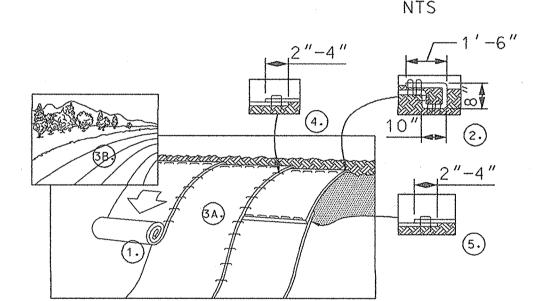
 MIX SHALL NOT CONTAIN LARGE PORTIONS OF
- SILTS, CLAYS OR FINE SANDS

 ORGANIC MATERIAL 20% 100% (DRY WEIGHT BASIS) ORGANIC PORTION MUST BE FIBROUS AND ELONGATED
- 4. SOLUBLE SALTS SHALL BE LESS THAN 4.0 mmhos/cm

EROSION CONTROL BERM



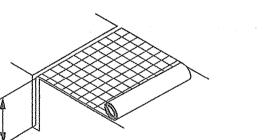
SILT FENCE DETAILS



- 1. PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER, AND SEED, NOTE: WHEN USING CELL-O-SEED DO NOT SEED PREPARED AREA. CELL-O-SEED MUST BE INSTALLED WITH PAPER SIDE DOWN.
- 2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN A 8"
 DEEP X 10" WIDE TRENCH WITH APPROXIMATELY 18" OF BLANKET
 EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE
 BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN
 THE SLOPE SIDE WALL OF THE TRENCH AND TWO ROWS OF STAPLES
 STAGGERED 6" APART IN THE BOTTOM OF THE TRENCH. BACKFILL AND
 COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED
 SOIL AND FOLD REMAINING 18" PORTION OF BLANKET BACK OVER SEED
 AND COMPACTED SOIL. SECURE BLANKET OVER COMPACTED SOIL WITH TWO
 ROWS OF STAPLES/STAKES SPACED APPROXIMATELY 4" APART STAGGERED
 WITH STAPLES 6" O.C. ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL THE BLANKETS (A.) DOWN OR (B.) HORIZONTALLY ACROSS THE SLOPE. BLANKETS WILL UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE. WHEN USING OPTIONAL DOT SYSTEM, STAPLES/STAKES SHOULD BE PLACED THROUGH EACH OF THE COLORED DOTS CORRESPONDING TO THE APPROPRIATE STAPLE PATTERN.
- 4. THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2"-4" OVERLAP DEPENDING ON BLANKET TYPE. TO ENSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE PREVIOUSLY INSTALLED BLANKET.
- 5. CONSECUTIVE BLANKETS SPLICED DOWN THE SLOPE MUST BE PLACED END OVER END (SHINGLE STYLE) WITH AN APPROXIMATE 2"-4" OVERLAP. STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12" (30cm) APART ACROSS ENTIRE BLANKET WIDTH.

EROSION CONTROL BLANKET INSTALLATION

6. BLANKET SHALL EXTEND 3'-0" MIN BEYOND TOE OF SLOPE. STAPLE 12" APART ALONG TERMINATION.





SECTION

PREFABRICATED UNIT: ENVIROFENCE OR

POSTS:

FENCE:

FILTER CLOTH:

STEEL "T" OR "U"

WOVEN WIRE. 14/2

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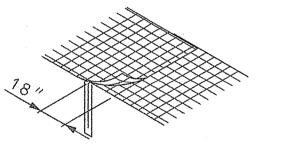
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TYPE OR 2" HARDWOOD.

OPENING.

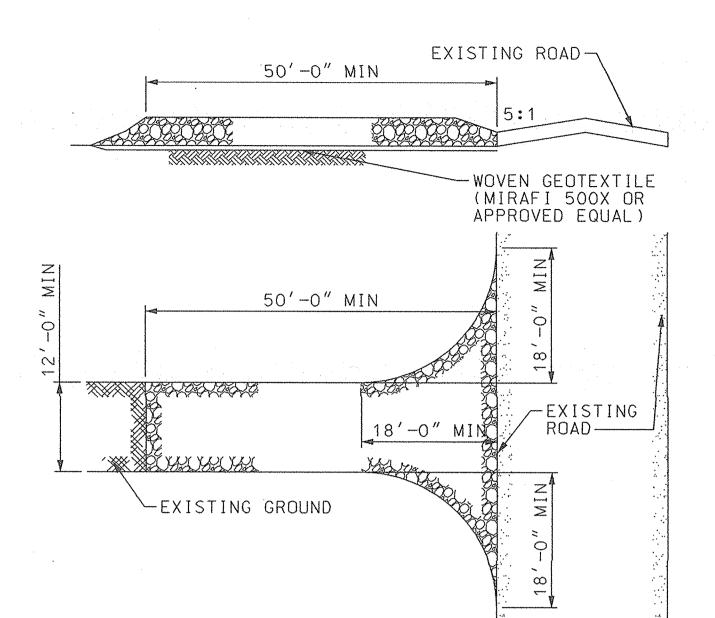
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JOIN STRIPS BY ANCHORING AND OVERLAPPING

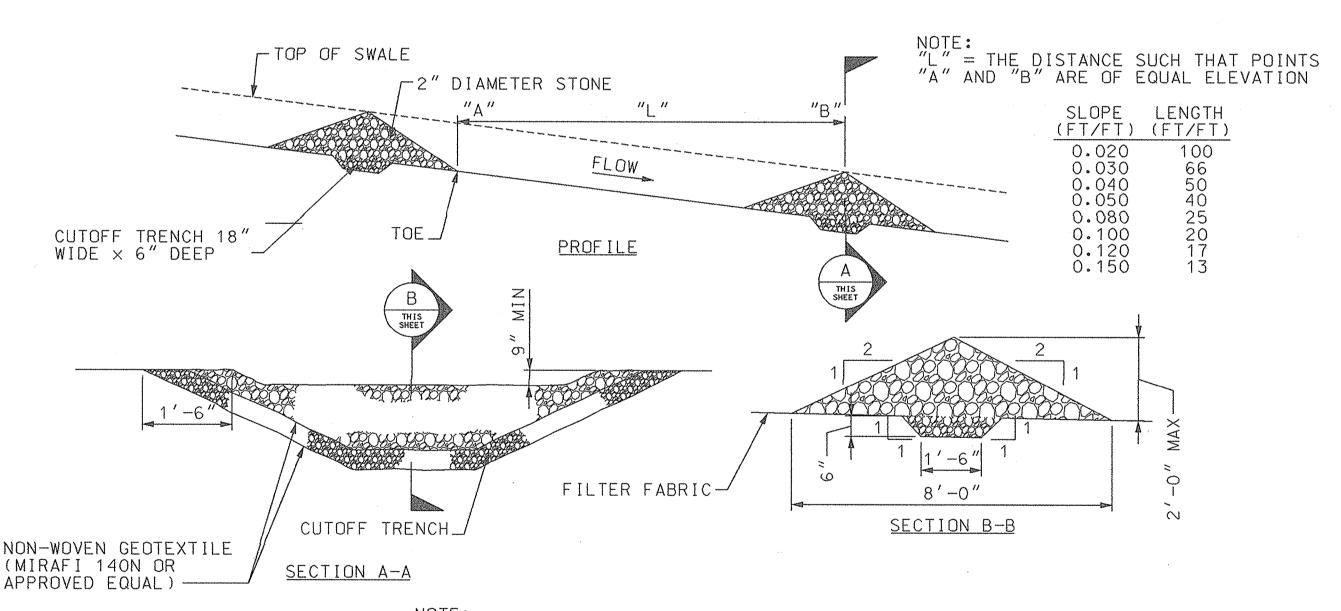
- 1. EXCAVATE THE CHANNEL AND SHAPE IT TO AN EVEN CROSS-SECTION AS SHOWN. WHEN STAKING INDICATE A 0.2' OVERCUT AROUND THE CHANNEL PERIMETER FOR SILTING AND BULKING.
- 2. GRADE SOIL AWAY FROM CHANNEL SO THAT SURFACE WATER MAY ENTER
- 3. APPLY LIME, FERTILIZER AND SEED TO THE CHANNEL AND ADJOINING AREAS IN ACCORDANCE WITH THE EROSION CONTROL PLAN.
- 4. SPREAD HAY OR STRAW MULCH AT THE RATE OF 100LB/1000 SF.
- 5. HOLD MULCH IN PLACE IMMEDIATELY AFTER SPREADING WITH A PLASTIC NETTING INSTALLED AS SHOWN.
- 6. START LAYING THE NET FROM THE TOP OF THE UPSTREAM END OF THE CHANNEL AND UNROLL IT DOWN GRADE. DO NOT STRETCH THE NETTING.
- 7. BURY THE UP SLOPE END AND STAPLE THE NET EVERY 12" ACROSS THE TOP END, EVERY 3 FT AROUND THE EDGES AND ACROSS THE NET SO THAT THE STRAW IS HELD CLOSELY AGAINST THE SOIL. HOWEVER, DO NOT STRETCH THE NETTING WHEN STAPLING.
- 8. NETTING STRIPS SHOULD BE JOINED TOGETHER ALONG THE SIDES WITH A 3" OVERLAP AND STAPLED TOGETHER.
- 9. TO JOIN ENDS OF STRIPS, INSERT A NEW ROLL OF NET IN A TRENCH AS WITH THE UP SLOPE END AND OVERLAP IT 18" WITH THE PREVIOUSLY LAID UPPER ROLL. TURN UNDER 6" OF THE 18" OVERLAP AND STAPLE EVERY 12" ACROSS THE END.

GRASS LINED CHANNEL NTS



- 1. STONE SIZE USE 2" STONE.
- 2. LENGTH NOT LESS THAN 50 FEET.
- 3. THICKNESS NOT LESS THAN SIX (6) INCHES.
- 4. WIDTH TWELVE (12) FOOT MIN. BUT NOT LESS THAN THE FULL WIDTH AT POINTS WHERE INGRESS OR EGRESS OCCURS. TWENTY-FOUR (24) FOOT IF SINGLE ENTRANCE TO SITE.
- 5. WOVEN GEOTEXTILE WILL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING THE STONE.
- 6. SURFACE WATER ALL SURFACE WATER FLOWING OR DIVERTED TOWARD CONSTRUCTION ENTRANCES SHALL BE PIPED ACROSS THE ENTRANCE. IF PIPING IS IMPRACTICAL, A MOUNTABLE BERM WITH 5:1 SLOPES WILL BE PERMITTED.
- 7. MAINTENANCE THE EXIT SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY.
- 8. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA STABILIZED WITH STONE THAT DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE.

STABILIZED CONSTRUCTION EXIT



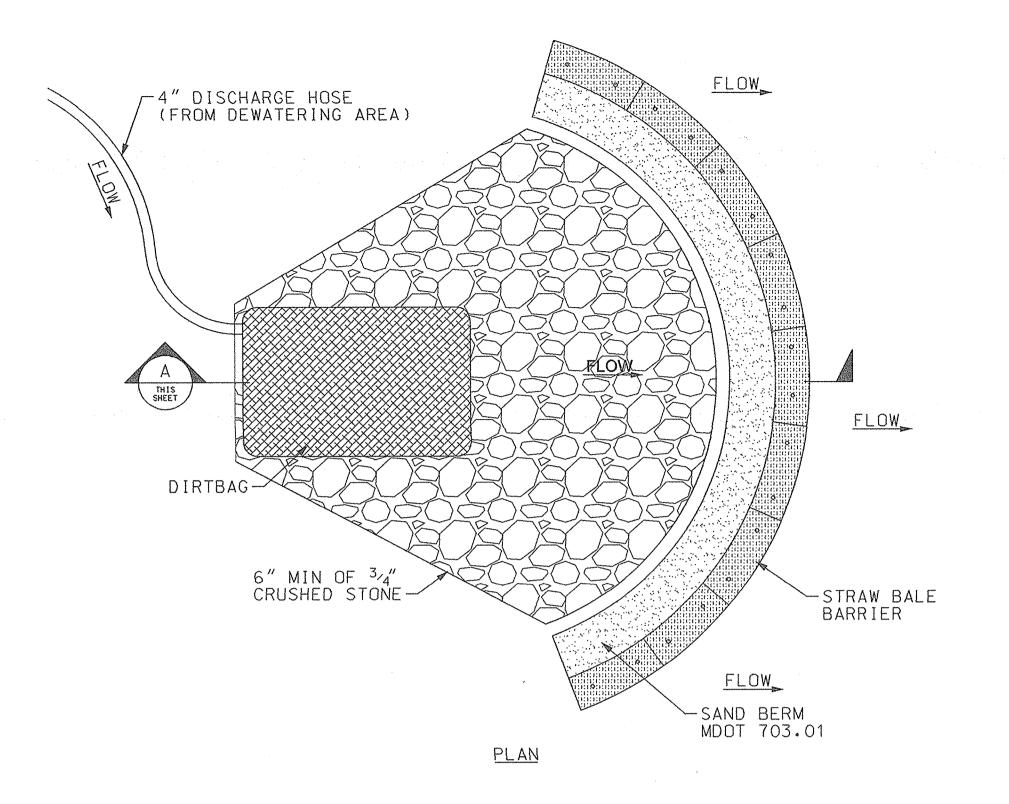
INSTALL WHERE INDICATED ON SITE GRADING PLAN AND AS NEEDED BY SPACING REQUIREMENTS.

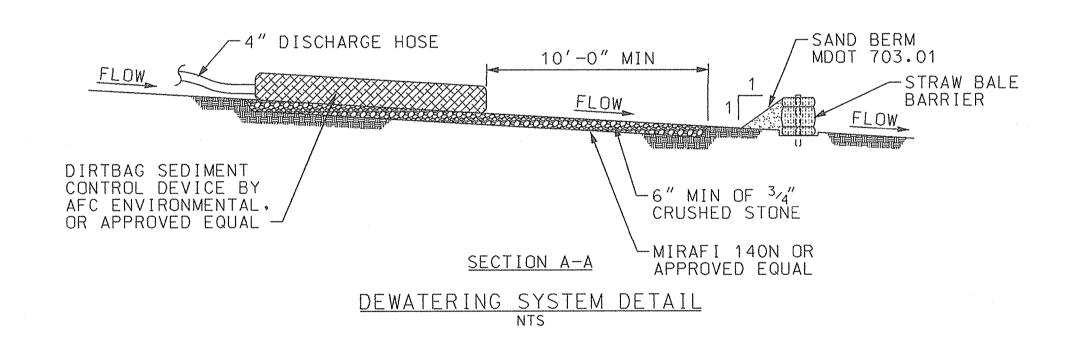
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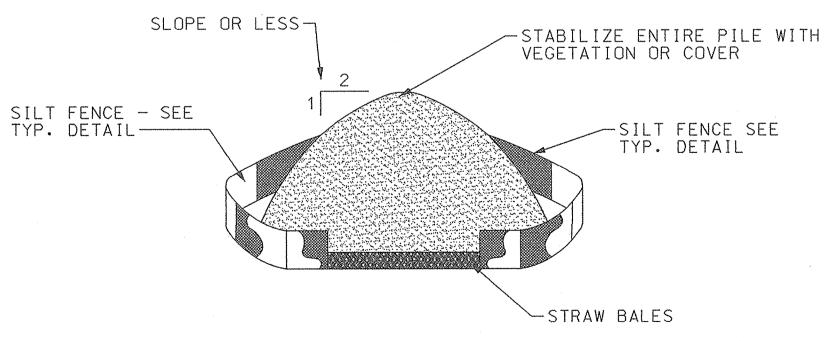
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INSTALLATION NOTES:

- 1. AREA CHOSEN FOR STOCKPILING OPERATIONS SHALL BE DRY AND STABLE.
- 2. MAXIMUM SLOPE OF STOCKPILE SHALL BE'2H:1V.
- 3. UPON COMPLETION OF SOIL STOCKPILING, EACH PILE SHALL BE SURROUNDED WITH EITHER SILT FENCING OR STRAW BALES, THEN STABILIZED WITH VEGETATION OR COVERED.

TYPICAL TOPSOIL STOCKPILE

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			DRAWING PREPARED BY:	ACCEPTED BY OE:

DESCRIPTION

DATE BY CK APP OWNER ENGINEER

DEWATERING NOTES:

- 1. THE CONTRACTOR SHALL INSTALL, MAINTAIN, AND OPERATE ALL CHANNELS, SUMPS, AND ALL OTHER TEMPORARY DIVERSION AND PROTECTIVE WORKS NEEDED TO DIVERT STREAM FLOW AND OTHER SURFACE WATER THROUGH OR AROUND THE CONSTRUCTION SITE. CONTROL OF SURFACE WATER SHALL BE CONTINUOUS DURING THE PERIOD THAT DAMAGE TO CONSTRUCTION WORK COULD OCCUR.
- OPEN EXCAVATIONS SHALL BE DEWATERED AND KEPT FREE OF STANDING WATER AND MUDDY CONDITIONS AS NECESSARY FOR THE PROPER EXECUTION OF THE WORK. THE CONTRACTOR SHALL FURNISH, INSTALL, OPERATE, AND MAINTAIN ALL DRAINS, SUMPS AND ALL OTHER EQUIPMENT REQUIRED TO PROPERLY DEWATER THE SITE. DEWATERING SYSTEMS THAT CAUSE A LOSS OF SOIL FINES FROM THE FOUNDATION AREAS WILL NOT BE PERMITTED.
- 3. INSTALL DIVERSION DITCHES OR BERMS IF NECESSARY TO MINIMIZE THE AMOUNT OF CLEAN STORMWATER RUNOFF ALLOWED INTO THE EXCAVATED AREA.
- 4. REMOVAL OF WATER FROM THE CONSTRUCTION SITE SHALL BE ACCOMPLISHED SO THAT EROSION AND THE TRANSPORTING OF SEDIMENT AND OTHER POLLUTANTS ARE MINIMIZED.
- 5. DISCHARGE DEWATERING EFFLUENT TO AREAS AS INDICATED ON THE SITE GRADING PLAN. DISCHARGE SHALL BE IN SHEET FLOW.
- 6. DEWATERING IN PERIODS OF INTENSE, HEAVY RAIN, WHEN THE INFILTRATIVE CAPACITY OF THE SOIL IS EXCEEDED, SHALL BE AVOIDED.
- 7. FLOW TO THE SEDIMENT REMOVAL STRUCTURE MAY NOT EXCEED THE STRUCTURE'S CAPACITY TO SETTLE AND FILTER FLOW OR THE STRUCTURE'S VOLUME CAPACITY.
- 8. WHEN TEMPORARY WORKS ARE NO LONGER NEEDED, THE CONTRACTOR SHALL REMOVE AND RETURN THE AREA TO A CONDITION SIMILAR TO THAT WHICH EXISTED BEFORE CONSTRUCTION. AREAS WHERE TEMPORARY WORKS WERE LOCATED SHALL BE GRADED FOR SIGHTLY APPEARANCE WITH NO OBSTRUCTION TO NATURAL SURFACE WATER FLOWS OR THE PROPER FUNCTIONING AND ACCESS TO THE WORKS OF IMPROVEMENT INSTALLED. THE CONTRACTOR SHALL EXERCISE EXTREME CARE DURING THE REMOVAL STAGES TO MINIMIZE THE LOSS OF SOIL SEDIMENT AND DEBRIS THAT WAS TRAPPED DURING CONSTRUCTION.

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CONSTRUCTION SEQUENCE:

- 1. ESTABLISH CONSTRUCTION WORKSPACE LIMITS; IDENTIFY AND MARK SENSITIVE RESOURCES.
- 2. PERFORM ALL WORK IN ACCORDANCE WITH MAINE EROSION AND SEDIMENT CONTROL PRACTICES FIELD GUIDE FOR CONTRACTORS (2015).
- 3. PRIOR TO USAGE, CONSTRUCT AND STABILIZE THE CONSTRUCTION ENTRANCE ON THE EXISTING PERMANENT ACCESS ROAD WITH A STONE PAD, MUD RACK, OR OTHER MATERIALS USED TO REDUCE THE TRACKING OR FLOWING OF SEDIMENT OFF THE SITE AND MAINTAIN UNTIL PAVING IS COMPLETED.
- 4. CLEAR TIMBER AND BRUSH; DO NOT GRUB UNTIL JUST PRIOR TO PRELIMINARY GRADING AND ESTABLISHMENT AND STABILIZATION OF TEMPORARY OR PERMANENT DRAINAGE COURSES.
- 5. INSTALL AND MAINTAIN SEDIMENT BARRIERS SUCH AS SILT FENCING AND/OR OTHER EROSION CONTROL BARRIERS ALONG THE DOWNHILL LIMIT OF WORK, AS SHOWN ON THE DRAWINGS. SEDIMENT BARRIER LOCATIONS MAY BE ADJUSTED IN THE FIELD BASED ON SITE CONDITIONS AS DETERMINED BY THE ENGINEERING INSPECTOR. WHERE SILT FENCE CANNOT BE TOED—IN PROPERLY DUE TO TREE ROOTS, ROCKS OR FROZEN GROUND, HAY BALES OR AN EROSION CONTROL MIX BERM MAY BE SUBSTITUTED. SILT FENCING WILL BE INSTALLED AFTER CLEARING BUT PRIOR TO GRUBBING AND GRADING ACTIVITIES. ANY EROSION ISSUES DEVELOPED DURING CLEARING WILL BE TEMPORARILY STABILIZED AS NECESSARY.
- 6. STABILIZE PERMANENT ACCESS ROAD SURFACE, PARKING AREAS AND EQUIPMENT STORAGE AND LAYDOWN AREAS WITH MATTING, CRUSHED STONE OR GRAVEL SUBBASE AS NECESSARY TO MINIMIZE RUTTING AND AVOID PONDING.
- 7. CONCURRENT WITH INITIATION OF SITE GRADING, CONSTRUCT AND STABILIZE TEMPORARY DRAINAGE SWALES, DIVERSION BERMS, CHECK DAMS, AND CULVERTS WITH TEMPORARY INLET AND OUTLET STRUCTURES TO MINIMIZE SEDIMENT IN SITE RUNOFF DURING THE CONSTRUCTION OF THE ROADWAY, DEWATER IN ACCORDANCE WITH DEWATERING NOTES BELOW.
- 8. INSTALL PROPERLY SPACED STONE CHECK DAMS IN ANY SECTION OF DITCH WITHIN 24 HOURS OF FORMING, SHAPING OR ROUGH GRADING THAT SECTION OF DITCH.
- 9. MINIMIZE THE AMOUNT OF DISTURBANCE AT ANY ONE TIME BY STAGING CONSTRUCTION AS MUCH AS PRACTICAL FOR EFFICIENT CONSTRUCTION OF THE FACILITY. NATURAL VEGETATIVE BUFFERS OR STRIPS SHOULD BE LEFT IN PLACE WHERE FEASIBLE TO AID IN SEDIMENT RETENTION AND REDUCE EROSION POTENTIAL.
- 10. STABILIZE ANY NEWLY GRADED SLOPE GREATER THAN EIGHT PERCENT AND ANY SECTION OF NEWLY CONSTRUCTED DITCH USING ANCHORED EROSION CONTROL BLANKETS OR OTHER APPROVED MULCHING TECHNIQUES WITHIN 24 HOURS. STABILIZE ANY SLOPE EXCEEDING EIGHT PERCENT AND BROUGHT TO FINAL GRADE WITHIN 24 HOURS USING THE APPROVED PERMANENT STABILIZATION MEASURES FOR SLOPES. STABILIZE ANY SECTION OF DITCH BROUGHT TO FINAL GRADE WITHIN 24 HOURS USING THE APPROVED PERMANENT STABILIZATION MEASURES FOR DITCHES.
- 11. DUST CONTROL METHODS WILL BE EMPLOYED AFTER GRADING AND PRIOR TO FINAL STABILIZATION TO PREVENT THE BLOWING AND MOVEMENT OF DUST THROUGH THE APPLICATION OF WATER AND/OR CALCIUM CHLORIDE TO REDUCE WIND EROSION. REPETITIVE TREATMENT WILL BE APPLIED AS NEEDED TO ACCOMPLISH CONTROL.
- 12. APPLY TEMPORARY SEED AND MULCH TO ANY EXPOSED AREAS WHERE ACTIVITY IS NOT ANTICIPATED FOR 30 DAYS OR MORE, OR WHERE ACTIVITY HAS NOT OCCURRED WITHIN 30 DAYS. TEMPORARILY MULCH ANY EXPOSED AREAS WHERE ACTIVITY IS NOT ANTICIPATED OR HAS NOT OCCURRED IN 7 DAYS.
- 13. REMOVE EXCESS SPOILS FROM SITE THAT WILL NOT BE USED FOR THE FINAL DESIGN AND STABILIZATION. STOCKPILED SOILS THAT REMAIN IN PLACE FOR 48 HOURS OR MORE WILL BE CONTAINED WITH SEDIMENT BARRIERS SUCH AS SILT FENCE, HAY BALES OR EQUIVALENT. THE SEDIMENT BARRIERS SHALL BE ADEQUATELY LOCATED AND REINFORCED TO HANDLE A SIGNIFICANT RAIN EVENT AND THE POTENTIAL SLUMPING OF THE PILE. BETWEEN MAY 1 AND OCTOBER 15, APPLY TEMPORARY SEED AND MULCH TO A STOCKPILE THAT IS NOT EXPECTED TO BE DISTURBED WITHIN 30 DAYS. APPLY ANCHORED MULCH DAILY, AS NEEDED, DURING WINTER CONSTRUCTION.
- 14. INSPECT AND REPAIR EROSION CONTROL MEASURES DAILY IN AREAS OF ACTIVE CONSTRUCTION; OTHERWISE WEEKLY AND AFTER RAINFALL OF 1/2" OR GREATER WITHIN A 24-HOUR PERIOD. REMOVE ACCUMULATED SEDIMENT WHEN IT REACHES 1/3 THE HEIGHT OF THE BARRIER.
- 15. MONITOR PUBLIC ROADS FOR SIGNS OF TRACKING OR SPILLING OF SPOIL MATERIAL AND CLEAN UP AS NEEDED.
- 16. COMPLETE FINAL GRADING AND STABILIZATION OF EARTHEN STRUCTURES SUCH AS DIVERSION BERMS, DITCH TURNOUTS AND SWALES THAT WILL CONTROL RUNOFF.
- 17. FINISH GRADE AND REPLACE TOPSOIL OR LOAM IN DISTURBED AREAS. SEED AND MULCH DISTURBED AREAS WITHIN 6 DAYS OF FINAL GRADING.
- 18. MAINTAIN ALL TEMPORARY EROSION CONTROLS AND SEDIMENT BARRIERS UNTIL VEGETATION HAS BEEN ESTABLISHED OVER 85-90% OF THE AREA TO BE RE-VEGETATED. RESEED SPARSELY VEGETATED AREAS.
- 19. REMOVE ALL TEMPORARY EROSION AND SEDIMENTATION CONTROL MEASURES ONCE THE SITE IS PERMANENTLY STABILIZED.

FERTILIZER AND LIMESTONE REQUIREMENTS:

IN GENERAL, FERTILIZER AND LIME APPLICATION RATES WILL FOLLOW THE GUIDELINES IDENTIFIED BELOW UNLESS SITE SPECIFIC SOIL TESTS IDENTIFY THE NEED FOR ALTERNATIVE FERTILIZER/LIME APPLICATION RATES, FERTILIZER WILL BE APPLIED TO UPLAND AREAS PRIOR TO SEEDING AT A RATE OF 800 POUNDS PER ACRE USING 10-20-20 OR EQUIVALENT, GROUND LIMESTONE (EQUIVALENT TO 50 PERCENT CALCIUM PLUS MAGNESIUM OXIDE) WILL BE APPLIED AT A RATE OF 3 TONS PER ACRE. AN EQUIVALENT MIXTURE OF FERTILIZER AND LIME MAY BE APPLIED USING THE HYDROSEEDING METHOD, NO LIME OR FERTILIZER WILL BE APPLIED TO WETLANDS.

MULCH AND SEEDING SPECIFICATIONS

CONDITION	TIMING	MULCH TYPE ^{1,2}	APPLICATION RATE
TEMPORARY			
	IF NO ACTIVITY IN EXPOSED AREAS FOR 7 DAYS, OR PRIOR TO A STORM EVENT	STRAW MULCH OR WOOD FIBER MULCH	2 TONS/ACRES 2000 LB./ACRES
ALL DISTRIBUTED AREAS OF THE CONSTRUCTION WORKSPACE	APPLY MULCH TO ALL EXPOSED AREAS IF NO ACTIVITY OCCURS WITHIN 30 DAYS. APPLY MULCH AND TEMPORARY SEEDING SOONER WHEN IT CAN BE ANTICIPATED THAT ACTIVITY IS NOT GOING TO OCCUR WITHIN 30 DAYS.	STRAW MULCH OR WOOD FIBER MULCH	2 TONS/ACRES 2000 LB./ACRES
ALL WORK AREAS EXPOSED ARE TO BE MULCHED DAILY EACH TIME SOIL IS DISTURBED	OCTOBER 15 - MAY 1	STRAW MULCH OR WOOD FIBER MULCH	3 TONS/ACRES 2000 LB./ACRES
PERMANENT		grown activities and activities are some or the statement of the control of the statement o	
ON ALL EXPOSED AREAS AFTER SEEDING TO STABILIZE THE SOIL SURFACE	PERMANENT GRASS AND/OR LEGUME SEEDING COVERED BY HAY OR STRAW MULCH ON ALL AREAS THAT HAVE BEEN RESTORED TO FINAL GRADE. THIS DOES NOT APPLY TO AREAS STABILIZED BY OTHER MEANS SUCH AS JUTE MATTING OR PERMANENT EROSION CONTROL MIX.	CRIMPED STRAW MULCH OR PAPER MULCH OR WOOD FIBER MULCH	2 TONS/ACRES 1500 LB./ACRES
WOOD CHIP APPLICATION AREAS	PERMANENT GRASS AND/OR LEGUME SEEDING COVERED BY HAY OR STRAW MULCH ON ALL AREAS THAT HAVE BEEN RESTORED TO FINAL GRADE. THIS DOES NOT APPLY TO AREAS STABILIZED BY OTHER MEANS SUCH AS JUTE MATTING OR PERMANENT EROSION CONTROL MIX.	CRIMPED STRAW MULCH OR PAPER MULCH OR WOOD FIBER MULCH	2 TONS/ACRES 1500 LB./ACRES 2000 LB./ACRES

NOTES:

1. STRAW AND HAY MULCH MAY BE USED INTERCHANGEABLY, EXCEPT IN WETLAND AREAS WHERE STRAW MULCH WILL BE REQUIRED.

. DOUBLE RATE OF WOOD FIBER MULCH WHEN USED IN CRITICAL AREAS.

STRAW, HAY, OR HYDROMULCH (WOOD FIBER OR PAPER MULCH AS APPROPRIATE) WILL PROVIDE 90 PERCENT GROUND

4. PAPER MULCH IS ACCEPTABLE FOR USE DURING THE GROWING SEASON. ON SLOPES GREATER THAN 30 PERCENT AND IN AREAS WHERE VEGETATION HAS NOT ESTABLISHED WELL, ADDITIONAL HAY MULCH WILL BE ADDED AS A WINTERIZING MEASURE.

MULCH ANCHORING REQUIREMENTS

ON SLOPES GREATER THAN 3 PER CENT, HAY OR STRAW MULCH WILL BE FIRMLY ANCHORED INTO THE SOIL UTILIZING ONE OF THE FOLLOWING METHODS:

-CRIMPING WITH A STRAIGHT OR NOTCHED MULCH CRIMPING TOOL (FARM DISCS WILL NOT BE ALLOWED);
-TRACK WALKING WITH DEEP-CLEATED EQUIPMENT OPERATING UP AND DOWN THE SLOPE (MULCH CRIMPED PERPENDICULAR TO THE SLOPE) ON SLOPES LESS THAN 25 PERCENT;

-APPLICATION OF MULCH NETTING;

-APPLICATION OF 500 LB./ACRE OF WOOD FIBER MULCH OVER STRAW/HAY MULCH; AND -COMMERCIALLY AVAILABLE TACKIFIERS (EXCEPT WITHIN 100 FEET OF WATERBODIES OR WETLANDS).

-	SUMMARY OF SEEDING REQUIREMENTS	
CONDITION	TIMING ^{1,2}	SEED MIX
TEMPORARY SEEDING ³	TEMPORARY SEED BETWEEN MAY 1 AND OCTOBER 15 ONLY. DISTURBED AREAS OR SPOIL STOCKPILES WILL BE SEEDED IMMEDIATELY IF FURTHER DISTURBANCE IS NOT EXPECTED FOR 30 DAYS OR MORE.	ANNUAL RYEGRASS
PERMANENT SEEDING3,4	·	
UPLAND PORTIONS OF THE CONSTRUCTION AREA	DISTURBED AREA WILL BE SEEDED WITHIN 6 DAYS OF FINAL GRADING.	PERMANENT UPLAND MIX
SLOPES GREATER THAN 3:1	DISTURBED AREA WILL BE SEEDED IMMEDIATELY AFTER SEEDBED PREPARATION.	PERMANENT UPLAND MIX
WETLANDS	DISTURBED WETLANDS WILL BE SEEDED WITHIN 6 DAYS OF FINAL GRADING.	ANNUAL RYEGRASS
WOOD CHIP APPLICATION AREAS	DISTURBED AREA WILL BE SEEDED WITHIN 6 DAYS OF FINAL GRADING.	WOODCHIP APPLICATION SEED MIX
WINTER DORMANT SEEDING	DORMANT SEED BETWEEN OCTOBER 15 AND MAY 1 ONLY. NO SEEDING WILL OCCUR IF SNOW DEPTHS EXCEED 1 INCH.	PERMANENT UPLAND MIX PLUS WINTER RYEGRASS

NOTES:

- WEATHER CONDITIONS PERMITTING.
- 2. AREAS THAT DO NOT SUCCESSFULLY REVEGETATE WITHIN APPROPRIATE PERIOD OF TIME WILL BE RESEDED AS
- . LOOSEN COMPACTED SOIL TO A MINIMUM DEPTH OF 4 INCHES.
- 4. TOP DRESS WITH 6 INCHES LOAM, AS NEEDED.

SEED N	MIX SPECIFICATIONS				
SEED MIX NAME	SEED MIX COMPONENTS	LB./ACRE			
TEMPORARY SEED MIX	ANNUAL RYEGRASS	40			
PERMANENT UPLAND SEED MIX	REDTOP CREEPING RED FESCUE TALL FESCUE BIRDSFOOT TREFOIL	4 40 40 16			
WOOD CHIP APPLICATION SEED MIX	CREEPING RED FESCUE REDTOP TALL FESCUE CROWNVETCH	20 4 30 30			
WETLAND SEED MIX	ANNUAL RYEGRASS	40			
SUPPLEMENTAL WINTER SEED MIX2	WINTER RYEGRASS	120			
NOTEC.					

NOTES

 INCREASE SEEDING RATES 10% WHEN HYDROSEEDING
 WINTER RYE WILL BE ADDED TO PERMANENT UPLAND MIX AT A RATE OF 120 LB./ACRE BETWEEN OCTOBER 15 AND MAY 1

ISSUED FOR PERMITTING
NOT FOR CONSTRUCTION 09/13/17

REV.	DESCRIPTION	DATE BY	CK APP	OWNER ENGINEER:	APPROVAL STAMP:	PE Stamp		IBERI	CMP DROLA - USA	SITE	DETAILS 5
						KENNETH X				Si	SH 5 OF 5
				DRAWING PREPARED BY:	ACCEPTED BY OE:	N6.11082				FICKETT ROAD/1077 DR. EVD SCALE: NONE	POWNAL, N
						18945 de Poenotrado	REV. DATE BY	DESCRIPTION	APP.	CK. KRV NO. APP. DATE:	1077-003-005

CADD Drawing, DO NOT REVISE MANUALLY.