

August 14, 2019

Project 171.05027

Mr. Kevin Martin
Compliance & Procedures Specialist
Maine Department of Environmental Protection
112 Canco Road
Portland, Maine 04103

RE: Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N

Dear Mr. Martin:

This letter provides responses to the Department of Environmental Protection letter from Kevin Martin to Elizabeth Ransom dated July 31, 2019. For clarity, the entire comment from the letter has been copied below and italicized. Responses are in regular text, and on the attached plans and figures as referenced below.

The Department is requesting the following information to further characterize the discharge from the proposed Nordic Aquafarms site in Belfast:

1. The location of the outfall, its configuration, and what the associated acute and chronic dilution factors will be and provide modeling details as to how they were derived.

As noted on EPA Form 2D, submitted as page 204 of the application, the proposed location of the outfall is at a latitude of 44 degrees, 23 minutes, 40 seconds, and a longitude of 68 degrees, 58 minutes, and 25 seconds. The outfall configuration is shown on the diagram in **Attachment A**.

The CORMIX modeling presented in our September 27, 2018 memorandum that was included with permit application evaluated a single port outfall as well as a multi-port diffuser outfall. The modeling evaluated single port and multi-port diffuser configurations for two different locations described by their depth and approximate distance from the shoreline. These included a deep location assuming 15 meters depth at Mean Lower Low Water (MLLW) as well as a shallow location assuming 8 meters depth at MLLW. After completion of the September 27, 2018 memorandum it was decided to go forward with the multi-port diffuser as described in the memorandum but located at an intermediate location with a depth of 11.5 meters.

CORMIX modeling has since been performed to simulate the final diffuser configuration and location assuming a depth 11.5 meters. With exception to the assumed depth at the outfall, the methods and inputs are the same as described in our September 27, 2018 memorandum. The

Mr. Kevin Martin
Maine Department of Environmental Protection

results are qualitatively similar to results for the multi-port diffuser described in the memo. A table summarizing dilution at 15 minutes travel time for the two current speeds and 4 seasons simulated are provided in **Attachment B** along with CORMIX session and prediction files for the simulations. The results show dilution at 15 minutes travel time ranging from 15.7 to 282.6, with median value of 52.5 and mean of 78.6. The lowest values for dilution at 15 minutes travel time are expected to occur during slack tides when stratification is stronger in the spring and summer and the MS4 flow classification is predicted.

The modeling indicates minimum dilution occurs during times with strong ambient stratification in the springtime. In those cases, CORMIX predicts the MS4 flow class during slack tide when the buoyancy dominates the cross flow, and the MS1 flow class during mid tide when ambient currents more strongly deflect the discharge. Both flow classes predict that the buoyant effluent becomes trapped as the effluent rises in the ambient stratification. For slack tide a dilution of 10.1 is reached at the terminal trapping level, and for mid-tide a dilution of 15.0 is reached at the terminal trapping level. Thus, according to 06-096 CMR 530 4.A.(2)(a) the acute and chronic dilution factors should be 10.1 and 15.0, respectively.

2. The final far-field dilution, which models were used, why they were used and substantial details about all assumptions used to develop the model(s)

Unlike the preliminary CORMIX analysis presented in our September 27, 2018 memorandum, the far-field analysis described in our October 2, 2018 memo is representative of the final discharge location and outfall configuration as described above.

The far-field modeling approach used a 2-dimensional vertically averaged finite element hydrodynamic model to simulate 15-minute snapshots of the tidal current field. Output from the hydrodynamic simulation was then used drive an offline particle tracking model to simulate mixing and dispersion of the effluent. The particle tracking model was configured to release particles randomly along a 50 m line at the diffuser location consistent with the results of the near-field discharge from CORMIX. Particles were released at regular intervals so that each particle represents an equal mass of effluent. Dilution was then calculated by counting particles within control volumes defined by the finite element grid and dividing the total volume in the control volume by the volume of effluent determined from the particle count. These methods were employed to evaluate far-field dilution because they allow for a dynamic assessment of mixing and dispersion of the effluent that is influenced by cyclic and residual tidal currents. In tidal environments a dynamic analysis is necessary to accurately account for re-circulation of the effluent past the outfall that can tend to increase effective background concentrations, which cannot be simulated by a steady-state model such as CORMIX.

The hydrodynamic model employed uses the ADvanced CIRCulation (ADCIRC) model code. The physics and numerical discretization of the ADCIRC model is well described in the literature (e.g. Luettich et al. 1992, see footnote in the October 2, 2018 memorandum). Details describing ADCIRC model input parameters and output files can be found in the online user's manual at www.adcirc.org. The particular ADCIRC model used for the far-field dilution analysis was initially developed for coastal flood hazard studies in the larger Penobscot Bay region. A report describing the development of the ADCIRC model for Penobscot Bay, including sources of

Mr. Kevin Martin
Maine Department of Environmental Protection

topographic and bathymetric data, frictional parameterization, grid resolution, and model validation, has been prepared for the Town of Islesboro and can be provided upon request. The model was adapted for far-field dilution modeling in Belfast Bay by turning on convective acceleration terms in the model parameterization and implementing the horizontal Smagorinsky turbulence closure scheme to improve physical accuracy of the velocity field simulation for dilution analysis (note, the original model application of simulating tide and storm surge water levels ignored these terms in favor of numerical stability). The Smagorinsky turbulence closure feature became available in version 53 of the ADCIRC model code and is not well documented in the user manual. An additional model validation comparison for the modified model was performed by comparing modeled water levels to NOAA's observed tides at Fort Point and NOAA's harmonic predicted tides at Belfast for the representative time period that was simulated and used for the dilution analysis. An annotated run control file for the ADCIRC simulation (fort.15) that describes the various model input parameters is provided in **Attachment C**. Model input and output files, and instructions for running the model code can be provided upon request.

Particle tracking was performed using the Maureparticle model, which has been developed to perform offline particle tracking given velocity field output from the ADCIRC model. Development of the Maureparticle code was originally described in a report to the Louisiana Department of Natural Resources¹, with further development described in the master's thesis referenced in the footnote in our October 2, 2018 memorandum. An annotated run control file (particles.inp) for the Maureparticle simulation used in the far-field dilution analysis, which describes the model input parameters, is provided in **Attachment C**. Maureparticle is a relatively simple Fortran90 program that is available on github². The specific version of the code used for the far-field analysis and additional detail and instructions on running the program can be provided upon request.

3. The far-field modeling information needs to include an analysis of the discharge's influence on ambient water quality relative to dissolved oxygen and total nitrogen. This analysis should be based on expected permit limits for BOD (technology-based limit for BOD (technology-based limit for BOD is expected to be 30 mg/l as a monthly average, and 50 mg/L as a daily maximum), and proposed loading for total nitrogen and discharge flow. The applicant's water quality monitoring contained DO values that were below the percent saturation criterion for the SB waterbody classification.

We understand that near-bottom observations in the vicinity of the proposed outfall have shown DO concentrations that are below saturation criteria for SB water classification, and that such conditions may occur as a result of natural processes, particularly when strong density stratification prevents mixing of the surface waters into bottom layers. The CORMIX modeling indicates the discharge is positively buoyant during all seasons due to density differences between the effluent and ambient water. Positive buoyancy will tend to keep higher total Nitrogen and BOD concentrations from the effluent within the upper layers of the water column where they will have limited effect on near bottom DO. In the winter season when ambient stratification

¹ URS, 2006. Mississippi River Reintroduction into Maurepas Swamp Project PO-29, Volume VII of VII Diversion Modeling. Final Report to the Louisiana Department of Natural Resources, December 2006. Online at: https://lacoast.gov/reports/project/Vol_VII_Diversion%20Modeling%20Report-Dec%208-FINAL.pdf

² https://github.com/natedill/maureparticle/tree/lose_wetdry

Mr. Kevin Martin
Maine Department of Environmental Protection

becomes weaker and the effluent is expected to become fully vertically mixed the colder water temperatures and full vertical ambient mixing will tend to prevent low near-bottom DO concentrations.

The far-field dilution analysis shows relatively low Total N and BOD concentrations given the proposed nitrogen loading (5.55 mg/l) and technology based daily limit for BOD (50 mg/l). Images showing time medial total N and BOD concentrations for those effluent concentrations based on the far-field dilution estimated in our October 2, 2018 memorandum are provided in **Attachment D**.

Nordic Aquafarms understand the concern raised by observed DO concentrations that do not meet SB water classification and intends to closely monitor DO and other water quality variables as the facility is developed and discharges increase to permitted rates.

4. A detailed list of all drugs, pesticides, and chemicals that may be used in the facility, their concentration, and an estimate of the amount used annually.

A detailed list of all drugs, pesticides, and chemicals that may be used in the facility, including their concentration and an estimate of the amount use annually, was included as Attachment 3 to the Fish Rearing Facility Form, Questions 10 and 11, submitted as pages 216 through 219 of the MEPDES application. An updated list is attached to this letter as **Attachment E**.

Nordic Aquafarms has removed methanol from the list of chemicals included in the initial submission of the company's MEPDES permit (October 19, 2019). The process of denitrification, which Nordic Aquafarms is using to reduce nitrogen in its discharge, requires the addition of a carbon source. Methanol is traditionally used as a carbon source in this application. Since the initial MEPDES submission, Nordic Aquafarms staff have identified and vetted a more favorable alternative to methanol that is USDA certified as a [Biobased Product](#). This product, MicroC 2000, should replace Methanol on the chemical list included as part of NAF's MEPDES application. Use of MicroC 2000 is further described on the attached list of chemicals, as well as the SDS and technical data sheets included.

5. Information regarding the temperature or thermal component of the discharge to the receiving water.

Temperature of the effluent is expected to be constant at 13 degrees centigrade. Ambient temperatures range from 0 centigrade to 22 centigrade (Normandeau, 1978). **Attachment F** shows estimated effluent temperatures that bracket the range of high and low ambient temperatures based on the far-field dilution estimated in our October 2, 2018 memorandum. Overall the far-field temperature anomaly is expected to be less than 0.2 degrees centigrade in either season based on this analysis.

Mr. Kevin Martin
Maine Department of Environmental Protection

Please contact me with any questions or comments.

Sincerely,

RANSOM CONSULTING, INC.

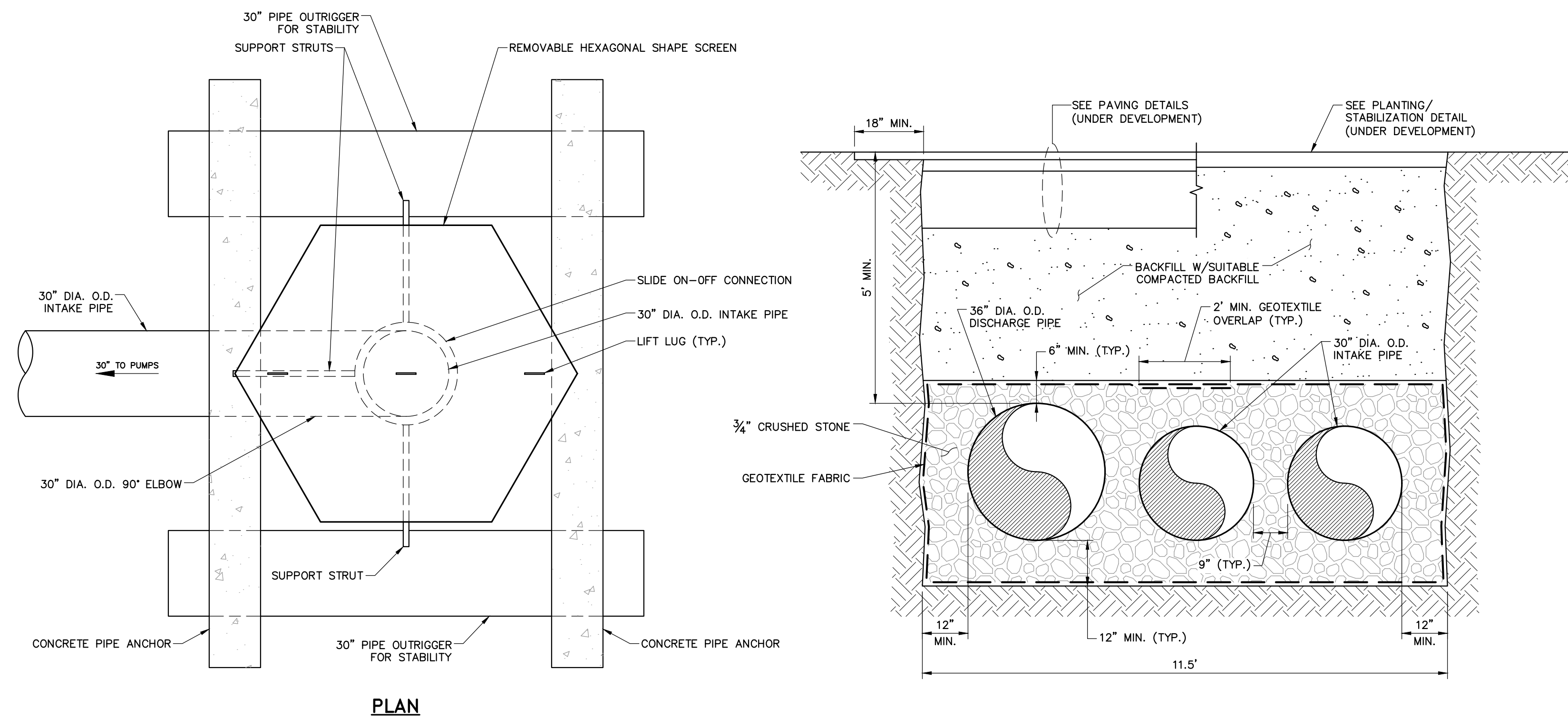
Elizabeth M. Ransom, P.G.
Senior Project Manager

EMR:jar

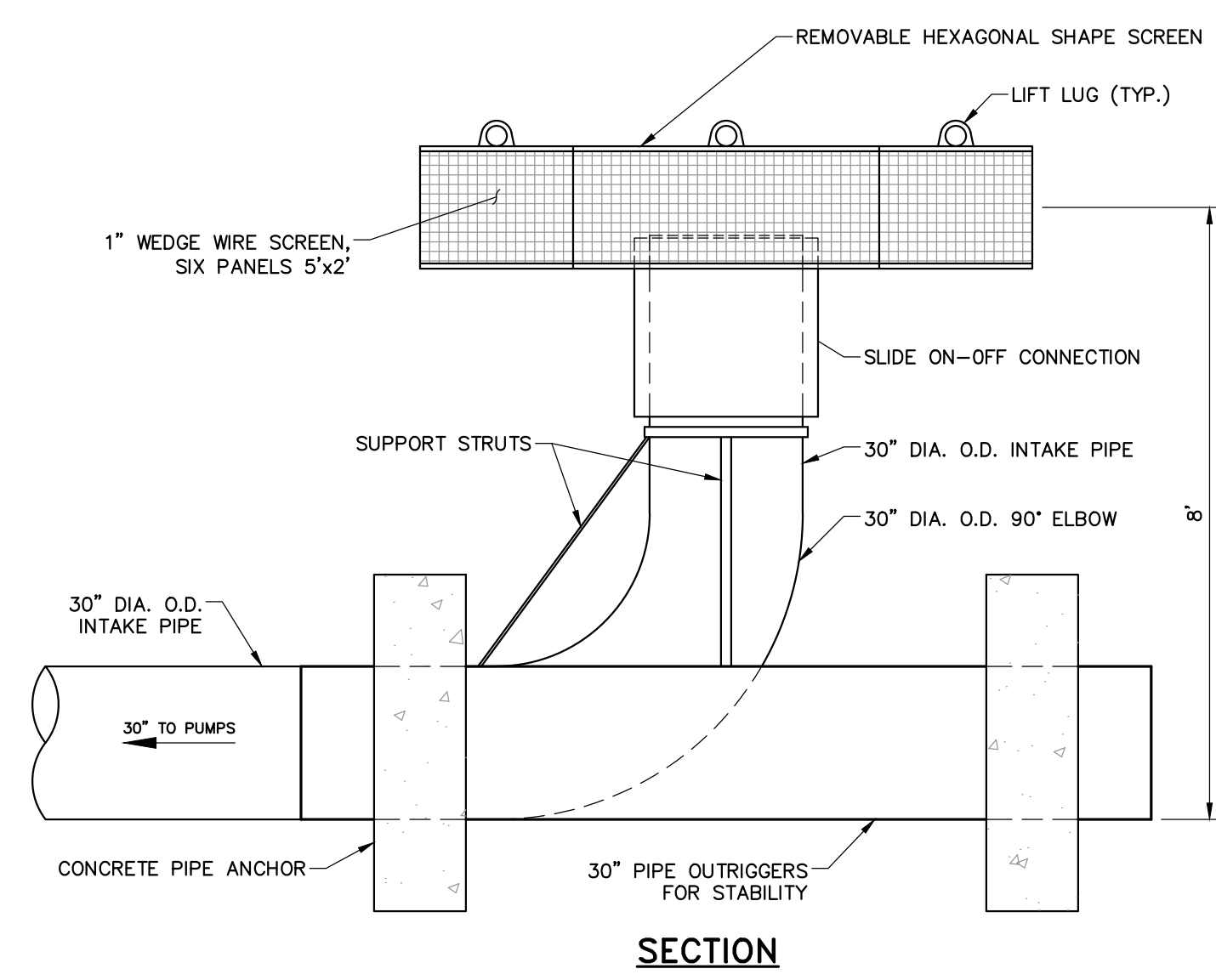
ATTACHMENT A

Discharge Diffuser Detail Drawing CS503

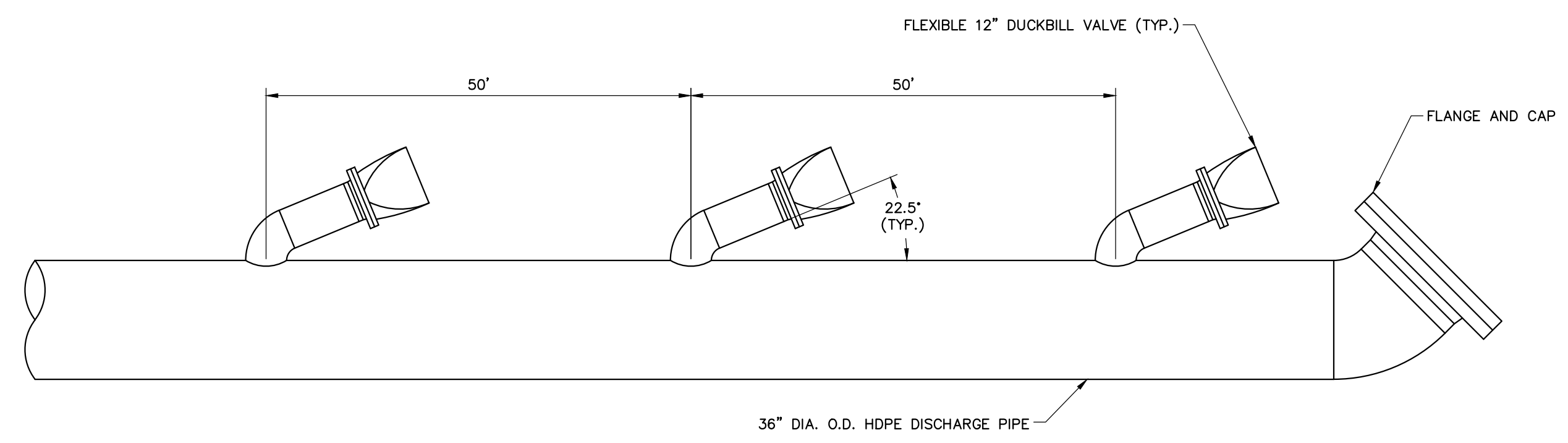
Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N



5 BURIED 3-PIPE TRENCH DETAIL (LAND)
SCALE: 1" = 2'



6 INTAKE STRUCTURE DETAIL
SCALE: NOT TO SCALE



7 DISCHARGE DIFFUSER DETAIL
SCALE: NOT TO SCALE

RANSOM Consulting Engineers and Scientists

WOODARD & CURRAN
41 Hutchins Drive
Portland, Maine 04102
800.426.4262 | www.woodardcurran.com
COMMITMENT & INTEGRITY DRIVE RESULTS

REV	DESCRIPTION	DATE
-----	-------------	------

ISSUED FOR PERMIT
05-02-19
CURRENT ISSUE STATUS:

TRUE NORTH:
SMRT Architects and Engineers
144 Fore Street, PO Box 618
Portland, Maine 04104

ARCHITECTURE | ENGINEERING | PLANNING | INTERIORS | ENERGY **SMRT**

NORDIC AQUAFARMS

BELFAST, MAINE

CIVIL DETAILS - 3

PROJECT MANAGER: PROJECT NO: 18076

JOB CAPTAIN: **CS503**

NOT FOR CONSTRUCTION

ATTACHMENT B

CORMIX Summary Table and Results

Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N

Summary of CORMIX Results at Intermediate Depth location for Diffuser at 15 minutes Travel Time

Location	Current (m/s)	Season	CORMIX Flow Class	Distance From Port* (m)	Dilution	% Initial Conc. Excess
Intermediate	0.2	Winter	MU6	180.4	282.6	0.4
Intermediate	0.2	Spring	MS1	191.6	54.0	1.9
Intermediate	0.2	Summer	MS1	195.1	69.4	1.5
Intermediate	0.2	Fall	MS1	197.7	82.3	1.2
Intermediate	0.05	Winter	MU6	45.8	51.1	2.0
Intermediate	0.05	Spring	MS4	54.7	15.7	6.4
Intermediate	0.05	Summer	MS4	58.1	22.3	4.5
Intermediate	0.05	Fall	MU6	45.8	51.1	2.0

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FRO = 70.56
Port/nozzle Froude number FRD0 = 8.92
Velocity ratio R = 7.69

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MU6 |

This flow configuration applies to a layer corresponding to the full water depth at the discharge site.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:
750 m from the right bank/shore.
Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 0.4841 deg.C
Dilution at edge of NFR s = 206.6
NFR Location: x = 57.5 m
(centerline coordinates) y = 0.56 m
z = 11.5 m

NFR plume dimensions: half-width (bh) = 15.13 m
thickness (bv) = 11.5 m

Cumulative travel time: 287.5 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.
Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Near-field instability behavior:

The diffuser flow will experience instabilities with full vertical mixing in the near-field.
There may be benthic impact of high pollutant concentrations.

FAR-FIELD MIXING SUMMARY:

Plume is vertically fully mixed WITHIN NEAR-FIELD (or a fraction thereof), but RE-STRATIFIES LATER.
Plume becomes vertically fully mixed again at 997.74 m downstream.

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****
No TDZ was specified for this simulation.
***** REGULATORY MIXING ZONE SUMMARY *****
No RMZ and no ambient water quality standard have been specified.
***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles (or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about $\pm 50\%$ (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
 750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

 BEGIN MOD202: DISCHARGE MODULE (STAGED DIFFUSER)

Due to complex near-field motions: EQUIVALENT SLOT DIFFUSER (2-D) GEOMETRY

Profile definitions:

BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory
 BH = Gaussian 1/e (37%) half-width in horizontal plane normal to trajectory
 S = hydrodynamic centerline dilution
 C = centerline concentration (includes reaction effects, if any)
 Uc = Local centerline excess velocity (above ambient)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.00	15.00	1.538	.00000E+00

END OF MOD202: DISCHARGE MODULE (STAGED DIFFUSER)

 BEGIN MOD275: STAGED PERPENDICULAR DIFFUSER IN STRONG CURRENT

Because of the strong ambient current the diffuser plume of this crossflowing discharge gets RAPIDLY DEFLECTED.

A near-field zone is formed that is VERTICALLY FULLY MIXED over the entire layer depth. Full mixing is achieved at a downstream distance of about five (5) layer depths.

Profile definitions:

BV = layer depth (vertically mixed)
 BH = top-hat half-width, measured horizontally in Y-direction
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	TT
0.00	0.00	2.00	1.0	0.100E+03	0.00	15.00	.00000E+00
2.88	0.03	2.19	47.0	0.213E+01	0.58	15.01	.14375E+02
5.75	0.06	2.38	66.0	0.151E+01	1.15	15.01	.28750E+02
8.62	0.08	2.56	80.6	0.124E+01	1.73	15.02	.43125E+02
11.50	0.11	2.75	92.9	0.108E+01	2.30	15.03	.57500E+02
14.38	0.14	2.94	103.8	0.964E+00	2.88	15.03	.71875E+02
17.25	0.17	3.12	113.6	0.880E+00	3.45	15.04	.86250E+02
20.12	0.20	3.31	122.6	0.816E+00	4.03	15.05	.10062E+03
23.00	0.23	3.50	131.0	0.763E+00	4.60	15.05	.11500E+03
25.88	0.25	3.69	138.9	0.720E+00	5.18	15.06	.12938E+03
28.75	0.28	3.88	146.4	0.683E+00	5.75	15.07	.14375E+03
31.62	0.31	4.06	153.5	0.652E+00	6.33	15.07	.15812E+03
34.50	0.34	4.25	160.2	0.624E+00	6.90	15.08	.17250E+03
37.38	0.37	4.44	166.7	0.600E+00	7.48	15.09	.18688E+03
40.25	0.39	4.62	173.0	0.578E+00	8.05	15.09	.20125E+03
43.12	0.42	4.81	179.0	0.559E+00	8.63	15.10	.21562E+03

46.00	0.45	5.00	184.9	0.541E+00	9.20	15.11	.23000E+03
48.88	0.48	5.19	190.5	0.525E+00	9.78	15.11	.24438E+03
51.75	0.51	5.38	196.0	0.510E+00	10.35	15.12	.25875E+03
54.62	0.54	5.56	201.4	0.497E+00	10.93	15.13	.27312E+03
57.50	0.56	5.75	206.6	0.484E+00	11.50	15.13	.28750E+03

Cumulative travel time = 287.5000 sec (0.08 hrs)

Plume centerline may exhibit slight discontinuities in transition to subsequent far-field module.

END OF MOD275: STAGED PERPENDICULAR DIFFUSER IN STRONG CURRENT

 ** End of NEAR-FIELD REGION (NFR) **

BEGIN MOD241: BUOYANT AMBIENT SPREADING

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

Plume Stage 1 (not bank attached):

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
57.50	0.56	11.50	206.6	0.484E+00	11.50	15.13	11.50	0.00	.28750E+03
104.51	0.56	11.50	239.8	0.417E+00	7.86	25.70	11.50	3.64	.52253E+03
151.51	0.56	11.50	266.2	0.376E+00	6.52	34.38	11.50	4.98	.75756E+03
198.52	0.56	11.50	293.2	0.341E+00	5.87	42.07	11.50	5.63	.99259E+03
245.52	0.56	11.50	323.3	0.309E+00	5.55	49.11	11.50	5.95	.12276E+04
292.53	0.56	11.50	358.0	0.279E+00	5.42	55.67	11.50	6.08	.14626E+04
339.53	0.56	11.50	398.3	0.251E+00	5.42	61.86	11.50	6.08	.16977E+04
386.54	0.56	11.50	444.6	0.225E+00	5.53	67.76	11.50	5.97	.19327E+04
433.55	0.56	11.50	497.7	0.201E+00	5.71	73.40	11.50	5.79	.21677E+04
480.55	0.56	11.50	557.8	0.179E+00	5.96	78.84	11.50	5.54	.24028E+04
527.56	0.56	11.50	625.5	0.160E+00	6.27	84.09	11.50	5.23	.26378E+04
574.56	0.56	11.50	700.9	0.143E+00	6.62	89.19	11.50	4.88	.28728E+04
621.57	0.56	11.50	784.5	0.127E+00	7.02	94.14	11.50	4.48	.31078E+04
668.58	0.56	11.50	876.4	0.114E+00	7.46	98.97	11.50	4.04	.33429E+04
715.58	0.56	11.50	977.0	0.102E+00	7.94	103.68	11.50	3.56	.35779E+04
762.59	0.56	11.50	1086.5	0.920E-01	8.45	108.28	11.50	3.05	.38129E+04
809.59	0.56	11.50	1205.1	0.830E-01	9.00	112.79	11.50	2.50	.40480E+04
856.60	0.56	11.50	1333.0	0.750E-01	9.58	117.22	11.50	1.92	.42830E+04
903.60	0.56	11.50	1470.4	0.680E-01	10.19	121.56	11.50	1.31	.45180E+04
950.61	0.56	11.50	1617.6	0.618E-01	10.83	125.83	11.50	0.67	.47531E+04
997.62	0.56	11.50	1774.6	0.563E-01	11.50	130.02	11.50	0.00	.49881E+04

Cumulative travel time = 4988.0820 sec (1.39 hrs)

END OF MOD241: BUOYANT AMBIENT SPREADING

 BEGIN MOD261: PASSIVE AMBIENT MIXING IN UNIFORM AMBIENT

Vertical diffusivity (initial value) = 0.515E-01 m²/s
 Horizontal diffusivity (initial value) = 0.988E+00 m²/s

Profile definitions:

BV = Gaussian s.d.*sqrt(pi/2) (46%) thickness, measured vertically
 = or equal to layer depth, if fully mixed
 BH = Gaussian s.d.*sqrt(pi/2) (46%) half-width,
 measured horizontally in Y-direction

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 94.75
Port/nozzle Froude number FRD0 = 11.97
Velocity ratio R = 7.69

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MS1 |

This flow configuration applies to a layer corresponding to the linearly stratified density layer at the discharge site.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:
750 m from the right bank/shore.
Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 4.5378 deg.C

Dilution at edge of NFR s = 22.0

NFR Location: x = 24.07 m

(centerline coordinates) y = 1.25 m

z = 3.23 m

NFR plume dimensions: half-width (bh) = 16.40 m

thickness (bv) = 1.13 m

Cumulative travel time: 62.7086 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.

Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Stratification assessment:

The specified ambient density stratification is dynamically important.

The discharge near field flow is trapped within the linearly stratified ambient density layer.

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****
No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****
No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles

(or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about +-50% (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

C0 = 0.1000E+03 CUNITS= deg.C
 NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
 750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

BEGIN MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00

END OF MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

BEGIN CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

Jet-like motion in linear stratification with strong crossflow.

Zone of flow establishment: THETA= 21.97 SIGMA= 86.67
 LE = 0.89 XE = 0.02 YE = 0.82 ZE = 2.33

Profile definitions:

- BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory
- BH = before merging: Gaussian 1/e (37%) half-width in horizontal plane normal to trajectory
- after merging: top-hat half-width in horizontal plane parallel to diffuser line
- S = hydrodynamic centerline dilution
- C = centerline concentration (includes reaction effects, if any)
- Uc = Local centerline excess velocity (above ambient)
- TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
Individual jet/plumes before merging:								
0.02	0.82	2.33	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00
0.02	0.82	2.33	1.0	0.100E+03	0.15	0.15	1.538	.20073E-02
0.98	1.15	2.48	1.7	0.581E+02	0.27	0.27	0.905	.78249E+00
2.06	1.21	2.54	2.5	0.405E+02	0.36	0.36	0.642	.19223E+01
3.15	1.24	2.61	3.2	0.309E+02	0.45	0.45	0.500	.33437E+01
4.23	1.25	2.67	4.0	0.249E+02	0.52	0.52	0.409	.50105E+01
5.31	1.25	2.74	4.8	0.208E+02	0.59	0.59	0.347	.68943E+01
6.40	1.25	2.80	5.6	0.178E+02	0.66	0.66	0.301	.89793E+01
7.48	1.25	2.86	6.4	0.156E+02	0.72	0.72	0.266	.11227E+02
8.56	1.25	2.91	7.2	0.139E+02	0.78	0.78	0.239	.13628E+02
9.64	1.25	2.96	8.0	0.125E+02	0.83	0.83	0.217	.16165E+02
10.73	1.25	3.01	8.8	0.114E+02	0.88	0.88	0.199	.18826E+02
11.81	1.25	3.05	9.6	0.105E+02	0.93	0.93	0.184	.21598E+02
12.89	1.25	3.08	10.3	0.970E+01	0.97	0.97	0.171	.24472E+02
13.98	1.25	3.12	11.1	0.905E+01	1.02	1.02	0.160	.27450E+02
15.06	1.25	3.15	11.8	0.850E+01	1.06	1.06	0.151	.30501E+02
16.15	1.25	3.17	12.5	0.802E+01	1.09	1.09	0.143	.33629E+02
17.23	1.25	3.19	13.1	0.761E+01	1.13	1.13	0.136	.36826E+02
18.31	1.25	3.21	13.8	0.725E+01	1.16	1.16	0.129	.40086E+02
19.40	1.25	3.22	14.4	0.694E+01	1.19	1.19	0.124	.43405E+02
20.48	1.25	3.23	15.0	0.666E+01	1.22	1.22	0.119	.46776E+02

Maximum jet height has been reached.

21.57 1.25 3.23 15.6 0.642E+01 1.25 1.25 0.115 .50195E+02

Terminal level in stratified ambient has been reached.

Cumulative travel time = 50.1949 sec (0.01 hrs)

Merging of individual jet/plumes not found in this module, but interaction will occur in following module. Overall jet/plume interaction dimensions:

21.57 1.25 3.23 15.6 0.642E+01 1.25 15.15 0.115 .50195E+02

END OF CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

 BEGIN MOD235: LAYER/BOUNDARY/TERMINAL LAYER APPROACH

Control volume inflow:

X	Y	Z	S	C	BV	BH	TT
21.57	1.25	3.23	15.6	0.642E+01	1.25	15.15	.50195E+02

Profile definitions:

BV = top-hat thickness, measured vertically

BH = top-hat half-width, measured horizontally in y-direction

ZU = upper plume boundary (Z-coordinate)

ZL = lower plume boundary (Z-coordinate)

S = hydrodynamic average (bulk) dilution

C = average (bulk) concentration (includes reaction effects, if any)

TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
20.31	1.25	3.23	15.6	0.642E+01	0.00	0.00	3.23	3.23	.50195E+02
21.06	1.25	3.23	15.6	0.642E+01	0.84	7.34	3.65	2.81	.50195E+02
21.82	1.25	3.23	15.8	0.631E+01	0.99	16.36	3.72	2.73	.51446E+02
22.57	1.25	3.23	18.6	0.537E+01	1.07	16.38	3.76	2.69	.55200E+02
23.32	1.25	3.23	21.1	0.473E+01	1.12	16.39	3.79	2.67	.58954E+02
24.07	1.25	3.23	22.0	0.454E+01	1.13	16.40	3.79	2.66	.62709E+02

Cumulative travel time = 62.7086 sec (0.02 hrs)

END OF MOD235: LAYER/BOUNDARY/TERMINAL LAYER APPROACH

 ** End of NEAR-FIELD REGION (NFR) **

 BEGIN MOD242: BUOYANT TERMINAL LAYER SPREADING

Profile definitions:

BV = top-hat thickness, measured vertically

BH = top-hat half-width, measured horizontally in y-direction

ZU = upper plume boundary (Z-coordinate)

ZL = lower plume boundary (Z-coordinate)

S = hydrodynamic average (bulk) dilution

C = average (bulk) concentration (includes reaction effects, if any)

TT = Cumulative travel time

Plume Stage 1 (not bank attached):

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
24.07	1.25	3.23	22.0	0.454E+01	1.13	16.40	3.79	2.66	.62709E+02
72.86	1.25	3.23	28.9	0.346E+01	0.80	30.48	3.63	2.83	.30669E+03
121.66	1.25	3.23	37.8	0.265E+01	0.75	42.15	3.61	2.85	.55067E+03
170.46	1.25	3.23	48.6	0.206E+01	0.77	53.51	3.61	2.85	.79466E+03
219.25	1.25	3.23	61.1	0.164E+01	0.79	65.05	3.62	2.83	.10386E+04
268.05	1.25	3.23	74.8	0.134E+01	0.82	76.90	3.64	2.82	.12826E+04
316.85	1.25	3.23	89.7	0.111E+01	0.85	89.08	3.65	2.80	.15266E+04
365.64	1.25	3.23	105.7	0.946E+00	0.88	101.57	3.67	2.79	.17706E+04
414.44	1.25	3.23	122.7	0.815E+00	0.90	114.37	3.68	2.78	.20146E+04
463.24	1.25	3.23	140.6	0.711E+00	0.93	127.45	3.69	2.76	.22586E+04

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 85.06
Port/nozzle Froude number FRD0 = 10.75
Velocity ratio R = 7.69

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MS1 |

This flow configuration applies to a layer corresponding to the linearly stratified density layer at the discharge site.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:

750 m from the right bank/shore.

Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 2.9421 deg.C

Dilution at edge of NFR s = 34.0

NFR Location: x = 35.99 m

(centerline coordinates) y = 1.24 m

z = 3.75 m

NFR plume dimensions: half-width (bh) = 16.75 m

thickness (bv) = 1.71 m

Cumulative travel time: 104.5347 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.

Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Stratification assessment:

The specified ambient density stratification is dynamically important.

The discharge near field flow is trapped within the linearly stratified ambient density layer.

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****
No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****
No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles

(or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about +-50% (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

C0 = 0.1000E+03 CUNITS= deg.C
 NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

BEGIN MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00

END OF MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

BEGIN CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

Jet-like motion in linear stratification with strong crossflow.

Zone of flow establishment: THETA= 21.97 SIGMA= 86.67
 LE = 0.89 XE = 0.02 YE = 0.82 ZE = 2.33

Profile definitions:

BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory

BH = before merging: Gaussian 1/e (37%) half-width in horizontal plane
normal to trajectory

after merging: top-hat half-width in horizontal plane
parallel to diffuser line

S = hydrodynamic centerline dilution

C = centerline concentration (includes reaction effects, if any)

Uc = Local centerline excess velocity (above ambient)

TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
Individual jet/plumes before merging:								
0.02	0.82	2.33	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00
0.02	0.82	2.33	1.0	0.100E+03	0.15	0.15	1.538	.20072E-02
1.54	1.19	2.52	2.1	0.472E+02	0.32	0.32	0.746	.13340E+01
3.18	1.23	2.63	3.3	0.304E+02	0.45	0.45	0.495	.34000E+01
4.83	1.24	2.75	4.5	0.221E+02	0.57	0.57	0.371	.60429E+01
6.47	1.24	2.86	5.8	0.173E+02	0.67	0.67	0.297	.91481E+01
8.12	1.24	2.97	7.1	0.141E+02	0.76	0.76	0.249	.12652E+02
9.76	1.24	3.06	8.4	0.120E+02	0.85	0.85	0.215	.16473E+02
11.41	1.24	3.16	9.7	0.104E+02	0.93	0.93	0.189	.20586E+02
13.05	1.24	3.24	10.9	0.915E+01	1.00	1.00	0.170	.24931E+02
14.70	1.24	3.32	12.2	0.820E+01	1.07	1.07	0.154	.29500E+02
16.34	1.24	3.40	13.4	0.744E+01	1.14	1.14	0.141	.34244E+02
17.99	1.24	3.46	14.7	0.682E+01	1.20	1.20	0.130	.39168E+02
19.63	1.24	3.52	15.9	0.630E+01	1.26	1.26	0.121	.44228E+02
21.28	1.24	3.58	17.0	0.587E+01	1.31	1.31	0.113	.49421E+02
22.92	1.24	3.62	18.1	0.551E+01	1.36	1.36	0.106	.54749E+02
24.57	1.24	3.66	19.2	0.520E+01	1.41	1.41	0.101	.60172E+02
26.22	1.24	3.70	20.3	0.493E+01	1.45	1.45	0.096	.65706E+02
27.86	1.24	3.72	21.3	0.470E+01	1.49	1.49	0.091	.71313E+02
29.51	1.24	3.74	22.2	0.451E+01	1.53	1.53	0.088	.77013E+02
31.16	1.24	3.75	23.1	0.433E+01	1.56	1.56	0.084	.82769E+02

Maximum jet height has been reached.

32.80 1.24 3.75 23.9 0.418E+01 1.59 1.59 0.081 .88586E+02

Terminal level in stratified ambient has been reached.

Cumulative travel time = 88.5862 sec (0.02 hrs)

Merging of individual jet/plumes not found in this module, but interaction will occur in following module. Overall jet/plume interaction dimensions:

32.80 1.24 3.75 23.9 0.418E+01 1.59 15.15 0.081 .88586E+02

END OF CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

 BEGIN MOD235: LAYER/BOUNDARY/TERMINAL LAYER APPROACH

Control volume inflow:

X	Y	Z	S	C	BV	BH	TT
32.80	1.24	3.75	23.9	0.418E+01	1.59	15.15	.88586E+02

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
31.21	1.24	3.75	23.9	0.418E+01	0.00	0.00	3.75	3.75	.88586E+02
32.16	1.24	3.75	23.9	0.418E+01	1.27	7.49	4.39	3.12	.88586E+02
33.12	1.24	3.75	24.3	0.412E+01	1.50	16.72	4.50	3.00	.90181E+02
34.08	1.24	3.75	28.7	0.349E+01	1.62	16.73	4.56	2.94	.94966E+02
35.03	1.24	3.75	32.6	0.307E+01	1.69	16.74	4.60	2.91	.99750E+02
35.99	1.24	3.75	34.0	0.294E+01	1.71	16.75	4.61	2.90	.10453E+03

Cumulative travel time = 104.5347 sec (0.03 hrs)

END OF MOD235: LAYER/BOUNDARY/TERMINAL LAYER APPROACH

 ** End of NEAR-FIELD REGION (NFR) **

 BEGIN MOD242: BUOYANT TERMINAL LAYER SPREADING

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

Plume Stage 1 (not bank attached):

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
35.99	1.24	3.75	34.0	0.294E+01	1.71	16.75	4.61	2.90	.10453E+03
84.19	1.24	3.75	42.8	0.234E+01	1.15	31.48	4.33	3.18	.34554E+03
132.39	1.24	3.75	52.8	0.189E+01	1.03	43.10	4.27	3.24	.58654E+03
180.59	1.24	3.75	65.1	0.154E+01	1.02	54.02	4.26	3.25	.82754E+03
228.79	1.24	3.75	79.4	0.126E+01	1.03	64.88	4.27	3.24	.10685E+04
276.99	1.24	3.75	95.3	0.105E+01	1.06	75.89	4.28	3.22	.13095E+04
325.19	1.24	3.75	112.5	0.889E+00	1.09	87.13	4.30	3.21	.15505E+04
373.39	1.24	3.75	131.0	0.764E+00	1.12	98.62	4.31	3.19	.17915E+04
421.59	1.24	3.75	150.6	0.664E+00	1.15	110.37	4.33	3.18	.20326E+04
469.80	1.24	3.75	171.3	0.584E+00	1.18	122.37	4.34	3.16	.22736E+04

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 81.23
Port/nozzle Froude number FRD0 = 10.27
Velocity ratio R = 7.69

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MS1 |

This flow configuration applies to a layer corresponding to the linearly stratified density layer at the discharge site.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:
750 m from the right bank/shore.
Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 2.2328 deg.C
Dilution at edge of NFR s = 44.8
NFR Location: x = 45.91 m
 y = 1.24 m
 z = 4.18 m

NFR plume dimensions: half-width (bh) = 17.00 m
 thickness (bv) = 2.22 m

Cumulative travel time: 141.5130 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.
Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Stratification assessment:

The specified ambient density stratification is dynamically important.
The discharge near field flow is trapped within the linearly stratified ambient density layer.

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****

No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****

No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles

(or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about +-50% (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

C0 = 0.1000E+03 CUNITS= deg.C
 NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:

750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

BEGIN MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00

END OF MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

BEGIN CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

Jet-like motion in linear stratification with strong crossflow.

Zone of flow establishment: THETA= 21.97 SIGMA= 86.67
 LE = 0.89 XE = 0.02 YE = 0.82 ZE = 2.33

Profile definitions:

BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory

BH = before merging: Gaussian 1/e (37%) half-width in horizontal plane
normal to trajectory

after merging: top-hat half-width in horizontal plane
parallel to diffuser line

S = hydrodynamic centerline dilution

C = centerline concentration (includes reaction effects, if any)

Uc = Local centerline excess velocity (above ambient)

TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
Individual jet/plumes before merging:								
0.02	0.82	2.33	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00
0.02	0.82	2.33	1.0	0.100E+03	0.15	0.15	1.538	.20072E-02
2.01	1.21	2.56	2.5	0.408E+02	0.36	0.36	0.651	.18598E+01
4.13	1.24	2.72	4.0	0.248E+02	0.52	0.52	0.415	.48531E+01
6.24	1.24	2.87	5.7	0.176E+02	0.66	0.66	0.306	.86929E+01
8.35	1.24	3.01	7.4	0.136E+02	0.78	0.78	0.244	.13183E+02
10.47	1.24	3.15	9.1	0.110E+02	0.89	0.89	0.204	.18208E+02
12.58	1.24	3.28	10.8	0.928E+01	0.99	0.99	0.176	.23666E+02
14.69	1.24	3.40	12.5	0.800E+01	1.09	1.09	0.155	.29473E+02
16.81	1.24	3.51	14.2	0.704E+01	1.17	1.17	0.139	.35600E+02
18.93	1.24	3.62	15.9	0.629E+01	1.25	1.25	0.126	.41978E+02
21.04	1.24	3.71	17.6	0.570E+01	1.33	1.33	0.115	.48602E+02
23.16	1.24	3.80	19.2	0.521E+01	1.40	1.40	0.106	.55430E+02
25.28	1.24	3.88	20.8	0.482E+01	1.46	1.46	0.099	.62426E+02
27.39	1.24	3.95	22.3	0.448E+01	1.53	1.53	0.093	.69598E+02
29.51	1.24	4.01	23.8	0.421E+01	1.58	1.58	0.087	.76916E+02
31.63	1.24	4.06	25.2	0.397E+01	1.64	1.64	0.082	.84348E+02
33.75	1.24	4.10	26.6	0.377E+01	1.69	1.69	0.078	.91911E+02
35.87	1.24	4.13	27.8	0.359E+01	1.73	1.73	0.075	.99578E+02
37.98	1.24	4.16	29.0	0.344E+01	1.77	1.77	0.072	.10732E+03
40.10	1.24	4.17	30.2	0.332E+01	1.81	1.81	0.069	.11516E+03

Maximum jet height has been reached.

42.22 1.24 4.18 31.2 0.321E+01 1.85 1.85 0.067 .12306E+03

Terminal level in stratified ambient has been reached.

Cumulative travel time = 123.0553 sec (0.03 hrs)

Merging of individual jet/plumes not found in this module, but interaction

will occur in following module. Overall jet/plume interaction dimensions:

42.22 1.24 4.18 31.2 0.321E+01 1.85 15.15 0.067 .12306E+03

END OF CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

 BEGIN MOD235: LAYER/BOUNDARY/TERMINAL LAYER APPROACH

Control volume inflow:

X	Y	Z	S	C	BV	BH	TT
42.22	1.24	4.18	31.2	0.321E+01	1.85	15.15	.12306E+03

Profile definitions:

BV = top-hat thickness, measured vertically

BH = top-hat half-width, measured horizontally in y-direction

ZU = upper plume boundary (Z-coordinate)

ZL = lower plume boundary (Z-coordinate)

S = hydrodynamic average (bulk) dilution

C = average (bulk) concentration (includes reaction effects, if any)

TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
40.37	1.24	4.18	31.2	0.321E+01	0.00	0.00	4.18	4.18	.12306E+03
41.48	1.24	4.18	31.2	0.321E+01	1.66	7.60	5.00	3.35	.12306E+03
42.59	1.24	4.18	31.7	0.315E+01	1.94	16.97	5.15	3.20	.12490E+03
43.70	1.24	4.18	37.6	0.266E+01	2.11	16.98	5.23	3.12	.13044E+03
44.80	1.24	4.18	42.9	0.233E+01	2.19	16.99	5.27	3.08	.13598E+03
45.91	1.24	4.18	44.8	0.223E+01	2.22	17.00	5.29	3.07	.14151E+03

Cumulative travel time = 141.5130 sec (0.04 hrs)

END OF MOD235: LAYER/BOUNDARY/TERMINAL LAYER APPROACH

 ** End of NEAR-FIELD REGION (NFR) **

 BEGIN MOD242: BUOYANT TERMINAL LAYER SPREADING

Profile definitions:

BV = top-hat thickness, measured vertically

BH = top-hat half-width, measured horizontally in y-direction

ZU = upper plume boundary (Z-coordinate)

ZL = lower plume boundary (Z-coordinate)

S = hydrodynamic average (bulk) dilution

C = average (bulk) concentration (includes reaction effects, if any)

TT = Cumulative travel time

Plume Stage 1 (not bank attached):

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
45.91	1.24	4.18	44.8	0.223E+01	2.22	17.00	5.29	3.07	.14151E+03
93.62	1.24	4.18	55.4	0.181E+01	1.45	32.15	4.90	3.45	.38004E+03
141.32	1.24	4.18	66.3	0.151E+01	1.27	43.83	4.81	3.54	.61856E+03
189.02	1.24	4.18	79.5	0.126E+01	1.23	54.55	4.79	3.56	.85708E+03
236.73	1.24	4.18	95.0	0.105E+01	1.23	65.04	4.79	3.56	.10956E+04
284.43	1.24	4.18	112.3	0.891E+00	1.25	75.58	4.80	3.55	.13341E+04
332.14	1.24	4.18	131.1	0.763E+00	1.28	86.27	4.82	3.54	.15726E+04
379.84	1.24	4.18	151.2	0.661E+00	1.31	97.17	4.83	3.52	.18112E+04
427.55	1.24	4.18	172.7	0.579E+00	1.34	108.27	4.85	3.50	.20497E+04
475.25	1.24	4.18	195.3	0.512E+00	1.38	119.60	4.86	3.49	.22882E+04

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 70.56
Port/nozzle Froude number FRD0 = 8.92
Velocity ratio R = 30.75

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MU6 |

This flow configuration applies to a layer corresponding to the full water depth at the discharge site.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:

750 m from the right bank/shore.

Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 1.7331 deg.C

Dilution at edge of NFR s = 57.7

NFR Location: x = 57.5 m

(centerline coordinates) y = 9.01 m

z = 11.5 m

NFR plume dimensions: half-width (bh) = 16.91 m

thickness (bv) = 11.5 m

Cumulative travel time: 1150 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.

Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Near-field instability behavior:

The diffuser flow will experience instabilities with full vertical mixing in the near-field.

There may be benthic impact of high pollutant concentrations.

FAR-FIELD MIXING SUMMARY:

Plume becomes vertically fully mixed WITHIN NEAR-FIELD at 0 m downstream, but RE-STRATIFIES LATER and is not mixed in the far-field.

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****

No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****

No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent

the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles (or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about $\pm 50\%$ (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
 750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

 BEGIN MOD202: DISCHARGE MODULE (STAGED DIFFUSER)

Due to complex near-field motions: EQUIVALENT SLOT DIFFUSER (2-D) GEOMETRY

Profile definitions:

BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory
 BH = Gaussian 1/e (37%) half-width in horizontal plane normal to trajectory
 S = hydrodynamic centerline dilution
 C = centerline concentration (includes reaction effects, if any)
 Uc = Local centerline excess velocity (above ambient)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.00	15.00	1.538	.00000E+00

END OF MOD202: DISCHARGE MODULE (STAGED DIFFUSER)

 BEGIN MOD275: STAGED PERPENDICULAR DIFFUSER IN STRONG CURRENT

Because of the strong ambient current the diffuser plume of this crossflowing discharge gets RAPIDLY DEFLECTED.

A near-field zone is formed that is VERTICALLY FULLY MIXED over the entire layer depth. Full mixing is achieved at a downstream distance of about five (5) layer depths.

Profile definitions:

BV = layer depth (vertically mixed)
 BH = top-hat half-width, measured horizontally in Y-direction
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	TT
0.00	0.00	2.00	1.0	0.100E+03	0.00	15.00	.00000E+00
2.88	0.45	2.19	13.7	0.731E+01	0.58	15.10	.57500E+02
5.75	0.90	2.38	18.9	0.528E+01	1.15	15.19	.11500E+03
8.62	1.35	2.56	23.0	0.436E+01	1.73	15.29	.17250E+03
11.50	1.80	2.75	26.4	0.379E+01	2.30	15.38	.23000E+03
14.38	2.25	2.94	29.4	0.341E+01	2.88	15.48	.28750E+03
17.25	2.70	3.12	32.1	0.312E+01	3.45	15.57	.34500E+03
20.12	3.15	3.31	34.5	0.289E+01	4.03	15.67	.40250E+03
23.00	3.60	3.50	36.9	0.271E+01	4.60	15.76	.46000E+03
25.88	4.06	3.69	39.0	0.256E+01	5.18	15.86	.51750E+03
28.75	4.51	3.88	41.1	0.243E+01	5.75	15.95	.57500E+03
31.62	4.96	4.06	43.1	0.232E+01	6.33	16.05	.63250E+03
34.50	5.41	4.25	44.9	0.223E+01	6.90	16.15	.69000E+03
37.38	5.86	4.44	46.7	0.214E+01	7.48	16.24	.74750E+03
40.25	6.31	4.62	48.4	0.206E+01	8.05	16.34	.80500E+03
43.12	6.76	4.81	50.1	0.200E+01	8.63	16.43	.86250E+03

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 94.75
Port/nozzle Froude number FRD0 = 11.97
Velocity ratio R = 30.75

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MS4 |

This flow configuration applies to a layer corresponding to the linearly stratified density layer at the discharge site.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:

750 m from the right bank/shore.

Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 6.6941 deg.C

Dilution at edge of NFR s = 14.9

NFR Location: x = 39.57 m

(centerline coordinates) y = 4.09 m

z = 4.13 m

NFR plume dimensions: half-width (bh) = 57.45 m

thickness (bv) = 0.88 m

Cumulative travel time: 604.5605 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.

Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Stratification assessment:

The specified ambient density stratification is dynamically important.

The discharge near field flow is trapped within the linearly stratified ambient density layer.

UPSTREAM INTRUSION SUMMARY:

Plume exhibits upstream intrusion due to low ambient velocity or strong discharge buoyancy.

Intrusion length = 27.93 m

Intrusion stagnation point = -17.08 m

Intrusion thickness = 1.38 m

Intrusion half width at impingement = 57.45 m

Intrusion half thickness at impingement = 0.88 m

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****

No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****

No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles (or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about +-50% (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

C0 = 0.1000E+03 CUNITS= deg.C
 NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
 750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

 BEGIN MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00

END OF MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

 BEGIN CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

Jet-like motion in linear stratification with weak crossflow.

Zone of flow establishment: THETA= 22.00 SIGMA= 89.17
 LE = 1.37 XE = 0.01 YE = 1.27 ZE = 2.51

Profile definitions:

BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory

BH = before merging: Gaussian 1/e (37%) half-width in horizontal plane
 normal to trajectory

after merging: top-hat half-width in horizontal plane
 parallel to diffuser line

S = hydrodynamic centerline dilution

C = centerline concentration (includes reaction effects, if any)

Uc = Local centerline excess velocity (above ambient)

TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
Individual jet/plumes before merging:								
0.01	1.27	2.51	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00
0.01	1.27	2.51	1.0	0.100E+03	0.15	0.15	1.538	.33790E-02
0.10	1.82	2.74	1.2	0.813E+02	0.22	0.22	1.473	.34724E+00
0.38	2.30	2.96	1.7	0.600E+02	0.30	0.30	1.085	.82311E+00
0.80	2.69	3.16	2.1	0.467E+02	0.37	0.37	0.846	.14389E+01
1.31	2.99	3.33	2.6	0.379E+02	0.45	0.45	0.690	.22051E+01
1.86	3.20	3.48	3.1	0.319E+02	0.52	0.52	0.586	.30988E+01
2.42	3.37	3.61	3.6	0.276E+02	0.59	0.59	0.511	.41223E+01
3.01	3.50	3.73	4.1	0.242E+02	0.66	0.66	0.453	.52848E+01
3.60	3.60	3.84	4.6	0.217E+02	0.73	0.73	0.408	.65544E+01
4.19	3.68	3.95	5.1	0.196E+02	0.79	0.79	0.371	.79406E+01
4.79	3.75	4.04	5.6	0.179E+02	0.86	0.86	0.341	.94407E+01
5.39	3.80	4.12	6.1	0.165E+02	0.92	0.92	0.314	.11072E+02
5.99	3.85	4.18	6.5	0.154E+02	0.98	0.98	0.292	.12793E+02
6.60	3.89	4.23	7.0	0.144E+02	1.03	1.03	0.274	.14618E+02
7.21	3.93	4.26	7.4	0.135E+02	1.09	1.09	0.257	.16567E+02
7.82	3.96	4.27	7.8	0.128E+02	1.14	1.14	0.243	.18589E+02
Maximum jet height has been reached.								
8.42	3.99	4.27	8.3	0.121E+02	1.19	1.19	0.231	.20702E+02
9.03	4.02	4.25	8.7	0.115E+02	1.24	1.24	0.220	.22930E+02
9.64	4.05	4.22	9.2	0.109E+02	1.29	1.29	0.210	.25219E+02

10.24	4.07	4.18	9.6	0.104E+02	1.35	1.35	0.201	.27596E+02
10.85	4.09	4.13	10.1	0.991E+01	1.40	1.40	0.192	.30059E+02

Terminal level in stratified ambient has been reached.

Cumulative travel time = 30.0588 sec (0.01 hrs)

Merging of individual jet/plumes not found in this module, but interaction will occur in following module. Overall jet/plume interaction dimensions:

10.85	4.09	4.13	10.1	0.991E+01	1.40	15.15	0.192	.30059E+02
-------	------	------	------	-----------	------	-------	-------	------------

END OF CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

BEGIN MOD237: TERMINAL LAYER INJECTION/UPSTREAM SPREADING

UPSTREAM INTRUSION PROPERTIES:

Maximum elevation of jet/plume rise	=	6.58 m
Layer thickness in impingement region	=	1.38 m
Upstream intrusion length	=	27.93 m
X-position of upstream stagnation point	=	-17.08 m
Thickness in intrusion region	=	1.38 m
Half-width at downstream end	=	57.45 m
Thickness at downstream end	=	0.88 m

Control volume inflow:

X	Y	Z	S	C	BV	BH	TT
10.85	4.09	4.13	10.1	0.991E+01	1.40	15.15	.30059E+02

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
-17.08	4.09	4.13	9999.9	0.000E+00	0.00	0.00	4.13	4.13	.58861E+03
-15.95	4.09	4.13	40.0	0.250E+01	0.35	8.81	4.31	3.96	.56595E+03
-10.40	4.09	4.13	16.7	0.601E+01	0.84	21.40	4.55	3.71	.45491E+03
-4.84	4.09	4.13	12.7	0.790E+01	1.10	28.96	4.69	3.58	.34387E+03
0.71	4.09	4.13	11.0	0.909E+01	1.27	34.92	4.77	3.50	.23283E+03
6.26	4.09	4.13	10.3	0.974E+01	1.36	40.00	4.81	3.45	.12179E+03
11.81	4.09	4.13	10.1	0.989E+01	1.38	53.53	4.83	3.44	.49364E+02
17.36	4.09	4.13	11.0	0.910E+01	1.29	54.43	4.78	3.49	.16040E+03
22.92	4.09	4.13	12.5	0.797E+01	1.13	55.26	4.70	3.57	.27144E+03
28.47	4.09	4.13	13.9	0.721E+01	0.99	56.03	4.63	3.64	.38248E+03
34.02	4.09	4.13	14.6	0.686E+01	0.91	56.76	4.59	3.68	.49352E+03
39.57	4.09	4.13	14.9	0.669E+01	0.88	57.45	4.57	3.70	.60456E+03

Cumulative travel time = 604.5605 sec (0.17 hrs)

END OF MOD237: TERMINAL LAYER INJECTION/UPSTREAM SPREADING

** End of NEAR-FIELD REGION (NFR) **

BEGIN MOD242: BUOYANT TERMINAL LAYER SPREADING

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution

(These refer to the actual discharge/environment length scales.)

 NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 85.06
 Port/nozzle Froude number FRD0 = 10.75
 Velocity ratio R = 30.75

 MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
 Water quality standard specified = no
 Regulatory mixing zone = no
 Region of interest = 1000 m downstream

 HYDRODYNAMIC CLASSIFICATION:

 | FLOW CLASS = MS4 |

This flow configuration applies to a layer corresponding to the linearly stratified density layer at the discharge site.
 Applicable layer depth = water depth = 11.5 m

 MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

 X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:
 750 m from the right bank/shore.
 Number of display steps NSTEP = 20 per module.

 NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 4.6424 deg.C
 Dilution at edge of NFR s = 21.5
 NFR Location: x = 46.31 m
 y = 3.95 m
 z = 5.09 m
 NFR plume dimensions: half-width (bh) = 62.18 m
 thickness (bv) = 1.17 m

Cumulative travel time: 671.3911 sec.

 Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.
 Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

 Stratification assessment:

The specified ambient density stratification is dynamically important.
 The discharge near field flow is trapped within the linearly stratified ambient density layer.

 UPSTREAM INTRUSION SUMMARY:

Plume exhibits upstream intrusion due to low ambient velocity or strong discharge buoyancy.
 Intrusion length = 31.41 m
 Intrusion stagnation point = -16.19 m
 Intrusion thickness = 1.94 m
 Intrusion half width at impingement = 62.18 m
 Intrusion half thickness at impingement = 1.17 m

 PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.

***** TOXIC DILUTION ZONE SUMMARY *****

No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****

No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****

CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent the actual three-dimensional diffuser geometry. Thus, it approximates the details of the merging process of the individual jets from each port/nozzle.

In the present design, the spacing between adjacent ports/nozzles (or riser assemblies) is of the order of, or less than, the local water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a final CORMIX1 (single port discharge) analysis, with discharge data for an individual diffuser jet/plume, in order to compare to the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the CORMIX predictions on dilutions and concentrations (with associated plume geometries) are reliable for the majority of cases and are accurate to within about +-50% (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges the design configuration as highly complex and uncertain for prediction.

C0 = 0.1000E+03 CUNITS= deg.C
 NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
 750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

BEGIN MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00

END OF MOD101: DISCHARGE MODULE (SINGLE PORT AT DIFFUSER CENTER)

BEGIN CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

Jet-like motion in linear stratification with weak crossflow.

Zone of flow establishment: THETA= 22.00 SIGMA= 89.17
 LE = 1.37 XE = 0.01 YE = 1.27 ZE = 2.51

Profile definitions:

- BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory
- BH = before merging: Gaussian 1/e (37%) half-width in horizontal plane normal to trajectory
- after merging: top-hat half-width in horizontal plane parallel to diffuser line
- S = hydrodynamic centerline dilution
- C = centerline concentration (includes reaction effects, if any)
- Uc = Local centerline excess velocity (above ambient)
- TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
Individual jet/plumes before merging:								
0.01	1.27	2.51	1.0	0.100E+03	0.15	0.15	1.538	.00000E+00
0.01	1.27	2.51	1.0	0.100E+03	0.15	0.15	1.538	.33789E-02
0.19	2.01	2.83	1.4	0.720E+02	0.25	0.25	1.308	.50834E+00
0.68	2.60	3.13	2.0	0.493E+02	0.35	0.35	0.903	.12654E+01
1.36	3.01	3.39	2.7	0.368E+02	0.46	0.46	0.687	.22813E+01
2.11	3.28	3.61	3.4	0.292E+02	0.56	0.56	0.558	.35427E+01
2.90	3.46	3.83	4.1	0.241E+02	0.65	0.65	0.474	.50321E+01
3.69	3.59	4.04	4.9	0.205E+02	0.75	0.75	0.413	.67353E+01
4.49	3.67	4.24	5.6	0.177E+02	0.84	0.84	0.367	.86422E+01
5.30	3.74	4.44	6.4	0.156E+02	0.93	0.93	0.330	.10746E+02
6.11	3.78	4.62	7.2	0.139E+02	1.02	1.02	0.299	.13043E+02
6.93	3.82	4.78	8.0	0.126E+02	1.11	1.11	0.274	.15529E+02
7.75	3.84	4.92	8.7	0.115E+02	1.19	1.19	0.252	.18202E+02
8.57	3.86	5.04	9.4	0.106E+02	1.27	1.27	0.233	.21059E+02
9.40	3.88	5.14	10.1	0.987E+01	1.35	1.35	0.217	.24094E+02
10.23	3.89	5.21	10.8	0.926E+01	1.42	1.42	0.204	.27300E+02
11.06	3.90	5.25	11.4	0.875E+01	1.49	1.49	0.192	.30664E+02
Maximum jet height has been reached.								
11.90	3.91	5.26	12.0	0.830E+01	1.55	1.55	0.183	.34175E+02
12.73	3.92	5.24	12.7	0.790E+01	1.61	1.61	0.174	.37820E+02
13.56	3.93	5.20	13.3	0.750E+01	1.67	1.67	0.167	.41599E+02

14.39	3.94	5.14	14.0	0.713E+01	1.74	1.74	0.159	.45516E+02
15.22	3.95	5.09	14.7	0.680E+01	1.80	1.80	0.152	.49571E+02

Terminal level in stratified ambient has been reached.

Cumulative travel time = 49.5707 sec (0.01 hrs)

Merging of individual jet/plumes not found in this module, but interaction will occur in following module. Overall jet/plume interaction dimensions:

15.22	3.95	5.09	14.7	0.680E+01	1.80	15.15	0.152	.49571E+02
-------	------	------	------	-----------	------	-------	-------	------------

END OF CORJET (MOD110): JET/PLUME NEAR-FIELD MIXING REGION

BEGIN MOD237: TERMINAL LAYER INJECTION/UPSTREAM SPREADING

UPSTREAM INTRUSION PROPERTIES:

Maximum elevation of jet/plume rise	=	7.98 m
Layer thickness in impingement region	=	1.94 m
Upstream intrusion length	=	31.41 m
X-position of upstream stagnation point	=	-16.19 m
Thickness in intrusion region	=	1.94 m
Half-width at downstream end	=	62.18 m
Thickness at downstream end	=	1.17 m

Control volume inflow:

X	Y	Z	S	C	BV	BH	TT
15.22	3.95	5.09	14.7	0.680E+01	1.80	15.15	.49571E+02

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	ZU	ZL	TT
-16.19	3.95	5.09	9999.9	0.000E+00	0.00	0.00	5.09	5.09	.67778E+03
-14.94	3.95	5.09	58.9	0.170E+01	0.48	8.79	5.33	4.84	.65278E+03
-8.81	3.95	5.09	24.5	0.408E+01	1.16	21.36	5.67	4.50	.53028E+03
-2.69	3.95	5.09	18.6	0.537E+01	1.53	28.90	5.85	4.32	.40778E+03
3.44	3.95	5.09	16.1	0.620E+01	1.77	34.84	5.97	4.20	.28527E+03
9.56	3.95	5.09	15.0	0.666E+01	1.90	39.91	6.03	4.14	.16277E+03
15.69	3.95	5.09	14.7	0.680E+01	1.94	57.01	6.05	4.12	.58875E+02
21.81	3.95	5.09	15.8	0.632E+01	1.81	58.20	5.99	4.18	.18138E+03
27.94	3.95	5.09	18.0	0.554E+01	1.56	59.29	5.87	4.30	.30388E+03
34.06	3.95	5.09	20.0	0.501E+01	1.34	60.31	5.76	4.41	.42638E+03
40.19	3.95	5.09	21.0	0.476E+01	1.23	61.27	5.70	4.47	.54889E+03
46.31	3.95	5.09	21.5	0.464E+01	1.17	62.18	5.67	4.50	.67139E+03

Cumulative travel time = 671.3912 sec (0.19 hrs)

END OF MOD237: TERMINAL LAYER INJECTION/UPSTREAM SPREADING

** End of NEAR-FIELD REGION (NFR) **

BEGIN MOD242: BUOYANT TERMINAL LAYER SPREADING

Profile definitions:

BV = top-hat thickness, measured vertically
 BH = top-hat half-width, measured horizontally in y-direction
 ZU = upper plume boundary (Z-coordinate)
 ZL = lower plume boundary (Z-coordinate)
 S = hydrodynamic average (bulk) dilution

(These refer to the actual discharge/environment length scales.)

NON-DIMENSIONAL PARAMETERS:

Slot Froude number FR0 = 86.93
Port/nozzle Froude number FRD0 = 10.99
Velocity ratio R = 30.75

MIXING ZONE / TOXIC DILUTION ZONE / AREA OF INTEREST PARAMETERS:

Toxic discharge = no
Water quality standard specified = no
Regulatory mixing zone = no
Region of interest = 1000 m downstream

HYDRODYNAMIC CLASSIFICATION:

| FLOW CLASS = MU6 |

This flow configuration applies to a layer corresponding to the full water depth at the discharge site. The ambient density stratification at the discharge site is relatively weak and unimportant so the discharge flow penetrates to the surface and/or breaks down the existing stratification through vigorous mixing.

Applicable layer depth = water depth = 11.5 m

MIXING ZONE EVALUATION (hydrodynamic and regulatory summary):

X-Y-Z Coordinate system:

Origin is located at the BOTTOM below the port/diffuser center:
750 m from the right bank/shore.
Number of display steps NSTEP = 20 per module.

NEAR-FIELD REGION (NFR) CONDITIONS :

Note: The NFR is the zone of strong initial mixing. It has no regulatory implication. However, this information may be useful for the discharge designer because the mixing in the NFR is usually sensitive to the discharge design conditions.

Pollutant concentration at NFR edge c = 1.7331 deg.C
Dilution at edge of NFR s = 57.7
NFR Location: x = 57.5 m
(centerline coordinates) y = 9.01 m
 z = 11.5 m

NFR plume dimensions: half-width (bh) = 16.91 m
 thickness (bv) = 11.5 m

Cumulative travel time: 1150 sec.

Buoyancy assessment:

The effluent density is less than the surrounding ambient water density at the discharge level.
Therefore, the effluent is POSITIVELY BUOYANT and will tend to rise towards the surface.

Stratification assessment:

The specified ambient density stratification is weak relative to the discharge conditions and is dynamically unimportant. The discharge will behave as if the ambient were unstratified.

Near-field instability behavior:

The diffuser flow will experience instabilities with full vertical mixing in the near-field.
There may be benthic impact of high pollutant concentrations.

FAR-FIELD MIXING SUMMARY:

Plume becomes vertically fully mixed WITHIN NEAR-FIELD at 0 m downstream, but RE-STRATIFIES LATER and is not mixed in the far-field.

PLUME BANK CONTACT SUMMARY:

Plume in unbounded section does not contact bank in this simulation.
***** TOXIC DILUTION ZONE SUMMARY *****
No TDZ was specified for this simulation.

***** REGULATORY MIXING ZONE SUMMARY *****
No RMZ and no ambient water quality standard have been specified.

***** FINAL DESIGN ADVICE AND COMMENTS *****
CORMIX2 uses the TWO-DIMENSIONAL SLOT DIFFUSER CONCEPT to represent
the actual three-dimensional diffuser geometry. Thus, it approximates
the details of the merging process of the individual jets from each
port/nozzle.

In the present design, the spacing between adjacent ports/nozzles
(or riser assemblies) is of the order of, or less than, the local
water depth so that the slot diffuser approximation holds well.

Nevertheless, if this is a final design, the user is advised to use a
final CORMIX1 (single port discharge) analysis, with discharge data
for an individual diffuser jet/plume, in order to compare to
the present near-field prediction.

REMINDER: The user must take note that HYDRODYNAMIC MODELING by any known
technique is NOT AN EXACT SCIENCE.

Extensive comparison with field and laboratory data has shown that the
CORMIX predictions on dilutions and concentrations (with associated
plume geometries) are reliable for the majority of cases and are accurate
to within about +-50% (standard deviation).

As a further safeguard, CORMIX will not give predictions whenever it judges
the design configuration as highly complex and uncertain for prediction.

C0 = 0.1000E+03 CUNITS= deg.C
 NTOX = 0
 NSTD = 0
 REGMZ = 0
 XINT = 1000.00 XMAX = 1000.00

X-Y-Z COORDINATE SYSTEM:

ORIGIN is located at the bottom and the diffuser mid-point:
 750.00 m from the RIGHT bank/shore.

X-axis points downstream, Y-axis points to left, Z-axis points upward.

NSTEP = 20 display intervals per module

 BEGIN MOD202: DISCHARGE MODULE (STAGED DIFFUSER)

Due to complex near-field motions: EQUIVALENT SLOT DIFFUSER (2-D) GEOMETRY

Profile definitions:

BV = Gaussian 1/e (37%) half-width, in vertical plane normal to trajectory
 BH = Gaussian 1/e (37%) half-width in horizontal plane normal to trajectory
 S = hydrodynamic centerline dilution
 C = centerline concentration (includes reaction effects, if any)
 Uc = Local centerline excess velocity (above ambient)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	Uc	TT
0.00	0.00	2.00	1.0	0.100E+03	0.00	15.00	1.538	.00000E+00

END OF MOD202: DISCHARGE MODULE (STAGED DIFFUSER)

BEGIN MOD275: STAGED PERPENDICULAR DIFFUSER IN STRONG CURRENT

Because of the strong ambient current the diffuser plume of this crossflowing discharge gets RAPIDLY DEFLECTED.

A near-field zone is formed that is VERTICALLY FULLY MIXED over the entire layer depth. Full mixing is achieved at a downstream distance of about five (5) layer depths.

Profile definitions:

BV = layer depth (vertically mixed)
 BH = top-hat half-width, measured horizontally in Y-direction
 S = hydrodynamic average (bulk) dilution
 C = average (bulk) concentration (includes reaction effects, if any)
 TT = Cumulative travel time

X	Y	Z	S	C	BV	BH	TT
0.00	0.00	2.00	1.0	0.100E+03	0.00	15.00	.00000E+00
2.88	0.45	2.19	13.7	0.731E+01	0.58	15.10	.57500E+02
5.75	0.90	2.38	18.9	0.528E+01	1.15	15.19	.11500E+03
8.62	1.35	2.56	23.0	0.436E+01	1.73	15.29	.17250E+03
11.50	1.80	2.75	26.4	0.379E+01	2.30	15.38	.23000E+03
14.38	2.25	2.94	29.4	0.341E+01	2.88	15.48	.28750E+03
17.25	2.70	3.12	32.1	0.312E+01	3.45	15.57	.34500E+03
20.12	3.15	3.31	34.5	0.289E+01	4.03	15.67	.40250E+03
23.00	3.60	3.50	36.9	0.271E+01	4.60	15.76	.46000E+03
25.88	4.06	3.69	39.0	0.256E+01	5.18	15.86	.51750E+03
28.75	4.51	3.88	41.1	0.243E+01	5.75	15.95	.57500E+03
31.62	4.96	4.06	43.1	0.232E+01	6.33	16.05	.63250E+03
34.50	5.41	4.25	44.9	0.223E+01	6.90	16.15	.69000E+03
37.38	5.86	4.44	46.7	0.214E+01	7.48	16.24	.74750E+03
40.25	6.31	4.62	48.4	0.206E+01	8.05	16.34	.80500E+03

ATTACHMENT C

Annotated ADCIRC Run Control File

Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

Page 1

```

PenobscotBay          ! 32 CHARACTER ALPHANUMERIC RUN DESCRIPTION  Comment line
Tides 6/20/1999 - 7/31/1999 ! 24 CHARACTER ALPHANUMERIC RUN IDENTIFICATION  Comment line
1                    ! NFOVER - NONFATAL ERROR OVERRIDE OPTION  Allow run to continue with non-fatal errors
0                    ! NABOUT - ABBREVIATED OUTPUT OPTION PARAMETER  Don't output debugging information
-1000                ! NSCREEN - OUTPUT TO UNIT 6 PARAMETER  Write timestepping output to adcirc.log every 1000 timesteps
0                    ! IHOT - HOT START OPTION PARAMETER  This is a coldstart run (i.e. run starts from still water)
2                    ! ICS - COORDINATE SYSTEM OPTION PARAMETER  Model grid is in geographic coordinates
5111111             ! IM  Indicates a 2D depth integrated barotropic run, Implicit GWCE solution, with symmetric lateral stress formula for Smagorinsky turbulence model
1                    ! NOLIBF - NONLINEAR BOTTOM FRICTION OPTION  use non-linear bottom friction (Manning's formula is used)
2                    ! NOLIFA - OPTION TO INCLUDE FINITE AMPLITUDE TERMS  Include wetting and drying
1                    ! NOLICA - OPTION TO INCLUDE CONVECTIVE ACCELERATION TERMS  Include "advective" terms
1                    ! NOLICAT - OPTION TO CONSIDER TIME DERIVATIVE OF CONV ACC TERMS  Include time derivative of advective terms
4                    ! NWP - Number of nodal attributes.
mannings_n_at_sea_floor -use spatially variable Manning's n bottom friction (described in the fort.13 file)
advection_state      - used to turn off NOLICA and NOLICAT near boundary to enhance model stability
primitive_weighting_in_continuity_equation Use spatially variable Tau0 parameter
elemental_slope_limiter Used to report but not attempt to correct potential model instabilities.
1                    ! NCOR - VARIABLE CORIOLIS IN SPACE OPTION PARAMETER  applies coriolis forcing
1                    ! NTIP - TIDAL POTENTIAL OPTION PARAMETER  apply tidal potential forcing
0                    ! NWS - WIND STRESS AND BAROMETRIC PRESSURE OPTION PARAMETER  no wind stress
1                    ! NRAMP - RAMP FUNCTION OPTION  use ramping function at beginning of simulation to ramp up boundary conditions
9.80665             ! G - ACCELERATION DUE TO GRAVITY - DETERMINES UNITS  this is g
-3                 ! TAU0 - WEIGHTING FACTOR IN GWCE  Use time and spatially dependent values based on supplied nodal attributes in fort.13
1.00000            ! DT - TIME STEP (IN SECONDS)  1 second model timestep
0.00000            ! STATIM - STARTING SIMULATION TIME IN DAYS  start simulation time at zero
0.00000            ! REFTIME - REFERENCE TIME FOR NODAL FACTORS AND EQUILIBRIUM ARGS  tidal reference time starts at zero
42.00000           ! RNDAY - TOTAL LENGTH OF SIMULATION (IN DAYS)  simulates 42 days of tides
14.00000           ! DRAMP - DURATION OF RAMP FUNCTION (IN DAYS)  ramp up boundary forcing over the first 14 days of the simulation
0.350000 0.300000 0.350000 ! TIME WEIGHTING FACTORS FOR THE GWCE EQUATION  for implicit solver
0.050000 12 12 0.050000 ! H0, NODEDRYMIN, NODEWETMIN, VELMIN  dry when less than 5 cm of water, wet when velocity toward node is 5 cm/s
-68.674774 43.956598 ! SLAM0, SFEAO - LONGITUDE AND LATITUDE FOR CPP PROJECTION  origin of projection for grid
0.002500           ! FFACTOR - 2DDI BOTTOM FRICTION COEFFICIENT  minimum quadratic bottom friction coefficient after determined from
-0.25             ! ESLM - Smagorinsky coefficient for horizontal turbulence closure  depth and Manning's n
0.000100           ! CORI - CONSTANT CORIOLIS COEFFICIENT
8      ! NTIF - TOTAL NUMBER OF TIDAL POTENTIAL CONSTITUENTS
M2
0.242334 0.000140518902509 0.693 1.02634 209.32
S2
0.112841 0.000145444104333 0.693 1.00000 0.00
N2
0.046398 0.000137879699487 0.693 1.02634 108.56
K2
0.030704 0.000145842317201 0.693 0.82235 162.19
K1
0.141565 0.000072921158358 0.736 0.92649 170.69
O1
0.100514 0.000067597744151 0.695 0.88023 42.28
P1
0.046843 0.000072522945975 0.706 1.00000 182.23
Q1
0.019256 0.000064958541129 0.695 0.88023 301.52

```

Tidal potential forcing parameters

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

8 !NFBR number of forcing frequencies on open boundaries

M2	!BOUNTAG		
0.0001405189027		1.02634	209.32
S2	!BOUNTAG		
0.0001454441043		1.00000	0.00
N2	!BOUNTAG		
0.0001378797074		1.02634	108.56
K2	!BOUNTAG		
0.0001458423017		0.82235	162.19
K1	!BOUNTAG		
7.29211508e-005		0.92649	170.69
O1	!BOUNTAG		
6.75977518e-005		0.88023	42.28
P1	!BOUNTAG		
7.25229535e-005		1.00000	182.23
Q1	!BOUNTAG		
6.49585572e-005		0.88023	301.52

Open Boundary Tidal harmonic forcing parameters
(determines timing of tides, depends on date of model run)

M2	!BOUNTAG		
0.039459791360291		100.730269079789	
0.039459791360291		100.730269079789	
0.039459791360291		100.730269079789	
0.098310568946937		100.488014297742	
0.157397900805293		100.248833387736	
0.216719153176965		100.01283395402	
0.276271830330723		99.780122735384	
0.336053564131591		99.5508054845139	
0.396062103358654		99.3249868913616	
0.456295303834117		99.1027704794273	
0.516751117801834		98.8842585325913	
0.577427587113876		98.6695519997414	
0.638322832637326		98.4587504060066	
0.69943504472154		98.2519517758479	
0.760762477658633		98.0492525633917	
0.822303440212044		97.8507475504521	
0.884056288709408		97.656529796246	
0.946019420315806		97.4666905499837	
1.0081912668298		97.2813191756336	
1.07485126157609		97.2113010760541	
1.14185341037351		97.18610483317	
1.2073428671345		97.1621678529297	
1.27137594111709		97.1392965647097	
1.33401090340396		97.1173482124421	
1.39530793375816		97.0962174011221	
1.44458491043903		97.0551816495127	
1.44325810382949		96.9185088214394	
1.44198853126279		96.7825132057632	
1.44077573230568		96.6471998213415	
1.43961923040219		96.512572584009	
1.43851853361721		96.3786343211824	
1.43747313531413		96.245386793811	
1.43648251490279		96.1128307047342	

Tidal amplitude and phase at boundary nodes for M2 tide constituent

fort_tides_June-July1999.15

Page 3

1.43554613830124 95.9809657259485
1.43466345892835 95.8497905176886
1.43383391799486 95.7193027470981
1.43305694545863 95.5894991175706
1.43233196047482 95.4603753895186
1.43165837215843 95.3319264101575
1.43103558019604 95.2041461410119
1.43046297538188 95.0770276855116
1.42993994031792 94.9505633207242
1.42946585006691 94.8247445274948
1.42904007263416 94.6995620257712
1.42866196960137 94.5750058038178
1.42833089685456 94.4510651558408
1.42804299866312 94.3273795308777
1.4276536685968 94.1882179260897
1.42731059002519 94.0496510637631
1.42701335751088 93.9116448750075
1.42676156897842 93.7741647699608
1.426554826067 93.6371757059818
1.42639273423918 93.5006422508008
1.4262749032989 93.364528656122
1.42620094737023 93.2287989165551
1.42617048528918 93.0934168420814
1.42618314078369 92.9583461245193
1.42623854263787 92.8235504017397
1.4263363249081 92.6889933246742
1.4264761271276 92.5546386273783
1.42665759436486 92.420450188746
1.42688037752248 92.2863921007049
1.42714413337128 92.152428733504
1.42744852459988 92.0185247975527
1.42779322019249 91.8846454116176
1.4281778951419 91.750756163222
1.42860223088466 91.616823168931
1.42898314944175 91.4912640101138
1.42914344635902 91.3919632798988
1.42933598195523 91.2929562156955
1.4295601352153 91.1942499357747
1.42981528724164 91.0958515108564
1.43010082137624 90.9977679700867
1.43041612391907 90.9000063116838
1.43076058441712 90.8025735184276
1.43113359613808 90.7054765630183
1.43153455652182 90.6087224253217
1.43196286749212 90.5123180979078
1.43241793591573 90.4162706025479
1.43289917406268 90.3205869955296
1.43340599982265 90.2252743848012
1.43421975762801 90.1303393622637
1.4350553779001 90.0358840185619
1.43393739913638 89.9432102503977

M2 continued

fort_tides_June-July1999.15

1.41302259886652 89.8603975448752
1.38903346113561 89.772935829432
1.36191700244595 89.6799259370572
1.33162352641344 89.5803113346625
1.29810669263806 89.4728349059984
1.26563734400394 89.3738479862302
1.24536392652364 89.3225028103617
1.22713378758259 89.2733415286878
1.21098814200685 89.2267719005113
1.19696515605271 89.1832001416828
1.18509991947968 89.1430220668376
1.1754244198905 89.1066137009585
1.16796752007277 89.0743217249401
1.16275493719571 89.0464541819033
1.15980922444224 89.0232718938097
1.15914975449469 89.004981030263
1.16079270561547 88.9917272310307
1.16475104712097 88.9835916048211
1.17103452980423 88.9805888192015
1.17964967452871 88.9826673774294
1.19059976470313 88.9897120376087
1.20388483817029 89.0015482084061
1.21950168310134 89.0179480405344
1.23744383256854 89.038637856205
1.2577015651616 89.0633064959261
1.2802619014186 89.0916141679451
1.30510861063293 89.1232013675168
1.33222221226052 89.1576975149104
1.36157998534712 89.1947289893577
1.39315597849888 89.2339263316114
1.42692102230498 89.2749304528571
1.46284274477663 89.3173977707068
1.49399330055194 89.3551898558721
1.49668794194173 89.3697047132969
1.49940033263897 89.3859970189539
1.50212981399331 89.4040417875475
1.50487571080734 89.4238129416887
1.50763733134028 89.4452833417106
1.51041396743737 89.4684248232098
1.47871483110615 89.4592451828508
1.44398534041431 89.4489602527267
1.41150168185055 89.4430835603807
1.38121052600288 89.441855591214
1.35305557623465 89.445487985132
1.32697761817433 89.4541588784618
1.30291456895667 89.4680087821449
1.2808015315083 89.487137169006
1.26057084827017 89.5115999325256
1.2421521559815 89.5414078458949
1.22547244221433 89.5765261109465
1.21045610475491 89.616875041731

fort_tides_June-July1999.15

1.19702501053165 89.6623318836878
 1.18509855634659 89.7127337121889
 1.17459373370185 89.7678813110314
 1.16542519254629 89.8275438998494
 1.15750530825829 89.8914645293586
 1.15074425008065 89.9593659630656
 1.14505005409431 90.0309568508807
 1.14032869295723 90.1059379875519
 1.13648415503657 90.1840084872597
 1.13341852110059 90.2648717116542
 1.13103204154673 90.3482408244898
 1.12922322257594 90.4338438730311
 1.12788890866618 90.5214283365917
 1.12692436762178 90.6107651229907
 1.12622338161297 90.7016520044969
 1.12567833412255 90.7939165425892
 1.12518030547496 90.8874185497658
 1.09902216834422 90.8938033802224
 1.06899099300548 90.8938033802224
 1.03699871950209 90.8938033802224
 1.00316546730883 90.8938033802224
 0.967612576555963 90.8938033802224
 0.930462510318372 90.8938033802224
 0.891838752104961 90.8938033802224
 0.858725015309219 90.8938033802224
 0.832275777863576 90.8938033802224
 S2
 !BOUNTAG
 0.00596375350149546 133.654939033855
 0.00596375350149546 133.654939033855
 0.00596375350149546 133.654939033855
 0.0148891602558564 133.374671696679
 0.0238870888692339 133.099104684069
 0.0329567642788451 132.828313591156
 0.0420973774489516 132.562371815463
 0.0513080843810247 132.301350530033
 0.0605880051437033 132.045318708879
 0.0699362231006868 131.794343122926
 0.0793517840715812 131.548488371691
 0.0888336961459881 131.307816890505
 0.0983809289744974 131.072388965759
 0.107992413265167 130.842262763555
 0.117667040936523 130.617494366075
 0.127403664743416 130.398137771613
 0.137201098293563 130.184244951266
 0.147058116168874 129.975865863393
 0.156973454158046 129.773048480457
 0.167429627759335 129.701910887736
 0.177869689493755 129.680717346837
 0.188071938582149 129.659883314723
 0.198045225911764 129.639376027611
 0.207798710064494 129.619177397033

M2 Continued

S2 tidal amplitude and phase at boundary nodes

fort_tides_June-July1999.15

0.217341849014347 129.599280386207
0.224991333950633 129.55640451423
0.224667306142131 129.40535031865
0.224352986451708 129.254841129213
0.2240482694541 129.104876878346
0.223753046447163 128.95545607598
0.223467205623332 128.806575826786
0.223190632237901 128.658231856636
0.222923208771253 128.510418523333
0.222664815070161 128.363128851214
0.222415328550583 128.216354553633
0.222174624304106 128.070086059343
0.221942575302742 127.924312547741
0.221719052525795 127.779021977463
0.221503925135988 127.634201123891
0.221297060631537 127.489835615208
0.221098324986897 127.345909969363
0.220907582817853 127.202407635053
0.220724697537288 127.059311031388
0.220549531491941 126.916601594969
0.220381946112063 126.774259819107
0.220221802080034 126.632265302313
0.220069683411564 126.490556385469
0.219957912660608 126.347321801782
0.219852930521152 126.204425419517
0.219754713253316 126.061836695427
0.219663237611658 125.919524715256
0.219578480881216 125.777458256145
0.219500420876819 125.63560584502
0.21942903600397 125.493935825728
0.219364305237436 125.352416413677
0.219306208163348 125.211015762465
0.219254724988714 125.069702025376
0.219209836547488 124.928443414631
0.219171524314996 124.787208263346
0.219139770421756 124.645965090793
0.219114557642814 124.504682659747
0.219095869424252 124.363330039451
0.219083689870204 124.221876666962
0.219078003730547 124.080292404865
0.219078796439075 123.938547604121
0.219086054051365 123.796613162079
0.219099763288612 123.654460576948
0.219100371888936 123.51971019639
0.219046113059979 123.408493798584
0.218996733776155 123.297275992693
0.218952129045334 123.18605911769
0.218912194725963 123.074845598865
0.218876827559297 122.963637961982
0.218845925291357 122.852438849355
0.218819386735381 122.74125104354

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.2187971111852377 122.630077478578
0.218779001836948 122.518921264553
0.218764959172917 122.407785699707
0.218754887718071 122.296674293902
0.218748692779375 122.185590779318
0.218746281161643 122.07453913586
0.218787892312339 121.961696426222
0.218832679299292 121.848957938618
0.218581158128101 121.739216328406
0.215327259557688 121.652404827514
0.211605338338794 121.558275354305
0.2074073785468 121.455674839023
0.202725876290227 121.343232759613
0.197553853152443 121.219302647036
0.192526392137394 121.106205554532
0.18930893313044 121.056426061397
0.186396070612424 121.007404345493
0.183794004930953 120.959460443893
0.181508480373171 120.91292657142
0.179544780633959 120.868141163531
0.177907724638203 120.825442109299
0.176601662829127 120.785159381097
0.175630473773385 120.747607339136
0.174997561189404 120.713077035429
0.174705851317777 120.681828869612
0.174757790774395 120.654085957071
0.175155344382955 120.630028540269
0.17589999385154 120.609789726107
0.176992736258136 120.593452758366
0.178434083173155 120.581049935128
0.180224059779977 120.572563191677
0.182362204614043 120.567926257994
0.184847569136991 120.567028224492
0.187678718223056 120.569718266844
0.190853729990963 120.575811250408
0.19437019717427 120.58509389145
0.198225227635863 120.5973331180133
0.202415446035033 120.612272770774
0.206936995522291 120.62965909941
0.211785539753256 120.649227029473
0.216956265291516 120.670714885215
0.221419254805462 120.691001408323
0.221652800912308 120.700779736745
0.22188945529055 120.712333128763
0.222129136644756 120.725636177134
0.22237176043805 120.740661905571
0.222617238896994 120.757381801805
0.22286548102641 120.775765856158
0.218106328841077 120.778804559054
0.212907274091205 120.783517229637
0.208034749953591 120.792841129994

fort_tides_June-July1999.15

```
0.203481040878605 120.806967659939
0.199237999770441 120.826057079329
0.195297054988434 120.850234564669
0.191649217306642 120.879586864673
0.188285087621279 120.914159706531
0.185194864580411 120.95395609162
0.182368352384336 120.998935584457
0.179794968867074 121.049014659828
0.177463754019569 121.104068131372
0.175363378472022 121.163931642099
0.173482152277518 121.228405144124
0.17180803432592 121.297257258245
0.170328641623065 121.370230375095
0.16903125908915 121.4470463133
0.167902849590031 121.527412358335
0.166930064641733 121.611027495025
0.166099254687903 121.697588631891
0.165396480743075 121.786796667825
0.164807525697803 121.878362248409
0.164317905706676 121.972011102557
0.16391288287962 122.067488876476
0.16357747743909 122.164565419792
0.16329648023691 122.263038522712
0.163054466145719 122.362737109553
0.162835806840786 122.463523953694
0.162624684823857 122.565297976007
0.15883479873756 122.57223593578
0.154494580834615 122.57223593578
0.149870937682152 122.57223593578
0.144981229396423 122.57223593578
0.139842992507373 122.57223593578
0.134473925837112 122.57223593578
0.128891875684695 122.57223593578
0.124106154458231 122.57223593578
0.120283611631119 122.57223593578
N2      !BOUNTAG
0.00901771495123393 70.5555559219938
0.00901771495123393 70.5555559219938
0.00901771495123393 70.5555559219938
0.0224649437452538 70.310225267698
0.0359640113857729 70.067967059948
0.0495143655551521 69.8288920685723
0.0631154874505923 69.5931102230778
0.0767668892995626 69.3607304865136
0.0904681118191357 69.1318607738739
0.104218721861176 68.9066078430122
0.11801830988834 68.6850772164901
0.131866488320961 68.4673730809075
0.145762889022663 68.2535981929221
0.159707161031136 68.0438537973009
0.173698969203885 67.838239552344
```

N2 tidal amplitude and phase at boundary nodes

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.187737991967235 67.6368534225649
0.201823919656784 67.4397916238477
0.215956452900412 67.2471485309979
0.230135301124718 67.0590165977006
0.245336257325806 66.9871507198574
0.260615387559981 66.9606746694446
0.275550001106763 66.9356756396178
0.290152940732471 66.9119217735443
0.304437496694596 66.8892407121229
0.318417394590978 66.8675037949496
0.329661645495821 66.8258549133374
0.32938954426064 66.6881191490572
0.329130528758285 66.5511390504911
0.328884519217216 66.4149186437776
0.328651432897423 66.2794608396605
0.328431184234058 66.1447674509834
0.328223684961888 66.010839217422
0.328028844262664 65.8776758166349
0.327846568833828 65.7452758940337
0.327676763092682 65.6136370847236
0.327519329206028 65.4827560344393
0.327374167281317 65.3526284315867
0.327241175435243 65.2232490302757
0.327120249937033 65.0946116825315
0.327011285315109 64.9667093680527
0.326914174444828 64.839534223938
0.326828808675974 64.7130775786021
0.326755077949365 64.5873299840043
0.326692870868615 64.4622812528453
0.326642074812532 64.3379204897291
0.326602576068682 64.2142361307158
0.326572514801655 64.0908032816656
0.326473390680927 63.9490121813591
0.326385697055523 63.8078415101812
0.326309314993679 63.6672547693086
0.326244126383192 63.5272148591046
0.326190014035386 63.3876841528044
0.326146861728718 63.2486245650385
0.326114554353796 63.1099976311919
0.3260929779249 62.9717645716779
0.326082019693886 62.8338863701621
0.326081568211674 62.6963238456242
0.326091513385839 62.5590377221356
0.326111746551125 62.4219887014994
0.32614216053714 62.2851375389869
0.326182649699969 62.1484451105289
0.326233110013015 62.0118724865325
0.326293439092685 61.8753810026578
0.326363536227871 61.7389323270586
0.326443302489953 61.6024885340973
0.326532640679653 61.466012169998

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.326631455450687 61.3294663184041
0.326720778371354 61.2011096793129
0.326760282374421 61.0985010206336
0.326807686835432 60.9961564625871
0.326862843067046 60.8940807208017
0.326925602980887 60.7922785046263
0.326995819112566 60.6907545263609
0.327073344792304 60.5895135151551
0.327158034210447 60.4885602359161
0.32724974252799 60.3878994976303
0.327348325981533 60.287536173909
0.327453641953946 60.1874752113797
0.327565549080905 60.0877216493048
0.327683907357669 59.988280627518
0.327808578186026 59.889157406638
0.328008432715425 59.7902149608225
0.328213713544604 59.6916818974407
0.327970363447388 59.5950800460069
0.323179434349891 59.51007190706
0.317686456423715 59.4198958756584
0.311479351952905 59.3235965123591
0.304546796876023 59.2200488413767
0.296878237345581 59.107912051104
0.289446874965744 59.003584263104
0.284796924700661 58.9465741144691
0.280617221372413 58.8910855527273
0.27691723514434 58.8375243919506
0.273705734314311 58.7863031804381
0.270990778714323 58.7378328685106
0.268779713667857 58.6925137126937
0.26707916468196 58.6507257437024
0.26589503262149 58.6128192012107
0.265232489503927 58.5791053767514
0.265095974785055 58.5498483156752
0.265489192302695 58.5252578085045
0.266415107144582 58.5054840374329
0.267875943697894 58.4906141534964
0.269873183322043 58.4806709481776
0.272407562937671 58.4756136468459
0.275479073490603 58.475340732958
0.279086959331564 58.4796945847762
0.283229717277149 58.4884676233628
0.287905097022174 58.5014095918668
0.293110100564079 58.518235575067
0.298840983951279 58.5386343386986
0.30509325775627 58.5622766307931
0.311861689335678 58.5888231071079
0.319140305173297 58.6179316272571
0.326922393743954 58.6492637282562
0.335200509038253 58.6824901606428
0.342380450044656 58.7118549368884

fort_tides_June-July1999.15

```

0.343012050571284 58.7197732158545
0.34364760083086 58.7295706939587
0.344286959120429 58.7412207815995
0.344929981181535 58.7546956290019
0.345576520184504 58.7699661590892
0.346226426747031 58.7870021073452
0.338935503135637 58.7760445961356
0.330946108818056 58.7639959892244
0.323473499902413 58.7556589870246
0.316505423667302 58.7512518142738
0.310028943739829 58.7509689412822
0.304030451455909 58.7549769120966
0.298495677209659 58.7634106020298
0.293409703004502 58.7763700581679
0.288756974921613 58.7939180691172
0.284521315875974 58.8160785826443
0.280685938813568 58.8428360569753
0.277233460592469 58.874135792961
0.274145915785905 58.9098852567631
0.271404770915262 58.9499563528179
0.268990939625711 58.9941885680005
0.26688479761203 59.0423928795769
0.265066198273695 59.0943562750014
0.2635144886806 59.1498467285157
0.262208526548889 59.2086184666949
0.261126696445391 59.2704173438613
0.260246928102294 59.3349861774369
0.25954671413562 59.4020698996955
0.259003127846641 59.4714204111123
0.258592843031706 59.5428010436318
0.258292152909205 59.6159905770968
0.258076989602737 59.6907867862245
0.257922944965308 59.76700950597
0.257805290440982 59.8445032527221
0.257698998868738 59.9231394387362
0.251708559035755 59.9285125641105
0.24483053228762 59.9285125641105
0.237503356097944 59.9285125641105
0.229754541376684 59.9285125641105
0.22161187859997 59.9285125641105
0.213103415431447 59.9285125641105
0.204257433244309 59.9285125641105
0.196673408814935 59.9285125641105
0.190615751711378 59.9285125641105
K2      !BOUNTAG
0.00150825759163014 132.428071896483
0.00150825759163014 132.428071896483
0.00150825759163014 132.428071896483
0.00376449637794318 132.120436802615
0.00603788444796918 131.81779781796
0.00832827428169586 131.520248997034

```

K2 tidal amplitude and phase at boundary nodes

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.0106355095970051 131.227881747362
0.0129594249996637 130.94078478752
0.0152998456444571 130.659044164026
0.0176565869520677 130.38274323712
0.0200294543156365 130.111962707185
0.0224182429782586 129.846780615513
0.0248227377848589 129.587272355125
0.0272427129927488 129.333510697539
0.0296779322546381 129.08556582921
0.0321281484744223 128.843505348954
0.0345931037694539 128.607394328903
0.0370725294649271 128.377295329834
0.0395661461231531 128.153268431048
0.0421982321266733 128.062954027113
0.0448277209914025 128.026070891508
0.047397845497059 127.99227081464
0.0499108156041722 127.961038986398
0.0523689185615633 127.931984957715
0.0547745167511344 127.904809259659
0.0567070648217321 127.858212953438
0.0566476324224609 127.714586078762
0.0565906939363829 127.572035690009
0.056536217847714 127.430563605406
0.0564841718632836 127.290170055363
0.0564345229544009 127.150853703849
0.0563872373963098 127.012611677345
0.0563422808093515 126.875439581843
0.0562996181899622 126.739331537045
0.0562592139612792 126.60428020726
0.0562210319967185 126.470276827438
0.0561850356691935 126.337311245269
0.0561511878804472 126.205371951825
0.05611945110248 126.074446123947
0.0560897874129104 125.944519663883
0.0560621585273301 125.815577239028
0.0560365258378124 125.687602327392
0.0560128504493418 125.560577261629
0.0559910932099537 125.434483277388
0.0559712147460678 125.309300557111
0.0559531755014728 125.18500828308
0.0559371294181477 125.061261693054
0.0559317544267484 124.923530502128
0.0559281015298501 124.786699667377
0.0559261583816277 124.650726744629
0.055925912883477 124.515568732483
0.0559273531893714 124.381182150221
0.055930467702207 124.24752310915
0.0559352450851599 124.114547396739
0.0559416742533725 123.982210542885
0.055949744380605 123.850467901965
0.0559594448982057 123.719274727581

fort_tides_June-July1999.15

0.05597076549367 123.588586244939
0.0559836961110594 123.458357726178
0.0559982269508195 123.328544568476
0.0560143484646098 123.199102363047
0.0560320513590046 123.069986971771
0.0560513265892687 122.941154599271
0.0560721653540297 122.812561861636
0.0560945591022314 122.684165863079
0.0561184995150706 122.555924261029
0.0561439785158482 122.427795335108
0.0561658740712031 122.307823588954
0.0561732582921557 122.213096685316
0.0561817699229986 122.118754842561
0.0561913774170757 122.024796467913
0.0562020494738273 121.931219958286
0.0562137550486106 121.838023714184
0.0562264633850038 121.745206161204
0.0562401440306075 121.652765773794
0.0562547668597895 121.560701090095
0.0562703020953339 121.469010738019
0.0562867203247633 121.377693449157
0.0563039925219894 121.28674808392
0.0563220900688607 121.196173645679
0.0563409847674185 121.10596930505
0.0563710798990834 121.017465944245
0.0564017677252068 120.92937546012
0.0563558018575696 120.843332386883
0.0555351113353837 120.76867332795
0.0545932440239254 120.6864047948
0.0535281220518416 120.595428632647
0.0523377996716942 120.494433993982
0.0510204666634096 120.381840889055
0.0497421867971047 120.281530678216
0.0489371359073286 120.250290824181
0.0482109389916698 120.222339251665
0.0475651981723558 120.198030179429
0.0470013980893987 120.177699591661
0.0465209048219544 120.161656538328
0.046124964879021 120.150174426675
0.0458147042859369 120.14348269176
0.0455911277218584 120.141759262779
0.0454551177322948 120.145124233481
0.0454074339953077 120.153635106909
0.0454487126759607 120.167283912342
0.0455794657446226 120.185996397332
0.0458000804856293 120.209633369361
0.0461108189344627 120.237994143318
0.0465118174701248 120.270821919351
0.0470030863983635 120.307810801222
0.0475845097030165 120.348614087322
0.048255844763962 120.392853406938

fort_tides_June-July1999.15

0.0490167223313771 120.440128248945
0.0498666463527905 120.490025466899
0.0508049942275033 120.542128349559
0.0518310168650136 120.596024955373
0.0529438390722631 120.651315451428
0.0541424599735968 120.707618303969
0.0554257535365034 120.764575236204
0.0567924692191478 120.821854952899
0.0579753721316581 120.875608040292
0.0580606794629923 120.915300660396
0.0581466074802386 120.95680062584
0.0582331335252182 121.000075674806
0.0583202340576297 121.045092218592
0.0584078846517977 121.091815377534
0.0584960599956711 121.140209024835
0.0572659287033866 121.152800065459
0.0559195698170358 121.165440668844
0.0546587194849984 121.184280668417
0.0534813506966598 121.209544010148
0.0523853238495554 121.241411103976
0.051368388551709 121.280014030913
0.0504281853931138 121.325432623291
0.0495622478948778 121.377691606297
0.0487680044208959 121.436758967156
0.0480427801193259 121.502545668369
0.0473837989257398 121.574906767474
0.0467881856753937 121.653643950029
0.0462529682012606 121.738509425506
0.0457750795115244 121.829211067161
0.0453513601394484 121.92541863261
0.0449785604678265 122.026770866929
0.0446533432015364 122.132883233646
0.0443722859186792 122.243356036991
0.0441318838196359 122.357782689199
0.0439285523787909 122.475757860253
0.0437586303805166 122.596885324946
0.0436183828837929 122.720785317111
0.0435040042274375 122.847101262715
0.043411621397804 122.975505798916
0.0433372972692288 123.10570603531
0.0432770339540478 123.237448072065
0.0432267763942344 123.370520795583
0.0431824158012018 123.50475904946
0.0431397934315853 123.64004627201
0.0421353207605903 123.649259747728
0.0409839579927021 123.649259747728
0.0397574088431458 123.649259747728
0.0384602785626124 123.649259747728
0.037097219200402 123.649259747728
0.0356729258582974 123.649259747728
0.0341921327604171 123.649259747728

fort_tides_June-July1999.15

```
0.032922587921688 123.649259747728
0.0319085527768608 123.649259747728
K1      !BOUNTAG
0.0039752880301854 -162.006810382162
0.0039752880301854 -162.006810382162
0.0039752880301854 -162.006810382162
0.00992279650808299 -162.152360753861
0.01591607880248 -162.295528162148
0.0219543614271663 -162.4362751111178
0.0280368676344652 -162.574564744889
0.0341628172674145 -162.710360875229
0.0403314265652848 -162.843627984497
0.0465419080391139 -162.974331244245
0.0527934702425199 -163.102436516713
0.059085317914863 -163.22791037004
0.0654166517146512 -163.350720090246
0.0717866680292811 -163.4708336871
0.0781945591613003 -163.588219896695
0.0846395130998703 -163.702848203693
0.0911207134971914 -163.81468883455
0.0976373396509934 -163.923712773302
0.104188566502803 -164.029891771293
0.111170493065742 -164.068154908814
0.118168470178139 -164.080621954315
0.125006233236755 -164.092872073779
0.131689655110608 -164.104926033799
0.138224813682176 -164.116795606022
0.144617986347188 -164.12848581119
0.149760629473447 -164.157131152087
0.149648571626342 -164.26525163478
0.149539354189374 -164.372715645788
0.149432958484749 -164.479542575103
0.149329365490764 -164.585752944421
0.149228555881263 -164.691368373776
0.149130510063793 -164.79641154177
0.149035208214365 -164.900906158138
0.148942630305731 -165.00487691833
0.148852756154917 -165.108349469449
0.148765565438403 -165.211350371269
0.148681037739981 -165.31390705385
0.148599152571872 -165.416047778565
0.148519889412394 -165.517801594434
0.148443227735207 -165.619198295439
0.148369147034398 -165.720268377293
0.148297626857829 -165.821042992558
0.148228646837151 -165.921553907037
0.148162186711378 -166.021833450416
0.148098226354479 -166.121914473759
0.148036745810025 -166.221830301389
0.147976692374732 -166.321502518223
0.147871474600161 -166.415937240281
```

K1 tidal amplitude and phase at boundary nodes

fort_tides_June-July1999.15

0.147768620687234 -166.510361477891
0.147668111098742 -166.604812277782
0.147569926569754 -166.69932696846
0.147474048142572 -166.793943109578
0.147380457187965 -166.888698442525
0.147289135450655 -166.983630837722
0.147200065062275 -167.078778246924
0.147113228580802 -167.174178650104
0.14702860901712 -167.269870004426
0.146946189859541 -167.365890194601
0.146865955102505 -167.462276981761
0.146787889276849 -167.559067950012
0.146711977468462 -167.656300457213
0.146638205351937 -167.754011583754
0.146566559210734 -167.852238080367
0.146497025955954 -167.951016318388
0.14642959316427 -168.050382239251
0.146364249080839 -168.15037130163
0.146300982655371 -168.251018437048
0.146237517530044 -168.342634482976
0.146168982473282 -168.404610128348
0.146102294546404 -168.466801172453
0.14603744390267 -168.529197467629
0.145974420623057 -168.591788794623
0.145913214712431 -168.654564862835
0.14585381612708 -168.717515314911
0.145796214786148 -168.780629723447
0.145740400584136 -168.843897596123
0.145686363411597 -168.907308373486
0.145634093160585 -168.97085143225
0.145583579745525 -169.034516083802
0.145534813116017 -169.098291579585
0.145487783267168 -169.162167106471
0.145456037706879 -169.229515402302
0.145426048751498 -169.296860178637
0.145199231001177 -169.362111492929
0.142990611243745 -169.409368307416
0.140489395769883 -169.458922090034
0.137690626811326 -169.511238529705
0.134589649465016 -169.566862299812
0.131182116585988 -169.626438390999
0.127863788324362 -169.681441015062
0.125680037569801 -169.712606914461
0.123697277813549 -169.744317768734
0.121919620819494 -169.776432184611
0.120350877942267 -169.80879203288
0.118994556965417 -169.841224259513
0.117853859146452 -169.873543361358
0.116931676542793 -169.905554497251
0.11623058952976 -169.937057157185
0.115752864591219 -169.967849271295

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.115500452337545 -169.997731603661
0.115474985860909 -170.026512242679
0.115677779098261 -170.054010988952
0.116109825791157 -170.08006343363
0.116771798364112 -170.104524536688
0.117664047267026 -170.127271547721
0.118786600376339 -170.148206142685
0.12013916284795 -170.167255713613
0.121721116912123 -170.184373788552
0.123531522310886 -170.199539619122
0.125569116334147 -170.212757012174
0.127832314895967 -170.224052521618
0.13031921306034 -170.233473134298
0.133027586331158 -170.241083600717
0.135954891957742 -170.24696355605
0.139098270442405 -170.251204569286
0.142454547286934 -170.253907240662
0.145335872576356 -170.257748919509
0.145390913602134 -170.271403489342
0.145447234080762 -170.284108616683
0.145504818641155 -170.295871463806
0.145563651512489 -170.306700013067
0.145623716525024 -170.316603057493
0.145684997119593 -170.325590189115
0.142486231657232 -170.336280879073
0.139002182022689 -170.346258610873
0.135731872486021 -170.355017555527
0.132670291224217 -170.362457192498
0.129812142950552 -170.368483015853
0.127151853513739 -170.373008274748
0.12468357453063 -170.375955643014
0.122401188566883 -170.37725875839
0.120298314323491 -170.376863570014
0.118368311988511 -170.374729438255
0.116604288820527 -170.370829938909
0.114999105052257 -170.365153335219
0.113545379791337 -170.357702692081
0.112235497132277 -170.34849562424
0.111061612670934 -170.337563685891
0.110015659912986 -170.324951420723
0.109089357000806 -170.310715110462
0.108274213547296 -170.294921266942
0.107561537847797 -170.277644921487
0.106942443782626 -170.258967772526
0.106407858526807 -170.238976250643
0.1059485299908 -170.217759558181
0.105555034256466 -170.195407735905
0.105217783794158 -170.172009802897
0.104927035291052 -170.147652003811
0.104672897658971 -170.122416187044
0.104445340569493 -170.096378332079

fort_tides_June-July1999.15

```

0.104234202560555 -170.069607225721
0.104029199913159 -170.04216328508
0.101600259394429 -170.040278543089
0.0988239958283055 -170.040278543089
0.0958664364812911 -170.040278543089
0.0927386859244751 -170.040278543089
0.089451961573723 -170.040278543089
0.0860175846566987 -170.040278543089
0.0824469707361602 -170.040278543089
0.079385736536458 -170.040278543089
0.0769406089833799 -170.040278543089
O1      !BOUNTAG
0.0030432406437242 -178.132994182303
0.0030432406437242 -178.132994182303
0.0030432406437242 -178.132994182303
0.00759648900370231 -178.257710146631
0.0121849887800745 -178.380378218499
0.0168081227505022 -178.50096696926
0.0214652721519668 -178.619445478771
0.0261558166133349 -178.73578335995
0.030879134048283 -178.849950761246
0.0356346005979301 -178.961918383397
0.0404215904892254 -179.071657481328
0.0452394761744093 -179.179139877921
0.0500876281526278 -179.284337975125
0.054965414845815 -179.387224759885
0.0598722027586824 -179.487773807353
0.0648073563169858 -179.58595930099
0.0697702378584226 -179.681756027897
0.0747602076240522 -179.775139393518
0.079776623757575 -179.866085431214
0.0851310242819895 -179.894911835504
0.0905003955227452 -179.900753617461
0.0957465087318853 -179.907024776452
0.100873868170054 -179.913635189672
0.105887135441566 -179.920512319254
0.110791125274541 -179.927596239972
0.114736033103139 -179.948707284117
0.114652237275289 179.965696835396
0.114570135766836 179.880571960003
0.114489716237538 179.795898375306
0.114410966002654 179.711655425602
0.114333872059214 179.627821542526
0.11425842111273 179.544374279141
0.114184599599729 179.461290333567
0.114112393709846 179.378545588298
0.114041789416959 179.296115138434
0.113972772492636 179.213973326136
0.113905328539039 179.132093775722
0.11383944300586 179.050449427536
0.113775101217683 178.969012574604

```

O1 tidal amplitude and phase at boundary nodes

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.113712288396372 178.887754898937
0.113650989681191 178.806647508505
0.113591190154061 178.725660974968
0.113532874862722 178.644765370456
0.113476028841261 178.563930309667
0.113420637131788 178.483124985737
0.113366684811289 178.402318210335
0.113313526002142 178.321643137645
0.113232681323784 178.248471054523
0.113153171779741 178.17516893509
0.113074987349513 178.101705476138
0.112998118103696 178.028049188573
0.11292255422737 177.954168436605
0.112848286035207 177.880031476885
0.112775304001561 177.805606498551
0.112703598770435 177.7308616614
0.112633161182185 177.65576513665
0.112563982292277 177.58028514683
0.112496053388596 177.504390004614
0.112429366011583 177.428048152563
0.112363911975856 177.35122820469
0.112299683384102 177.273898985282
0.112236672650448 177.196029568239
0.112174872515987 177.117589318258
0.112114276063058 177.038547929996
0.11205487674139 176.958875466396
0.11199666837353 176.878542401694
0.1119339645178949 176.797519654616
0.111882081157484 176.723618455273
0.111820328176266 176.673472159881
0.111759671233928 176.623020349108
0.111700106691 176.572272785397
0.111641630888042 176.52123929821
0.1115842401435 176.469929783644
0.111527930770107 176.418354197949
0.111472699083456 176.366522559186
0.111418541408744 176.314444494133
0.111365454094892 176.262131474305
0.111313433517389 176.209592340209
0.111262476092315 176.156837772695
0.111212578283225 176.103878050825
0.111163736609457 176.050723501974
0.11112350480597 175.99342321754
0.111084369191134 175.936019982121
0.110895660225714 175.880602413263
0.109202848447153 175.843567229767
0.10728742152984 175.805124180419
0.105145608566347 175.764942456082
0.102773867909192 175.722637296929
0.100168890645198 175.677755245474
0.0976323414590626 175.636963633167

fort_tides_June-July1999.15

0.0959604560223453 175.614851063491
0.0944412763559682 175.59228215883
0.0930779318957749 175.569352612005
0.0918733237717168 175.546170554473
0.0908301224107812 175.522855421352
0.0899507652930452 175.499536338963
0.0892374549160514 175.476350047818
0.0886921568993853 175.453438407977
0.0883165982909415 175.430945563095
0.0881122660399792 175.409014866587
0.0880804057225271 175.387785698801
0.0882220202667406 175.367390313866
0.0885378691308443 175.347950863507
0.0890284674166684 175.329576735971
0.0896940853352415 175.312362327324
0.0905347477198704 175.296385342973
0.0915502338844161 175.28170568321
0.0927400774413577 175.268364939081
0.0941035666146456 175.256386482054
0.0956397442498913 175.245776101982
0.0973474086243013 175.236523118934
0.0992251138407823 175.228601879183
0.101271170809517 175.221973532097
0.103483648245093 175.216587986133
0.105860373821405 175.2123859458
0.108398935509987 175.209300942308
0.110576472718856 175.205076748358
0.110605665403877 175.192426779637
0.110635867276731 175.180548012059
0.110667066801535 175.169435097068
0.110699251936598 175.159082006274
0.110732410137653 175.149482038704
0.110766528366551 175.140627829811
0.108332509432193 175.131471634968
0.105682859639455 175.123048267015
0.103195403937967 175.115606601025
0.100866339079041 175.109229197702
0.098691646585094 175.103993860772
0.0966670962334616 175.099972216652
0.0947882495666465 175.097228348037
0.0930504638206563 175.095817529637
0.0914488958592256 175.095785116084
0.0899785062353355 175.097165627761
0.088634063430802 175.099982074043
0.087410148341134 175.104245544285
0.0863011587598602 175.10995508821
0.0853013140251372 175.117097893273
0.0844046599737242 175.125649753891
0.0836050738150762 175.135575818028
0.0828962692486364 175.146831581111
0.0822718016625362 175.15936409139

fort_tides_June-July1999.15

```

0.0817250736190808 175.173113323603
0.0812493401054394 175.188013671965
0.0808377143963834 175.203995514412
0.0804831737116754 175.220986801775
0.0801785648684763 175.238914629005
0.0799166105257715 175.257706750541
0.0796899151320265 175.277293011655
0.0794909710071684 175.297606676027
0.0793121648239598 175.318585634111
0.0791457837619768 175.340173491907
0.0789840222452675 175.362320541241
0.0771394462016708 175.363842076242
0.0750315831383572 175.363842076242
0.0727860722361499 175.363842076242
0.0704113445804548 175.363842076242
0.0679159169334613 175.363842076242
0.0653083848759046 175.363842076242
0.0625974156119282 175.363842076242
0.0602731901398072 175.363842076242
0.058416740299412 175.363842076242
P1      !BOUNTAG
0.00119821980981623 -156.546706291886
0.00119821980981623 -156.546706291886
0.00119821980981623 -156.546706291886
0.00299059303583058 -156.705592759611
0.00479640561568283 -156.861909620129
0.00661543580373862 -157.015613995479
0.00844746096096781 -157.166663736291
0.0102922574918203 -157.315017454214
0.0121496007679975 -157.460634525965
0.0140192650741281 -157.603475115369
0.0159010235229494 -157.743500176213
0.0177946480835008 -157.880671470043
0.0196999094868633 -158.014951580344
0.0216165771559752 -158.146303919928
0.0235444192499153 -158.274692734637
0.0254832025840245 -158.400083128448
0.0274326926131921 -158.522441056768
0.0293926534177082 -158.641733344296
0.0313628476949802 -158.757927696198
0.0334655239185288 -158.799789581654
0.035574037971025 -158.813219228297
0.0376341720308098 -158.82622553851
0.039647697036224 -158.838866680814
0.0416164457557774 -158.851183315407
0.0435423111290041 -158.86320317212
0.0450910078179692 -158.892625006292
0.0450550757477234 -159.003965672174
0.0450199530919693 -159.114539402092
0.0449856330641469 -159.224371138785
0.0449521088120018 -159.333487130402

```

P1 tidal amplitude and phase at boundary nodes

fort_tides_June-July1999.15

0.0449193734304045 -159.441914891629
0.0448874199740574 -159.549683158149
0.0448562414684378 -159.656821853658
0.0448258309199744 -159.763362038316
0.0447961813304794 -159.869335868786
0.0447672857032665 -159.974776553061
0.0447391370579397 -160.079718301808
0.0447117284378644 -160.184196283032
0.0446850529221705 -160.288246571931
0.0446591036354047 -160.391906101645
0.0446338737560451 -160.49521261333
0.0446093565272223 -160.598204604544
0.0445855452664358 -160.700921278883
0.0445624333738424 -160.803402489543
0.0445400143411769 -160.90568868995
0.0445182817628166 -161.007820878669
0.0444969452562166 -161.109689566361
0.0444631820528806 -161.204557778385
0.0444300574604662 -161.299445331723
0.044397568553801 -161.394395953763
0.044365712540214 -161.489453661497
0.0443344867680679 -161.584662705134
0.0443038887315404 -161.680067512603
0.0442739160820961 -161.775712631205
0.0442445666309396 -161.871642673591
0.0442158383588937 -161.967902258767
0.0441877294227047 -162.064535954906
0.0441602381607176 -162.161588223473
0.0441333630997708 -162.25910336191
0.0441071029626561 -162.357125443942
0.0440814566721812 -162.455698263866
0.0440564233594586 -162.554865279216
0.0440320023685437 -162.654669551982
0.0440081932605533 -162.755153692282
0.043984995823144 -162.856359801904
0.0439624100703704 -162.958329414162
0.043940436251378 -163.061103443745
0.0439177495033714 -163.15443562803
0.0438915238252007 -163.216527801225
0.0438658194404143 -163.278968539764
0.0438406344347594 -163.341750850382
0.0438159668927292 -163.404867601816
0.0437918148964058 -163.468311521218
0.04376817653296 -163.532075196458
0.0437450498982334 -163.596151069545
0.0437224330997487 -163.660531438998
0.0437003242628171 -163.725208454892
0.0436787215316225 -163.790174119119
0.0436576230752474 -163.855420281313
0.0436370270906283 -163.92093864178
0.0436169318057723 -163.986720743763

fort_tides_June-July1999.15

0.0436009380530282 -164.057004106194
0.0435854611317262 -164.127474605499
0.0435112696621505 -164.195612734756
0.0428456613667557 -164.241966735575
0.0420922344638892 -164.290774003154
0.0412494999952956 -164.342509459974
0.0403160600167036 -164.397729914055
0.0392906090788977 -164.457096117667
0.0382919077183864 -164.511009072144
0.0376334948574837 -164.538121717481
0.0370351187431373 -164.565846629348
0.0364980089423918 -164.594069264799
0.0360233053092389 -164.622659316199
0.0356120570392439 -164.651472008628
0.0352652217851531 -164.680349993671
0.0349836648550273 -164.709125828834
0.0347681584665321 -164.737624989784
0.0346193810816315 -164.765669325645
0.0345379168080274 -164.793080833171
0.0345242549010188 -164.819685592704
0.0345787892666808 -164.845317695317
0.034701818143644 -164.869822977887
0.0348935437607482 -164.893062392759
0.0351540721333286 -164.914914862879
0.0354834128787136 -164.935279496137
0.0358814791670479 -164.95407708663
0.0363480876563686 -164.971250864267
0.03688295862099 -164.98676650737
0.037485715960994 -165.000611469671
0.038155887524001 -165.012793709447
0.0388929052634808 -165.023339929024
0.0396961056262301 -165.032293450434
0.0405647299452277 -165.03971185255
0.0414979248935172 -165.045664491329
0.0424947430094802 -165.050230012255
0.0433502036293672 -165.055675603608
0.0433635682827285 -165.069362975756
0.0433774205765143 -165.082159826668
0.0433917545541437 -165.094073015344
0.043406563981438 -165.105110228526
0.0434218423485693 -165.115279971169
0.0434375828743937 -165.124591554988
0.0424839078374348 -165.133140127297
0.0414455476008231 -165.14049520621
0.0404709090257765 -165.146523223935
0.0395584978370186 -165.15112959415
0.0387067352524869 -165.154226881283
0.0379139593528961 -165.155736490069
0.0371784264609806 -165.155590254416
0.03649831268386 -165.153731866454
0.0358717154569476 -165.150118085943

fort_tides_June-July1999.15

```

0.0352966551369813 -165.144719677125
0.0347710766640819 -165.137522029346
0.0342928513193317 -165.128525429951
0.0338597784816385 -165.117744969938
0.0334695874477634 -165.105210080885
0.0331199393726961 -165.090963716924
0.0328084291787875 -165.075061207166
0.0325325875601939 -165.057568822861
0.032289883019679 -165.03856210857
0.0320777240186526 -165.018124034598
0.0318934610352952 -164.996343035008
0.0317343888638994 -164.973310990031
0.031597748834323 -164.94912121056
0.0314807310303487 -164.923866475291
0.031380476741284 -164.897637164034
0.031294080797804 -164.870519518202
0.0312185939615023 -164.842594047498
0.0311510254717802 -164.813934097094
0.031088345464998 -164.784604570029
0.0310274876233135 -164.75466079821
0.0303030566113154 -164.752608448971
0.0294750147095171 -164.752608448971
0.0285928999505777 -164.752608448971
0.0276600243579936 -164.752608448971
0.0266797336120815 -164.752608448971
0.0256554043558229 -164.752608448971
0.0245904413683645 -164.752608448971
0.0236774047894525 -164.752608448971
0.0229481267432699 -164.752608448971
Q1      !BOUNTAG
0.000407293233490401 175.92278399982
0.000407293233490401 175.92278399982
0.000407293233490401 175.92278399982
0.00101715047333827 175.803882116181
0.00163228216622233 175.687040105332
0.00225259699771432 175.57228228723
0.00287800282476582 175.459632505597
0.00350840667702982 175.349114111075
0.00414371475304611 175.240749965333
0.00478383242354025 175.134562431512
0.00542866422350322 175.030573378713
0.00607811388244337 174.928804175109
0.0067320843122398 174.829275683508
0.00739047760238953 174.732008261721
0.00805319505356 174.637021765379
0.0087201371685957 174.544335534689
0.00939120366356126 174.453968404468
0.0100662934795854 174.365938695775
0.0107453047958525 174.280264212267
0.0114702826737617 174.2495582276
0.0121972584748035 174.240028944132

```

Q1 tidal amplitude and phase at boundary nodes

fort_tides_June-July1999.15

0.0129075113782142 174.230970075099
0.0136016478104226 174.222307937076
0.0142802954224395 174.213988418713
0.0149441025217472 174.205971738808
0.015478969413895 174.187181955565
0.015472759973866 174.11731743041
0.0154666387408621 174.048048695418
0.0154606045084513 173.979355525993
0.0154546560621341 173.911216898423
0.0154487921812102 173.843611016075
0.0154430116407919 173.776515339455
0.0154373132132407 173.709906608377
0.0154316956700737 173.643760875262
0.0154261577837901 173.578053531378
0.0154206983291786 173.512759335797
0.01541531608536 173.447852446643
0.0154100098371244 173.383306449923
0.0154047783767339 173.319094391311
0.0153996205054846 173.255188807173
0.0153945350351676 173.191561755868
0.0153895207897303 173.128184850016
0.0153845766068 173.065029287857
0.0153797013392483 173.002065888207
0.0153748938565797 172.939265121003
0.015370153046648 172.876597141268
0.0153654396349121 172.814122340316
0.0153590266042501 172.755890310958
0.0153526680164926 172.69769978779
0.0153463654628714 172.639515697181
0.0153401205675833 172.581302831317
0.0153339349873912 172.523025886169
0.0153278104108442 172.464649498957
0.0153217485582141 172.406138287175
0.0153157511804411 172.347456885143
0.0153098200589487 172.288569983415
0.015303957005067 172.229442367128
0.0152981638593508 172.170038953558
0.0152924424910766 172.110324830484
0.0152867947978851 172.050265295991
0.0152812227049509 171.989825895939
0.015275728164675 171.928972462172
0.0152703131560352 171.867671151829
0.0152649796838123 171.805888485145
0.0152597297784655 171.743591382887
0.0152545654949984 171.680747206827
0.0152494889126307 171.617323793151
0.0152438925257157 171.560175107665
0.0152364906355923 171.523878095219
0.0152291599955399 171.487277320333
0.0152219014204489 171.450372852846
0.0152147157232135 171.413164902254

fort_tides_June-July1999.15

0.0152076037141465 171.375653823891
0.0152005662013842 171.337840120354
0.0151936039911857 171.299724448939
0.0151867178876604 171.261307623401
0.0151799086933677 171.222590619945
0.0151731772088713 171.183574580419
0.0151665242332835 171.144260817627
0.0151599505639761 171.104650816424
0.0151534569968938 171.064746241591
0.0151473842593321 171.021303784268
0.0151414040406733 170.9775773009
0.0151151976974156 170.935512090471
0.0148860585808147 170.910242396268
0.0146267883720734 170.883122255569
0.0143368783961372 170.853852074871
0.0140158509190801 170.822078311563
0.0136632596170687 170.787379300251
0.0133194047820644 170.757202639964
0.0130910387267379 170.747995516891
0.012883261706161 170.738772598931
0.0126964972284952 170.729583349503
0.0125311379576634 170.720480905295
0.0123875453910982 170.711521305764
0.0122660495578225 170.702762549897
0.0121669487442162 170.694263500487
0.012090509238077 170.686082669652
0.0120369650993228 170.678276929767
0.0120065179524345 170.670900202356
0.0119993368125491 170.664002183974
0.0120155579104111 170.657627167996
0.0120552845784727 170.65181301926
0.0121185871275348 170.646590350492
0.0122055027705814 170.641981936605
0.0123160355532108 170.638002391011
0.0124501563305805 170.634658108976
0.0126078027390167 170.631947470211
0.0127888792335398 170.629861276115
0.0129932570951135 170.628383387813
0.013220774519833 170.627491520446
0.0134712366886963 170.627158148086
0.0137444158900522 170.627351470184
0.0140400516556149 170.628036395431
0.0143578509166109 170.629175503063
0.0146974881848424 170.630729949204
0.0149882209933314 170.63125619828
0.0149882433029171 170.626254743999
0.0149883771553232 170.621758270515
0.0149886215364859 170.617762977844
0.0149889753476041 170.614264620833
0.0149894374057899 170.611258513214
0.014990064450534 170.608739532988

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

0.0146597215987901 170.60582314391
0.0143005822091637 170.6039688888331
0.0139632362526271 170.603432656652
0.0136471726917316 170.604285668391
0.013351851550179 170.606591282415
0.0130767043801322 170.610403649406
0.0128211347326768 170.61576649471
0.0125845186845852 170.622712080724
0.0123662053655127 170.631260396765
0.0121655175021516 170.64141861644
0.0119817519863408 170.65318085305
0.0118141804762513 170.666528232242
0.0116620499973954 170.681429289582
0.01152458356571 170.697840684717
0.0114009808523122 170.715708211569
0.0112904188374497 170.734968074201
0.0111920524978158 170.755548382033
0.0111050155050142 170.777370817056
0.0110284209627912 170.800352419839
0.0109613621132789 170.824407434835
0.0109029131258418 170.849449166153
0.0108521298585545 170.875391793875
0.0108080506192181 170.902152110883
0.0107696970064549 170.929651147034
0.01073607471110255 170.957815658769
0.0107061743351719 170.986579474712
0.0106789722661308 171.015884690801
0.0106534315053951 171.045682727093
0.0106285025767792 171.075935258722
0.010380076981886 171.078003202127
0.0100964376515326 171.078003202127
0.00979427608340785 171.078003202127
0.00947472678546908 171.078003202127
0.00913893579455634 171.078003202127
0.00878805975353042 171.078003202127
0.00842326494307724 171.078003202127
0.00811051134538089 171.078003202127
0.00786070280765905 171.078003202127

90 ! ANGINN - MINIMUM ANGLE FOR TANGENTIAL FLOW

1 !NFFR
STEADY

0.0 1.0 0.0 !freq,nodal factor, equ arg for flux bnd

STEADY

1.67264702454175 0.0 ! unitFlux for bndId 3, node 3, 10000 cfs

1.67264702454175 0.0 ! unitFlux for bndId 3, node 1, 10000 cfs

-1 14 100.000000 360

-1

0 0.000000 00.000000 0

0

-1 14 100.000000 900

-1 14 100.000000 900

Input 10,000 cfs inflow at Penobscot River boundary

! NOUTE, TOUTSE, TOUTFE, NSPOOLE - FORT 61 OPTIONS Don't write any station output

! NSTAE - NUMBER OF ELEVATION RECORDING STATIONS,

! NOUTV, TOUTSV, TOUTFV, NSPOOLV - FORT 62 OPTIONS

! NSTAV - NUMBER OF VELOCITY RECORDING STATIONS,

! NOUTGE, TOUTSGE, TOUTFGE, NSPOOLGE - GLOBAL ELEVATION OUTPUT Global water level and

! NOUTGE, TOUTSGE, TOUTFGE, NSPOOLGE - GLOBAL ELEVATION OUTPUT velocity output every 900 seconds

ADCIRC run control file (fort.15)

fort_tides_June-July1999.15

```
0 ! NHARF - NUMBER OF FREQUENCIES IN HARMONIC ANALYSIS no harmonic analysis
0.000000 0.000000 0 0.000000 ! THAS,THAF,NHAINC,FMV - HARMONIC ANALYSIS PARAMETERS
0 0 0 0 ! NHASE,NHASV,NHAGE,NHAGV - CONTROL HARMONIC ANALYSIS
0 0 ! NHSTAR,NHSINC - HOT START FILE GENERATION PARAMETERS Don't write hotstart files
1 0 1e-010 50 ! ITITER, ISLDIA, CONVCR, ITMAX - ALGEBRAIC SOLUTION PARAMETERS
&timeBathyControl !NDDT, BTIMINC, BCHGTIMINC -- BATHYMETRY TIME RECORDS (IN SECONDS) AND TRANSITION TIME
  NDDT = 0 do not use time varying bathymetry.
  BTIMINC = 0
  BCHGTIMINC = 43200
/
```

Maureparticle run control input file (particles.inp)

particles.inp

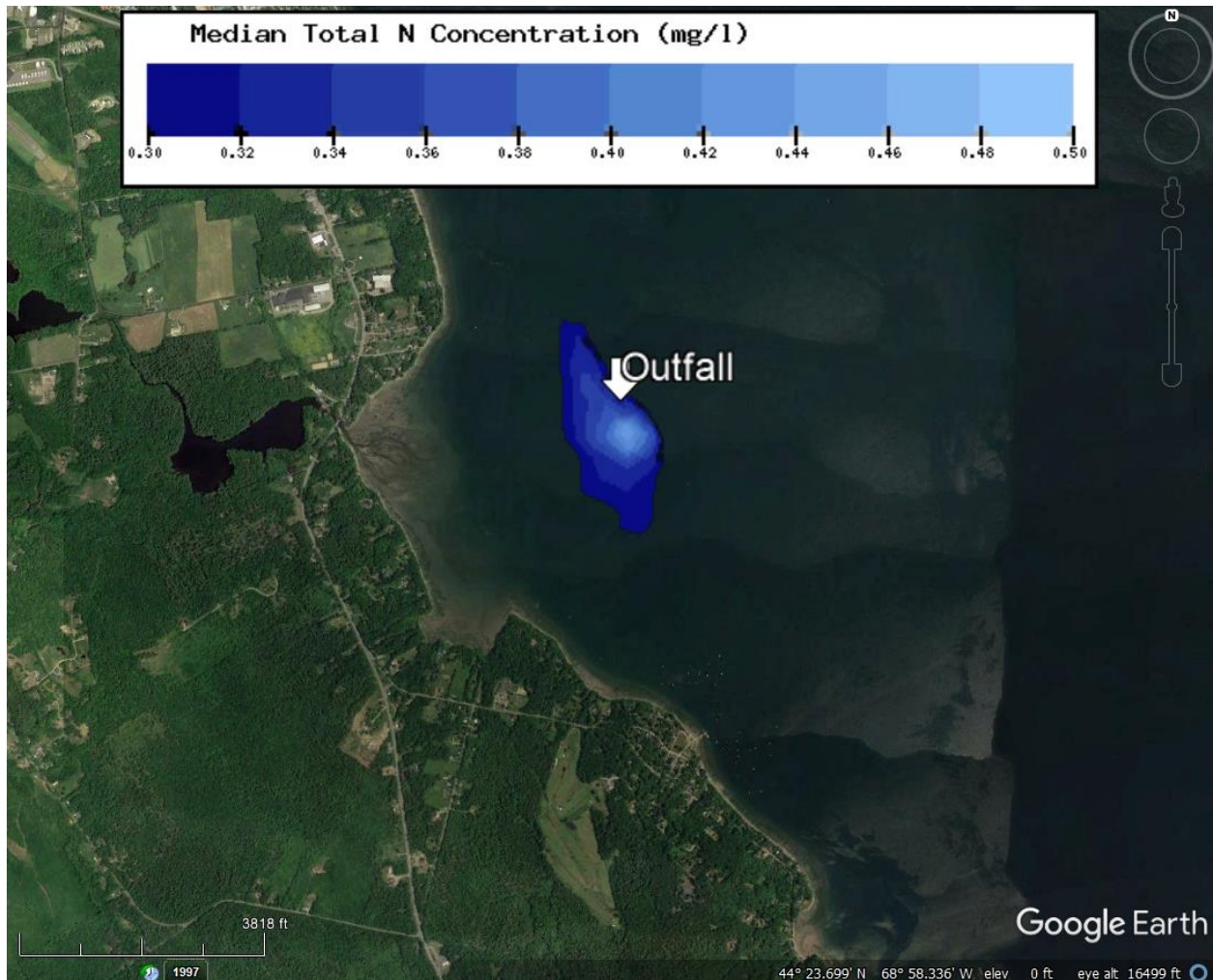
```
DESC line      Comment
80641      ! NP - Number of particles      Track this many particles
10         ! TS - Tracking time Step      Use a 10 second timestep for particle tracking
2419200    ! RUNTIM - Run time in seconds  Track particles for 28 days
3600       ! OUTPER- Output time period seconds Write particle position output every hour
1         ! RK2 - 1 for RK2 0 for Euler   use 2nd order Runge-Kutta method for velocity integration
1         ! DYN - 1 for dynamic           perform dynamic tracking (i.e. read in time variable velocity field from ADCIRC output)
1296000    ! STEADY_TIME Start tracking 15 days into ADCIRC run (1 day after ramp period)
2         ! EDDY_DIF Use random walk diffusion with eddy diffusivity of 2 m^2/s
0         ! NWS      Don't use wind input
0         ! WFACTOR
2         ! ICS      Model grid is in geographic coordinates
-68.972526 44.395004 !SLAM0 SFEA0      Center of grid projection
-68.972042998587 44.3951383396213 1296000 0
-68.9721128856857 44.3951189015697 1296030 0
-68.9719417577511 44.3951664982461 1296060 0
-68.9713344943316 44.3953353994865 1296090 0
-68.9721400784224 44.3951113383166 1296120 0
-68.9722573064172 44.3950787331026 1296150 0
-68.971525059672 44.3952823965864 1296180 0
-68.9712900435013 44.3953477628204 1296210 0
-68.9723470956067 44.3950537595821 1296240 0
-68.9715643702078 44.3952714629486 1296270 0
-68.9724049451828 44.3950376695874 1296300 0
-68.972508252885 44.3950089360947 1296330 0
-68.972224310385 44.3950879104556 1296360 0
-68.9719548333597 44.395162861461 1296390 0
-68.9714753893273 44.3952962116501 1296420 0
-68.9716112541552 44.3952584228797 1296450 0
-68.972072081047 44.3951302507699 1296480 0
-68.9721727202621 44.395102259477 1296510 0
-68.9714076050658 44.395315064829 1296540 0
-68.9720582916215 44.3951340860924 1296570 0
-68.9721651790628 44.3951043569488 1296600 0
-68.9713814528221 44.3953223386845 1296630 0
-68.9719041844601 44.3951769486952 1296660 0
-68.9714518678501 44.3953027537973 1296690 0
-68.972295041213 44.3950682377334 1296720 0
-68.9721890753873 44.3950977105434 1296750 0
-68.9718002048658 44.3952058690647 1296780 0
-68.971692747777 44.3952357566472 1296810 0
-68.9719956381685 44.3951515122136 1296840 0
-68.9717017408174 44.3952332553675 1296870 0
-68.9724470497233 44.395025958839 1296900 0
-68.9717862998787 44.3952097365289 1296930 0
-68.9716636242827 44.3952438569117 1296960 0
-68.9717488263801 44.3952201592222 1296990 0
-68.9721825334599 44.3950995300827 1297020 0
-68.9724196964316 44.3950335667481 1297050 0
-68.9719648202737 44.3951600837502 1297080 0
-68.9718999018028 44.3951781398523 1297110 0
-68.9724590541271 44.3950226199936 1297140 0
-68.9720604800221 44.3951334774215 1297170 0
-68.9714684822846 44.3952981327408 1297200 0
-68.9718411237501 44.3951944880888 1297230 0
-68.9720893202235 44.3951254559507 1297260 0
-68.9716959341392 44.3952348704082 1297290 0
-68.9714506532955 44.3953030916075 1297320 0
-68.9721388913946 44.3951116684706 1297350 0
-68.9723574167398 44.3950508889132 1297380 0
-68.9720626383327 44.3951328771197 1297410 0
-68.9725024142956 44.395010560011 1297440 0
-68.9725237392372 44.3950046287974 1297470 0
-68.9719386093244 44.3951673739339 1297500 0
-68.9721856719237 44.3950986571659 1297530 0
-68.9720271038021 44.3951427605181 1297560 0
```

List of 80641 initial particle positions and their release time every 30 seconds distributed randomly along the diffuser location

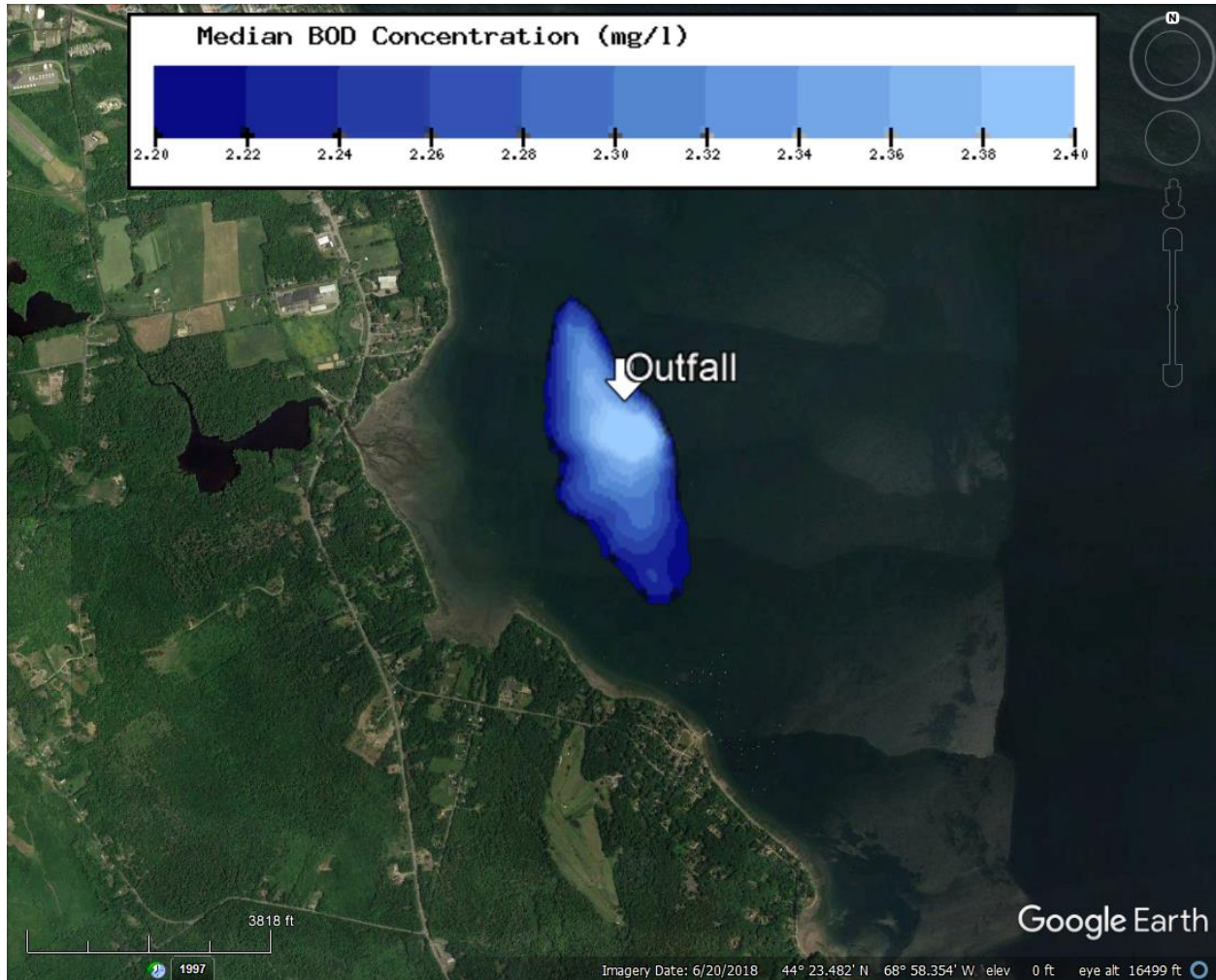
ATTACHMENT D

Time Median Total Nitrogen & BOD Concentrations

Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N



Time Median Total Nitrogen concentration above 0.3 mg/l derived from far-field dilution analysis with effluent concentration of 23 mg/l and background concentration of 0.17 mg/l.



Time Median BOD concentration above 2.2 mg/l derived from far-field dilution analysis with effluent concentration of 50.0 mg/l and background concentration of 2.0 mg/l.

ATTACHMENT E

Chemicals for the Fish Farm

Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N

Chemicals for the Fish Farm

Note: Annual usage estimates represent approximate quantity required given a product is the only one used for this application. The quantities needed will be dependent on the site-specific conditions experienced which are difficult to establish prior to operations and are indicated as estimates only. Likely a fraction of the estimated annual use of each of these products will be used. All products listed will be used according to label.

Cleaners

Detergents

Aqualife® Multipurpose Cleaner. A biodegradable, nonhazardous cleaner that is designed specifically for use in fish hatcheries, aquaculture facilities, fish & food processing plants, & agricultural farms. Active ingredients: sodium hydroxide (1-5%), the product is phosphate free, contains no volatile organic compounds and is NSF certified for use in food processing facilities. Used according to the label at dilutions of 1:20. Approximate annual use: 2232 gallons/year (8449 l/year).

Gil Save®. High-foaming chlorinated, alkaline, liquid detergent, Gil Save is designed for foam and high pressure spray cleaning of meat and poultry plants, breweries, dairies and canneries. It is a complete product containing alkalis, water conditioners, chlorine and high-foaming wetting agents. Gil Save is an effective cleaner of food processing equipment by removing fatty and protein soils, pectin, mold, yeast and organic greases. Active ingredients: sodium hydroxide (7-9%), sodium hypochlorite (3-4%). Use according to label at concentrations of 0.2-3% (¼-4 oz/gal). Approximate annual use: 678 gallons/year (2567 l/year).

Clean in Place (CIP)

Gil Super CIP®. A heavy-duty, chelated-liquid caustic cleaner for use in CIP, boil-out, soak, spray clean and atomization cleaning systems, Gil Super CIP is formulated to remove protein, fatty and carbonized soils typically found in dairy and food processing. Active ingredients: sodium hydroxide (49%). Used according to label at 0.1-3% (1/8-4 oz/gal). Approx. annual use: 5840 gallons/year (22107 l/year).

Gil Hydrox®. A concentrated organic, liquid acid cleaner, Gil Hydrox rapidly removes milk/beer stone, alkaline/hard water film and stains/protein build-up from dairy and food processing equipment. It is specially formulated for use in CIP, spray and acid rinse operations. Active ingredients: glycolic acid (29-31%). Used according to label at 0.3-1.5% (½-2 oz/gal). Approx. annual use: 5840 gallons/year (22107 l/year).

Disinfectants/Sanitizers

Bleach. Active ingredient: sodium hypochlorite (8%) in concentrated form. Typically used at 100-1000 ppm for general cleaning/disinfection. Approximate annual use: 1500 gallons/year (5700 l/year).

Ozone. Ozone can be dissolved into water to provide an aqueous ozone solution that is stable, safe, easy to control, leaves no residue and has been granted GRAS approval by both the USDA and FDA for direct contact with food. This water containing ozone can replace chlorine as an antimicrobial agent or be used to supplement existing water rinses and achieve improved antimicrobial intervention. This is now a common application to sanitize fillet machines, cutting tables, knives, and all equipment that may be used in the seafood processing areas. Approximate annual use: TBD. Concentration in discharge = 0 ppm

Virkon® Aquatic. A powerful cleaning and disinfecting solution with efficacy against fish viruses, bacteria, fungi, and molds. Virkon® Aquatic is EPA registered (except in California where registration is pending) for the disinfection of environmental surfaces associated with aquaculture. Active ingredient: Potassium monopersulfate (21.4%). Used in accordance with label as a general cleaner and in footbaths. Working solution strengths normally range from 0.5% - 2.0%. Approx. annual use: 1100 lbs/year (500 kg/year).

Zep FS Formula 12167® Chlorinated Disinfectant and Germicide. A liquid chlorine sanitizer and deodorant for use in all types of food-handling establishments. Authorized as no rinse sanitizer for equipment. Provides deodorizing activity by destroying bacteria which generate many disagreeable odors. Can also be used to sanitize commercial laundry. Active ingredients: Sodium hypochlorite (5-10%) and sodium hydroxide (1-3%). Used according to label, effective at concentrations as low as 0.3% (1 oz/ 2 gallons). USDA applicable and EPA and Maine registered. Approx. annual use: 1980 gallons/year (7495 l/year).

Therapeutants

Compounds Potentially Used:

Note: the quantities needed will be dependent on the site-specific conditions experienced which are difficult to establish prior to operations and so are indicated as estimates only. All products listed will be used according to label use or a licensed veterinarian's prescription.

Parasite-S, Formalin-F, and Formacide-B. (Formalin). Active ingredient 37% formaldehyde. Used periodically according to the label if needed to alleviate fish health issues due to *saprolegniasis*, external protozoa and monogenetic trematodes. Typical dose rates from 25 ppm to 1,000 ppm. Approximate annual use: 925 gallons/year (3500 l/year).

Finquel® or Tricane-S. (Tricaine methanesulfonate). Used periodically in accordance with the label to reduce stress on the fish when handling small numbers for examination. Typical dose rates of 15-330 mg/L. Approximate annual use: 1.1 lbs/year (500 g/year).

Halamid® Aqua. (Chloramine-T). Active ingredients N-chloro, p-toluenesulfonamide and sodium salt trihydrate. Used periodically according to the label if needed to alleviate fish health issues due to bacterial gill disease. Typical dose range 12-20 ppm. Approximate annual use: 1100 lbs/year (500 kg/year).

Ovadine® (PVP Iodine). A buffered 1% Iodine solution (Iodophor) specifically formulated for use in disinfecting fish eggs. It contains a 10% Povidone-Iodine (PVP Iodine) complex, which provides 1% available iodine. Used according to the label at dose rates of 50 -100 ppm as available iodine solution. Estimated usage: 160 gallons/year (600 l/year).

Compounds Rarely Used Only in Emergency Situations:

Praziquantel. Considered as 100% active. Can be used if fish are suffering from trematode/cestode infections. Typical dose ranges from 5-200 ppm depending on length of standing bath treatment. Used as needed/intermittent or emergency use only, according to label use or as prescribed by a licensed veterinarian. Approx. annual use: 0 lbs/year (0 kg/year).

Potassium permanganate. Considered as 97% active. Can be used if fish are suffering from certain parasites and fungal infections in younger fish life-stages. Typical dose range 1.5-2.5 ppm. Used as needed/intermittent or emergency use only, according to label use or as prescribed by a licensed veterinarian. Approx. annual use: 0 lbs/year (0 kg/year).

Terramycin® 200. (oxytetracycline dehydrate, 44% active): Can be used as an in-feed treatment (maximum of 0.08 g active oxytetracycline/kg fish/day) if fish are suffering from certain bacterial infections. Used as needed/intermittent or emergency use only, according to label use or as prescribed by a licensed veterinarian. Approx. annual use: 0 lbs/year (0 kg/year).

Aquaflor®. (florfenicol; 50% active). Can be used as an in-feed treatment (maximum of 15 mg/kg fish/day) if fish are suffering from certain bacterial infections. Used as needed/intermittent or emergency use only, according to label use or as prescribed by a licensed veterinarian. Approx. annual use: 0 lbs/year (0 kg/year).

Romet® 30/Romet® TC. (sulfadimethoxine/ormetoprim, 30% active or 20% active, respectively). Can be used as an in-feed treatment (maximum of 50 mg/kg fish/day) if fish are suffering from certain bacterial infections. Used as needed/intermittent or emergency use only, according to label use or as prescribed by a licensed veterinarian. Approx. annual use: 0 lbs/year (0 kg/year).

Waste Water Treatment

Formic Acid (85%). Used for pH correction of fish processing water prior to disinfection with sodium hypochlorite. Approx. annual use: 18200 gallons/year (69000 l/year).

Bleach. Active ingredient: sodium hypochlorite (15%). Used to disinfect water used in fish processing. Applied at concentration of 50 mg/l. Estimated discharge concentration: 0.4 mg/l. Approx. annual use: 14800 gallons/year (56000 l/year).

MicroC® 2000. (1.1 million mg/l COD). A non-hazardous, green chemical developed specifically for use as an electron donor / carbon source for wastewater denitrification applications. It is used as supplemental carbon source in wastewater treatment plants to stimulate denitrification processes. Approx. annual use: 1.0 million gallons/year (3.8 million l/year).

MicroC® 2000

PRODUCT INFORMATION

MicroC® 2000 is a proprietary, non-hazardous, green chemical designed specifically for use as a carbon source for biological contaminant removal applications in water/wastewater treatment.

COST EFFECTIVENESS

- ▶ Best value among non-hazardous alternative carbon sources

NON-HAZARDOUS

- ▶ Eliminates flammability and toxicity concerns of traditional chemicals such as methanol
- ▶ Provides capital cost savings vs. installation of flammable liquid storage and feed system
- ▶ Non-hazardous product enables rapid and flexible deployment of carbon augmentation solutions

PERFORMANCE ADVANTAGES

- ▶ Rapid start-up/acclimation
- ▶ Superior cold weather performance

ENVIRONMENTALLY SUSTAINABLE

- ▶ Derived from abundant, renewable resources produced in the United States vs. largely imported fossil-fuel derived carbon sources (methanol)
- ▶ USDA BioPreferred designation

CONSISTENT AND SUPERIOR QUALITY

- ▶ Rigorous end to end quality control program
- ▶ Consistent Chemical Oxygen Demand (COD) values
- ▶ No product degradation during long-term storage

VALIDATED PERFORMANCE

- ▶ MicroC® products in use at over 550 plants in North America
- ▶ Performance validated by leading equipment/process suppliers, consulting engineers and academic institutions
- ▶ Full scale, documented performance validation for:
 - ▶ Nitrate removal
 - ▶ Enhanced Biological Phosphorus Removal (EBPR)
 - ▶ Metals removal
 - ▶ BOD augmentation
 - ▶ Perchlorate removal
 - ▶ Fixed film biological processes (i.e. denitrification filters)
 - ▶ Startup/acclimation dynamics
 - ▶ Cold weather performance
- ▶ Denitrification rates and kinetic parameters determined by Northeastern University

TECHNICAL SERVICES

- ▶ Application guidance from team of BNR/contaminant removal experts
- ▶ Dedicated support to ensure achievement of contaminant removal goals

SUPPLY CHAIN CAPABILITY & EXPERIENCE

- ▶ 20 nationwide MicroC® manufacturing facilities provides redundancy and flexibility, reducing the risk of supply and quality interruptions even during drastic demand changes
- ▶ Extensive multi-industry raw material sourcing capability and vast storage infrastructure facilitates ability to offer long term, fixed pricing
- ▶ An expansive supply chain infrastructure designed for proximity to customers, reduces transportation costs and improves responsiveness

PACKAGING

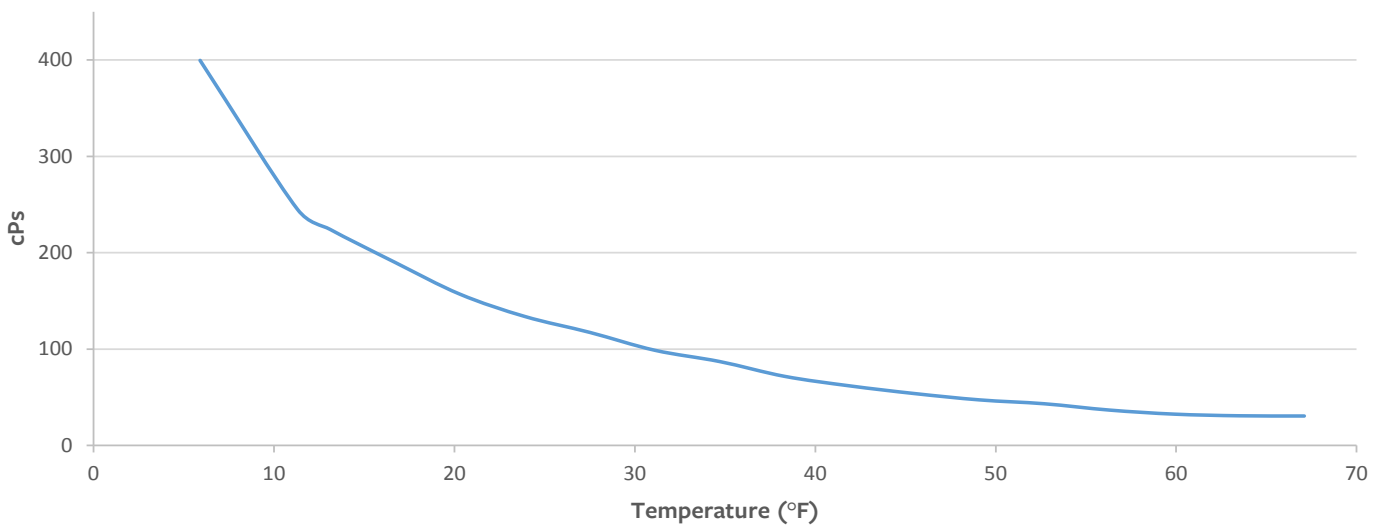
- ▶ Bulk (1000-4500 gallon) *
- ▶ 265-gallon IBC/tote
- ▶ 55-gallon drum
- ▶ 30-gallon drum
- ▶ 5-gallon pail

*Maximum volume 4800 gallons in some markets

TECHNICAL SPECIFICATIONS

PROPERTY	SPECIFICATIONS	TYPICAL VALUE	TEST METHOD
Glycerin Content	70% - 74%	71%	ASTM D7637-10
Methanol Content	0.3%, max	< 0.1%	EN 14110
Fatty Acid Content	0.75%, max	0.3%	ASTM D5555-95
COD (mg/L)	1,050,000 - 1,150,000	1,100,000	ASTM D1252
pH	4.0 - 11.0	6	ASTM E-70
Specific Gravity at 20°C	1.21 - 1.25	1.235	ASTM D891-00
Bulk Density (lbs/gal)	10.09 - 10.43	10.30	ASTM D891-00
Viscosity (cPs) at 20°C	75, max	45	ASTM D2196
Flash Point	None to 93°C	None to Boil	ASTM D93
Freezing Point (°C)	-18, max	-35	ASTM D1177

TEMPERATURE / VISCOSITY RELATIONSHIP



Note: Although product freezes below 0°F, viscosity analyses stopped at 0°F due to practical considerations



MicroC[®] 2000



1. PRODUCT AND COMPANY IDENTIFICATION

Product Name: MicroC[®] 2000 **Publication Date:** March 6, 2018
Product Code: NA **Replaces:** December 28, 2016
Product Use: A reducing agent for biological processes

Supplier Information:

Environmental Operating Solutions, Inc Phone: 508-743-8440
 160 MacArthur Blvd., Unit 6 Fax: 508-743-8443
 Bourne, MA 02532 Website: www.microc.com

EMERGENCY TELEPHONE NUMBER: CHEMTREC 800-424-9300

2. HAZARDS IDENTIFICATION

OSHA Regulatory Status:

This product when used as intended is not hazardous according to 29 CFR 1910.1200

This product when used as intended is not hazardous according to GHS categories

GHS Pictograms: None Applicable
Signal Word: None Applicable
GHS Hazard Classification: None Applicable
Hazard Statements: None Applicable

Note: When vaporized, glycerin mist may cause irritation of the respiratory tract.

Potential Health Effects

Routes of Exposure	Ingestion, inhalation, skin contact, eye contact
Eyes	May cause slight irritation
Skin	May cause slight irritation
Inhalation	High mist concentrations may cause irritation of respiratory tract.
Ingestion	May be harmful if swallowed in large quantities

3. COMPOSITION / INFORMATION ON INGREDIENTS

Chemical Name	CAS #	% by Weight
Glycerin; glycerol	56-81-5	70-74%
Water	7732-18-5	22-26%
Sodium Chloride	7647-14-5	4-6%
Methanol	67-56-1	< 1%

Safety Data Sheet

4. FIRST AID MEASURES

Eye Contact	Immediately flush eyes thoroughly with plenty of water for 15 minutes and consult a physician immediately.
Skin Contact	Remove contaminated clothing and wash affected area with water and soap. Consult physician if irritation develops
Inhalation	Remove individual to fresh air. Seek medical attention if breathing problems persist
Ingestion	Do not induce vomiting. Rinse mouth thoroughly. Seek medical attention.
General Advice	If individual feels unwell following the exposure to the product consult a physician immediately. Present this Safety Data Sheet to the doctor in attendance
Note to physician	Treat patient symptomatically

5. FIRE FIGHTING MEASURES

Flammability Summary (OSHA and NFPA)	Non-flammable Material
Protection of Firefighters:	Wear suitable protective equipment. Wear self contained breathing apparatus if necessary
Extinguishing Media	Use equipment appropriate to the main source of the fire. Water spray, alcohol foam, dry chemical or CO2. Water or alcohol foam may cause frothing
Specific hazards arising from the chemical	Carbon oxides

6. ACCIDENTAL RELEASE MEASURES

Personal Protection for Spills	Keep unnecessary personnel away from spill. Use personal protective equipment. Ventilate area of leak or spill. Avoid breathing vapors and mist.
Methods for Containment	Eliminate all sources of ignition. Stop flow of material if safe to do so. Dike spilled material. Absorb spill with inert absorbent material. Sand, earth and vermiculite are suitable absorbent materials.
Environmental Precautions	Prevent further leakage. Contain spill if safe to do so. Do not let product enter storm drains if possible.

7. HANDLING AND STORAGE

Precautions for Safe Handling	See other relevant sections of this SDS. Avoid contact with skin and eyes. Avoid breathing mist. Use with adequate ventilation. Do not handle and store near open flames, high heat or sources of ignition.
Storage	Keep containers closed when not in use. Minimize evaporative losses. Keep away from ignition sources.
Incompatible Materials for Storage	None known

8. EXPOSURE CONTROLS / PERSONAL PROTECTION

INSUFFICIENT DATA ON MIXTURE. DATA ON INDIVIDUAL COMPONENTS PROVIDED BELOW

Component	Concentration in Product	ACGIH TLV	OSHA TABLE Z-1 Limits for Air Contaminants	NIOSH
Glycerin CAS No: 56-81-5	70-74% w/w	Form: Glycerin Mist TWA: 10 mg/m ³	Form: Total Dust PEL: 15 mg/m ³ Form: Respirable Fraction PEL: 5 mg/m ³	Insufficient Data on Glycerin Mist
Methanol CAS No: 67-56-1	< 1 % w/w	TWA: 260 mg/m ³	PEL: 260 mg/m ³	TWA: 260 mg/m ³

Engineering Controls

Use proper equipment and storage conditions to control airborne levels below recommended exposure limits.

Personal Protective Equipment

Eye Protection:

Use normal eye protection practices such as safety glasses with side shields. Use chemical goggles if risk of splashing is high.

Skin Protection

Handle with chemical resistant gloves. Dispose of contaminated gloves after use. Nitrile gloves recommended.

Respiratory Protection

If workers could be exposed to concentrations above the exposure limits in Section 8, use a full face respirator with multipurpose combination cartridges.

9. PHYSICAL AND CHEMICAL PROPERTIES

Physical State	Liquid	Flash Point	None to Boil (ASTM D93)
Color	Light brown	Boiling Point	Not determined
Odor	Musty – Sweet Odor	Evaporation Rate	Not determined
Odor Threshold	Not determined	UEL/LEL	Not determined
		Flammability (solid, gas)	Not determined
pH	4.00-11.00	Vapor Pressure	Not determined
Solubility in Water	Highly soluble in water	Vapor Density	Not determined
		Relative Density	Not Determined
Bulk Density	10.22 lbs/gal	Partition Coefficient	Not determined
Specific gravity	1.225@ 20°C	Autoignition Temperatures	
		Decomposition	
Viscosity	45 cPs @ 20C	Temperature	Not determined

Safety Data Sheet

10. STABILITY AND REACTIVITY

Reactivity	Avoid contact with oxidizing agents (e.g. nitric acid, peroxides, chromates)
Chemical Stability	Stable under normal storage conditions
Possibility of hazardous reactions	None known
Conditions to Avoid	Heat, flames, sparks. Contact with oxidizing agents
Incompatible Materials	None known
Hazardous Decomposition Products	Oxides of carbon under high heat

11. TOXICOLOGY

INSUFFICIENT DATA ON MIXTURE. DATA ON INDIVIDUAL COMPONENTS PROVIDED BELOW

Eye Contact	The components in this product may result in mild eye irritation from contact with liquid or vapors. Symptoms include redness, swelling, watering.
Skin Contact	The components in this product may result in mild skin irritation. Symptoms include redness, itching, burning, dermatitis.
Inhalation	Breathing high mist concentrations may be harmful. Inhalation can cause irritation of the throat and lungs.
Ingestion	Ingestion of this product may result in nausea, vomiting and diarrhea. Aspiration into the lungs can cause damage and inflammation to the lungs.
Target Organs	Lungs, Kidneys
Prolonged Exposure	Symptoms include nausea, headache, vomiting

Glycerin; Glycerol CAS No. 56-81-5

Acute Toxicity	Dermal LD50 = > 10,000 mg/kg (Rabbit) Inhalation LC50 = > 570 mg/m ³ 1 hr (Rat) Oral LD50 = 12,600 mg/kg (Rat)
Carcinogenicity	Not listed by ACGIH, IARC, NIOSH, NTP or OSHA
Mutagenicity	No data available
Reproductive Toxicity	No data available

Methanol 67-56-1

Acute Toxicity	Dermal LD50 = 15,800 mg/kg (Rabbit) Inhalation LC50 = 64,000 mg/m ³ 4 hr (Rat) Oral LD50 = 5,600 mg/kg (Rat)
Carcinogenicity	Not listed by ACGIH, IARC, NIOSH, NTP or OSHA
Mutagenicity	No data available
Reproductive Toxicity	No data available

12. ECOLOGICAL INFORMATION

Ecotoxicity	Glycerin: 96 hr LC50: 51,000-57,000 mg/L (Rainbow Trout), > 5000 mg/L Goldfish Methanol: 96 hr LC50: > 15,400-29,400 mg/L (Fish)
Persistence and degradability	No data available
Bioaccumulative potential	No data available
Mobility in soil	No data available
Other adverse effects	No data available

13. DISPOSAL CONSIDERATIONS

This product as supplied is not classified as a RCRA hazardous waste according to 40 CFR 261. However it should be fully characterized prior to disposal as contamination with other materials may subject it to hazardous waste regulations. RCRA requires the user of the product to determine whether the product meets RCRA criteria for hazardous waste. Always consult with local, state and federal regulations prior to disposal.

14. TRANSPORTATION INFORMATION

US Domestic DOT	Not Regulated
Shipping Name	Glycerin; Glycerol
IMDG	Not dangerous goods
IATA	Not dangerous goods
Marine pollutant	No

15. REGULATORY INFORMATION

United States

Toxic Substances Control Act

The components of this product are listed on the TSCA Inventory of Existing Chemical Substances

Section 302 (EHS) TPQ Not applicable

Section 304 (EHS) TPQ Not applicable

SARA Section 311/312 Hazard Categories

Acute - NO
Chronic - NO
Physical - None
Pressure Hazard - NO
Fire Hazard - NO

Safety Data Sheet

SARA Section 313

This product may contain trace amounts of a chemical that is subject to reporting requirements of SARA
Methanol CAS # 67-56-1 Typical % Weight in Product 0.0-0.10%

CERCLA

This product may contain trace amounts of a chemical that is subject to reporting requirements of CERCLA
Methanol RQ # 5,000. Typical % Weight in Product 0.0-0.10%

Clean Water Act Section 311 Hazardous Substances (40 CFR 117.3): None

State Right to Know Regulations

Chemical Name: Glycerin

California – Proposition 65 Not applicable

Massachusetts Right to Know Glycerin

Minnesota Hazardous Substances List Glycerin mist

New Jersey Right to Know None

Pennsylvania Right to Know Glycerin

Rhode Island Right to Know Glycerin

16. ADDITIONAL INFORMATION

MSDS REVISION STATUS: March 6, 2018 | Replaces December 28, 2016

THIS SAFETY DATA SHEET (SDS) HAS BEEN PREPARED IN COMPLIANCE WITH THE FEDERAL OSHA HAZARD COMMUNICATION STANDARD, 29 CFR 1910.1200. THE INFORMATION IN THIS SDS SHOULD BE PROVIDED TO ALL WHO WILL USE, HANDLE, STORE, TRANSPORT, OR OTHERWISE BE EXPOSED TO THIS PRODUCT. WE BELIEVE THIS INFORMATION TO BE RELIABLE AND UP TO DATE AS OF ITS PUBLICATION DATE, BUT MAKE NO WARRANTY THAT IT IS. IF THIS SDS IS MORE THAN THREE YEARS OLD YOU SHOULD CONTACT THE SUPPLIER TO MAKE CERTAIN THAT THE INFORMATION IS CURRENT.

CASE STUDY

MUNICIPAL WWTP IMPLEMENTS NITRACK[®] PROGRAM TO MEET NITROGEN PERMIT LIMITS

MicroC[®] and Nitrack[®] Program Enable BNR System to Outperform its Design Basis Without Capital Improvements

Client: Large Water Pollution Abatement District

Location: Northeast

Flow (Average Design/Actual):
45 MGD/30 MGD

Treatment Technology: Anaerobic/Anoxic/Oxic (A2/O) process

Total Nitrogen Limit: 6 mg/L
(Monthly Average) May to October

Total Phosphorus Limit: 0.45 mg/L
(Monthly Average) April to October

Study Period: 2015

Scope: MicroC[®] Evaluation & Application Support (ME&AS) and Nitrack[®] Program

Product: MicroC[®] 2000A



Environmental Operating Solutions, Inc. (EOSi) helped this Water Pollution Abatement District find an operational solution to meet stricter seasonal discharge requirements for nitrogen and phosphorus. A pilot study in 2015 was conducted in one of the treatment trains to demonstrate that by using MicroC[®] 2000A supplemental

carbon source in conjunction with EOSi's Nitrack[®] Program, the District could meet new permit requirements with its existing treatment facilities.

Background

The District had recently completed a plant improvement project that included an upgraded biological nutrient removal (BNR) system. The District anticipated enhanced nitrogen and phosphorus removal requirements to meet new NPDES limits on nutrient discharges to protect receiving waters, including a sensitive coastal bay. However, the new NPDES permit included

discharge standards for nitrogen and phosphorus that were much more stringent than the design basis for the BNR system. To avoid another capital improvement project, the District began exploring operational solutions.

The BNR system uses the A2/O process with four treatment trains. The system has sequential anaerobic, anoxic and aerobic zones that facilitate denitrification and phosphorus removal. By optimizing this process, the District was able to achieve lower effluent nitrogen concentrations than expected based on the process design, but

could not consistently meet the average monthly total nitrogen limit of 6.0 mg/L (May to October). The District retained EOSi to conduct a pilot study of denitrification with MicroC® 2000A supplemental carbon in one of the four treatment trains.

Challenge

The District and EOSi agreed on the following success criteria for the evaluation study:

- ▶ **Meet permit requirements:** Achieve an average effluent of nitrate-nitrogen (NO₃-N) concentration of less than 4.5 mg/L, and of total nitrogen of less than 6.0 mg/L.
- ▶ **Minimize supplemental carbon costs:** Achieve a carbon-to-nitrogen (COD:N) ratio less than or equal to the theoretical minimum (i.e., 5.5 pounds of COD added per pound of nitrogen removed). This ensures that carbon in the primary effluent is used for denitrification, minimizing supplemental carbon needs.

Solution Summary

EOSi conducted a MicroC® Evaluation & Application Support (ME&AS) study to design the MicroC® program, including determination of optimal feed rates, injection points and control strategies. EOSi provided in-line analyzers, a chemical storage tank, and pumping equipment for the evaluation study. EOSi also set up the Nitrack® Program, including the installation of a Nitrack® Controller and all related monitoring, control, and automation equipment. A process flow diagram is shown in Figure 1.

MicroC® 2000A was fed to the anoxic zone of the A2/O process beginning in April 2015. EOSi began optimizing the supplemental carbon program to consistently meet the permit requirement for total nitrogen of 6 mg/L while minimizing MicroC® 2000A usage. EOSi's technical staff continuously monitored key process parameters, optimized set-points, and modified the process control strategy. One challenge with the District's treatment system configuration was finding the right combination of feedforward (FF) control and feedback (FB) control. Feedforward control actively adjusts process conditions as influent conditions change, but does not make adjustments based on system performance. Feedback control actively adjusts process conditions as system performance changes, but does not make adjustments based on changes in influent conditions. Combining feedforward and feedback control strategies

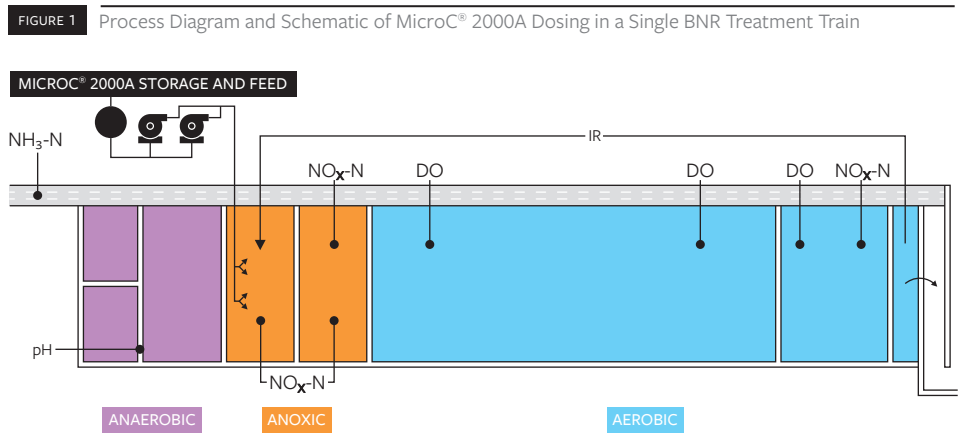
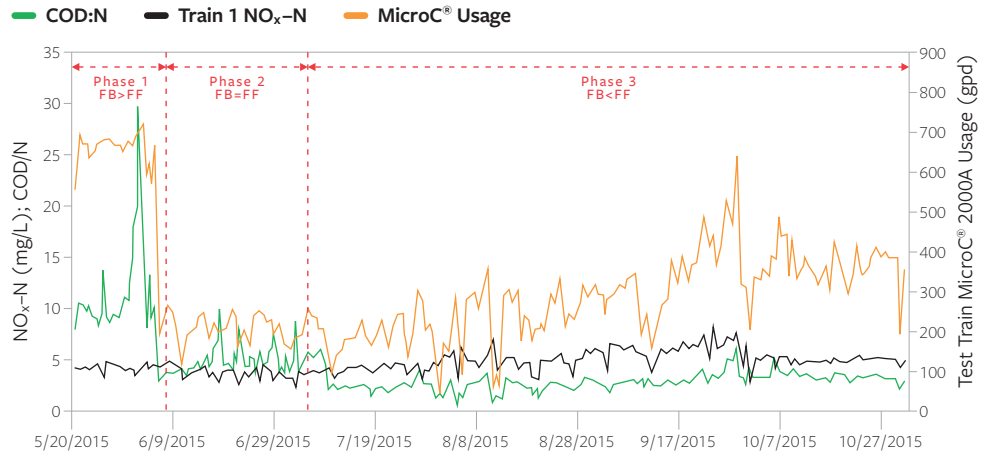


FIGURE 2 Process Performance Data with Control Phases



enables the most consistent effluent quality with the lowest supplemental carbon usage.

EOSi technical staff completed regular data analysis and systematically evaluated possible control strategies, considering factors such as ambient temperature, kinetics, loading, flows, and internal recirculation rates. EOSi concluded that this process responded best to a control mode that favored feedforward control over feedback control, with an internal recirculation rate of 3.25 times the influent flow. These conditions promoted the use of internal COD while returning enough nitrate to the anoxic zone for denitrification. Results of the evaluation study are summarized in Figure 2.

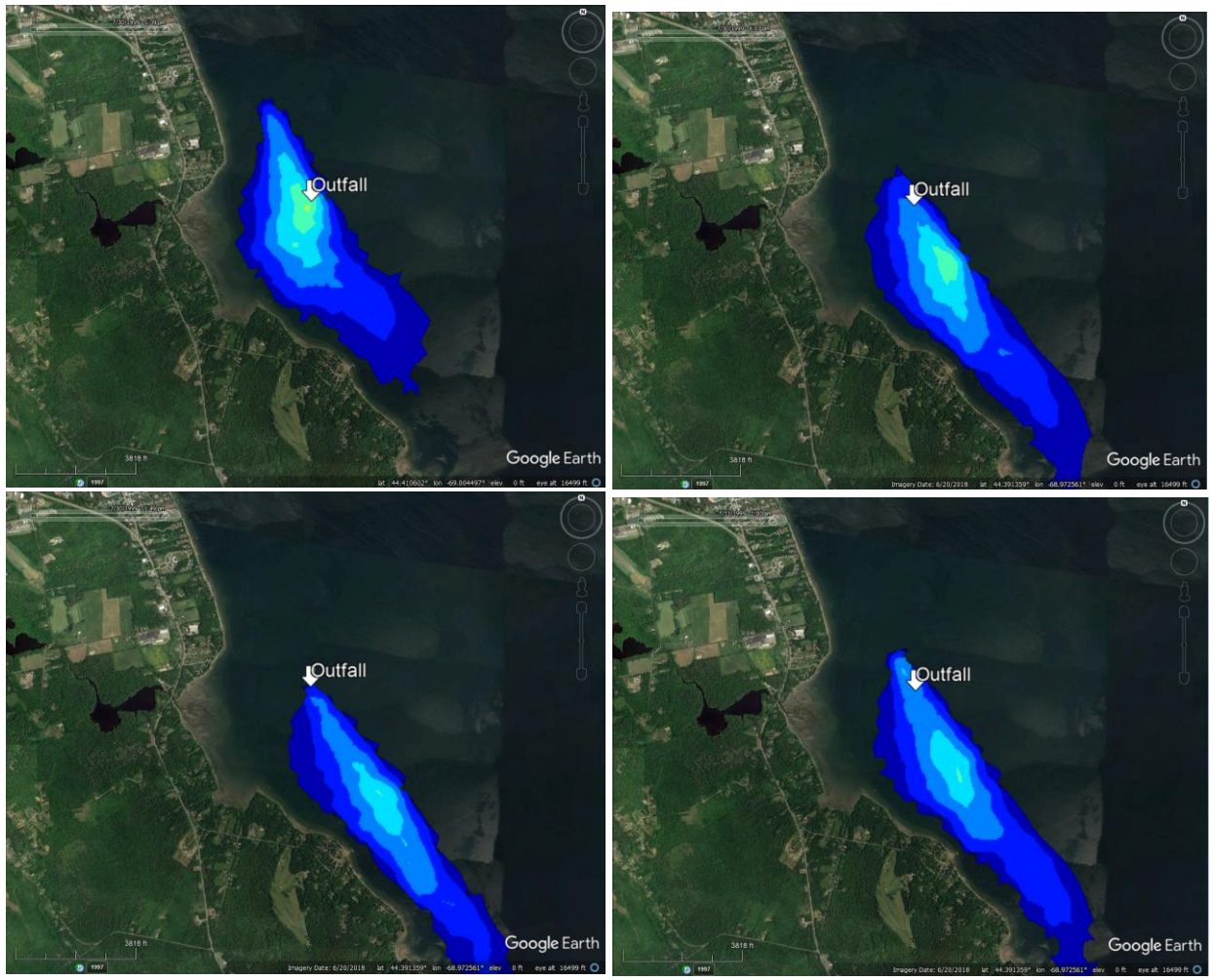
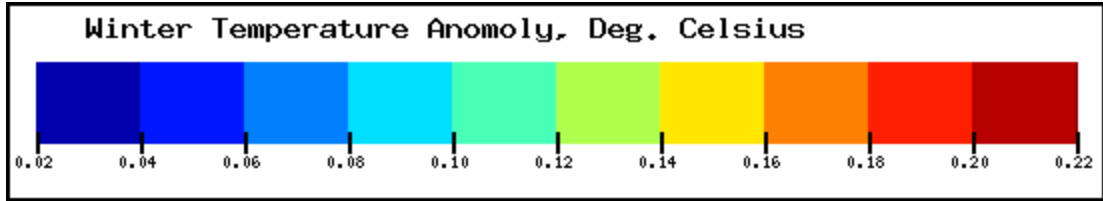
Benefits

Results of the pilot study met the success criteria, described in the Challenge section. By using MicroC® 2000A as a supplemental carbon source and real-time dosage optimization using EOSi's Nitrack® Program, the selected treatment train was able to achieve effluent total nitrogen concentrations largely consistent with the target limit of 6.0 mg/L. The Nitrack® Controller allowed internal COD to be used for denitrification when available, and achieved an average COD:N ratio of less than 5.5. Based on the success of the evaluation, the District has decided to expand the supplemental carbon program to all four biological treatment trains in 2016.

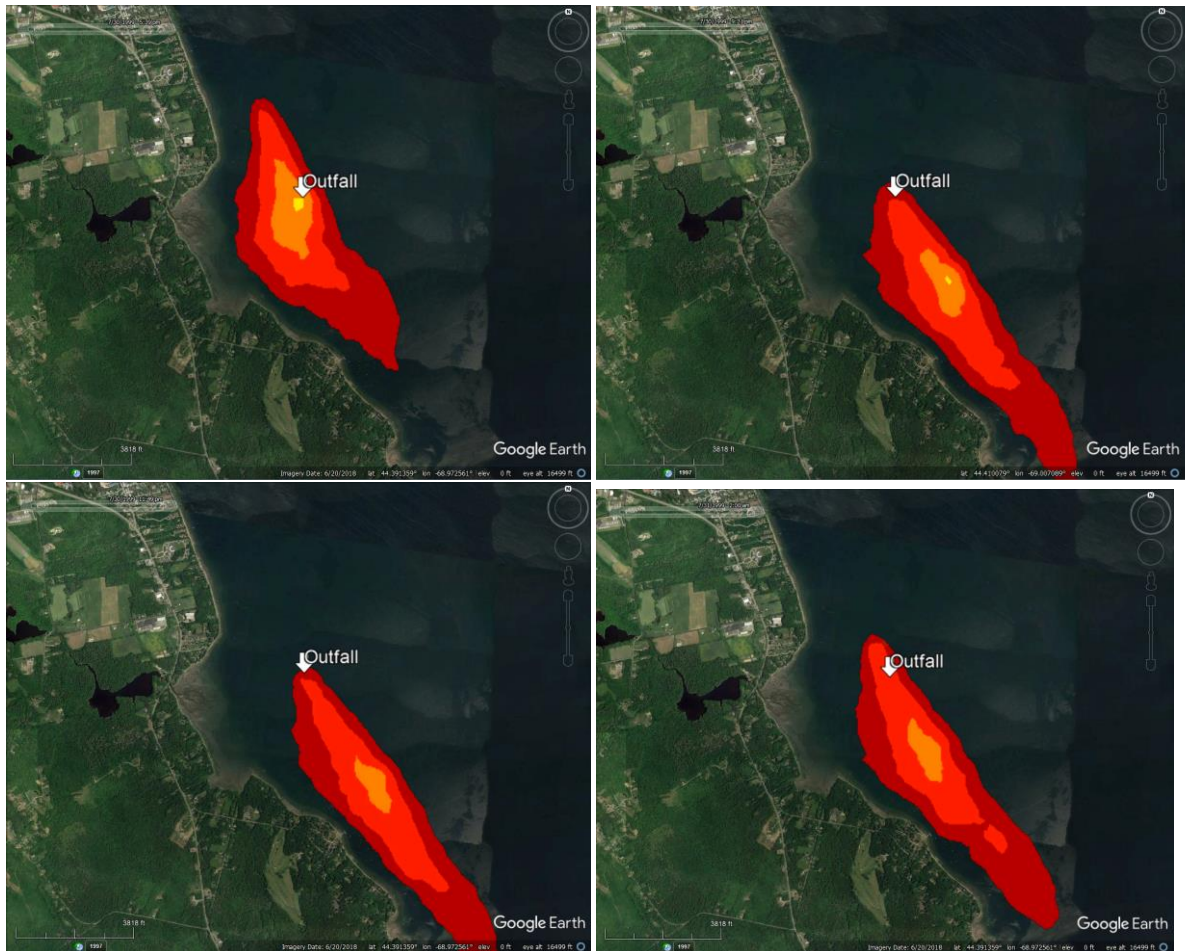
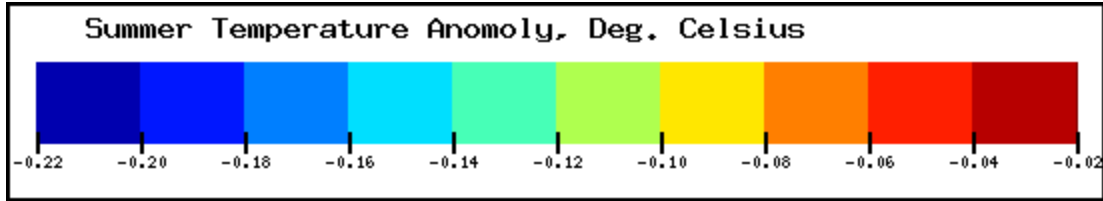
ATTACHMENT F

Summer/Winter Effluent Temperatures

Response to Review Comments
Nordic Aquafarms Inc., Land-based Aquaculture Facility
Belfast, Maine
L-28319-26-A-N



Temperature anomaly in winter assuming 0 degree C ambient temperature. high slack (upper left), mid-ebb (upper right), low slack (lower left), mid-flood (lower right)



Temperature anomaly in Summer assuming 22 degree C ambient temperature. high slack (upper left), mid-ebb (upper right), low slack (lower left), mid-flood (lower right)